





# Segment 1A – RFU Walls Package 2 Grade Separation Barrier 05.33R; Walls 05.55L, 05.85L-A, and 05.85L-B; and Embankment EMB: I-405 SB MP 5.97 to 5.83

| Wood Environmen | t & Infrastrycture, Inc. |
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WSDOT I-405 Renton to Bellevue Design-Build Renton to Bellevue, Washington Project # PS19-20316-0

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Geotechnical Engineering Report: Grade Separation Barrier 05.33R; Walls 05.55L, 05.85L-A, and 05.85L-B; and Embankment EMB: I-405 SB MP 5.97 to 5.83

File Name: I-405 R2B Segment 1A - Walls Package 2 - RFU







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# List of acronyms

**AASHTO** American Association of State Highway and Transportation Officials

Site Class-Adjusted Peak Ground Acceleration  $A_{s}$ 

**ASTM** American Society of Testing and Materials

**BDM** Bridge Design Manual bgs Below Ground Surface

**CALTRANS** California Department of Transportation

CIP Cast-In-Place

COV Coefficient of Variation Coefficient of Uniformity Cu **EPS Expanded Polystyrene** 

**ESU** Engineering Stratigraphic Unit **FHWA** Federal Highway Administration

F\* Pullout Resistance Factor

FS Factor of Safety

**GBR** Geotechnical Baseline Report **GDM** Geotechnical Design Manual **GDR** Geotechnical Data Report

**GLE** Generalized Limit Equilibrium

HRM Highway Runoff Manual

H:V Horizontal:Vertical

I-405 Interstate 405

ka Active Earth Pressure Coefficient

Static + Seismic Earth Pressure Coefficient kae kh Horizontal Seismic Acceleration Coefficient

ksf Kips Per Square Foot

**LRFD** Load and Resistance Factor Design

Minimum Allowable Distance to the Travel Lane **MADTL** 

М-О Mononobe-Okabe

MOT Maintenance of Traffic

MP Milepost

 $N1_{60}$ Field Blow Count Corrected for Overburden Pressure and Hammer Efficiency

Equivalent Clean Sand Corrected Field Blow Count  $N1_{60}(cs)$ 

NAVD 88 North American Vertical Datum of 1988

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**NCHRP** National Cooperative Highway Research Program

pcf Pounds Per Cubic Foot **PGA** Peak Ground Acceleration

Project GDM Project Geotechnical Design Manual, consisting of WSDOT's 2015 Geotechnical Design Manual, along

with project-specific Chapters 6 (Seismic) and 15 (Retaining Walls) from Request for Proposal Addendum 9

psf Pounds Per Square Foot Pounds Per Square Inch psi **RECO** Reinforced Earth Company

RFU Released for Use

**RFP** Request for Proposal

SEE Safety Evaluation Earthquake

**SEW** Structural Earth Wall

SPT Standard Penetration Test

Sta. Station

**USCS** Unified Soil Classification System **USGS** United States Geological Survey

WADNR Washington State Department of Natural Resources Wood Wood Environment & Infrastructure Solutions, Inc. **WSDOT** Washington State Department of Transportation







#### Introduction 1.0

- 2 This geotechnical engineering report provides conclusions and recommendations to facilitate final design and construction of
- 3 proposed Grade Separation Barrier 05.33R; retaining Walls 05.55L, 05.85L-A, and 05.85L-B; and embankment EMB: I-405
- 4 SB MP 5.97 to 5.83. The referenced barrier, walls, and embankment are part of Segment 1A of the Interstate 405 (I-405)
- 5 Renton to Bellevue Widening and Express Toll Lanes project. A Vicinity Map of Segment 1A is included as Figure 1.
- Locations of the proposed barrier, walls, and embankment addressed in this geotechnical engineering report are presented on 6
- 7 Retaining Wall Plan Figures 2S, 2T, and 2U. Barrier, wall, and embankment profiles and design sections are presented in
- 8 Appendices C through G.

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- 9 This geotechnical engineering report has been prepared in accordance with the requirements presented in the I-405 Renton to
- Bellevue Widening Project conformed Request for Proposal (RFP), specifically Section 2.6.5.3, and the applicable sections of 10
- 11 the Washington State Department of Transportation (WSDOT) Geotechnical Design Manual (GDM) M 46-03.11 including the
- project-specific revised GDM Chapters 6 and 15 provided in the conformed RFP (Project GDM). 12

### Description of Barrier, Walls, and Embankment 2.0

- 14 Grade Separation Barrier 05.33R; Walls 05.55L, 05.85L-A, and 05.85L-B; and embankment EMB: I-405 SB MP 5.97 to 5.83
- are addressed in this geotechnical engineering report. The barrier, walls, and embankment are described below. Table 1 15
- presents a summary of the barrier, wall, and embankment sections considered in design. 16
- 17 Grade Separation Barrier 05.33R: Grade Separation Barrier 05.33R is a rigid, concrete barrier located on the east side of
- northbound I-405, west of the North Southport Drive on-ramp. It is approximately 100 feet in length and 4 feet tall at its 18
- maximum exposed height. It is our understanding that the back of the barrier will be battered at 4H:21V (horizontal to vertical) 19
- 20 (10.8 degrees from vertical). The critical design section was selected based on maximum barrier height.
- 21 Grade Separation Barrier 05.33R will be designed in accordance with WSDOT Bridge Design Manual (BDM) Section 10.3.1
- 22 for differential grade concrete barriers. Design calculations for Grade Separation Barrier 05.33R will be submitted under
- 23 separate cover by the design-build team's wall designers.
- 24 Wall 05.55L: Wall 05.55L is a cast-in-place (CIP) concrete retaining wall located on the west side of the southbound I-405 off-
- 25 ramp to Southport Drive. It is approximately 130 feet in length and 4.5 feet tall at its maximum exposed height. The critical
- 26 design section was selected based on maximum wall height.
- 27 Walls 05.85L-A and 05.85L-B: Walls 05.85L-A and 05.85L-B are Structural Earth Walls (SEWs) located on the west side of
- southbound I-405, north of the North Southport Drive off-ramp. Wall 05.85L-A is approximately 100 feet in length and about 28
- 29 17 feet tall at its maximum exposed height. Wall 05.85L-B is approximately 335 feet in length and about 20 feet tall at its
- 30 maximum exposed height. Walls 05.85L-A and 05.85L-B will be designed with consideration of forward compatible loading
- 31 for future widening of I-405. The critical design sections for these walls were selected based on maximum wall height. Based
- on wall/slope geometry and maintenance of traffic (MOT) requirements, temporary shoring will be required to facilitate 32
- 33 construction of Walls 05.85L-A and 05.85L-B.
- 34 Embankment EMB: I-405 SB MP 5.97 to 5.83: Embankment EMB: I-405 SB MP 5.97 to 5.83 is located on the west side of
- 35 southbound I-405 between Walls 05.85L-A and 05.85L-B. EMB: I-405 SB MP 5.97 to 5.83 is a widening of the existing
- embankment and will be constructed with 2H:1V side slopes. As noted in the reference report in the RFP "General Geologic 36
- Characterization and Unstable Slope Evaluation" dated December 14, 2018, a fill slope failure (SB2: SB I-405 MP 5.90 5.94) 37
- 38 occurred at the location of proposed EMB: I-405 SB MP 5.97 to 5.83 during the I-405 widening in 1985. The slope failure was
- 39 mitigated by construction of a rock buttress and toe drainage system that will remain in-place for the proposed embankment
- 40 construction. The critical design section was selected near the midpoint of the embankment.







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### Table 1: Summary of Critical Design Sections by Barrier/Wall/Embankment

| Design<br>Element                                 | Cut/Fill | Design<br>Section<br>Stations/<br>Mileposts | Maximum<br>Exposed<br>Height<br>(feet) | Minimum<br>Reinforcement<br>Length (feet)                           | Foreslope<br>(degrees) | Backslope<br>(degrees) | Wall Type                |
|---|----------|---|--|---|------------------------|------------------------|--------------------------|
| Grade<br>Separation<br>Barrier 05.33R             | Fill     | Sta. 1+58                                   | 4.0                                    | NA  | 0                      | 17.5                   | NA                       |
| Wall 05.55L                                       | Fill     | Sta. 1+50                                   | 4.5                                    | NA  | 15                     | 0                      | Cast-In-Place            |
| Wall 05.85L-A                                     | Fill     | Sta. 1+90                                   | 16.7                                   | 15.5 <sup>1</sup> (upper 6 rows)<br>20 <sup>2</sup> (bottom 2 rows) | 27                     | 27                     | Structural Earth<br>Wall |
| Wall 05.85L-B                                     | Fill     | Sta. 2+60                                   | 19.6                                   | 16.5 <sup>3</sup>   | 15                     | 27                     | Structural Earth<br>Wall |
| Embankment<br>EMB: I-405 SB<br>MP 5.97 to<br>5.83 | Fill     | MP 5.88                                     | NA                                     | NA  | NA                     | NA                     | NA                       |

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- 1. To satisfy minimum global and compound stability requirements, the reinforcement length is approximately 0.8 times the height of the wall (exposed height plus embedment depth).
- 2. To satisfy minimum compound stability requirements, the reinforcement length is approximately 1.0 times the height of the wall (exposed height plus embedment depth).
- 3. Reinforcement length is approximately 0.7 times the height of the wall (exposed height plus embedment depth).

#### 9 Abbreviations: 10

- MP = Mile Post 11
- NA = Not Applicable 12
  - Sta. = Station

#### Surface Conditions 3.0

- 15 Grade Separation Barrier 05.33R: The existing ground surface at Grade Separation Barrier 05.33R is a vegetated slope with grass and some small trees. 16
- 17 Wall 05.55L: The existing ground surface at Wall 05.55L is a relatively steep slope covered with mature trees and grasses.
- Wall 05.85L-A: The existing ground surface at Wall 05.85L-A is a relatively steep slope covered with mature trees and grasses. 18
- 19 Wall 05.85L-B: The existing ground surface at Wall 05.85L-B is a relatively steep slope covered with trees and grasses.
- Embankment EMB: I-405 SB MP 5.97 to 5.83: The existing ground surface at embankment EMB: I-405 SB MP 5.97 to 5.83 20
- is a steep slope covered with mature trees and grasses. Quarry spalls are placed at the toe of the slope as a rock buttress 21
- installed as part of the 1985 fill landslide repair. 22

#### **Explorations and Laboratory Testing** 4.0

#### Conformed RFP Explorations and Laboratory Testing 4.1

- 25 We reviewed previous subsurface explorations and laboratory test results provided in the RFP Geotechnical Data Report
- (GDR). Information reviewed included historic data from previous studies along the project alignment and project-specific data 26
- 27 from explorations completed prior to preparation of the RFP (RFP explorations). Exploration logs and laboratory test results







1 used for soil property and subsurface profile development are reproduced in Appendices A and B, respectively. The historic and RFP exploration locations are shown on Retaining Wall Plan Figures 2S, 2T, and 2U. 2

#### **Explorations Completed by Design-Build Team** 4.2

- 4 To supplement the information provided in the project GDR, subsurface explorations were completed by the design-build team
- 5 in compliance with the exploration location, spacing, and depth requirements per Project GDM Section 15-3.4 for the walls and
- 6 barrier, and per Project GDM Section 9.1 for the embankment. The supplemental (Post-RFP) explorations consisted of four
- 7 borings, W-207-20, W-215-20, W-217-20, and W-218-20, drilled between July and August 2020 near the proposed locations
- for Grade Separation Barrier 05.33R, and Walls 05.55L, 05.85L-A, and 05.85L-B, respectively. At Grade Separation Barrier 8
- 9 05.33R and Wall 05.55L, historical and RFP borings were not located within the contractual baseline boundary for retaining
- walls outlined in the RFP Geotechnical Baseline Report (GBR); therefore, to characterize subsurface conditions, boring 10
- W-207-20 was drilled near the face of Grade Separation Barrier 05.33R, at approximately the center of the alignment, and 11
- boring W-215-20 was drilled upslope of Wall 05.55L, approximately 23 feet east of the center of the alignment. Boring W-12
- 217-20 was drilled upslope of Wall 05.85L-A to confirm subsurface conditions behind the south end of the wall. Boring W-13
- 14 218-20 was drilled upslope of Wall 05.85L-B to confirm subsurface conditions behind the north end of the wall.
- 15 RFP borings R2B-10-17 and R2B-11-17 were drilled approximately 13 and 28 feet east of the centerline of the Wall 05.85L-B
- alignment, respectively, which confirmed subsurface conditions near the wall face. 16
- We used both historical borings H-1-85 and H-2-85 to develop the soil properties at Wall 05.85L-A and embankment EMB: 17
- I-405 SB MP 5.97 to 5.83, however, these borings align at approximately the same location when projected onto the respective 18
- wall and embankment design sections. We used boring H-1-85, which is located within the embankment, to define the 19
- subsurface at the embankment, and we used boring H-2-85, which is located below Wall 05.85L-A, to define the subsurface at 20
- 21 Wall 058.85L-A.
- 22 A summary of the historical, RFP, and Post-RFP explorations at the barrier, wall, and embankment locations is presented in
- 23 Table 2.

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Table 2: Summary of Explorations by Barrier/Wall/Embankment

| Design<br>Element                     | Nearby Explorations<br>(Total Explorations)      | Maximum<br>Boring<br>Spacing<br>(feet) | Project GDM<br>Exploration<br>Compliance<br>Requirements  | Notes   |
|---------------------------------------|--|--|---|---|
| Grade<br>Separation<br>Barrier 05.33R | W-207-20<br>(1)                                  | Not<br>Applicable                      | Meets exploration<br>requirements for walls<br>under 10 feet in height<br>per Project GDM<br>Section 15-3.4         | Exploration compliance requirements for retaining walls were applied to Grade Separation Barriers |
| Wall 05.55L                           | W-215-20<br>(1)                                  | Not<br>Applicable                      | Meets exploration<br>requirements for walls<br>under 10 feet in height<br>per Project GDM<br>Section 15-3.4         | -   |
| Wall 05.85L-A                         | W-217-20,<br>H-1-85,<br>H-2-85,<br>H-3-85<br>(4) | 95                                     | Meets exploration<br>requirements for walls<br>greater than 100 feet in<br>length per Project GDM<br>Section 15-3.4 | -   |

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| Design<br>Element                              | Nearby Explorations<br>(Total Explorations)      | Maximum<br>Boring<br>Spacing<br>(feet) | Project GDM<br>Exploration<br>Compliance<br>Requirements  | Notes |
|--|--|--|---|-------|
| Wall 05.85L-B                                  | W-218-20,<br>R2B-10-17,<br>R2B-11-17<br>(3)      | 170                                    | Meets exploration<br>requirements for walls<br>greater than 100 feet in<br>length per Project GDM<br>Section 15-3.4 | -     |
| Embankment<br>EMB: I-405 SB<br>MP 5.97 to 5.83 | W-217-20,<br>H-1-85,<br>H-2-85,<br>H-3-85<br>(4) | Not<br>Applicable                      | Meets exploration requirements for embankments per Project GDM Section 9.1  | -     |

Post-RFP explorations and accompanying Post-RFP laboratory test results used for soil property and subsurface profile development are reproduced in Appendices A and B, respectively. The Post-RFP exploration locations are shown on Retaining Wall Plan Figures 2S, 2T, and 2U.

#### **Subsurface Conditions** 5.0

#### 5.1 Regional Geology

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Geologic maps available through the Washington State Department of Natural Resources (WADNR) indicate that the surficial soils in the vicinity of Grade Separation Barrier 05.33R; Walls 05.55L, 05.85L-A, and 05.85L-B; and embankment EMB: I-405 SB MP 5.97 to 5.83 include Pleistocene continental glacial drift (Qpa) and continental glacial till (Qgt). Glacial drift and glacial till are both glacially derived and typically glacially overridden, resulting in a very compact nature. Particle size distribution typically includes sandy silt, silty sand, and sand with silt, all with variable gravel content. Cobbles and boulders are also commonly present. These units are typically dense to very dense.

#### **Engineering Stratigraphic Units** 5.2

Based on our review of subsurface explorations and accompanying laboratory test results, we have defined engineering stratigraphic units (ESUs) for use in design along the Segment 1A alignment. ESUs were subdivided to account for variations in soil density/consistency and dominant grain size. ESUs defined for design of Grade Separation Barrier 05.33R; Walls 05.55L, 05.85L-A, and 05.85L-B; and embankment EMB: I-405 SB MP 5.97 to 5.83 are summarized below. Subsurface conditions showing the distribution of ESUs are provided on the profiles and design sections presented in Appendices C through G.

#### ESU 1 – Existing Fill

- ESU 1A Loose to Medium Dense Coarse-Grained Fill: This ESU consists of existing fill, typically very loose to loose silty sand and sand with varying amounts of silt, gravel, cobbles, and wood. ESU 1A was encountered directly below the ground surface in borings H-1-85, H-2-85, and H-3-85 near Wall 05.85L-A and embankment EMB: I-405 SB MP 5.97 to 5.83. The elevation range at which ESU 1A was observed is above the existing ground surface at Wall 05.85L-A; therefore, ESU 1A is not expected to be encountered during construction of the wall.
- ESU 1B Medium Dense to Very Dense Coarse-Grained Fill: This ESU consists of existing fill, typically medium dense to very dense silty sand and sand with varying amounts of silt and gravel and localized zones of debris. This ESU was encountered directly below the ground surface in boring W-207-20 near Grade Separation Barrier 05.33R, boring W-215-20 near Wall 05.55L, and borings W-218-20, R2B-10-17, and R2B-11-17 near Wall 05.85L-B.



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### In Association with

ESU 1C - Very Soft to Medium Stiff/Very Loose to Loose Fine-Grained Fill: This ESU consists of existing fill comprised of soft lean clay and construction debris, including brick, coal, plaster, and burnt wood, in boring W-207-20 near Grade Separation Barrier 05.33R. A 16-foot-thick layer of ESU 1C was encountered below ESU 1B and above ESU 4B in boring W-207-20 near Grade Separation Barrier 05.33R.

### ESU 2 - Coarse-Grained Recent Deposits

- ESU 2A Very Loose to Loose Sand/Gravel: This ESU consists of very loose to medium dense silty sand with gravel. Wood may be present locally within this ESU. ESU 2A was encountered in borings H-1-85, H-2-85, and H-3-85 near Wall 05.85L-A and embankment EMB: I-405 SB MP 5.97 to 5.83. This ESU was encountered below ESU 1A and above ESU 2B in borings H-1-85, H-2-85, and H-3-85.
- ESU 2B Medium Dense Sand/Gravel: This ESU consists of loose to dense silty sand and sandy silt with varying amounts of gravel and organics. ESU 2B was encountered in borings H-2-85 and H-3-85 near Wall 05.85L-A and embankment EMB: I-405 SB MP 5.97 to 5.83, and in borings R2B-10-17, R2B-11-17, and W-218-20 near Wall 05.85L-B. Loose to medium dense soils in the unit encountered below the groundwater showed liquefaction potential in boring H-2-85 near Wall 05.85L-A.

### ESU 4 - Glacially Consolidated Coarse-Grained Deposits

ESU 4B - Dense to Very Dense Sand/Gravel. This ESU is typically composed of dense to very dense sand with varying amounts of silt and gravel. Very dense silt was encountered in ESU 4B in boring W-215-20 near Wall 05.55L. ESU 4B was encountered in all borings included in Appendix A of this geotechnical report. All borings included in Appendix A terminated in this unit.

### ESU 5 – Glacially Consolidated Fine-Grained Deposits

ESU 5B - Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt. This ESU consists of hard to very hard clay and hard/very dense silt. A zone of ESU 5B was encountered within ESU 4B in boring W-217-20 near Wall 05.85L-A and embankment EMB: I-405 SB MP 5.97 to 5.83, and in boring W-218-20 near Wall 05.85L-B.

#### 5.3 **Groundwater Conditions**

- 26 The design groundwater elevations used in our engineering analyses were typically based on the highest groundwater levels
- 27 reported on each respective boring log or the nearest available groundwater measurement. The groundwater levels used in
- 28 design are shown on the design sections in Appendices C through G.
- 29 Groundwater was not observed in boring W-207-20 at Grade Separation Barrier 05.33R. We used a groundwater elevation of
- 30 117.3 feet at Bridge 23W based on groundwater observations at the time of drilling in nearby boring H-3-65.
- 31 At Wall 05.55L, we used groundwater observations at the time of drilling boring W-215-20 to define a groundwater level at
- 32 approximately Elevation 140.2 feet.
- 33 At Wall 05.85L-A, groundwater was reported in borings H-1-85, H-2-85, and H-3-85 between Elevation 163 and 210 feet. These
- three borings were advanced in 1985. Groundwater was not observed in boring W-217-20, which was advanced in 2020. Because 34
- of the variability in groundwater observations, we developed a steady state seepage model to evaluate the groundwater level at 35
- Wall 05.85L-A. We used the piezometer data collected in 1985 from boring H-3-85 and measured groundwater at the time of 36
- 37 drilling from boring H-2-85 to inform our model.
- 38 We also used the steady-state seepage analysis results at Wall 05.85L-A to model the groundwater level at the embankment.
- 39 Discussion of our seepage analysis methodology and conclusions are presented in Sections 7.7 and 8.5, respectively. Steady-
- 40 state seepage analysis results are presented in Appendix E.
- 41 Groundwater was not observed in boring W-218-20 at Wall 05.85L-B. Bail tests were performed in 2017 in borings R2B-10-17
- 42 and R2B-11-17. However, both of these borings were advanced using bentonite drilling fluid. In our experience, bail tests
- performed in borings advanced with bentonite drilling fluid can produce unreliable measurements of groundwater level. 43
- 44 Therefore, we also used the steady-state seepage analysis results at Wall 05.85L-A to model the groundwater level at Wall
- 45 05.85L-B.







1 Discussion of our seepage analysis methodology and conclusions are presented in Sections 7.7 and 8.5, respectively. Steadystate seepage analysis results are presented in Appendix E. 2

#### **Engineering Soil Properties** 6.0

#### 6.1 **Design Soil Properties for Existing Soils**

- 5 We selected design soil properties for each ESU based on the subsurface explorations, laboratory testing, and conditions
- described in the GDR, RFP reference documents, and explorations and laboratory testing completed by the design-build team. 6
- 7 Soil properties were developed in accordance with the procedures outlined in the Geotechnical Soil Properties Methodology
- 8 report for this project (Wood 2020).

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- 9 A more detailed description of analyses completed for soil property development is included in Section 7.1 of this report. The
- analyses completed for soil property development for Grade Separation Barrier 05.33R; and Walls 05.55L, 05.85L-A, and 10
- 11 05.85L-B are presented in Appendices C through F, respectively. We applied the soil properties developed for Wall 05.85L-A
- (presented in Appendix E) to embankment EMB: I-405 SB MP 5.97 to 5.83 since we used the same borings to define the ESUs 12
- at the wall and the embankment. Soil properties selected for use in design of Grade Separation Barrier 05.33R; Walls 05.55L, 13
- 05.85L-A, and 05.85L-B; and embankment EMB: I-405 SB MP 5.97 to 5.83 are presented in Tables 3 through 6. 14

# Table 3. Grade Separation Barrier 05.33R Soil Properties by Engineering Stratigraphic Unit (Existing Soil)

|        | ESU Description   |     | Strength                                       | Property                          |                                 |                    |
|--------|---|-----|--|-----------------------------------|---------------------------------|--------------------|
| ESU    |   |     | Effective<br>Friction<br>Angle, φ<br>(degrees) | Effective<br>Cohesion, c<br>(psf) | Elastic<br>Modulus, Es<br>(ksf) | Poisson's<br>Ratio |
| ESU 1B | Medium Dense<br>to Very Dense<br>Coarse-<br>Grained Fill                        | 120 | 36   | 0                                 | 725                             | 0.35               |
| ESU 1C | Very Soft to<br>Medium<br>Stiff/Very<br>Loose to<br>Loose Fine-<br>Grained Fill | 115 | 27   | 0                                 | ND                              | ND                 |
| ESU 4B | Dense to Very<br>Dense<br>Sand/Gravel   | 130 | 43   | 0                                 | ND                              | ND                 |

Abbreviations:

ESU = Engineering Stratigraphic Unit

ND = not developed

ksf = kips per square foot

pcf = pounds per cubic foot

psf = pounds per square foot

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Geotechnical Engineering Report: Grade Separation Barrier 05.33R; Walls 05.55L, 05.85L-A, and 05.85L-B; and Embankment EMB: I-405 SB MP 5.97 to 5.83

File Name: I-405 R2B Segment 1A - Walls Package 2 - RFU







Table 4. Wall 05.55L Soil Properties by Engineering Stratigraphic Unit (Existing Soil)

|        |  | Strength Property          |  |                            |     |                    |
|--------|--|----------------------------|--|----------------------------|-----|--------------------|
| ESU    | Description  | Unit<br>Weight, γ<br>(pcf) | Effective<br>Friction<br>Angle, φ<br>(degrees) | Friction Cohesion, c (ksf) |     | Poisson's<br>Ratio |
| ESU 1B | Medium Dense<br>to Very Dense<br>Coarse-<br>Grained Fill | 130                        | 40   | 0                          | 800 | 0.40               |
| ESU 4B | Dense to Very<br>Dense<br>Sand/Gravel                    | 120                        | 43   | 0                          | ND  | ND                 |

Abbreviations:

ESU = Engineering Stratigraphic Unit

ND = not developed

ksf = kips per square foot

pcf = pounds per cubic foot

psf = pounds per square foot

Table 5. Wall 05.85L-A and Embankment EMB: I-405 SB MP 5.97 to 5.83 Soil Properties by Engineering Stratigraphic Unit (Existing Soil)

|        |  | Total                         | Si   | trength Prope                        |  |                                      |                                    |                    |
|--------|--|-------------------------------|--|--------------------------------------|--|--------------------------------------|------------------------------------|--------------------|
| ESU    | Description  | Unit<br>Weight,<br>γ<br>(pcf) | Effective<br>Friction<br>Angle, φ<br>(degrees) | Effective<br>Cohesion,<br>c<br>(psf) | Apparent<br>Cohesion,<br>c <sub>app</sub><br>(psf) | Residual<br>Strength,<br>Sr<br>(psf) | Elastic<br>Modulus,<br>Es<br>(ksf) | Poisson's<br>Ratio |
| ESU 1A | Loose to<br>Medium Dense<br>Coarse-<br>Grained Fill                | 110                           | 34   | 0                                    | ND   | -                                    | 330 <sup>2</sup>                   | ND                 |
| ESU 2A | Very Loose to<br>Loose Sand/<br>Gravel                             | 110                           | 32   | 0                                    | 100  | -                                    | 530 <sup>3</sup>                   | 0.33               |
| ESU 2B | Medium Dense<br>Sand/<br>Gravel                                    | 110                           | 32   | 0                                    | 200  | 497 <sup>1</sup>                     | 800²                               | ND                 |
| ESU 4B | Dense to Very<br>Dense Sand/<br>Gravel                             | 130                           | 43   | 0                                    | ND   | -                                    | 2,670 <sup>2</sup>                 | ND                 |
| ESU 5B | Very Stiff to<br>Hard Silt and<br>Clay/Dense to<br>Very Dense Silt | 130                           | 43   | 0                                    | ND   | -                                    | ND                                 | ND                 |

Geotechnical Engineering Report: Grade Separation Barrier 05.33R; Walls 05.55L, 05.85L-A, and 05.85L-B; and Embankment EMB: I-405 SB MP 5.97 to 5.83

File Name: I-405 R2B Segment 1A - Walls Package 2 - RFU

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<sup>1.</sup> Residual shear strength was calculated for saturated, potentially liquefiable ESU 2B encountered in boring H-2-85 near Wall 05.85L-A. At embankment EMB: I-405 SB MP 5.97 to 5.83, ESU 2B was encountered above the groundwater, and therefore the residual strength value presented in the table above is not applicable to the embankment.







- 2. Elastic modulus estimated for elastic settlement evaluation at embankment EMB: I-405 SB MP 5.97 to 5.83.
- 3. Elastic modulus estimated for elastic settlement evaluation at Wall 05.85L-A and embankment EMB: I-405 SB MP 5.97 to 5.83.

### Abbreviations:

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ESU = Engineering Stratigraphic Unit

ND = not developed

ksf = kips per square foot

psi = pounds per square inch

pcf = pounds per cubic foot

psf = pounds per square foot

### Table 6. Wall 05.85L-B Soil Properties by Engineering Stratigraphic Unit (Existing Soil)

|        |   |                               | :  | Strength Prope                    |  |                                 |                    |  |
|--------|---|-------------------------------|--|-----------------------------------|--|---------------------------------|--------------------|--|
| ESU    | Description   | Unit<br>Weight,<br>γ<br>(pcf) | Effective<br>Friction<br>Angle, φ<br>(degrees) | Effective<br>Cohesion, c<br>(psf) | Apparent<br>Cohesion,<br>c <sub>app</sub><br>(psf) | Elastic<br>Modulus, Es<br>(ksf) | Poisson's<br>Ratio |  |
| ESU 1B | Medium<br>Dense to<br>Very Dense<br>Coarse-<br>Grained Fill           | 130                           | 41   | 0                                 | 100  | ND                              | ND                 |  |
| ESU 2B | Medium<br>Dense<br>Sand/Gravel  | 115                           | 34   | 0                                 | 200  | 660                             | 0.33               |  |
| ESU 4B | Dense to<br>Very Dense<br>Sand/Gravel                                 | 130                           | 43   | 0                                 | ND   | ND                              | ND                 |  |
| ESU 5B | Very Stiff to<br>Hard Silt and<br>Clay/Dense<br>to Very<br>Dense Silt | 130                           | 42   | 0                                 | ND   | ND                              | ND                 |  |

### Abbreviations:

ESU = Engineering Stratigraphic Unit

ND = not developed

ksf = kips per square foot

psi = pounds per square inch

pcf = pounds per cubic foot

psf = pounds per square foot

#### 6.2 Design Soil Properties for Proposed Fill

Table 7 presents our selected design soil properties to be used for typical WSDOT-specified fill materials. The values shown are derived from Project GDM Section 5.12 and Table 5-2: Presumptive Design Property Ranges for Compacted Borrow and Other WSDOT Standard Specification Materials. The ranges of friction angle and total unit weight values provided in Project GDM Section 5.12 and Table 5-2 are shown in parentheses. We used lightweight expanded polystyrene (EPS) geofoam for backfill in our analyses of future I-405 widening above Walls 05.85L-A and 05.85L-B. Since the configuration we analyzed is







only one potential option for the forward compatible walls, we conservatively selected a high unit weight (above the range provided in Project GDM Section 5.12) and a low shear strength for the EPS properties.

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### Table 7. WSDOT Standard Fill Soil Properties (Proposed Fill)<sup>1</sup>

| Material                                      | WSDOT<br>Standard<br>Specification | Friction<br>Angle², φ<br>(degrees) | Cohesion, c<br>(psf) | Total Unit<br>Weight <sup>2</sup><br>(pcf) |
|---|------------------------------------|------------------------------------|----------------------|--|
| Common Borrow                                 | 9-03.14(3)                         | 32<br>(30 to 34)                   | 03                   | 120<br>(115 to 130)                        |
| Select Borrow                                 | 9-03.14(2)                         | 36<br>(34 to 38)                   | 0                    | 125<br>(120 to 135)                        |
| Gravel Borrow                                 | 9-03.14(1)                         | 38<br>(36 to 40)                   | 0                    | 130<br>(130 to 145)                        |
| Gravel Borrow<br>for Structural<br>Earth Wall | 9-03.14(4)                         | 38<br>(36 to 40)                   | 0                    | 130<br>(130 to 145)                        |
| Gravel Backfill for Walls                     | 9-03.12(2)                         | 38<br>(36 to 40)                   | 0                    | 130<br>(125 to 135)                        |
| Quarry Spalls                                 | 9-13.1(5)                          | 42<br>(40 to 45)                   | 0                    | 110<br>(105 to 120)                        |
| Expanded<br>Polystyrene<br>(EPS) Geofoam      | See Note 4                         | 0                                  | 100 <sup>5</sup>     | 5 <sup>6</sup><br>(1 to 2)                 |

### Notes:

- 1. Based on Project GDM Section 5.12 and Table 5-2.
- 2. Range of soil properties shown in parentheses.
- 3. 50psf apparent cohesion added in pseudo-static analyses for Wall 05.85L-B. See Section 8.7 for discussion.
- 4. Per Project GDM Section 5.12, EPS shall be manufactured according to ASTM C 303 for minimum density and ASTM D 1621 for compressive strength.
- Shear strength is conservatively low.
- Unit weight is conservatively high and outside the typical range.

### Abbreviations:

ASTM = American Society for Testing and Materials

GDM = Geotechnical Design Manual

pcf = pounds per cubic foot

psf = pounds per square foot

WSDOT = Washington State Department of Transportation

#### 7.0 Geotechnical Engineering Analysis Methodology

The following sections describe the methodology associated with the following geotechnical engineering analyses and evaluations:

- Soil property development,
- Seismic hazard analysis,
- Lateral earth pressures,
- Sliding coefficients of friction,
- Shallow foundation bearing resistance and elastic settlement,







- 1 Consolidation settlement,
- 2 Seepage analysis,
- 3 Global stability, and
  - Compound stability

#### **Soil Property Development** 7.1

#### 7.1.1 General 6

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- 7 Design soil properties were developed in accordance with the Project GDM, American Association of State Highway and
- Transportation Officials (AASHTO) Load and Resistance Factor Design (LRFD) Bridge Design Specifications, and Federal 8
- 9 Highway Administration (FHWA) documents, using methods presented in the Geotechnical Soil Properties Methodology
- 10 report for this project (Wood 2020). We calculated the average, geometric mean, and standard deviation within each ESU. We
- checked the reliability of the ESU data set by comparing the coefficient of variation (COV) of each calculated geometric mean 11
- value to measured and interpreted values presented in Sabatini et al. (2002) Table 52. Soil property development supporting 12
- calculations are provided in Appendices C through F. 13

#### 7.1.2 **Unit Weight**

- 15 ESU unit weights were estimated using the procedure outlined in the Geotechnical Soil Properties Methodology report (Wood
- 16 2020) and the 2014 California Department of Transportation (CALTRANS) Geotechnical Manual Unified Soil Classification
- System (USCS) classification based on the field blow counts corrected for overburden pressure and hammer efficiency (N160). 17
- We selected an initial unit weight for each soil sample based on the field (uncorrected) Standard Penetration Test (SPT) blow 18
- 19 count and the soil classification. We used these initial unit weights to calculate the overburden pressure and develop N160 for
- each soil sample. Per CALTRANS, we used the developed N160 of each soil sample to revise our initial selected unit weights. 20
- Revised unit weights were used to estimate the geometric mean unit weight for each ESU. We used the geometric mean to 21
- 22 assign a design unit weight for each ESU. Design unit weights are rounded to the nearest 5 pounds per cubic foot (pcf).
- 23 Initial unit weights selected for each soil sample are presented on the liquefaction input page for each boring in the Design
- 24 Calculations section of Appendices C through F. Revised unit weights for each soil sample and design unit weights for each
- 25 ESU are presented in the ESU Soil Property Calculations section of Appendices C through F.

#### 7.1.3 N<sub>160</sub> and Friction Angle 26

- N1<sub>60</sub> and friction angles were developed in accordance with the Project GDM Section 5.5 and Table 5-1, respectively, using a 27
- 28 spreadsheet developed by GeoEngineers.
- 29 For each ESU, we used the design fines content to estimate the design friction angle from the range of values presented in the
- Project GDM Table 5-1. For soils not subjected to glacial consolidation, the friction angle range lower limit was selected for 30
- design fines contents greater than 30 percent and the upper limit was selected for design fines contents less than 5 percent. For 31
- 32 non-glacially consolidated ESUs with design fines contents between 5 percent and 30 percent, friction angles were selected by
- 33 interpolation between the upper and lower limits presented in the Project GDM Table 5-1. For glacially consolidated soils, we
- 34 capped the friction angle at 43 degrees for ESUs with design fines contents less than 70 percent and used the interpolated
- 35 friction angle for ESUs with fines contents greater than 70 percent.

#### 7.1.4 **Apparent Cohesion**

- 37 Apparent cohesion values were developed for surficial ESUs in accordance with FHWA Geotechnical Engineering Circular
- No. 3, Table 11-2 based on the selected design fines content of the ESU. Where the groundwater is present within or intersects 38
- 39 an ESU, apparent cohesion was applied only to ESUs in which the majority of the ESU layer was above the groundwater table.
- Per Project GDM Section 5.10, apparent cohesion values were only used in pseudo-static global and compound stability 40
- analyses. 41

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#### 7.1.5 **Elastic Modulus and Poisson's Ratio**

- 43 We used soil type and density/consistency to estimate the ESU elastic modulus and Poisson's ratio from empirical relationships
- 44 presented in AASHTO LRFD Table C10.4.6.3-1.





# 7.1.6 Hydraulic Conductivity

- 2 We estimated the hydraulic conductivity of saturated, normally consolidated ESU 2A and ESU 2B using the Schlichter method
- 3 as outlined in the WSDOT Highway Runoff Manual (HRM). We selected hydraulic conductivities for glacially consolidated
- 4 ESU 4B and ESU 5B based on the Laprade and Robinson (1989) values presented in Table 2 of the United States Geological
- 5 Survey (USGS) Open-File Report 00-228. Hydraulic conductivities were used in the seepage analysis (described in Sections
- 6 7.7 and 8.5).

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# 7.2 Seismic Hazard Analysis

## 8 7.2.1 Ground Motion Parameters

- 9 The project site is located within a seismically active area. To select appropriate seismic design parameters, we first evaluated
- site class at each relevant boring using a spreadsheet developed by GeoEngineers in accordance with AASHTO LRFD Section
- 3.10.3.1. Because the explorations did not extend to 100 feet below the ground surface (bgs), we extrapolated soil conditions
- beyond the bottom of the boring. We selected a design site class for the barriers, walls, and embankment, considering the
- distribution of site classes represented by the borings as well as the depths of the borings and the amount of extrapolation to
- 14 100 feet bgs.
- 15 Seismic design parameters for this project were developed using the WSDOT Bridge Engineering Software
- 16 BEToolbox/BridgeLink in accordance with the WSDOT BDM. Seismic parameters, including the peak ground acceleration
- 17 (PGA) and site class adjusted PGA (A<sub>s</sub>), were derived directly from the BEToolbox/BridgeLink software using the latitude,
- longitude, and design site class of each barrier, wall, and embankment. Per Project GDM Section 6.3.1, the ground motion
- 19 parameters for design of the barrier, walls, and the embankment are based on the projected ground motion at the project site
- that has a 7 percent (Safety Evaluation Earthquake [SEE]) probability of exceedance in a 75-year period (approximate
- 21 1,000-year return period).
- 22 Per the National Cooperative Highway Research Program (NCHRP) Report 611 and AASHTO LRFD Section A11.5.2, As can
- 23 be corrected to account for wave scattering effects (vertical variations in the average ground acceleration) for retaining walls,
- slopes, and wall-slope combinations greater than 20 feet in height by applying a wave scatter coefficient, α, to A<sub>s</sub>. In addition,
- a 50 percent reduction can be applied to A<sub>s</sub> for flexible wall systems and slopes capable of 1- to 2-inch displacements during
- the design seismic event.
- 27 Based on the Hart Crowser seismic design report "I-405 R2B Segment 1a Site-Specific Hazard Analysis RFU," dated March
- 28 25, 2021, the mean earthquake magnitude at the PGA period is 6.97 for site class C and 7.0 for site class D for the SEE.
- Design site class and A<sub>s</sub> for Grade Separation Barrier 05.33R; Walls 05.55L, 05.85L-A, and 05.85L-B; and embankment EMB:
- 30 I-405 SB MP 5.97 to 5.83 are presented in Section 8.1.1. The WSDOT BEToolbox/BridgeLink software outputs, calculations
- of corrected A<sub>s</sub> for Walls 05.85L-A and 05.85L-B, and our site class calculations are provided in Appendices C through F.

# **7.2.2 Liquefaction Potential**

- We evaluated the factor of safety (FS) against liquefaction and liquefaction-induced settlement of saturated, very loose to
- medium dense soils in accordance with Chapter 6 of the Project GDM using a spreadsheet developed by GeoEngineers. The
- 35 spreadsheet uses methodology from Youd et al. (2001) and Idriss and Boulanger (2008 with 2014 updates) to identify
- 36 liquefaction potential. Per Section 6-4.2.3 of the Project GDM, soils with liquefaction potential are defined as those with FS
- against liquefaction less than 1.2.
- 38 Liquefaction potential is presented in Section 8.1.2, and supporting calculations are provided in Appendices C through F.

# 39 7.2.3 Residual Shear Strength

- 40 Residual shear strength was calculated for liquefiable soils from existing relationships and procedures outlined in Project GDM
- 41 Section 6-2.2 using a spreadsheet developed by GeoEngineers. Residual strength calculations become unconservatively high
- 42 for liquefiable soils with an N160 corrected to an equivalent clean sand [N160(cs)] that is greater than 20. Using guidance
- 43 presented in WSDOT Report WA-RD 668.1 (Kramer 2008), we capped N160(cs) at 20 to calculate a residual shear strength for
- soils exhibiting liquefaction potential (FS against liquefaction < 1.2).







Residual shear strengths are presented in Section 8.1.3 and supporting calculations are provided in Appendix E. 1

#### **Lateral Earth Pressures** 7.3 2

- 3 Imported backfill will be placed between the existing and proposed grades at Grade Separation Barrier 05.33R and Walls
- 05.55L, 05.85L-A, and 05.85L-B. At Walls 05.85L-A and 05.85L-B, imported fill will also be placed within the reinforced 4
- 5 zone and between the reinforced zone and the face of the temporary shoring.
- Lateral earth pressures for native soils and imported fill materials were calculated in accordance with AASHTO LRFD 3.11.5 6
- 7 for the proposed slopes in front of and behind the barrier and walls. In addition, active lateral earth pressures on Grade
- 8 Separation Barrier 05.33R were calculated using a barrier back face batter of 4H:21V (10.8 degrees from vertical).
- 9 We analyzed seismic earth pressures for Walls 05.55L, 05.85L-A, and 05.85L-B. Seismic earth pressures on Wall 05.55L were
- 10 calculated in accordance with AASHTO LRFD Section 11.6.5.3 using the Mononobe-Okabe (M-O) Method. Seismic earth
- pressures on Walls 05.85L-A and 05.85L-B were developed using the Generalized Limit Equilibrium (GLE) Method in 11
- 12 accordance with AASHTO LRFD Section A11.3.3 and NCHRP Report 611 Section 7.4. The GLE analysis was evaluated for
- 13 Spencer's method using the computer design software Slope/W (Geo Slope International, Ltd. 2020). To calculate seismic
- 14 earth pressures, we used a modified horizontal seismic coefficient, kh, coupling a 50 percent reduction for flexible wall
- 15 displacements with a reduction for wave scattering effects.
- 16 Lateral earth pressures and load factor recommendations are presented in Section 8.2. Supporting calculations are provided in
- 17 Appendices C through F.

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#### 7.4 Sliding Coefficients of Friction

- 19 Coefficients of friction for sliding were calculated using AASHTO LRFD equation 10.6.3.4-2. Sliding coefficients were
- 20 calculated for CIP and precast concrete barriers at Grade Separation Barrier 05.33R, and for CIP concrete footings at Wall
- 21 05.55L on surficial native soils and imported fills. Per AASHTO LRFD Section 11.10.5.3, sliding coefficients of friction for
- Walls 05.85L-A and 05.85L-B were calculated for SEW discontinuous reinforcements (strips). For the discontinuous 22
- 23 reinforcements at Walls 05.85L-A and 05.85L-B, sliding coefficients of friction were calculated using the friction angle of the
- foundation soil (surficial native soils or imported fills) or the reinforced fill soil (gravel borrow for structural earth wall), 24
- 25 whichever was less.
- Sliding coefficients are presented in Section 8.3. Supporting calculations are provided in Appendices C through F. 26

# Shallow Foundation Bearing Resistance and Elastic Settlement

- 28 Bearing resistance for nominal (unfactored), Service, Strength, and Extreme Event Limit States was calculated using a
- spreadsheet developed by GeoEngineers in accordance with the methodology described in AASHTO LRFD Section 10.6.3. We 29
- 30 estimated elastic settlement for the barriers and walls from procedures outlined in AASHTO LRFD Section 10.6.2.4. Sliding
- and overturning of the barrier and walls are being evaluated by the design-build team's wall designers and will be submitted 31
- under separate cover. 32
- We estimated the bearing resistance and elastic settlement of the barrier and walls for the following effective widths: 33
  - Grade Separation Barrier 05.33R- effective barrier widths between 2 and 6 feet
  - Wall 05.55L effective footing widths between 3 and 11 feet
  - Wall 05.85L-A effective SEW widths between 5 and 25 feet
  - Wall 05.85L-B effective SEW widths between 5 and 21 feet
- We estimated the static elastic settlement of embankment EMB: I-405 SB MP 5.97 to 5.83 following the placement of new fill 38
- (common borrow) using the computer design software Settle3 (Rocscience 2021). We modeled the applied fill load along the 39
- approximate length of the embankment (160 feet) and the approximate length of the fill slope (80 feet) at the design section. 40
- We used the elastic moduli of the ESUs presented in Table 5 to evaluate immediate settlement of the embankment. 41
- 42 Bearing resistance and elastic settlement results are presented in Section 8.4. Supporting calculations are provided in
- Appendices C through F. Settle3 output reports for embankment EMB: I-405 SB MP 5.97 to 5.83 are provided in Appendix H. 43







#### 7.6 Consolidation Settlement

- 2 Compressible soils, such as organic soil or normally consolidated/slightly over consolidated high plasticity silts or clays, were
- 3 not identified in the explorations near Grade Separation Barrier 05.33R; Walls 05.55L, 05.85L-A, and 05.85L-B; and
- embankment EMB: I-405 SB MP 5.97 to 5.83. Therefore, we do not anticipate long-term consolidation settlement to occur as a 4
- 5 result of new loads.

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#### 7.7 Seepage Analysis

- 7 Seepage analysis was performed using the finite element seepage modeling software, Seep/W (Geo Slope International, Ltd.
- 2020) to estimate a steady state groundwater level for Wall 05.85L-A. Groundwater levels developed in the seepage analysis 8
- 9 for Wall 05.85L-A were also used in our evaluations of Wall 05.85L-B, and embankment EMB: I-405 SB MP 5.97 to 5.83. We
- used existing groundwater measurements from piezometers in borings H-2-85 and H-3-85, soil hydraulic conductivity 10
- properties, and typical local precipitation data to develop a model of groundwater conditions and seepage patterns. 11
- 12 A discussion of the model development and conclusions is presented in Section 8.5 and the steady-state seepage results are
- presented in Appendix E. Seep/W output reports are provided in Appendix I. 13

#### 7.8 **Global Stability**

- 15 Global stability was evaluated using limit equilibrium analysis following the procedure outlined in the Project GDM. We
- 16 evaluated global stability of Grade Separation Barrier 05.33R; Walls 05.55L, 05.85L-A, and 05.85L-B; and embankment
- 17 EMB: I-405 SB MP 5.97 to 5.83 using the computer design software Slope/W (Geo Slope International, Ltd. 2020). Factors of
- safety were developed using both Spencer's method and the Morgenstern-Price method with entry and exit search limits for a 18
- 19 circular failure surface.
- 20 We modeled Grade Separation Barrier 05.33R and Wall 05.55L as a "High Strength" material having a unit weight of 150 pcf.
- We modeled the SEW and forward compatible walls at Walls 05.85L-A and 05.85L-B as a "High Strength" material having a 21
- 22 unit weight of 130 pcf. We used the design backfill properties presented in Table 7 for the materials listed below at the
- following fill locations: 23
  - Backfill behind Grade Separation Barrier 05.33R and Wall 05.55L common borrow
  - Backfill between reinforced zone and temporary shoring at Walls 05.85L-A and 05.85L-B gravel borrow
  - Fill between existing and proposed grades for Walls 05.85L-A and 05.85L-B common borrow
  - Backfill behind forward compatible walls at Walls 05.85L-A and 05.85L-B EPS
  - Embankment fill (EMB: I-405 SB MP 5.97 to 5.83) common borrow
- Rock buttress to mitigate 1985 fill slope failure (EMB: I-405 SB MP 5.97 to 5.83) gravel borrow and quarry spalls. 29
- 30 Grade Separation Barrier 05.33R will be designed in accordance with WSDOT BDM Section 10.3.1 for differential grade
- concrete barriers of 4 feet or less. Grade Separation Barrier 05.33R and embankment EMB: I-405 SB MP 5.97 to 5.83 follow 31
- procedures in Project GDM Chapter 9 for embankments to evaluate global stability. Per Project GDM Section 9.2.3.1, seismic 32
- global stability analyses are not required for the barrier or the embankment since they are not supporting or potentially 33
- 34 impacting structures.
- 35 The Hart Crowser Released for Use (RFU) geotechnical letter "Design Requirements and Geotechnical Assessment of
- Retaining Walls" dated January 26, 2021, defines the minimum allowable distance to the travel lane (MADTL) as the "the 36
- minimum distance the wall must exist from the travel lane to prevent an elevation change of greater than 1 foot". If the 37
- MADTL is less than the distance between the wall and the travel lane, seismic failure of the wall will not severely impact the 38
- 39 traveled way or compromise the life safety of the public, and therefore a detailed seismic analysis is not necessary. Based on
- Figure 1A in the Hart Crowser RFU geotechnical letter, the MADTL at Wall 05.55L is 6.4 feet. It is our understanding that an 40
- 8-foot-wide shoulder will separate the back of Wall 05.55L and the travel lane. According to the criteria outlined in the Hart 41
- 42 Crowser RFU geotechnical letter noted above, a seismic slope instability analysis is not required for Wall 05.55L since
- 43 collapse of the wall would not affect the travel lane or compromise public safety.
- For pseudo-static analyses of Walls 05.85L-A and 05.85L-B, we used an apparent cohesion in surficial native soils based on 44
- 45 the fines content ranges presented in Table 11-2 of the FHWA Geotechnical Engineering Circular No. 3.







- 1 We evaluated post-seismic global stability using residual shear strengths for potentially liquefiable soil.
- 2 A uniform traffic surcharge of 250 pounds per square foot (psf) was included in the static global stability analysis where a
- 3 roadway is present above the wall or barrier. In accordance with Section 15-4.12 of the Project GDM, we used a load factor of
- 4 1.0 for traffic surcharge for the static global stability analysis because it is a non-structural load. A uniform traffic surcharge of
- 5 125 psf, which is 50 percent of the static traffic surcharge, was included in the seismic (pseudo-static and post-seismic) global
- stability analyses where a roadway is present above the wall. Per AASHTO LRFD Section 3.4.1, we used an extreme event 6
- 7 limit state load factor of 0.5 for the traffic surcharge for the seismic (pseudo-static and post-seismic) global stability analyses.
- Groundwater levels were modeled using a piezometric surface. The piezometric surface was based on measured or observed 8
- 9 groundwater levels at Grade Separation Barrier 05.33R and Wall 05.55L. We used the results from the seepage analysis to
- 10 model the piezometric surface at Walls 05.85L-A and 05.85L-B, and embankment EMB: I-405 SB MP 5.97 to 5.83.
- 11 The results of our global stability analyses for Grade Separation Barrier 05.33R; Walls 05.55L, 05.85L-A, and 05.85L-B; and
- 12 embankment EMB: I-405 SB MP 5.97 to 5.83 are presented in Section 8.6. Global stability models showing FS for critical
- 13 failures at the design sections are provided in Appendices C through G. Slope/W output reports for global stability are provided
- 14 in Appendix J.

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#### 7.9 **Compound Stability**

- 16 We evaluated compound stability at Walls 05.85L-A and 05.85L-B using the computer design software Slope/W (Geo Slope
- 17 International, Ltd. 2020) to perform limit equilibrium analysis following the procedure outlined in Project GDM Section 15-
- 5.3.4. Factors of safety were developed using both Spencer's method and the Morgenstern-Price method with entry and exit 18
- 19 search limits for a circular failure surface.
- 20 We modeled the soil reinforcements as inextensible ribbed steel strips connected to precast concrete facing panels. The
- 21 reinforcing strips are 2 inches wide and 5/32 inches thick grade 65 steel with galvanized corrosion protection. We calculated
- 22 the corrosion loss over 75 years using steel corrosion rates presented in AASHTO LRFD Section 11.10.6.4.2a and FHWA
- 23 Geotechnical Engineering Circular No. 11 Tables 3-7 and 3-8. We used the Reinforced Earth Company (RECO) standard
- 24 precast concrete 5 feet by 5 feet facing panel "A" shop drawings provided in Project GDM Appendix 15-I to model the spacing
- of the reinforcing strips. Based on the facing panel "A" layout, each panel contains 2 rows and each row contains 2 reinforcing 25
- 26 strips.
- 27 We applied resistance factors presented in AASHTO LRFD Section 11.5 and FHWA Geotechnical Engineering Circular No.
- 28 11 Table 4-7 to calculate the pullout resistance and tensile capacity of the reinforcing strips. We modeled the reinforced fill as
- gravel borrow with a coefficient of uniformity (Cu) of 6.3. Per AASHTO LRFD Section 11.10.6.3.2 and FHWA Geotechnical 29
- 30 Engineering Circular No. 11 Section 3.4.2, a pullout resistance factor, F\*, is equivalent to 2.0 at the ground surface when Cu is
- 31 equal to or greater than 6.3. The reinforced zone fill, Gravel Borrow for Structural Earth Wall, imported during construction
- shall have a minimum Cu value of 6.3, as specified in Section 8.13.4. We used an F\* of 2.0 at the ground surface to estimate 32
- 33 the pullout resistance of the reinforcing strips. We used the pullout resistance to calculate an interface shear friction angle at
- 34 each reinforcing strip, considering the strip width and spacing. The calculated tensile capacity and interface shear friction
- 35 angles were input into Slope/W to model the reinforcing strips in the reinforced zone.
- For pseudo-static analyses of Walls 05.85L-A and 05.85L-B, we used an apparent cohesion in the surficial native soils based 36
- 37 on the fines content ranges presented in Table 11-2 of the FHWA Geotechnical Engineering Circular No. 3.
- 38 We evaluated post-seismic compound stability using residual shear strengths for potentially liquefiable soil.
- 39 Per Project GDM Section 15-5.3.4 and AASHTO LRFD Table 3.4.1-1, a strength limit state load factor of 1.75 was applied to
- 40 the standard traffic surcharge of 250 psf directly over the reinforced zone, resulting in a uniform traffic surcharge of 437.5 psf
- 41 directly over the reinforced zone and a uniform traffic surcharge of 250 psf outside of the reinforced zone in the static
- 42 compound stability analysis of Walls 05.85L-A and 05.85L-B. Per AASHTO LRFD Section 3.4.1, an extreme event limit state
- load factor of 0.5 was applied to the standard traffic surcharge of 250 psf, resulting in a uniform traffic surcharge of 125 psf 43
- across all traffic lanes (both directly over and outside the reinforced zone) for the seismic (pseudo-static and post-seismic) 44
- 45 compound stability analyses.







- 1 Groundwater levels for Walls 05.85L-A and 05.85L-B were modeled using a piezometric surface based on the results from the 2 seepage analysis at Wall 05.85L-A.
- 3 The results of our compound stability analyses for Walls 05.85L-A and 05.85L-B are presented in Section 8.7. Compound
- stability models showing FS for critical failures at the design sections are provided in Appendices E and F. Slope/W output 4
- 5 reports for compound stability are provided in Appendix K.

#### **Conclusions and Recommendations** 8.0

#### 8.1 Seismic Design

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#### 8.1.1 **Ground Motion Parameters**

- 9 We selected the design site class for the barrier, walls, and embankment using SPT blow counts of nearby explorations and the
- methodology presented in AASHTO LRFD Section 3.10.3.1. Ground motion parameters for a ground motion with 7 percent 10
- probability of exceedance in a 75-year period (approximate 1,000-year return period) (SEE hazard level) were developed using 11
- 12 the WSDOT Bridge Engineering Software BEToolbox/BridgeLink. Based on deaggregation data from Hart Crowser (2021),
- we used a mean earthquake magnitude of 6.97 for site class C and 7.0 for site class D for the SEE. 13
- 14 We used a horizontal seismic acceleration coefficient (kh) to estimate seismic lateral earth pressures and evaluate pseudo-static
- 15 global and compound stability. For our analyses, kh is reduced to 50 percent of  $A_s$  (kh = 0.5 \*  $A_s$ ) for flexible wall
- displacements of 1- to 2-inches, and reduced for the wall height-dependent seismic coefficient (wave scatter coefficient), α (kh 16
- $= \alpha * A_s$ ) for wave scattering effects. Per AASHTO LRFD Section 11.6.5.2.2, the wall height was taken as the distance from 17
- the bottom of the back of the wall to the ground surface directly above the back of the wall for seismic lateral earth pressure 18
- analyses. For global and compound pseudo-static analyses, wave scatter was based on the height of the failure surface 19
- mobilized in the design seismic event. Wave scatter reductions were not applied for heights less than 20 feet. 20
- The representative design site class, SEE As, and kh are summarized in Table 8. WSDOT BDM software outputs, site class 21 determination, and wave scatter calculations are provided in Appendices C through F. 22

Table 8. Design Site Class and Adjusted Peak Ground Acceleration Parameters

| Design Element  | Site Class | SEE As | Seismic Analysis       | Wave Scatter<br>Coefficient, α<br>(Proposed/FC) | Horizontal Seismic<br>Acceleration<br>Coefficient, kh<br>(kh = 0.5 * α * A <sub>s</sub> )<br>(Proposed/FC) |
|---|------------|--------|------------------------|---|--|
| Grade Separation<br>Barrier 05.33R <sup>1</sup>               | D          | 0.505  | Lateral Earth Pressure | Not Applicable                                  | 0.253  |
| Wall 05.55L <sup>2</sup>                                      | D          | 0.505  | Lateral Earth Pressure | Not Applicable                                  | 0.253  |
|   | D          |        | Lateral Earth Pressure | 0.815   | 0.206  |
| Wall 05.85L-A   |            | 0.505  | Global Stability       | 0.753 / 0.756                                   | 0.190 / 0.191  |
|   |            |        | Compound Stability     | 0.765 / 0.765                                   | 0.193 / 0.193  |
|   |            |        | Lateral Earth Pressure | 0.808   | 0.210  |
| Wall 05.85L-B   | С          | 0.520  | Global Stability       | 0.755 / 0.756                                   | 0.196/ 0.197   |
|   |            |        | Compound Stability     | 0.799 / 0.753                                   | 0.208 / 0.196  |
| Embankment<br>EMB: I-405 SB<br>MP 5.97 to 5.83 <sup>1,3</sup> | D          | 0.505  | Not Applicable         | Not Applicable                                  | Not Applicable   |

Notes:

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Per Project GDM Section 9.2.3.1, seismic stability analyses are not required.







- 2. Per Hart Crowser's RFU geotechnical letter "Design Requirements and Geotechnical Assessment of Retaining Walls" 1 (2021), seismic stability analyses are not required. 2
- 3. Lateral earth pressures are not applicable for the embankment. 3
  - Abbreviations:

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- A<sub>s</sub> = site class adjusted peak ground acceleration 5
- FC = forward compatible wall 6
- SEE = Safety Evaluation Earthquake 7

# **Liquefaction and Liquefaction-Induced Settlement**

- 9 We analyzed the borings at the barrier, wall, and embankment locations for liquefaction potential of saturated, loose to medium 10 dense soil. We used the SEE As for our liquefaction evaluation.
- 11 Potentially liquefiable soil was not encountered in any of the borings near Grade Separation Barrier 05.33R, Wall 05.55L, and
- 12 Wall 05.85L-B. Potentially liquefiable soil was encountered in boring H-2-85 near Wall 05.85L-A and embankment EMB: I-
- 405 SB MP 5.97 to 5.83. Based on our review, saturated, low-plasticity portions of ESU 2B at Wall 05.85L-A may be 13
- liquefiable. Estimated liquefaction related settlement ranges from 2 to 4 inches, considering the full thickness of ESU 2B 14
- present at H-2-85. We estimate that differential liquefaction settlements in ESU 2B could be on the order of 1 to 2 inches. 15
- However, based on the planned base of wall elevation, we do not anticipate that a significant thickness of ESU 2B will remain 16
- 17 below the base of the wall. In addition, based on our groundwater model, we anticipate that any ESU 2B material remaining
- below the wall will not be saturated. Therefore, we do not anticipate liquefaction or related settlement of soil beneath the wall. 18
- Saturated portions of ESU 2B downslope of the wall may experience liquefaction and related settlement. 19
- 20 We used boring H-2-85 to develop the soil properties at embankment EMB: I-405 SB MP 5.97 to 5.83. Based on our
- interpretation of the subsurface, ESU 2B is above the groundwater table at the embankment and therefore, potentially 21
- 22 liquefiable soils were not encountered at the embankment.
- 23 In our analysis, we did not allow glacially consolidated deposits (ESU 4B and ESU 5B) to liquefy.
- 24 Details of our liquefaction analyses, including plots and liquefaction spreadsheet input and output pages, are provided in
- 25 Appendices C through F. Summaries of our liquefaction results for the barrier, walls, and embankment during the design SEE
- event are presented in Tables 9 through 12 below. Potential impacts of liquefaction on global and compound stability are 26
- addressed in Sections 8.6 and 8.7, respectively. 27

### Table 9. Grade Separation Barrier 05.33R Liquefaction Summary

| Boring<br>Designation | Liquefaction<br>(Y/N) | Top of<br>Boring<br>Elevation<br>(NAVD 88)<br>(feet) | Groundwater<br>Elevation <sup>1</sup><br>(NAVD 88)<br>(feet) | Estimated<br>Liquefaction<br>Depth<br>Range<br>(feet) | Estimated<br>Liquefaction<br>Elevation<br>Range<br>(NAVD 88)<br>(feet) | Estimated<br>Cumulative<br>Settlement<br>Range<br>(inch) |
|-----------------------|-----------------------|--|--|---|--|--|
| W-207-20              | N                     | 128.2  | 117.3  | -   | -  | -  |

#### Notes:

1. Groundwater elevation based on piezometric data in nearby boring H-3-65.

Abbreviations:

NAVD 88 = North American Vertical Datum of 1988

Y/N = Yes/No34

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| Boring<br>Designation | Liquefaction<br>(Y/N) | Top of<br>Boring<br>Elevation<br>(NAVD 88)<br>(feet) | Groundwater<br>Elevation <sup>1</sup><br>(NAVD 88)<br>(feet) | Estimated<br>Liquefaction<br>Depth<br>Range<br>(feet) | Estimated<br>Liquefaction<br>Elevation<br>Range<br>(NAVD 88)<br>(feet) | Estimated<br>Cumulative<br>Settlement<br>Range<br>(inch) |
|-----------------------|-----------------------|--|--|---|--|--|
| W-215-20              | N                     | 171.2  | 140.2  | -   | -  | -  |

Table 10. Wall 05.55L Liquefaction Summary

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1. Groundwater elevation based on observations at time of drilling.

Abbreviations:

NAVD 88 = North American Vertical Datum of 1988

Y/N = Yes/No

Table 11. Wall 05.85L-A and Embankment EMB: I-405 SB MP 5.97 to 5.83 Liquefaction Summary

| Boring<br>Designation | Liquefaction<br>(Y/N) | Top of<br>Boring<br>Elevation<br>(NAVD 88)<br>(feet) | Groundwater<br>Elevation <sup>1</sup><br>(NAVD 88)<br>(feet) | Estimated<br>Liquefaction<br>Depth<br>Range<br>(feet) | Estimated<br>Liquefaction<br>Elevation<br>Range<br>(NAVD 88)<br>(feet) | Estimated<br>Cumulative<br>Settlement<br>Range<br>(inch) |
|-----------------------|-----------------------|--|--|---|--|--|
| W-217-20              | N                     | 219.6  | 209.0  | -   | -  | -  |
| H-1-85                | N                     | 200.6  | 181.0  | -   | -  | -  |
| H-2-85                | Y <sup>2</sup>        | 186.1  | 162.0  | 24 to 36  | 162.1 to 150.1   | 2 to 4   |
| H-3-85                | N                     | 216.0  | 186.0  | -   | -  | -  |

### Notes:

- 1. Groundwater elevation based on results from seepage analysis at Wall 05.85L-A.
- 2. Potentially liquefiable soils were encountered at Wall 05.85L-A. Potentially liquefiable soils were not encountered at embankment EMB: I-405 SB MP 5.97 to 5.83.

Abbreviations:

NAVD 88 = North American Vertical Datum of 1988

Y/N = Yes/No

Table 12. Wall 05.85L-B Liquefaction Summary

| Boring<br>Designation | Liquefaction<br>(Y/N) | Top of<br>Boring<br>Elevation<br>(NAVD 88)<br>(feet) | Groundwater<br>Elevation <sup>1</sup><br>(NAVD 88)<br>(feet) | Estimated<br>Liquefaction<br>Depth<br>Range<br>(feet) | Estimated<br>Liquefaction<br>Elevation<br>Range<br>(NAVD 88)<br>(feet) | Estimated<br>Cumulative<br>Settlement<br>Range<br>(inch) |
|-----------------------|-----------------------|--|--|---|--|--|
| W-218-20              | N                     | 238.6  | 210.0  | -   | -  | -  |
| R2B-11-17             | N                     | 219.2  | 199.0  | -   | -  | -  |
| R2B-10-17             | N                     | 210.2  | 194.0  | -   | -  | -  |

Notes:

1. Groundwater elevation based on seepage analysis at Wall 05.85L-A.

Abbreviations: 23

NAVD 88 = North American Vertical Datum of 1988 24

Y/N = Yes/No25





# 8.1.3 Residual Shear Strength

- 2 We evaluated post-earthquake residual shear strengths of saturated, loose to medium dense soil exhibiting liquefaction
- 3 potential. Residual shear strengths were estimated for potentially liquefiable soil identified in ESU 2B in boring H-2-85 at Wall
- 4 05.85L-A. We applied a residual shear strength to portions of ESU 2B below the water table in our post-seismic global and
- 5 compound stability analyses at Wall 05.85L-A.
- 6 The calculated residual shear strength of liquefiable soils is provided on the liquefaction spreadsheet output pages in Appendix
- 7 E. For our analysis of Wall 05.85L-A, we used the geomean residual shear strength of 497 psf calculated in Appendix E and
- 8 presented in Table 5.

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# 8.2 Lateral Earth Pressures

- We estimated the lateral earth pressures of the backfill placed between the existing and proposed grades at Grade Separation
- Barrier 05.33R and Wall 05.55L. At Grade Separation Barrier 05.33R and Wall 05.55L, the backfill will consist of compacted
- 12 common borrow or better imported fill; in our analyses, we estimated the lateral earth pressures of common borrow, select
- borrow, and gravel borrow at Grade Separation Barrier 05.33R and Wall 05.55L. We used a 4H:21V (10.8 degrees from
- vertical) batter on the back face of the barrier to calculate lateral earth pressures. We evaluated a 3.2H:1V (17.5 degrees from
- horizontal) backslope for Grade Separation Barrier 05.33R and a 3.7H:1V (15 degrees from horizontal) foreslope for Wall
- 16 05.55L. We applied an interface friction angle,  $\delta$ , equal to two-thirds of the backfill friction angle to estimate the active earth
- 17 pressures on Wall 05.55L; we did not apply a δ to Grade Separation Barrier 05.33R.
- We estimated the active static and active static + seismic lateral earth pressures for Grade Separation Barrier 05.33R and Wall
- 19 05.55L using the M-O method. Per AASHTO LRFD Section 11.6.5.2.2, the seismic horizontal acceleration coefficient, kh, can
- 20 be reduced to 50 percent of A<sub>s</sub> for retaining structures capable of 1- to 2-inches of displacement during the design seismic
- event. Accordingly, we reduced kh to 50 percent of As to evaluate the active static + seismic earth pressures. The kh value used
- 22 in our analysis for Grade Separation Barrier 05.33R and Wall 05.55L is presented in Table 8.
- At Walls 05.85L-A and 05.85L-B, the backfill between the reinforced zone and the temporary shoring will consist of gravel
- backfill for walls. However, since this backfill zone will be relatively thin, we conservatively estimated active static lateral
- earth pressures for native soils ESU 2A and ESU 2B behind Walls 05.85L-A and 05.85L-B, respectively. We evaluated the
- lateral earth pressures for a 2H:1V (27 degrees from horizontal) backslope at each wall, with a 2H:1V (27 degrees from
- horizontal) and a 3.7H:1V (15 degrees from horizontal) foreslope at Walls 05.85L-A and 05.85L-B, respectively. Per
- 28 AASHTO LRFD Section 11.10.5.2, we applied a δ equal to two-thirds of the retained soil friction angle for Walls 05.85L-A
- 29 and 05.85L-B.
- We estimated the active static lateral earth pressures for Walls 05.85L-A and 05.85L-B using the M-O method. We estimated
- 31 the active static + seismic lateral earth pressures for Walls 05.85L-A and 05.85L-B using the GLE method. To evaluate the
- active static + seismic earth pressures at the back of the walls, we removed the SEW and all soil directly above the SEW in our
- 33 models to simulate the interface between the reinforced soil and the retained soil. We applied a force at the face of the retained
- 34 soil at heights of one-third and one-half from the base of the wall to determine the maximum active static + seismic earth
- pressure. The applied force was inclined at the friction angle of ESU 2A and ESU 2B at Walls 05.85L-A and 05.85L-B,
- 36 respectively. We varied the magnitude of the force until a FS equal to 1.0 was achieved. We back-calculated the active static +
- 37 seismic earth pressure coefficient, kae, and active static + seismic lateral earth pressure from the selected maximum seismic
- 38 force on the wall.
- 39 Per the Project GDM and AASHTO, flexible SEWs are capable of 1- to 2-inches of displacement during the design seismic
- 40 event, and therefore the seismic horizontal acceleration coefficient, kh, can be reduced to 50 percent of A<sub>s</sub> to evaluate seismic
- 41 earth pressures. Per AASHTO and NCHRP Report 611, kh can be further reduced for wave scattering effects using the height-
- dependent seismic coefficient (wave scatter coefficient), α. We applied the reduction for flexible wall systems and wave scatter
- 43 to kh for the seismic earth pressure analyses using the GLE method for Walls 05.85L-A and 05.85L-B. The kh value used in
- our analyses for Walls 05.85L-A and 05.85L-B is presented in Table 8.
- 45 Passive resistance for Grade Separation Barrier 05.33R and Walls 05.55L, 05.85L-A, and 05.85L-B shall be ignored due to the
- 46 shallow embedment and foreslope condition at the barrier and walls. Active static lateral earth pressure coefficients, ka, and
- 47 active static + seismic earth pressure coefficients, kae, and the corresponding lateral earth pressures on the back of Grade



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### In Association with

Separation Barrier 05.33R and Walls 05.55L, 05.85L-A, and 05.85L-B are presented in Table 13. We recommend active lateral earth pressures be applied using a triangular distribution. We recommend applying an LRFD load factor of 1.5 to the static earth pressures in accordance with AASHTO LRFD Table 3.4.1-2 and an LRFD load factor of 1.0 to the static + seismic earth pressures in accordance with AASHTO LRFD Table 3.4.1-1. Supporting calculations are provided in Appendices C through F. Appropriate surcharge loads (such as traffic loading, fill loads above the barrier and walls, and forward compatible loads) and the corresponding load factors shall be applied when evaluating wall stability. All surcharge loads shall apply load factors in accordance with AASHTO LRFD Tables 3.4.1-1 and 3.4.1-2.

Table 13. Grade Separation Barrier 05.33R, and Walls 05.55L, 05-85L-A, and 05.85L-B Active Lateral Earth Pressure Coefficients and Active Lateral Earth Pressures<sup>1,2</sup>

| Design                | Foreslope | Backslope | Material  | Pres          | teral Earth<br>ssure<br>ficient |        | -ateral Earth<br>ure (pcf) <sup>1, 2</sup> |
|-----------------------|-----------|-----------|---|---------------|---------------------------------|--------|--|
| Element               | (degrees) | (degrees) |   | Static,<br>ka | Static +<br>Seismic,<br>kae     | Static | Static +<br>Seismic                        |
| Grade                 |           |           | Common Borrow   | 0.49          | 1.04                            | 59*H   | 125*H                                      |
| Separation<br>Barrier | 0         | 17.5      | Select Borrow   | 0.42          | 0.76                            | 52*H   | 95*H                                       |
| 05.33R <sup>3</sup>   |           |           | Gravel Borrow   | 0.39          | 0.69                            | 50*H   | 90*H                                       |
|                       |           | 0         | Common Borrow   | 0.28          | 0.48                            | 33*H   | 57*H                                       |
| Wall 05.55L           | 15        |           | Select Borrow   | 0.23          | 0.42                            | 29*H   | 53*H                                       |
|                       |           |           | Gravel Borrow   | 0.22          | 0.39                            | 28*H   | 51*H                                       |
| Wall<br>05.85L-A      | 27        | 27        | ESU 2A (static)<br>Retained Native Soil<br>(static + seismic) | 0.46          | 0.87                            | 51*H   | 95*H                                       |
| Wall<br>05.85L-B      | 15        | 27        | ESU 2B (static)<br>Retained Native Soil<br>(static + seismic) | 0.41          | 1.1                             | 47*H   | 126*H                                      |

### Notes:

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- 1. Active lateral earth pressures (static and static + seismic) shall be applied using a triangular distribution.
- 2. Earth pressures do not include surcharge loads, such as traffic loading or forward compatible wall loading.
- 3. Barrier back face batter = 4H:21V (horizontal:vertical)

#### Abbreviations:

- ESU = Engineering Stratigraphic Units 16
- H = Height of the retained soil behind the wall 17

#### 8.3 Sliding Coefficients of Friction

- 19 We used AASHTO LRFD equation 10.6.3.4-2 to estimate the sliding coefficients of friction for native soils and for imported fills (common borrow, select borrow, and gravel borrow) beneath the barrier and walls. 20
- Sliding coefficients for CIP and precast concrete barriers for Grade Separation Barrier 05.33R and CIP concrete footings for 21
- Wall 05.55L are presented in Table 14 and supporting calculations are provided in Appendices C and D. Sliding coefficients 22
- for SEW discontinuous reinforcements for Walls 05.85L-A, and 05.85L-B are presented in Table 15 and supporting 23
- calculations are provided in Appendices E and F. 24







Table 14. Grade Separation Barrier 05.33R and Wall 05.55L Sliding Coefficients of Friction

| Grade                      | Foundation    | Sliding Coefficients of Friction |                 |  |
|----------------------------|---------------|----------------------------------|-----------------|--|
| Separation<br>Barrier/Wall | Material      | CIP Barrier                      | Precast Barrier |  |
|                            | ESU 1B        | 0.73                             | 0.58            |  |
| Grade Separation           | Common Borrow | 0.62                             | 0.50            |  |
| Barrier 05.33R             | Select Borrow | 0.73                             | 0.58            |  |
|                            | Gravel Borrow | 0.78                             | 0.63            |  |
|                            | ESU 1B        | 0.84                             | Not Applicable  |  |
| Wall 05.55L                | Common Borrow | 0.62                             | Not Applicable  |  |
| Wall 05.55L                | Select Borrow | 0.73                             | Not Applicable  |  |
|                            | Gravel Borrow | 0.78                             | Not Applicable  |  |

Abbreviations:

CIP = cast-in-place

ESU = Engineering Stratigraphic Unit

Table 15. Walls 05.85L-A and 05.85L-B Sliding Coefficients of Friction

| Wall     | Foundation<br>Material | Sliding<br>Coefficients of<br>Friction –<br>Discontinuous<br>Reinforcements |
|----------|------------------------|---|
|          | ESU 2A                 | 0.62  |
| 05.85L-A | Common Borrow          | 0.62  |
| 05.65L-A | Select Borrow          | 0.73  |
|          | Gravel Borrow          | 0.78  |
|          | ESU 2B                 | 0.67  |
| 05 05L D | Common Borrow          | 0.62  |
| 05.85L-B | Select Borrow          | 0.73  |
|          | Gravel Borrow          | 0.78  |

Abbreviations:

ESU = Engineering Stratigraphic Unit

#### **Shallow Foundation Bearing Resistance and Elastic Settlement** 8.4

We evaluated bearing resistance for effective footing widths of 2 to 6 feet at Grade Separation Barrier 05.33R, 3 to 11 feet at Wall 05.55L, 5 to 25 feet at Wall 05.85L-A, and 5 to 21 feet at Wall 05.85L-B. For Grade Separation Barrier 05.33R and Wall 05.55L, our bearing resistance calculations include resistance factors of 0.55 (Strength Limit State), 1.0 (Service Limit State),

and 0.8 (Extreme Event Limit State) for semi-gravity walls per AASHTO LRFD Table 11.5.7.1 and AASHTO LRFD Section 11.5.8. For Walls 05.85L-A and 05.85L-B, our bearing resistance calculations include resistance factors of 0.65 (Strength

Limit State), 1.0 (Service Limit States), and 0.9 (Extreme Event Limit State) for MSE (SEW) per AASHTO LRFD Table

Geotechnical Engineering Report: Grade Separation Barrier 05.33R; Walls 05.55L, 05.85L-A, and 05.85L-B; and Embankment EMB: I-405 SB MP 5.97 to 5.83

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11.5.7.1 and AASHTO LRFD Section 11.5.8. Sliding, overturning, and internal stability are being evaluated by the design-1 build team's wall designers and will be submitted under separate cover. 2

Bearing resistances for Grade Separation Barrier 05.33R and Walls 05.55L, 05.85L-A, and 05.85L-B are presented in

Tables 16 through 19. As noted in Section 8.9.3 below, all soft, loose, or otherwise unsuitable soils observed in foundation excavations shall be removed and replaced with compacted structural fill.

Table 16. Grade Separation Barrier 05.33R Bearing Resistance and Elastic Settlement

| Effective<br>Footing Width,<br>B | Unfactored<br>Bearing<br>Resistance | Extreme Event<br>Limit State<br>Bearing<br>Resistance | Strength Limit<br>State Bearing<br>Resistance | Resis         | State Bearing<br>tance<br>sf) |
|----------------------------------|-------------------------------------|---|---|---------------|-------------------------------|
| (feet)                           | (ksf)                               | (ksf)   | (ksf)   | 1" Deflection | 2" Deflection                 |
| 2.0                              | 6.7                                 | 5.4   | 3.7   | 6.7           | 6.7                           |
| 2.5                              | 8.3                                 | 6.7   | 4.6   | 6.7           | 8.3                           |
| 3.0                              | 10.0                                | 8.0   | 5.5   | 6.1           | 10.0                          |
| 3.5                              | 11.6                                | 9.3   | 6.4   | 5.6           | 11.3                          |
| 4.0                              | 13.3                                | 10.6  | 7.3   | 5.3           | 10.5                          |
| 4.5                              | 14.9                                | 11.9  | 8.2   | 5.0           | 9.9                           |
| 5.0                              | 16.5                                | 13.2  | 9.1   | 4.7           | 9.4                           |
| 5.5                              | 18.1                                | 14.5  | 10.0  | 4.5           | 9.0                           |
| 6.0                              | 19.7                                | 15.8  | 10.8  | 4.3           | 8.6                           |

Abbreviations:

ksf = kips per square foot

Table 17. Wall 05.55L Bearing Resistance and Elastic Settlement

| Effective<br>Footing Width,<br>B | Unfactored<br>Bearing<br>Resistance | Extreme Event<br>Limit State<br>Bearing<br>Resistance | Strength Limit<br>State Bearing<br>Resistance | Service Limit<br>Resis<br>(k: |               |
|----------------------------------|-------------------------------------|---|---|-------------------------------|---------------|
| (feet)                           | (ksf)                               | (ksf)   | (ksf)   | 1" Deflection                 | 2" Deflection |
| 3.0                              | 38.2                                | 30.5  | 21.0  | 5.7                           | 11.3          |
| 4.0                              | 45.2                                | 36.2  | 24.9  | 4.9                           | 9.8           |
| 50                               | 52.2                                | 41.8  | 28.7  | 4.4                           | 8.8           |
| 6.0                              | 59.2                                | 47.4  | 32.6  | 4.0                           | 8.0           |
| 7.0                              | 66.2                                | 52.9  | 36.4  | 3.7                           | 7.4           |
| 8.0                              | 73.0                                | 58.4  | 40.2  | 3.5                           | 6.9           |
| 9.0                              | 79.9                                | 63.9  | 43.9  | 3.3                           | 6.5           |
| 10.0                             | 86.7                                | 69.4  | 47.7  | 3.1                           | 6.2           |
| 11.0                             | 93.5                                | 74.8  | 51.4  | 3.0                           | 5.9           |

Abbreviations:

ksf = kips per square foot

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Table 18. Wall 05.85L-A Bearing Resistance and Elastic Settlement

| Effective<br>Footing Width,<br>B | Unfactored<br>Bearing<br>Resistance | Extreme Event<br>Limit State<br>Bearing<br>Resistance | Strength Limit<br>State Bearing<br>Resistance | Resis         | State Bearing<br>tance<br>sf) |
|----------------------------------|-------------------------------------|---|---|---------------|-------------------------------|
| (feet)                           | (ksf)                               | (ksf)   | (ksf)   | 1" Deflection | 2" Deflection                 |
| 5.0                              | 12.0                                | 10.8  | 7.8   | 3.1           | 6.3                           |
| 7.0                              | 13.6                                | 12.3  | 8.9   | 2.6           | 5.3                           |
| 9.0                              | 15.3                                | 13.8  | 9.9   | 2.3           | 4.7                           |
| 11.0                             | 16.9                                | 15.2  | 11.0  | 2.1           | 4.1                           |
| 13.0                             | 18.5                                | 16.7  | 12.0  | 1.8           | 3.7                           |
| 15.0                             | 20.1                                | 18.1  | 13.1  | 1.7           | 3.3                           |
| 17.0                             | 21.6                                | 19.5  | 14.1  | 1.5           | 3.1                           |
| 19.0                             | 23.1                                | 20.8  | 15.0  | 1.4           | 2.8                           |
| 21.0                             | 24.6                                | 22.2  | 16.0  | 1.3           | 2.7                           |
| 23.0                             | 26.1                                | 23.5  | 17.0  | 1.3           | 2.5                           |
| 25.0                             | 27.5                                | 24.8  | 17.9  | 1.2           | 2.4                           |

Abbreviations:

ksf = kips per square foot

Table 19. Wall 05.85L-B Bearing Resistance and Elastic Settlement

| Effective<br>Footing Width,<br>B | Unfactored<br>Bearing<br>Resistance | Extreme Event<br>Limit State<br>Bearing<br>Resistance | Strength Limit<br>State Bearing<br>Resistance | Resis         | State Bearing<br>tance<br>sf) |
|----------------------------------|-------------------------------------|---|---|---------------|-------------------------------|
| (feet)                           | (ksf)                               | (ksf)   | (ksf)   | 1" Deflection | 2" Deflection                 |
| 5.0                              | 17.8                                | 16.0  | 11.6  | 2.1           | 4.2                           |
| 7.0                              | 20.2                                | 18.2  | 13.1  | 1.8           | 3.6                           |
| 9.0                              | 22.6                                | 20.3  | 14.7  | 1.6           | 3.1                           |
| 11.0                             | 24.9                                | 22.4  | 16.2  | 1.4           | 2.8                           |
| 13.0                             | 27.3                                | 24.5  | 17.7  | 1.3           | 2.6                           |
| 15.0                             | 29.6                                | 26.6  | 19.2  | 1.2           | 2.4                           |
| 17.0                             | 31.9                                | 28.7  | 20.7  | 1.1           | 2.3                           |
| 19.0                             | 34.2                                | 30.8  | 22.2  | 1.1           | 2.2                           |
| 21.0                             | 36.5                                | 32.9  | 23.7  | 1.0           | 2.1                           |

Abbreviations:

ksf = kips per square foot

We evaluated the elastic settlement of placed fill on embankment EMB: I-405 SB MP 5.97 to 5.83. Based on our analyses, total settlement of the embankment is less than 1 inch, which meets the settlement criteria outline in RFP Chapter 2.6.6.7.

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1 Bearing resistance and elastic settlement calculations are presented in Appendices C through G. Settle3 output reports are 2 presented in Appendix H.

#### 8.5 Seepage Analysis

- 4 We evaluated the groundwater levels at Wall 05.85L-A, Wall 05.85L-B, and embankment EMB: I-405 SB MP 5.97 to 5.83 by
- 5 performing a seepage analysis at the design section at Wall 05.85L-A using measured piezometer data in borings H-2-85 and
- H-3-85. 6

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- 7 We set hydraulic boundary conditions at the edges of the model to avoid influencing seepage results. In an attempt to match the
- 8 groundwater measured in boring H-3-85, we used a constant head boundary condition equal to elevation 218 feet on the
- 9 upslope edge of the model under I-405. We consider this boundary condition to be very conservative based on available
- groundwater data. We used a constant head boundary condition equal to elevation 160 feet on the downslope edge of the model 10
- to develop a phreatic surface similar to the measured groundwater level in boring H-2-85. We used a 2.6 x 10<sup>-7</sup> feet per second 11
- flux boundary condition for surficial precipitation infiltration based on average rainfall of 8.1 inches per month in Renton, 12
- 13 Washington in November (website: en.climate-data.org, accessed 4/9/2021), conservatively assuming all precipitation
- 14 infiltrates.

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- 15 We modeled each ESU encountered at Wall 05.85L-A (ESU 2A, ESU 2B, ESU 4B, and ESU 5B) with the following material 16 properties:
  - Saturated and unsaturated hydraulic properties to allow each material the potential for saturated and unsaturated flow;
  - Saturated hydraulic conductivities estimated by using the Schlichter method for ESU 2A and ESU 2B and using recommended values from Laprade and Robinson, 1989 (see discussion in Section 7.1.6) for ESU 4B and ESU 5B;
  - Volumetric water contents estimated from sample functions provided in Seep/W based on soil descriptions and saturated water content:
  - Horizontal hydraulic conductivity functions estimated from the volumetric water content function using curve-fitting parameters from the Fredlund-Xing-Huang method; and
  - Permeability anisotropy estimated by selecting the anisotropy ratio (vertical hydraulic conductivity to horizontal hydraulic conductivity). Anisotropy ratios are based on geologic setting, material composition, published values, and our engineering judgement.
- 27 To calibrate the seepage model, we used the saturated hydraulic conductivities and anisotropy ratios presented in Table 20.

Table 20. Saturated Hydraulic Conductivities and Anisotropy Ratios

| ESU | Saturated<br>Hydraulic<br>Conductivity<br>(feet/second) | Anisotropy Ratio,<br>ky/kx |
|-----|---|----------------------------|
| 2A  | 1.1 x 10 <sup>-4</sup>                                  | 0.8                        |
| 2B  | 3.3 x 10 <sup>-5</sup>                                  | 0.5                        |
| 4B  | 3.8 x 10 <sup>-7</sup>                                  | 0.025                      |
| 5B  | 3.8 x 10 <sup>-8</sup>                                  | 0.005                      |

Abbreviations:

ESU = Engineering Stratigraphic Unit

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We used the Seep/W model results in Slope/W to represent pore pressure distributions from the seepage analysis in the global stability analysis. By coupling the two analyses, we avoided overly conservative results that would have been obtained using a simple phreatic surface reflecting the higher measured groundwater in boring H-3-85 and potentially unconservative results that would have been obtained using a simple phreatic surface reflecting the deeper measured groundwater in boring H-2-85. Furthermore, this coupling approach cancels small negative pore pressures occurring at the base of the slices within the failure







- 1 surface, effectively maintaining a degree of conservatism in the stability analysis by not allowing increases in soil strength as a
- 2 result of matric suction.

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3 The steady-state seepage model is presented in Appendix E. The Seep/W output report is presented in Appendix I.

#### 8.6 Global Stability

- 5 We evaluated global stability of Grade Separation Barrier 05.33R; Walls 05.55L, 05.85L-A, and 05.85L-B; and embankment
- EMB: I-405 SB MP 5.97 to 5.83 at the design sections presented in Table 1. Per Project GDM Section 15-4.12 and Section 6-6
- 7 4.3.2, a static resistance factor of 0.75 (FS = 1.3) and seismic resistance factor of 0.9 (FS = 1.1) shall be used for global
- 8 stability of Walls 05.85L-A and 05.85L-B. Per Project GDM Section 15-4.12, a static resistance factor of 0.75 (FS = 1.3) shall
- 9 be used for global stability of Wall 05.55L. Per Project GDM Section 9.2.3, a static resistance factor of 0.8 (FS = 1.25) shall be
- used for global stability of Grade Separation Barrier 05.33R and embankment EMB: I-405 SB MP 5.97 to 5.83 since they do 10
- not support or potentially impact structures. 11
- 12 Per AASHTO LRFD Section 11.10.2.2, we modeled a 4-foot horizontal bench in front of Walls 05.55L, 05.85L-A, and
- 05.85L-B. Based on preliminary drawings from Wood received on November 11, 2021, we modeled a 2-foot embedment at 13
- 14 Wall 05.55L. We modeled the front face embedment depth as 3 feet and 3.5 feet for Walls 05.85L-A and 05.85L-B,
- 15 respectively, using criteria outlined in AASHTO LRFD Table C11.10.2.2-1. For Wall 05.85L-B, the embedment depth was
- 16 based on the slope from the front of the horizontal bench to the existing ground surface.
- 17 We initially evaluated global stability using a minimum reinforcement length of 70 percent of the overall wall height (0.7H) at
- 18 Walls 05.85L-A and 05.85L-B. To meet the minimum FS for global stability, we increased the reinforcement length to 0.8H
- 19 for Wall 05.85L-A. We modeled a 1.5-foot clearance backfilled with imported gravel borrow between the reinforced zone
- 20 (back of the wall) and the face of the temporary shoring for Wall 05.85L-B and the bottom two rows at Wall 05.85L-A, and a
- 6-foot clearance backfilled with imported gravel borrow between the reinforced zone and the face of the temporary shoring for 21
- the upper six rows at Wall 05.85L-A. See Section 8.8.3 for discussion on temporary shoring. 22
- 23 We used the horizontal seismic coefficients, kh, for global stability presented in Table 8 for the pseudo-static analyses at Walls
- 24 05.85L-A and 05.85L-B. We applied the apparent cohesion values presented in Tables 5 and 6 in the pseudo-static analyses at
- 25 Walls 05.85L-A and 05.85L-B, respectively. We used 50 psf apparent cohesion in the common borrow backfill behind Wall
- 05.85L-B for the pseudo-static analyses; see Section 8.7 below for a discussion on apparent cohesion in common borrow at 26
- 27 Wall 05.85L-B. We used the residual shear strength presented in Table 5 for liquefiable soils to evaluate post-seismic global
- stability at Wall 05.85L-A. 28
- 29 Groundwater levels were modeled using a piezometric surface based on measured or observed groundwater levels at Grade
- 30 Separation Barrier 05.33R and Wall 05.55L, and the seepage analysis to model the piezometric surface at Walls 05.85L-A and
- 31 05.85L-B, and embankment EMB: I-405 SB MP 5.97 to 5.83, as discussed in Section 5.3.
- 32 Per Project GDM Section 15-4.12, static, non-structural loads (such as traffic surcharge) shall be evaluated with a load factor of
- 33 1.0. For the static stability analysis, we applied a uniform traffic surcharge of 250 psf to Walls 05.55L, 05.85L-A, and 05.85L-
- 34 B, and embankment EMB: I-405 SB MP 5.97 to 5.83. Per AASHTO LRFD Section 3.4.1, a load factor of 0.5 shall be applied
- to the traffic surcharge during the design seismic event. A uniform traffic surcharge of 125 psf was included for the seismic 35
- (pseudo-static and post-seismic) global stability analyses at Walls 05.55L, 05.85L-A, and 05.85L-B. A traffic surcharge was 36
- 37 not included in our analysis of Grade Separation Barrier 05.33R since a roadway is not present above the barrier.
- 38 Where applicable, the required minimum static, pseudo-static, and post-seismic FSs were met for the walls, barrier, and
- 39 embankment. Per the RFU geotechnical letter "Design Requirements and Geotechnical Assessment of Retaining Walls" (Hart
- 40 Crowser, 2021), a seismic analysis is not required for Wall 05.55L since failure of the wall would not impact the travel lanes.
- Per Project GDM Section 9.2.3, seismic analyses are not required for global stability of the Grade Separation Barrier 05.33R or 41
- 42 embankment EMB: I-405 SB MP 5.97 to 5.83 since neither support or would potentially impact structures.
- 43 We also evaluated the global stability of Walls 05.85L-A and 05.85L-B considering forward compatible walls for future I-405
- widening. We modeled the forward compatible walls directly above Walls 05.85L-A and 05.85L-B with the face of the 44
- forward compatible wall set back 7 feet from the face of the proposed walls. For our analyses, we modeled the forward 45
- compatible wall as a high strength material with a unit weight of 130 pcf, a height extending from the top of the proposed walls 46



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- 1 to the existing grade of I-405, and the width as 8 feet. We modeled the backfill behind the forward compatible wall as 2 lightweight EPS using the strength properties presented in Table 7. Per RFP Section 1-01.3(1), forward compatible is defined 3 as "project elements that are constructed so they can be integrated into the future configuration...without significant demolition or reconstruction of the Project Elements". To meet the requirements outlined in the RFP, we truncated the EPS behind the 4
  - forward compatible walls at 4 feet from the proposed edge of the traveled way for the current project. The required minimum static, pseudo-static, and post-seismic FSs were met for all forward compatible wall cases.
- 7 Structural loads were not included in our analyses. Any structural foundation loads applied to the barrier, walls, or 8 embankment shall include the appropriate load factors in AASHTO LRFD Table 3.4.1-1 consistent with Strength Limit State 9 and Extreme Event Limit State design.
  - The results of our global stability analyses for Grade Separation Barrier 05.33R; Walls 05.55L, 05.85L-A, and 05.85L-B; and embankment EMB: I-405 SB MP 5.97 to 5.83 are summarized in Table 21. Global stability models showing FS for critical failures at the design sections are provided in Appendices C through G. Global stability Slope/W reports are provided in Appendix J.

Table 21. Grade Separation Barrier 05.33R; Walls 05.55L, 05.85L-A, and 05.85L-B; and Embankment EMB: I-405 SB MP 5.97 to 5.83 Global Stability Results

| Design Element<br>(Design Section)                          | Loading Type  | Minimum<br>Required<br>Factor of<br>Safety | Calculated<br>Factor of Safety<br>(Spencer/<br>Morgenstern-<br>Price) | Minimum<br>Reinforcement<br>Length       | Minimum Wall<br>Embedment |
|---|---------------|--|---|--|---------------------------|
| Grade Separation<br>Barrier 05.33R<br>(Sta. 1+58)           | Static        | 1.25                                       | 1.69 / 1.69   | Not Applicable                           | Not Applicable            |
| Wall 05.55L<br>(Sta. 1+50)                                  | Static        | 1.3  | 2.5 / 2.5   | Not Applicable                           | 2 feet                    |
|   | Static        | 1.3  | 1.6 / 1.6<br>(FC: 1.7 / 1.7)  | 0.8H (upper 6<br>rows)<br>1.0H (bottom 2 | 3 feet                    |
| Wall 05.85L-A<br>(Sta. 1+90)                                | Pseudo-Static | 1.1  | 1.2 / 1.2<br>(FC: 1.3 / 1.3)  |  |                           |
|   | Post-Seismic  | 1.1  | 1.6 / 1.6<br>(FC: 1.7 / 1.7)  | rows)                                    |                           |
| Wall 05.85L-B   | Static        | 1.3  | 1.4 / 1.4<br>(FC: 1.5 / 1.5)  | 0.7H                                     | 3.5 feet                  |
| (Sta. 2+60)   | Pseudo-Static | 1.1  | 1.3 / 1.3<br>(FC: 1.3 / 1.3)  | U./H                                     |                           |
| Embankment<br>EMB: I-405 SB MP<br>5.97 to 5.83<br>(MP 5.88) | Static        | 1.25                                       | 1.28 / 1.27   | Not Applicable                           | Not Applicable            |

Abbreviations: 16

FC = Forward Compatible 17

H = Height of the wall (exposed face and embedded depth), in feet

18 MP = Mile Post 19

Sta. = Station 20







#### 8.7 Compound Stability

- 2 We used the results of the global stability analyses to model and evaluate compound stability of Walls 05.85L-A and 05.85L-B
- 3 at the design sections presented in Table 1. Per Project GDM Section 15-4.12 and Section 6-4.3.2, a static resistance factor of
- 0.75 (FS = 1.3) and seismic resistance factor of 0.9 (FS = 1.1) shall be used for compound stability. 4
- 5 We used the horizontal seismic coefficients, kh, for compound stability presented in Table 8 for the pseudo-static analyses at
- 6 Walls 05.85L-A and 05.85L-B. We applied the apparent cohesion values presented in Tables 5 and 6 for the native soils in the
- 7 pseudo-static analyses at Walls 05.85L-A and 05.85L-B, respectively. To meet minimum FSs for the pseudo-static analysis at
- 8 Wall 05.85L-B, we modeled the common borrow backfill with 50 psf apparent cohesion. Per FHWA Geotechnical Engineering
- 9 Circular No. 3 Table 11-2, 50 psf apparent cohesion should be assumed for a backfill soil with a fines content between 5 and
- 15 percent by weight. Per the soil plasticity table presented in WSDOT Standard Specification 9-03.14(3), Option 2 common 10
- borrow contains 12.1 to 35 percent fines content by weight. The common borrow imported during construction shall be 11
- 12 Option 2, as specified in Section 8.13.1.
- We used the residual shear strength presented in Table 5 for liquefiable soils to evaluate post-seismic compound stability at 13
- 14 Wall 05.85L-A.

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- 15 Per Project GDM Section 15-5.3.4 and AASHTO LRFD Table 3.4.1-1, a strength limit state load factor of 1.75 shall be applied
- 16 to the standard traffic surcharge of 250 psf directly over the reinforced zone. For the static stability analysis, we applied a
- uniform traffic surcharge of 437.5 psf directly over the reinforced zone and a uniform traffic surcharge of 250 psf outside of the 17
- 18 reinforced zone to Walls 05.85L-A and 05.85L-B. Per AASHTO LRFD Section 3.4.1, an extreme event limit state load factor
- 19 of 0.5 shall be applied to the standard traffic surcharge of 250 psf during the design seismic event. A uniform traffic surcharge
- of 125 psf was included across all traffic lanes (both directly over and outside of the reinforced zone) for the seismic (pseudo-20
- 21 static and post-seismic) compound stability analyses at Walls 05.85L-A and 05.85L-B.
- 22 Groundwater levels for Walls 05.85L-A and 05.85L-B were modeled using the piezometric surface from the seepage analysis
- 23 at Wall 05.85L-A, as discussed in Section 5.3.
- 24 We evaluated compound stability using the minimum reinforcement lengths required to meet the minimum FSs from the global
- 25 stability analyses. For compound stability of Wall 05.85L-A, we modeled 8 rows of reinforcing strips (2 strips per row in each
- 26 facing panel) at a length of 0.8H. We set the horizontal spacing of the reinforcing strips at 2.5 feet, and the vertical spacing of
- 27 the upper 7 rows at 2.4 feet, with the bottom row at 1.7 feet above the bottom of the leveling pad. For compound stability of
- 28 Wall 05.85L-B, we modeled 10 rows of reinforcing strips at a length of 0.7H. We set the horizontal spacing of the reinforcing
- 29 strips at 2.5 feet, and the vertical spacing of the upper 9 rows at 2.4 feet, with the bottom row at 0.5 feet above the bottom of
- the leveling pad. 30
- 31 The required minimum static and pseudo-static FSs were met for proposed Wall 05.85L-B. To meet the minimum static and
- seismic (pseudo-static and post-seismic) FSs for proposed Wall 05.85L-A, we increased the reinforcing strips to a length of 32
- 33 1.0H with 4 strips in each of the bottom 2 rows and decreased the horizontal spacing to 1.25 feet.
- 34 We also evaluated the compound stability of Walls 05.85L-A and 05.85L-B considering forward compatible walls for future I-
- 405 widening. We used the same geometry and strength properties from the global stability analyses to model the forward 35
- compatible walls in the compound stability analyses. To meet required compound stability minimum FSs for the forward 36
- 37 compatible wall cases at Walls 05.85L-A and 05.85L-B, we modeled the forward compatible walls as a simple block with a set
- 38 width and set unit weight and the backfill as lightweight EPS. Another option to meet required compound stability minimum
- 39 FSs would be to optimize the design of the forward compatible walls. We did not explore all potential options as design of the
- forward compatible walls is outside the scope of this project, however, we have demonstrated that walls for future I-405 40
- 41 widening projects can be designed and constructed without demolition or reconstruction of Walls 05.85L-A and 05.85L-B.
- 42 Structural loads were not included in our analyses. Any structural foundation loads applied to Walls 05.85L-A and 05.85L-B
- 43 shall include the appropriate load factors in AASHTO LRFD Table 3.4.1-1 consistent with Strength Limit State and Extreme
- 44 Event Limit State design.







The results of our compound stability analyses for Walls 05.85L-A and 05.85L-B are summarized in Table 22. Compound stability models showing FS for critical failures at the design sections are provided in Appendices E and F. Compound stability Slope/W reports are provided in Appendix K.

# Table 22. Walls 05.85L-A and 05.85L-B Compound Stability Results

| Wall<br>(Design Section) | Loading Type  | Minimum<br>Required<br>Factor of<br>Safety | Calculated<br>Factor of Safety<br>(Spencer/<br>Morgenstern-<br>Price) | Minimum<br>Reinforcing Strip<br>Length/ Number<br>of Reinforcement<br>Rows |
|--------------------------|---------------|--|---|--|
| 05.85L-A<br>(Sta. 1+90)  | Static        | 1.3  | 1.3 / 1.3<br>(FC: 1.3 / 1.3)  | 0.8H / upper 6 rows<br>1.0H / bottom 2 rows                                |
|                          | Pseudo-Static | 1.1  | 1.1 / 1.1<br>(FC: 1.1 / 1.1)  |  |
|                          | Post-Seismic  | 1.1  | 1.3 / 1.3<br>(FC: 1.4 / 1.4)  |  |
| 05.85L-B<br>(Sta. 2+60)  | Static        | 1.3  | 1.4 / 1.4<br>(FC: 1.4 / 1.5)  | 0.7H / 10 rows   |
|                          | Pseudo-Static | 1.1  | 1.1 / 1.1<br>(FC: 1.3 / 1.3)  | 0.7 H / 10 lows  |

### Abbreviations:

FC = Forward Compatible

H = Height of the wall (exposed face and embedded depth), in feet

Sta. = Station

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### 8.8 Structural Earth Wall (SEW) Fill Material Properties, Drainage, and **Temporary Shoring Recommendations**

#### **SEW Soil Parameters** 8.8.1

Internal stability of Walls 05.85L-A and 05.85L-B will be evaluated by the design-build team's wall designers and submitted under separate cover. We developed geotechnical properties for the reinforced zone fill in the SEW, the retained fill behind the SEW, and the foundation soil below the SEW to support the internal design calculations. SEW soil parameter recommendations are presented in Table 23.

17 18

# Table 23. Walls 05.85L-A and 05.85L-B SEW Soil Parameter Recommendations

| SEW Soil Recommendations |   |  |
|--------------------------|---|--|
| Reinforced Zone Fill     | Gravel Borrow for Structural Earth Wall wSDOT Standard Specification 9-03.14(4) |  |
| Unit Weight (pcf)        | 130   |  |
| Friction Angle (degrees) | 38  |  |
| Cohesion (psf)           | 0   |  |







| SEW Soil Recommendations |  |                         |  |  |
|--------------------------|--|-------------------------|--|--|
| Retained Fill            | Gravel Backfill for Walls<br>WSDOT Standard Specification 9-03.12(2) |                         |  |  |
| Unit Weight (pcf)        | 130  |                         |  |  |
| Friction Angle (degrees) | 38   |                         |  |  |
| Cohesion (psf)           | 0  |                         |  |  |
| Foundation Soil          | Wall 05.85L-A<br>ESU 2A  | Wall 05.85L-B<br>ESU 2B |  |  |
| Unit Weight (pcf)        | 110  | 115                     |  |  |
| Friction Angle (degrees) | 32   | 34                      |  |  |
| Cohesion (psf)           | 0  | 0                       |  |  |

#### Abbreviations:

ESU = Engineering Stratigraphic Unit WSDOT = Washington State Department of Transportation

pcf = pounds per cubic foot

psf = pounds per square foot

ESU = Engineering Stratigraphic Unit

#### 8.8.2 **SEW Drainage**

- 9 The SEWs shall be designed and constructed with a permanent drainage system. The surface drainage system shall intercept
- 10 surface water at the top of the SEW to prevent sheet flow across the wall face and reduce infiltration and groundwater buildup
- in the reinforced zone. Gutters shall be installed behind the wall to intercept surface water and convey it to an appropriate 11
- discharge point. Where possible, the ground surface adjacent to the wall shall be sloped such that water is diverted away from 12
- 13 the wall toe.

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- 14 Positive drainage shall consist of placing a minimum 18-inch-wide zone of free draining gravel backfill immediately behind
- 15 the SEW zone. Drainage material shall consist of WSDOT Standard Specification is Section 9-03.12(2), Gravel Backfill for
- 16 Walls. A 4-inch minimum diameter perforated drainpipe shall be embedded in the drainage layer and routed to an appropriate
- 17 discharge location.

#### 8.8.3 **Temporary Shoring**

- 19 Since the proposed locations of the SEWs are adjacent to and below I-405 and temporary excavations would intersect the
- roadway, temporary shoring will be required prior to constructing Walls 05.85L-A and 05.85L-B. For access and equipment 20
- during construction of the proposed SEWs, the shoring wall will need to be installed an adequate distance behind the back of 21
- the walls. The temporary shoring wall shall be designed for live traffic loads and appropriate surcharges, including soil slopes 22
- 23 and construction traffic. Any groundwater or surface water encountered during shoring construction shall be dewatered
- 24 following recommendations presented in Section 8.9.2.

#### 8.9 Site Preparation and Earthwork

#### 8.9.1 **Earthwork Considerations**

- 27 We anticipate that the site soils at each barrier or wall discussed in this geotechnical engineering report can be excavated with
- 28 conventional excavation equipment, such as trackhoes or dozers. Excavations extending into glacially consolidated soils
- 29 (ESU 4B and ESU 5B) may be difficult. Excavations may encounter debris, large cobbles, and boulders.

#### 30 8.9.2 Dewatering

- 31 Based on our understanding of site conditions, we do not anticipate that excavations will extend below the seasonal high-water
- 32 table. However, it is possible that perched groundwater seepage may be encountered during excavations at Walls 05.85L-A and





#### In Association with

- 1 05.85L-B. Any groundwater seepage or surface water that cannot be handled successfully with sumps and pumps shall be
- 2 routed away from the excavation areas to an appropriate location where it can be treated (if necessary) and discharged.

#### **8.9.3 Bearing Surface Preparation**

- 4 Bearing surfaces for the barrier and walls must be evaluated by GeoEngineers before installation of the barrier and wall
- 5 foundations to identify loose, soft, or otherwise unsuitable soils. This evaluation shall be identified as a hold point on the
- 6 relevant barrier and wall plans. If unsuitable soils are identified during evaluation, GeoEngineers will provide
- 7 recommendations for remediation or repair of the unsuitable areas. Based on nearby borings, we expect to encounter the
- 8 following ESUs at or near the foundation bearing elevations:
  - Grade Separation Barrier 05.33R– ESU 1B
  - Wall 05.55L ESU 1B

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- Wall 05.85L-A ESU 2A
- Wall 05.85L-A ESU 2B

#### 13 8.10 Temporary Shoring

- To facilitate construction of Walls 05.85L-A and 05.85L-B, a shoring wall will be required. Temporary shoring
- recommendations for Walls 05.85L-A and 05.85L-B are presented in Section 8.8.3.

#### 16 8.11 Temporary Cut Slopes

17 Temporary cut slopes shall not exceed the maximum allowable inclinations presented in Project GDM Section 15-7.4.

#### 18 8.12 Permanent Slopes

- 19 Permanent slopes shall be inclined no steeper than 2H:1V. Permanent slopes shall be planted or hydroseeded as soon as
- 20 practicable after grading. Temporary erosion control measures, such as erosion control blankets, shall be incorporated until
- 21 permanent vegetation and erosion control has been established.

#### 22 8.13 Materials

- 23 8.13.1 Common Borrow
- 24 Common borrow shall conform to WSDOT Standard Specification 9-03.14(3) and, at specifically at Wall05.58L-B, shall
- 25 consist of Option 2 for soil plasticity.
- 26 8.13.2 Select Borrow
- 27 Select borrow shall conform to WSDOT Standard Specification 9-03.14(2).
- 28 8.13.3 Gravel Borrow
- 29 Gravel borrow shall conform to WSDOT Standard Specification 9-03.14(1).
- 30 8.13.4 Gravel Borrow for Structural Earth Wall
- 31 Gravel borrow for structural earth wall shall conform to WSDOT Standard Specification 9-03.14(4) and Cu shall be 6.3 or
- 32 greater.
- 33 8.13.5 Gravel Backfill for Walls
- 34 Gravel backfill for walls shall conform to WSDOT Standard Specification 9-03.12(2).
- 35 8.13.6 Crushed Surfacing Base Course
- 36 CSBC shall conform to WSDOT Standard Specification 9-03.9(3).
- 37 8.14 Fill Placement
- 38 Barrier and wall backfill and foundation subgrade shall be placed and compacted in accordance with Method C of
- 39 Section 2-03.3(14)C of the WSDOT Standard Specifications.

Geotechnical Engineering Report: Grade Separation Barrier 05.33R; Walls 05.55L, 05.85L-A, and 05.85L-B; and Embankment EMB: I-405 SB MP 5.97 to 5.83







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4

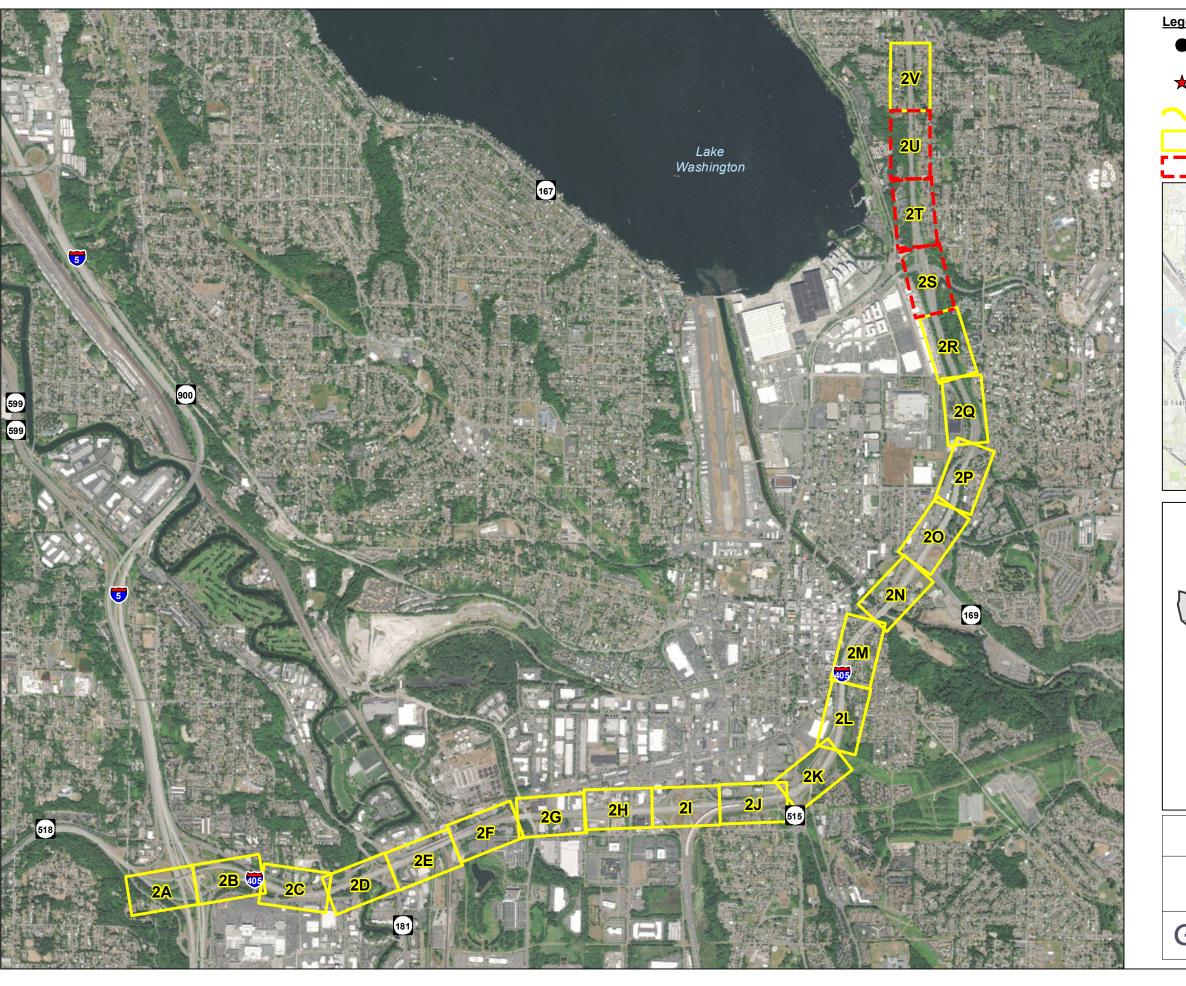




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#### <u>Legend</u>

**Project Location** 



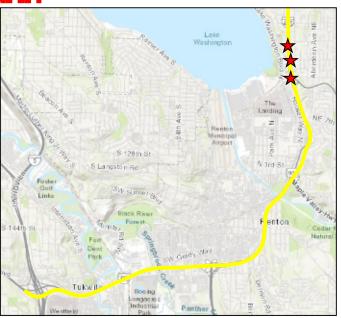
Grade Separation Barrier 05.33R; Walls 05.55L, 05.85L-A, and 05.85L-B; and Embankment EMB: I-405 SB MP 5.97 to 5.83

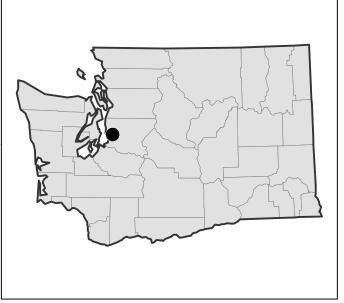






Site Plan Index Sheets Included in this Report



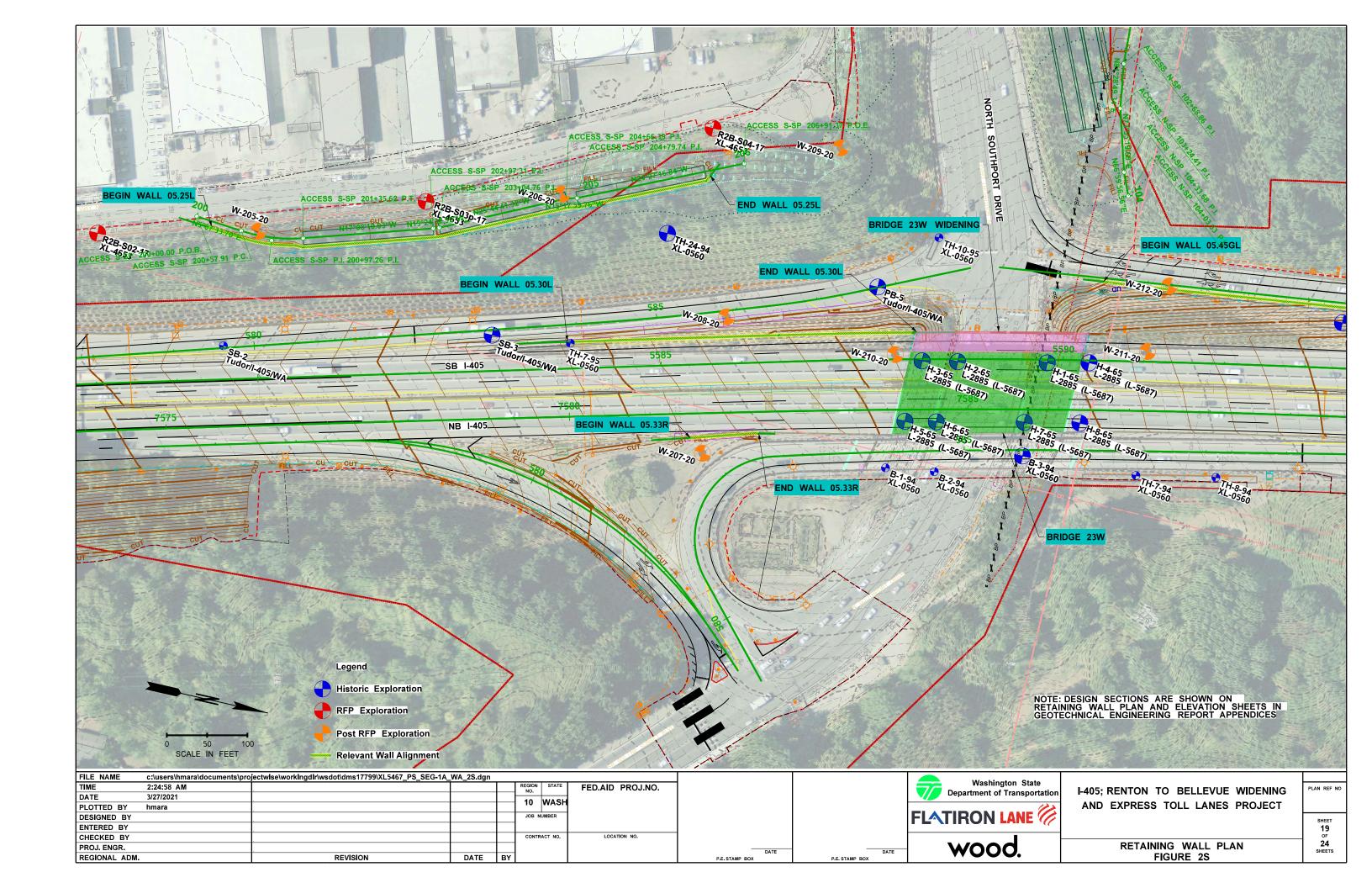


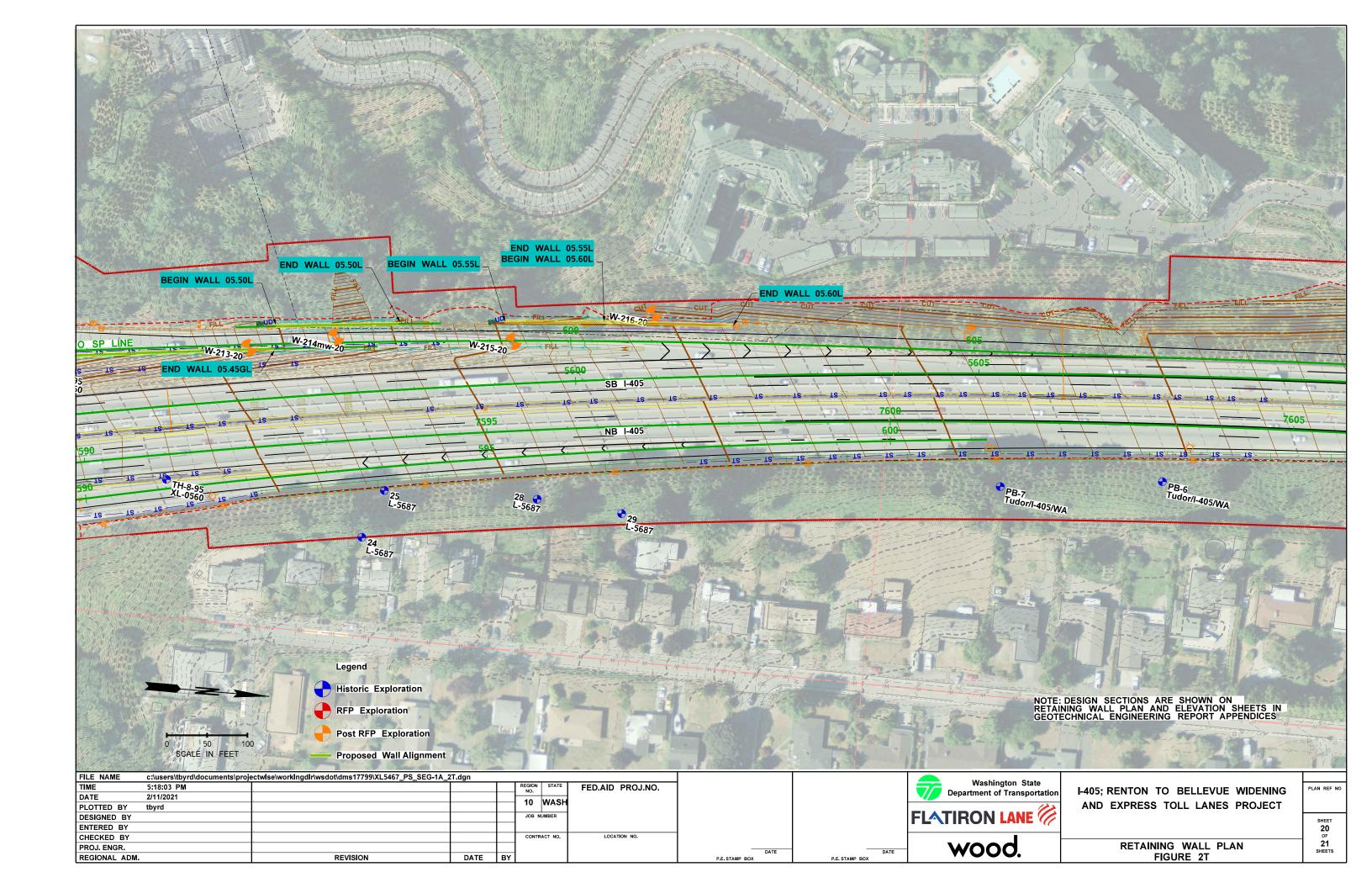
### Vicinity Map

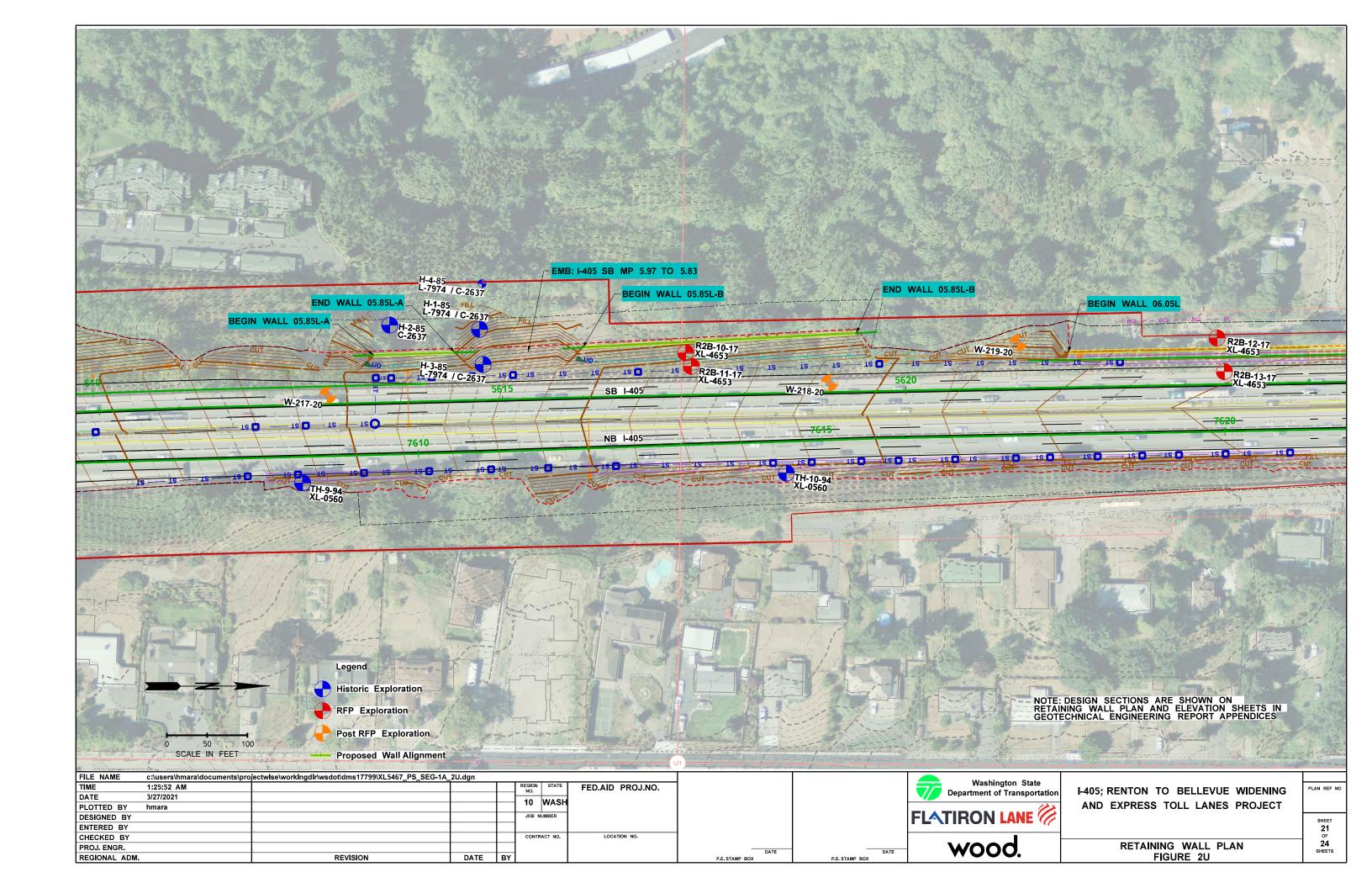
I-405 Renton to Bellevue Segment 1A - Walls Package 2 King County, Washington



Figure 1













In Association with

### Appendix A **Field Exploration Logs**



#### **TABLE A-1** I-405 RENTON TO BELLEVUE WIDENING AND EXPRESS TOLL LANES PROJECT **GEOLOGIC UNITS AND DESCRIPTIONS**

| Unit Name                                       | Abbreviation | Unit Description  |
|---|--------------|---|
|   |              | Quaternary Units  |
| Fill  | Af           | Fill placed by humans, both engineered and uncontrolled fill consisting of various materials, including debris; typically dense or stiff if engineered, but very loose to dense or very soft to stiff if uncontrolled fill.   |
| Landslide Debris                                | Qls          | Soil deposits associated with slope failures, mass wasting and mud flows of soils. Normally found at and adjacent to the toes of hillslopes or in drainage channels, consisting of disturbed, heterogeneous mixtures of all soil types and intermixed debris; loose or soft, with random dense to hard pockets.   |
| Peat  | Qp           | Depression fillings of organic materials consisting of peat, peaty silt; peaty silty clay, peaty sandy silt, and organic silts and clays with sand; very soft to medium stiff.  |
| Alluvium  | Qal          | Mainly river, creek or overbank deposits, consisting of sand, silty sand; gravelly sand and sandy gravel with scattered organics that are typically very loose to dense, and includes interbedded slack water or lake deposits that consist of silts, clays and sandy silts.  |
| Recessional Deposits                            | Qvr          | Sediments deposited after glacial ice retreated that have not been glacially overridden. These recessional deposits include: Outwash- glaciofluvial sediment deposited off the retreating glacier consisting of sand or silty sand; locally gravelly; loose to dense; Ablation Till- heterogeneous soils deposited during the wasting of glacial ice; generally not reworked consisting of gravelly, silty sand, gravelly, sandy silt or clayey silt; loose to dense or soft to very stiff; lce Contact Deposits- heterogeneous soils deposited against or adjacent to ice during the wasting of glacial ice; commonly reworked, consisting of stratified to irregular bodies of gravel, sand and silt; loose to dense; and Lacustrine Deposits- sediments deposited as glacial ice retreated consisting of silt and clay; locally fine sand; soft to very stiff. |
| Vashon Glacial Till                             | Qvt          | Lodgment till laid down along the base of the glacial ice and overridden by the weight of glacial ice, consisting of gravelly, silty sand or gravelly, sandy silt ("hardpan"); boulders and cobbles common; gray and very dense, and in its weathered state may be oxidized brown and medium dense to dense. Sometimes referred to as a diamicton.  |
| Advance Outwash                                 | Qva          | Glaciofluvial sediment deposited as the glacial ice advanced through the Puget Lowland and overridden by the weight of glacial ice; typically stratified, light brown to gray, sand, gravelly sand, and sandy gravel; dense to very dense.  |
| Proglacial Lacustrine<br>Deposits (Lawton Clay) | Qgl          | Fine-grained glacial sediment deposited in pro-glacial lake in Puget Lowland consisting of interbedded brown, gray to blue-gray silt, clayey silt; silty clay; fine sand; massive to locally laminated or locally disturbed (fractures and slickensides); scattered wood near base; very stiff to hard or dense to very dense.  |
| Pre-Fraser Deposits                             | Qpf          | Undifferentiated interbedded gravel, sands and silts; typically, oxidized orange or reddish brown, dense to very dense.   |
|   |              | Tertiary Formations   |
| Intrusive Andesite                              | Oian         | Igneous bedrock consisting mainly of andesite.  |
| Renton Formation                                | Tr           | Sedimentary bedrock; tan friable silty sandstone, siltstone with interbedded coal seams.  |

Retaining Wall Report: Eastside Rail Corridor Trail South File Name: Table A-1 Lithology

## **Field Soil Description**



#### ORDER OF CLASSIFICATION TERMS **GRAIN SIZE** 1. Soil classification Relative density/consistency 3. Color (based on Munsell Color Chart) 4. Moisture 5. Structure 6. Other - plasticity, dilatancy, organics, odor Medium Sand Fine Sand Geologic Name: Fill, Glacial Till, etc. (optional - ask project manager) UNIFIED SOIL CLASSIFICATION SYSTEM **EXAMPLES** (From ASTM D-2488 & 2487-90) Well graded GRAVEL, with cobbles and boulders, subrounded, medium dense, **GROUP TYPICAL** grayish brown, wet, homogeneous, no HCL reaction or HCL not tested (Alluvium) **MAJOR DIVISIONS** SYMBOL **DESCRIPTION** SM Well-Graded Gravels, Silty fine SAND with gravel, prevalent roots and fine organics, subrounded, loose, Clean GW Gravel-Sand Mixtures, Little brownish black, moist, no HCL reaction or HCL not tested (Relict Topsoil) SM Gravels (less or No Fines Fibrous or amorphous PEAT with or without some silt/clay; PT Gravels (more than 10% Poorly-Graded Gravels, than 50% of fines) GP Fat CLAY with sand, medium stiff, dark gray, wet, blocky, no HCL reaction or HCL Gravel-Sand Mixutres coarse fraction not tested (Lawton Clay) CH Silty Gravels, Gravel-Sandretained on GM **RELATIVE DENSITY OF GRANULAR SOILS** Gravels with Silt Mixtures No. 4 sieve) Fines (>10% (Cohesionless Silt, Sand, and Gravel) Coarse-Clavey Gravels, Gravelfines) GC Grained N, SPT, FIELD TEST FOR RELATIVE DENSITY OF Sand-Clay Mixtures RELATIVE Soils (more **BLOWS/FT** DENSITY SAND\* Well-Graded Sands, than 50% 0-4 Gravelly Sands, Little or No Very loose Penetrated 3 feet or more by hand probe SW retained on Clean Sands Fines 4-10 Loose Penetrated 1 to 2 feet by hand probe No. 200 (<10% fines) Poorly-Graded Sand, sieve) Sands (50% 11-24 Med-dense Penetrated 3 to 12 inches by hand probe SP Gravelly Sands, Little or No or more of 25-50 Dense Penetrated 1 to 3 inches by hand probe Fines coarse fraction Silty Sands, Sand-Silt Penetrated less than 1 inch by hand probe passes the SM Very Dense Over 50 \* varies with soil type No. 4 sieve) Mixtures Sands with Fines (>10% **RELATIVE CONSISTENCY OF COHESIVE SOILS** Clayey Sands, Sand-Clay fines) SC (Cohesive, Silt, and Clay) Mixtures N. SPT. RELATIVE TORVANE, tsf POC. PEN., tsf **MANUAL** Inorganic silts and Very UNCONF. STR. **DENSITY BLOWS/FT** SHEAR STR. PENETRATION TEST Fine Sands, Rock Flour, ML Silty or Clayey Fine Sands Easy several inches by <0.25 0-1Very soft < 0.13 or Clayey Silts with Slight fist Silts and Plasticity Easy several inches by Inorganic 2-4 Soft 0.13 - 0.250.25 - 0.5Clays (liquid thumb Inorganic Clays of Low to limit less than Medium Moderate several Medium Plasticity, Gravelly CL 0.25 - 0.50.5 - 150) 5-8 stiff inches by thumb Fine-Clays, Sandy Clays, Silty Clays, Lean Clays Readily indented by Grained 9-15 Stiff 0.5 - 11 - 2 thumb Soils (50% Organic Silts and Organic Organic OL Readily Indented by or more Silty Clays of Low Plasticity 16-30 Very stiff 1 - 2 2 - 4 passes the thumbnail Inorganic Clays of Medium No. 200 30-60 Hard >2 >4 Difficulty by thumbnail CH to High Plasticity, Sandy sieve) **SOIL STRUCTURE** Fat Clay, Gravelly Fat Clay Silts and Inorganic Inorganic Silts, Micaceous Alternating layers of varying material or color with layers at least Stratified Clays (liquid or Diatomaceous Fine 6mm (1/4") thick MH limit 50 or Sands or Silty Soils, Elastic Alternating layers of varying material or color with layers less than Laminated more) Silt 6 mm (1/4") thick Organic Clays of Medium to 2 to 13 mm (1/16" - 1/2") thick Seam Organic OHHigh Plasticity, Organic 13 to 305 mm (1/2" - 12") thick Layer Silts Primarily organic matter, Peat, Humus, Swamp Soils Occasional One or less per foot of thickness Highly Organic dark in color, and organic with High Organic Content Frequent More than one per foot of thickness (See D 4427-92) ordor

**Fissured** 

Slickensided

**Blocky** 

Lensed

Homogeneous







Breaks along definite planes of fracture with little resistance to

fracturing Fracture planes appear to be polished or glossy, sometimes

striated

Cohesive soil that can be broken down into small angular lumps

which resist further breakdown

Inclusion of small pockets of different soils, generally

discontinuous, such as small lenses of sand through out a mass of

clay; note thickness.

Same color and appearance throughout







Wet - Visible free water

Dry - Dusty, dry to touch





**ADJECTIVE** 

Scattered

Numerous

Organic

PEAT



**ORGANIC CONTENT** 

1 - 10

10 - 30

PERCENT BY VOLUME

30 - 50 minor constituent

50 - 100 MAJOR constituent



Light Yellow Brown Light Olive Brown Gravish Brown

**MOISTURE CONTENT** 

Moist - Damp but no visible water

| MAJOR DIVISIONS -                                    |  | SYME                        | BOLS   | TYPICAL              |   |
|--|--|-----------------------------|--|----------------------|---|
| IVI  | AJON DIVISIO                           | NO                          | GRAPH  | LETTER               | DESCRIPTIONS  |
|  | GRAVEL AND<br>GRAVELLY                 | CLEAN<br>GRAVELS            | XX   | GW                   | WELL-GRADED GRAVELS, GRAVEL -<br>SAND MIXTURES, LITTLE OR NO FINES  |
|  | SOILS                                  | (LESS THAN 5%<br>FINES)     |  | GP                   | POORLY-GRADED GRAVELS, GRAVEL -<br>SAND MIXTURES, LITTLE OR NO FINES  |
| COARSE<br>GRAINED<br>SOILS                           | MORE THAN 50%<br>OF COARSE<br>FRACTION | GRAVELS<br>WITH FINES       |  | GM                   | SILTY GRAVELS, GRAVEL - SAND - SILT<br>MIXTURES   |
| SOILS  | RETAINED ON<br>NO. 4 SIEVE             | (GREATER THAN<br>12% FINES) |  | GC                   | CLAYEY GRAVELS, GRAVEL - SAND -<br>CLAY MIXTURES  |
|  | SAND AND<br>SANDY SOILS                | CLEAN<br>SANDS              |  | SW                   | WELL-GRADED SANDS, GRAVELLY<br>SANDS, LITTLE OR NO FINES  |
| MORE THAN<br>50% OF<br>MATERIAL IS                   |  | (LESS THAN<br>5% FINES)     |  | SP                   | POORLY-GRADED SANDS, GRAVELLY<br>SAND, LITTLE OR NO FINES   |
| LARGER THAN<br>NO. 200 SIEVE<br>SIZE                 | MORE THAN 50 OF<br>COARSE FRACTION     | SANDS WITH<br>FINES         |  | SM                   | SILTY SANDS, SAND - SILT MIXTURES   |
|  | PASSING<br>NO. 4 SIEVE                 | (GREATER THAN 12%<br>FINES) |  | SC                   | CLAYEY SANDS, SAND - CLAY<br>MIXTURES   |
|  | SILTS<br>AND                           | INORGANIC                   |  | ML                   | INORGANIC SILTS AND VERY FINE<br>SANDS, ROCK FLOUR, SILTY OR<br>CLAYEY FINE SANDS OR CLAYEY SILTS<br>WITH SLIGHT PLASTICITY |
| FINE<br>GRAINED<br>SOILS                             | CLAYS                                  |                             |  | PLASTICITY, GRAVELLY | INORGANIC CLAYS OF LOW TO MEDIUM<br>PLASTICITY, GRAVELLY CLAYS, SANDY<br>CLAYS, SILTY CLAYS, LEAN CLAYS                     |
|  | LIQUID LIMIT LESS<br>THAN 50           | ORGANIC                     |  | OL                   | ORGANIC SILTS AND ORGANIC SILTY<br>CLAYS OF LOW PLASTICITY  |
| MORE THAN<br>50% OF                                  | SILTS<br>AND                           | INORGANIC                   |  | МН                   | INORGANIC SILTS, MICACEOUS OR<br>DIATOMACEOUS FINE SAND OR SILTY<br>SOILS   |
| MATERIAL IS<br>SMALLER<br>THAN NO. 200<br>SIEVE SIZE | CLAYS                                  |                             |  | СН                   | INORGANIC CLAYS OF HIGH<br>PLASTICITY   |
| 5.2.12 5/22  | LIQUID LIMIT<br>GREATER THAN 50        | ORGANIC                     |  | ОН                   | ORGANIC CLAYS OF MEDIUM TO HIGH<br>PLASTICITY, ORGANIC SILTS  |
| Н  | IGHLY ORGANIC S                        | OILS                        | 77 77 77 77 77<br>7 77 77 77 77<br>77 77 77 77 | PT                   | PEAT, HUMUS, SWAMP SOILS WITH<br>HIGH ORGANIC CONTENTS  |
|  | FILL SOILS                             |                             |  | FILL<br>(AF)         | HUMAN ALTERED SOIL OR MODIFIED LAND   |

#### NOTES:

- SOIL DESCRIPTIONS ARE BASED ON THE GENERAL APPROACH PRESENTED IN THE STANDARD PRACTICE FOR DESCRIPTION AND IDENTIFICATION OF SOILS (VISUAL-MANUAL PROCEDURE), AS OUTLINED IN ASTM D 2488. WHERE LABORATORY INDEX TESTING HAS BEEN CONDUCTED, SOIL CLASSIFICATIONS ARE BASED ON THE STANDARD TEST METHOD FOR CLASSIFICATION OF SOILS FOR ENGINEERING PURPOSES, AS OUTLINED IN ASTM D 2487.
- 2. SOIL DESCRIPTION TERMINOLOGY IS BASED ON VISUAL ESTIMATES (IN THE ABSENCE OF LABORATORY TEST DATA) OF THE PERCENTAGES OF EACH SOIL TYPE AND IS DEFINED AS DESCRIBED BELOW:
- 3. DUAL SYMBOLS (E.G. SP-SM, OR GP-GM) ARE USED TO INDICATE A SOIL WITH AN ESTIMATED 5-12% FINES.

PRIMARY CONSTITUENT: >50% - "GRAVEL", "SAND", "SILT", "CLAY", etc. SECONDARY CONSTITUENTS: >12% and ≤50% - "gravelly", "sandy", "silty", etc. ADDITIONAL CONSTITUENTS: >5% and ≤12% - "some gravel", "some sand", "some silt", etc. ≤5% - "trace gravel", "trace sand", "trace silt" etc. or not noted.

4. RELATIVE DENSITY OF SOIL IS BASED ON STANDARD TEST METHOD FOR PENETRATION TEST (SPT) AND SPLIT-BARREL SAMPLING OF SOILS ASTM D 1586 OR CORRELATIONS FOR OTHER SIMPLER TYPES AND METHODS FOR SPT SAMPLING, THE FOLLOWING BLOW COUNT CORRELATION APPLIES.

A. RELATIVE DENSITY OF COARSE GRAINED SOILS VERY LOOSE: N =  $\leq$ 4 (N = BLOWS/FOOT LOOSE: N = >4 AND  $\leq$ 10 SPT METHOD) MEDIUM DENSE: N = >10 AND  $\leq$ 30

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SOIL CLASSIFICATION CHART / KEY

B. RELATIVE CONSISTENCY OF FINE GRAINED SOILS VERY SOFT: N = <2 (N = BLOWS/FOOT

SPT METHOD)

JUNE 2018

NOT TO SCALE

PROJECT NO.

FIGURE

DATE

SCALE

A-1

| CLIENT W                               |  | PROJECT LOC    |                       |  |                |  |
|--|--|----------------|-----------------------|--|----------------|--|
|  | RTED 7/30/20 COMPLETED 7/30/20   |                |                       |  | HOLE           |  |
|  | CONTRACTOR Holt Services   |                |                       |  | IAMMER EFFICI  |  |
|  | METHOD HSA   |                |                       |  | OFFSET (FT)    |  |
|  | Y Patricia Reed CHECKED BY Bill Lockard  | NORTHING 1     | 86017.629             |  | EASTING 13     | 03588.587                                |
| NOTES                                  |  | G              | W LEVEL (             | (ATD) Dry                              |                |  |
| _                                      |  | %              | М                     |  | N VALUE ▲      |  |
| ELEVATION<br>(ft)<br>DEPTH<br>GRAPHIC  |  | RECOVERY (RQD) | SAMPLE TYPE<br>NUMBER | 20 40<br>PL                            | 60 80<br>MC LL | TESTS                                    |
|  | SOIL & ROCK DESCRIPTION  | SVE            | PLE                   | l —                                    | 60 80          | AND<br>REMARKS                           |
|  |  | Ä<br>Ö         | N N                   |  |                | KLIVIARRO                                |
| 0                                      |  | <u> </u>       | 0)                    | 20 40                                  | , ,            |  |
| - \\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\ | Grass (8 inches) over  |                |                       |  |                |  |
| _ 💥                                    | Silty SAND, medium dense, grayish brown, dry, [FILL] (SM)  |                |                       |  |                | +  |
|  |  |                |                       |  |                |  |
| - +                                    |  |                |                       |  |                | †  |
| 🛞                                      | No recovery  | 0              | SPT-1                 | 23                                     |                |  |
| <u>12</u> 5 -                          |  |                | 12                    | <u>z</u> 3                             |                | †  |
|  |  |                | 11                    |  |                |  |
| - 💥                                    | ×  |                |                       |  |                |  |
| _5                                     |  | 92             | SPT-2                 |  |                | -  |
| - 💥                                    |  | 83             | 2                     | • A:                                   |                | MC = 11%<br>Fines = 37%                  |
| 💥                                      |  |                | 16<br>21              |  |                | Rock in barrel, SP                       |
|  |  |                |                       | 1 ! !                                  |                | values may be<br>verstated               |
| - Ж                                    |  |                |                       |  |                | †  |
|  |  | 11             | SPT-3                 | <b>●</b> ▲:                            |                | MC = 13%                                 |
| 120                                    |  |                | 8 10                  |  | : :            |  |
|  |  |                | 10                    | ļ <u>i</u> i.                          |                |  |
| - 💥                                    |  |                |                       |  |                |  |
| _ 10                                   | X<br>X<br>X<br>Recomes with gravel and scattered hits of clear glass                                     | 11             | SPT-4                 | ļ. <u></u>                             |                | 100/                                     |
|  | Becomes with gravel and scattered bits of clear glass  | ''             | 5 6                   | 12                                     |                | MC = 10%<br>Fines = 31%                  |
| - 💥                                    |  |                | 6                     |  |                | †  |
|  | ×  |                |                       | 1 ! !                                  |                |  |
| - T                                    |  |                |                       |  | : :            | <b>†</b>                                 |
| 115                                    |  |                |                       |  |                | 1  |
| <u></u> ⊗                              | Sandy lean CLAY with gravel, soft, grayish brown, wet, dilatant scattered fragments of coal, [FILL] (CL) | with           |                       |  |                |  |
|  | ×  |                |                       |  |                | +  |
|  |  |                |                       |  |                |  |
| _ 15                                   |  | 83             | SPT-5                 | <b>▲ ●</b>                             |                | MC = 17%                                 |
| $\otimes$                              |  |                | $ \mathbf{Y} $ 1      | 2 : :                                  |                | LL = 28                                  |
| - 🗱                                    | ×  |                | 1                     |  |                | PL = 20<br>Fines = 50%                   |
|  | ×<br>  |                |                       | ]                                      |                |  |
| - ////                                 | Construction DEBRIS; coal, brick, plaster, burnt wood within a matrix, [FILL] (CL)                       | CLAY           |                       |  |                |  |
| 110                                    | ,  |                | ST-1                  | ļ                                      |                | Shelby tube likely                       |
|  |  |                |                       |  |                | contains demolition debris, rock stuck i |
|  |  |                |                       | ······································ |                | . lower end                              |
| 20///                                  |  |                |                       | †                                      |                |  |
| 2017///                                | · 1  | 1              | 1                     | 1                                      | . :            | 1  |

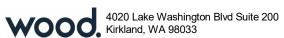
BORING NUMBER W-207-20 PROJECT NAME 1-405 Renton to Bellevue Widening PROJECT NUMBER 20316 **CLIENT** WSDOT PROJECT LOCATION Renton, WA SAMPLE TYPE NUMBER ▲ SPT N VALUE ▲ ELEVATION (ft) DEPTH GRAPHIC RECOVERY % (RQD) 40 60 **TESTS** MC AND REMARKS SOIL & ROCK DESCRIPTION 40 60 80 ☐ FINES CONTENT (%) ☐ Construction DEBRIS; coal, brick, plaster, burnt wood within a CLAY 2 1 2 matrix, [FILL] (CL) (continued) WSDOT GEOTECH DRILLING - 1405 WSDOT, GDT - 10/13/20 11:08 - C:\USERS\CHELSEA.FOSTER\DOCUMENTS\PROJECTWISE\WORKINGDIR\WSDOT\DMS08721\1405 WSDOT - SEG. 1.GPJ 72 Silty SAND, dense, yellowish brown to grayish brown, moist, oxidized in places, stratified, disturbed, [Qvt] (SM) 94 MC = 14% 1 9 Fines = 28% 20 SPT-9 20 16 50/5" 100 Becomes very dense 100 SPT-10 18 40 Bottom of borehole at 41.4 feet.

| CLIENT WSDOT                    |  | PROJECT LOCATION Renton, WA |                       |   |              |                        |  |
|---------------------------------|--|-----------------------------|-----------------------|---|--------------|------------------------|--|
| DATE STARTED 7/2                | 7/20 <b>COMPLETED</b> 7/28/20                      | GROUND ELE\                 | /ATION _17            | 71.2 ft NAVD88                          | HOLE S       | IZE 8 inches           |  |
| RILLING CONTRAC                 | OR Holt Services                                   |                             |                       | SPT HAMI                                |              | •                      |  |
| RILLING METHOD _                | HSA  | STATION (FT)                | 5599+25.1             | 14 O                                    | FFSET (FT) _ | 52.4 L                 |  |
| OGGED BY Patricia               | Reed CHECKED BY Bill Lockard                       | NORTHING _18                | 87332.8835            | EA                                      | ASTING _1303 | 3168.587               |  |
| IOTES                           |  | G                           | W LEVEL (             | ATD) 31.0 ft / Ele                      | v 140.2 ft   |                        |  |
|                                 |  | %                           | Ш                     | ▲ SPT N VA                              | LUE 📤        |                        |  |
| (ft)<br>DEPTH<br>GRAPHIC<br>LOG |  | RECOVERY (RQD)              | SAMPLE TYPE<br>NUMBER | 20 40 6<br>PL MC                        | 80 80<br>LL  | TESTS                  |  |
| (ft)<br>DEPTH<br>GRAPHIC<br>LOG | SOIL & ROCK DESCRIPTION                            | SVE 3VE                     | MB                    | L                                       | 60 80        | AND                    |  |
|                                 |  |                             | AM UN                 | ☐ FINES CONTI                           |              | REMARKS                |  |
| o                               |  | <u>~</u>                    | Š                     |   | 60 80        |                        |  |
| ASPHAL                          | Γ (14 inches) over                                 |                             |                       | : :                                     |              |                        |  |
| 70                              |  |                             |                       |   |              |                        |  |
| Silty SAN                       | D with gravel, dense, light gray, dry, [FILL] (SM) |                             |                       |   |              |                        |  |
|                                 |  |                             |                       |   | <u>.</u>     |                        |  |
|                                 |  | 78                          | SPT-1                 | ● □ <b>▲</b>                            |              | MC = 10%               |  |
|                                 |  |                             | 9<br>25               | 46                                      |              | Fines = 30%            |  |
|                                 |  |                             | 21                    |   |              |                        |  |
|                                 |  |                             |                       |   |              |                        |  |
| _5                              |  |                             |                       |   |              |                        |  |
| gravel gr                       | ades out   | 100                         | SPT-2                 | 32                                      |              |                        |  |
| 55 -                            |  |                             | 13                    |   | <u></u>      |                        |  |
| -                               |  |                             |                       |   |              |                        |  |
|                                 |  |                             |                       |   |              |                        |  |
| Silty SAN                       | D, dense, light olive yellow, moist, [FILL] (SM)   | 78                          | SPT-3                 | ●□ ▲                                    |              | MC = 15%               |  |
|                                 | ,            |                             | 5<br>15               | 32.:                                    | :            | Fines = 23%            |  |
|                                 |  |                             | 17                    |   |              |                        |  |
|                                 |  |                             |                       |   |              |                        |  |
| 10                              |  |                             |                       |   | <u>.</u>     |                        |  |
|                                 |  | 100                         | SPT-4<br>6<br>18      | 39                                      |              |                        |  |
| <u>50</u>                       |  |                             | 18 21                 |   | <u>.</u>     |                        |  |
| - 💥                             |  |                             |                       |   |              |                        |  |
|                                 |  |                             |                       | ļ <u>.</u>                              | <u>:</u>     |                        |  |
|                                 |  |                             |                       |   |              |                        |  |
| -                               |  |                             |                       |   |              |                        |  |
|                                 |  |                             |                       |   |              |                        |  |
|                                 |  |                             |                       |   | : :          |                        |  |
| 15                              |  |                             | <u> </u>              |   |              |                        |  |
|                                 |  | 100                         | SPT-5                 | 23                                      |              |                        |  |
| 55                              |  |                             | 10                    | ======================================= | <u> </u>     | MO 400/                |  |
| SILT with                       | sand, dense, light olive yellow, moist, [Qvt] (ML) |                             | 13                    |   |              | MC = 19%<br>LL = NP    |  |
| 4                               |  |                             |                       |   |              | PL = NP<br>Fines = 72% |  |
|                                 |  |                             |                       |   |              | Filles = 72%           |  |
| -                               |  |                             |                       |   | ÷            |                        |  |
|                                 |  |                             |                       |   |              |                        |  |
|                                 |  |                             |                       |   | ÷            |                        |  |
| 20                              |  |                             |                       |   |              |                        |  |
|                                 |  |                             |                       |   |              |                        |  |

| Solid   Soli |
|--|
| Sitty SAND, very dense, light olive yellow, moist, [Qvt] (SM)  25  45  SPT-6  16  36  SPT-7  34  MC = 1  Fines = 2  SILT, dense, light olive yellow, wet, stratified with silty sand, [Qvt] (ML)  67  SPT-8  31  |
| 94 SPT-7 6 34 Fines = 2  |
| SILT, dense, light olive yellow, wet, stratified with silty sand, [Qvt] (ML)  67 SPT-8  8 31   |
| Bottom of borehole at 31.5 feet.   |

|                                 | ME L 405 Penten to Pellevije Widening DDO IECT NIIM   | IDED 202     | 016            |                       | PORING      | NIIMPED W/ 2        | 17 20                  |
|---------------------------------|---|--------------|----------------|-----------------------|-------------|---------------------|------------------------|
| CLIENT <u>WS</u>                | AME _I-405 Renton to Bellevue Widening PROJECT NUM  | ·            |                | ATION Re              |             | NUMBER W-2          | 17-20                  |
|                                 | FED _7/29/20  |              |                |                       |             | HOLE S              | IZF 8 inches           |
|                                 | ONTRACTOR Gregory Drilling  |              |                |                       |             | MMER EFFICIE        | ·                      |
| ORILLING MI                     |   |              |                |                       | OFFSET (FT) |                     |                        |
|                                 | Carlos Mendoza CHECKED BY Pat Reed  |              |                |                       |             | <b>EASTING</b> 1303 |                        |
|                                 |   |              |                |                       | ATD) Dry    |                     |                        |
|                                 |   |              |                |                       | I           | \/ALLIE <b>A</b>    |                        |
| <u> </u>                        |   |              | %<br><b>≻</b>  | SAMPLE TYPE<br>NUMBER | 20 40       | VALUE ▲<br>60 80    |                        |
| (ft)<br>DEPTH<br>GRAPHIC<br>LOG | SOIL & ROCK DESCRIPTION   |              | RECOVERY (RQD) | ABE                   | PL M        |                     | TESTS<br>AND           |
|                                 |   |              | SE             | MPI                   |             | 60 80               | REMARKS                |
| 1 1                             |   |              | 쀭              | S.                    | ☐ FINES COI |                     |                        |
| 0                               | ASPHALT (18 inches) over  |              |                |                       | 20 40       | 60 80               |                        |
|                                 |   |              |                |                       |             |                     |                        |
|                                 |   |              |                |                       |             |                     |                        |
|                                 | Well graded SAND with gravel, olive yellow, subangular gravel, [FILL/Crushed rock base coarse] (SW) |              |                |                       |             |                     |                        |
|                                 |   |              | 67             | SPT-1                 | • -         |                     | NO 00/                 |
|                                 | Silty SAND, very dense, light olive brown, dry, subrounded grave                                    | <br>I, [Qvt] | 0.             | 14<br>43              |             | 93.                 | MC = 8%<br>Fines = 45% |
|                                 | (SM)  |              |                | 50                    |             |                     |                        |
| 15                              |   |              |                |                       |             |                     |                        |
| 5 : : :                         | Silty SAND with gravel, very dense, light yellow brown, dry, subrogravel, [Qvt] (SM)                | ounded       |                |                       |             |                     |                        |
|                                 | graver, [QVI] (SIVI)  |              | 67             | SPT-2<br>10           |             | 63                  |                        |
| -1111                           |   |              |                | 28<br>35              |             |                     |                        |
|                                 |   |              |                |                       |             |                     |                        |
|                                 | Silty SAND, very dense, bluish gray, moist, oxidation stains, [Qvt                                  |              |                |                       |             |                     |                        |
|                                 |   |              | 63             | SPT-3<br>17           |             | 50/4"               | MC = 9%                |
|                                 |   |              |                |                       |             |                     | Fines = 37%            |
|                                 |   |              |                | 50/4"                 |             |                     |                        |
| <u>1</u> 0                      |   |              |                |                       |             |                     |                        |
| 10                              | Becomes bluish gray   |              | 67             | SPT-4                 |             | 50/6*               |                        |
|                                 | Decornes bidistrigray   |              | 0,             | 15<br>50              |             |                     |                        |
|                                 |   |              |                |                       |             |                     |                        |
|                                 |   |              |                |                       |             |                     |                        |
| 7:133                           |   |              |                |                       |             |                     |                        |
|                                 |   |              |                |                       |             |                     |                        |
|                                 |   |              |                |                       |             |                     |                        |
| -1111                           |   |              |                |                       |             |                     |                        |
| 05<br>15                        |   |              |                |                       |             |                     |                        |
|                                 |   |              | 67             | SPT-5<br>15           | •           | 50/6*               | MC = 12%               |
|                                 |   |              |                | 50                    |             |                     | Fines = 40%            |
|                                 |   |              |                |                       |             |                     |                        |
|                                 |   |              |                |                       | ļ           |                     |                        |
|                                 |   |              |                |                       |             |                     |                        |
| -1343                           |   |              |                |                       |             |                     |                        |
|                                 |   |              |                |                       |             |                     |                        |
|                                 |   |              |                |                       |             |                     |                        |
| <u>00</u>                       |   |              |                |                       |             |                     |                        |

PROJECT NAME 1-405 Renton to Bellevue Widening PROJECT NUMBER 20316 BORING NUMBER W-217-20 CLIENT WSDOT PROJECT LOCATION Renton, WA SAMPLE TYPE NUMBER ▲ SPT N VALUE ▲ ELEVATION (ft) DEPTH GRAPHIC RECOVERY % (RQD) 20 40 60 **TESTS** MC AND REMARKS SOIL & ROCK DESCRIPTION 40 60 ☐ FINES CONTENT (%) ☐ Silty SAND, very dense, bluish gray, moist, [Qvt] (SM) 30 50/2' WSDOT GEOTECH DRILLING - 1405 WSDOT GDT - 10/19/20 15:17 - C:USERS/CHELSEA FOSTERIDOCUMENTS/PROJECTWISE/WORKINGDIR/WSDOTIDMS08721/1405 WSDOT - SEG. 1.GPJ SILT, very dense, gray, dry, [Qgl] (ML) <u> 195</u> 25  $\Box$ MC = 23%4 27 24 LL = 48 PL = 30 Fines = 90% 30 SPT-8 12 32 50 Lean CLAY, hard, bluish gray, dry, [Qgl] (CL) SPT-9 10 20 35 67 MC = 24% LL = 42 PL = 26 Fines = 92% SPT-10 5 50 Fat CLAY with sand, very hard, bluish gray, dry, homogeneous, [Qgl] (CH) 58 MC = 15% LL = 56 PL = 28 Fines = 73% Lean CLAY, very hard, bluish gray, dry, [Qgl] (CL)



BORING NUMBER W-217-20 PROJECT NAME 1-405 Renton to Bellevue Widening PROJECT NUMBER 20316 **CLIENT** WSDOT PROJECT LOCATION Renton, WA SAMPLE TYPE NUMBER ▲ SPT N VALUE ▲ ELEVATION (ft) DEPTH GRAPHIC RECOVERY % (RQD) 20 40 60 **TESTS** MC AND REMARKS SOIL & ROCK DESCRIPTION 40 60 80 ☐ FINES CONTENT (%) ☐ Lean CLAY, very hard, bluish gray, dry, [Qgl] (CL) (continued) 175 WSDOT GEOTECH DRILLING - 1405 WSDOT.GDT - 10/19/20 15:17 - C:UVSERSICHELSEA.FOSTERIDOCUMENTSIPROJECTWISEIWORKINGDIRIWSDOTIDMS08721/1405 WSDOT - SEG. 1.GPJ SPT-1 20 35 50/4" 75 Well graded SAND with silt and gravel, very dense, grayish brown, moist, [Qvt] (SW) 100 SPT-12 50/2" MC = 5% Fines = 11% Silty SAND with gravel, very dense, light olive brown, moist, [Qvt] (SM) 50/5" 73 SPT-13 15 50/5" 160 60 Silty GRAVEL with sand, very dense, brownish yellow to olive yellow, 100 SPT-14 50/5" moist, oxidation, [Qvt] (GM) Bottom of borehole at 60.4 feet.

| LIENT <u>W</u>                    |   | PROJECT LOCATION Renton, WA |                         |   |                                      |                         |  |
|-----------------------------------|---|-----------------------------|-------------------------|---|--------------------------------------|-------------------------|--|
| ATE STAF                          | TED <u>8/31/20</u> COMPLETED <u>9/1/20</u>  | GROUND ELEV                 | /ATION _23              | 38.6 ft NAVD88  | HOLE SI                              | ZE 6 inches             |  |
| RILLING C                         | ONTRACTOR Boretec   | DRILL RIG EC                | 295                     | SPT HAMM  | IER EFFICIEN                         | ICY <u>60%</u>          |  |
|                                   | ETHOD HSA   |                             | 5619+05.4               | 41 OF   | FSET (FT) _                          | 11.7 L                  |  |
| OGGED B                           | / JP Bourquin CHECKED BY Pat Reed   | NORTHING 18                 | 89315.321               | EA  | STING 1303                           | 096.815                 |  |
| OTES                              |   | G                           | W LEVEL (               | ATD) Dry  |                                      |                         |  |
| (ft)<br>o DEPTH<br>GRAPHIC<br>LOG | SOIL & ROCK DESCRIPTION   | RECOVERY % (RQD)            | SAMPLE TYPE<br>NUMBER   | △ SPT N VAL  20 40 60  PL MC  20 40 60  □ FINES CONTE  20 40 60 | 0 80<br>LL<br>0 80<br>ENT (%) $\Box$ | TESTS<br>AND<br>REMARKS |  |
|                                   | ASPHALT (14 inches) over  |                             |                         |   |                                      |                         |  |
|                                   | Well graded SAND with silt and gravel, very dense, light yellowis moist, fine to coarse sand and gravel, homogenous, [Qva] (SP) | sh brown,                   |                         |   |                                      |                         |  |
| 5                                 |   | 61                          | SPT-1<br>29<br>36<br>32 |   | 68                                   | MC = 3%<br>Fines = 9%   |  |
|                                   | Silty SAND, medium dense, light olive brown, moist, homogenou (SM)  | us, [Qva]                   |                         |   |                                      |                         |  |
| 5                                 | (GW)  | 89                          | SPT-2<br>11<br>12<br>11 | <b>≜</b><br>23  |                                      |                         |  |
|                                   |   |                             |                         |   |                                      |                         |  |
| 0                                 | Becomes dense, brownish gray, moisture increases  | 56                          | SPT-3<br>5<br>10<br>15  | ● ▲□<br>25  |                                      | MC = 15%<br>Fines = 33% |  |
| 10                                | Becomes medium dense, light olive brown, fine to medium sand  | I and 56                    | SPT-4<br>5              | <b>≜</b><br>22  |                                      |                         |  |
| -0.00                             | gravel  |                             | 5<br>10<br>12           |   |                                      |                         |  |
|                                   |   |                             |                         |   |                                      |                         |  |
| 5                                 |   |                             |                         |   |                                      |                         |  |
| 13                                | Becomes very dense with gravel  | 89                          | SPT-5<br>14<br>26<br>39 | • 🗓   | 65                                   | MC = 11%<br>Fines = 419 |  |
| (10 kg)<br>                       |   |                             |                         |   |                                      |                         |  |
|                                   |   |                             |                         | ļ   |                                      |                         |  |

PROJECT NAME 1-405 Renton to Bellevue Widening PROJECT NUMBER 20316 BORING NUMBER W-218-20 **CLIENT** WSDOT PROJECT LOCATION Renton, WA ▲ SPT N VALUE ▲ SAMPLE TYPE NUMBER ELEVATION (ft) DEPTH GRAPHIC RECOVERY % (RQD) 40 60 **TESTS** MC SOIL & ROCK DESCRIPTION AND 40 60 80 **REMARKS** ☐ FINES CONTENT (%) ☐ Silty SAND with gravel, very dense, grayish brown, moist, homogenous, MC = 10% 35 50/5" [Qva] (SM) LL = 17 PL = 14 Fines = 45% WSDOT GEOTECH DRILLING - 1405 WSDOT, GDT - 11/4/20 12:31 - C;USERSICHELSEA,FOSTERIDOCUMENTSIPROJECTWISEWORKINGDIRWSDOTIDMS08721/1405 WSDOT - SEG. 1.GPJ 50/5" 100 Lenses of sand (~2 to 3 inches thick) 39 Becomes olive brown <u>210</u> SPT-8 50/5" 100 MC = 5% Fines = 36% Poorly graded SAND, very dense, olive brown, moist, fine to medium sand, [Qva] (SP) <u> 20</u>5 120 SPT-9 50/5" 200 100 SPT-10 50/2" SILT, very dense, olive brown, moist, non plastic, homogenous, [Qgl] (ML)

Fines = 15%

PROJECT NAME 1-405 Renton to Bellevue Widening PROJECT NUMBER 20316 BORING NUMBER W-218-20 CLIENT WSDOT PROJECT LOCATION Renton, WA SAMPLE TYPE NUMBER ▲ SPT N VALUE ▲ ELEVATION (ft) DEPTH GRAPHIC RECOVERY % (RQD) 20 40 60 **TESTS** MC AND REMARKS SOIL & ROCK DESCRIPTION 40 60 ☐ FINES CONTENT (%) ☐ SILT, very dense, olive brown, moist, non plastic, homogenous, [Qgl] <u> 19</u>5 (ML) (continued) WSDOT GEOTECH DRILLING - 1405 WSDOT, GDT - 1/14/20 12:31 - C;USERSICHELSEA.FOSTERIDOCUMENTSIPROJECTWISEIWORKINGDIRIWSDOTIDMS08721/1405 WSDOT - SEG. 1.GPJ 45 SPT-11 26 50 100 MC = 22% LL = 33 PL = 25 Fines = 98% <u> 19</u>0 50 100 Becomes bluish gray 16 29 50 <u> 185</u> 55 MC = 25% LL = 36 PL = 23 Fines = 95% Lean CLAY, hard, dark gray, moist, [Qgl] (CL) 100 44 100 50/6 **Dropstones** 44 50 <u>175</u> SPT-15 Silty SAND with gravel, very dense, reddish brown, moist, [Qpf] (SP) 100 MC = 8% 50

BORING NUMBER W-218-20 PROJECT NAME 1-405 Renton to Bellevue Widening PROJECT NUMBER 20316 **CLIENT** WSDOT PROJECT LOCATION Renton, WA SAMPLE TYPE NUMBER ▲ SPT N VALUE ▲ ELEVATION (ft) DEPTH GRAPHIC RECOVERY % (RQD) 20 40 60 **TESTS** MC AND REMARKS SOIL & ROCK DESCRIPTION 40 60 80 ☐ FINES CONTENT (%) ☐ Hard drilling at 65 feet with soil change Silty SAND with gravel, very dense, reddish brown, moist, [Qpf] (SP) (continued) Hard drilling at 67.5 WSDOT GEOTECH DRILLING - 1405 WSDOT.GDT - 114/20 12:31 - C:USERSICHELSEA.FOSTERIDOCUMENTSIPROJECTWISEWORKINGDIRWSDOTIDMS08721/1405 WSDOT - SEG. 1.GPJ feet 170 70 50/6" Silt content increases 100 40 50 165 50/2" 100 SPT-17 50/2" MC = 6% Silty GRAVEL with sand, very dense, moist, [Qpf] (GM) Fines = 25% Very hard drilling at <u>16</u>0 80 feet when drilling deeper to cover auger in the road with steel plate 100/1" 0 SPT-18 100/1" Bottom of borehole at 81.5 feet.





## Boring and Test Pit Legend

|                           | Sampler Symbols                        |  |  |  |  |  |  |
|---------------------------|--|--|--|--|--|--|--|
|                           | Standard Penetration Test              |  |  |  |  |  |  |
|                           | Non-Standard Sized<br>Penetration Test |  |  |  |  |  |  |
| Shelby Tube               |  |  |  |  |  |  |  |
| P                         | Piston Sample                          |  |  |  |  |  |  |
|                           | Washington Undisturbed                 |  |  |  |  |  |  |
|                           | Vane Shear Test                        |  |  |  |  |  |  |
|                           | Core                                   |  |  |  |  |  |  |
| Becker Hammer  Bag Sample |  |  |  |  |  |  |  |

| Well Symbols  |  |  |  |  |  |  |  |
|---|--|--|--|--|--|--|--|
| Cement Surface Seal                                       |  |  |  |  |  |  |  |
| Piezometer Pipe in<br>Granular Bentonite Seal             |  |  |  |  |  |  |  |
| Piezometer Pipe in Sand                                   |  |  |  |  |  |  |  |
| Well Screen in Sand                                       |  |  |  |  |  |  |  |
| Granular Bentonite Seal                                   |  |  |  |  |  |  |  |
| Inclinometer Casing or PVC Pipe in Cement Bentonite Grout |  |  |  |  |  |  |  |
| Sand  |  |  |  |  |  |  |  |
| Vibe Wire in Grout  |  |  |  |  |  |  |  |
| Miscellaneous, noted on boring log                        |  |  |  |  |  |  |  |

### Laboratory Testing Codes

| AL  | Atterberg Limits                 |
|-----|----------------------------------|
| CD  | Consolidated Drained Triaxial    |
| CN  | Consolidation Test               |
| CSS | Cyclic Simple Shear              |
| CU  | Consolidated Undrained Triaxial  |
| DĞ  | Degradation                      |
| ĎΝ  | Density                          |
| DS  | Direct Shear Test                |
| DSS | Direct Simple Shear              |
| GS  | Grain Size Distribution          |
| HŤ  | Hydrometer Test                  |
| JS  | Jar Slake                        |
| LA  | LA Abrasion                      |
| LOI | Loss on Ignition                 |
| MC  | Moisture Content                 |
| pН  | pH of Soil                       |
| PT  | Point Load Compressive Test      |
| RES | Resistivity                      |
| RM  | Resilient Modulus                |
| RS  | Torsional Ring Shear Test        |
| SG  | Specific Gravity                 |
| SL  | Slake Test                       |
| ÜC  | Unconfined Compression Test      |
| ŬŬ  | Unconsolidated Undrained Triaxia |
| HC  | Hydraulic Conductivity           |
|     | ,                                |

| Soil Density Modifiers          |              |                 |                  |  |  |  |  |
|---------------------------------|--------------|-----------------|------------------|--|--|--|--|
| Gravel, Sand & Non-plastic Silt |              | Elasti          | c Silts and Clay |  |  |  |  |
| SPT<br>Blows/ft                 | Density      | SPT<br>Blows/ft | Consistency      |  |  |  |  |
| 0 - 4                           | Very Loose   | 0 - 1           | Very Soft        |  |  |  |  |
| 5 - 10                          | Loose        | 2 - 4           | Soft             |  |  |  |  |
| 11 - 24                         | Medium Dense | 5 - 8           | Medium Stiff     |  |  |  |  |
| 25 - 50                         | Dense        | 9 - 15          | Stiff            |  |  |  |  |
| > 50                            | Very Dense   | 16 - 30         | Very Stiff       |  |  |  |  |
| (REF)                           | Refusal      | 31 - 60         | Hard             |  |  |  |  |
| (1127)                          | Neiusai      | > 60            | Very Hard        |  |  |  |  |

|            | Angularity  |
|------------|---|
| Angular    | Coarse particles have sharp edges and relatively plane sides with unpolished surfaces.    |
| Subangular | Coarse grained particles are similar to angular but have rounded edges.                   |
| Subrounded | Coarse grained particles have nearly plane sides but have well rounded corners and edges. |
| Rounded    | Coarse grained particles have smoothly curved sides and no edges.                         |

|       | Soil Moisture Modifiers                  |
|-------|--|
| Dry   | Absence of moisture; dusty, dry to touch |
| Moist | Damp but no visible water                |
| Wet   | Visible free water                       |

|              | Soil Structure  |
|--------------|---|
| Stratified   | Alternating layers of varying material or color at least 6 mm thick; note thickness and inclination.  |
| Laminated    | Alternating layers of varying material or color less than 6 mm thick; note thickness and inclination. |
| Fissured     | Breaks along definite planes of fracture with little resistance to fracturing.                        |
| Slickensided | Fracture planes appear polished or glossy, sometimes striated.  |
| Blocky       | Cohesive soil that can be broken down into smaller angular lumps which resist further breakdown.      |
| Disrupted    | Soil structure is broken and mixed. Infers that material has moved substantially - landslide debris.  |
| Homogeneous  | Same color and appearance throughout.   |

|                     | HCl Reaction                                       |
|---------------------|--|
| No HCl Reaction     | No visible reaction.                               |
| . Weak HCl Reaction | Some reaction with bubbles forming slowly.         |
| Strong HCl Reaction | Violent reaction with bubbles forming immediately. |

| Degree of '          | Vesicularity of Pyroclastic Rocks |
|----------------------|-----------------------------------|
| Slightly Vesicular   | 5 to 10 percent of total          |
| Moderately Vesicular | 10 to 25 percent of total         |
| Highly Vesicular     | 25 to 50 percent of total         |
| Scoriaceous          | Greater than 50 percent of total  |



### Boring and Test Pit Legend

Page 2 of 2

|                |                | Grain Size  |
|----------------|----------------|---|
| Fine Grained   | < 0.04 in      | Few crystal boundaries/grains are distinguishable in the field or with hand lens. |
| Medium Grained | 0.04 to 0.2 in | Most crystal boundaries/grains are distinguishable with the aid of a hand lens.   |
| Coarse Grained | > 0.2 in       | Most crystal boundaries/grains are distinguishable with the naked eye.            |

|                         | Weathered State   |       |
|-------------------------|---|-------|
| Term                    | Description   | Grade |
| Fresh                   | No visible sign of rock material weathering; perhaps slight discoloration in major discontinuity surfaces.  | I     |
| Slightly<br>Weathered   | Discoloration indicates weathering of rock material and discontinuity surfaces. All the rock material may be discolored by weathering and may be somewhat weaker externally than its fresh condition. | П     |
| Moderately<br>Weathered | Less than half of the rock material is decomposed and/or disintegrated to soil. Fresh or discolored rock is present either as a continuous framework or as core stones.                               | Ш     |
| Highly<br>Weathered     | More than half of the rock material is decomposed and/or disintegrated to soil. Fresh or discolored rock is present either as discontinuous framework or as core stone.                               | IV    |
| Completely<br>Weathered | All rock material is decomposed and/or disintegrated to soil. The original mass structure is still largely intact.  | v     |
| Residual<br>Soil        | All rock material is converted to soil. The mass structure and material fabric is destroyed. There is a large change in volume, but the soil has not been significantly transported.                  | VI    |

|       | Relative Rock Strength |  |   |  |  |  |  |  |  |
|-------|------------------------|--|---|--|--|--|--|--|--|
| Grade | Description            | Field Identification   | Uniaxial Compressive<br>Strength approx |  |  |  |  |  |  |
| R1    | Very<br>Weak           | Specimen crumbles under sharp blow from point of geological hammer, and can be cut with a pocket knife.                          | 0.15 to 3.6 ksi                         |  |  |  |  |  |  |
| R2    | Moderately<br>Weak     | Shallow cuts or scrapes can be made in a specimen with a pocket knife.<br>Geological hammer point indents deeply with firm blow. | 3.6 to 7.3 ksi                          |  |  |  |  |  |  |
| R3    | Moderately<br>Strong   | Specimen cannot be scraped or cut with a pocket knife, shallow indentation can be made under firm blows from a hammer.           | 7.3 to 15 ksi                           |  |  |  |  |  |  |
| R4    | Strong                 | Specimen breaks with one firm blow from the hammer end of a geological hammer.   | 15 to 29 ksi                            |  |  |  |  |  |  |
| R5    | Very<br>Strong         | Specimen requires many blows of a geological hammer to break intact sample.  | Greater than 29 ksi                     |  |  |  |  |  |  |

### Discontinuities

| S             | pacing                  |  |  |  |
|---------------|-------------------------|--|--|--|
| Very Widely   | Greater than 10 ft      |  |  |  |
| Widely        | 3 ft to 10 ft           |  |  |  |
| Moderately    | 1 ft to 3 ft            |  |  |  |
| Closely       | 2 inches to 12 inches   |  |  |  |
| Very Closely  | Less than 2 inches      |  |  |  |
| RQD (%)       |                         |  |  |  |
| 100(length of | core in pieces > 100mm) |  |  |  |
| Leng          | th of core run          |  |  |  |

|   | Condition  |  |  |  |  |  |  |
|---|--|--|--|--|--|--|--|
| Excellent Very rough surfaces, no separation, hard discontinuity wall |  |  |  |  |  |  |  |
| Good  | Slightly rough surfaces, separation less than 0.05 in, hard discontinuity wall.                      |  |  |  |  |  |  |
| Fair  | Slightly rough surfaces, separation greater than 0.05 in, soft discontinuity wall.                   |  |  |  |  |  |  |
| Poor  | Slickensided surfaces, or soft gouge less than 0.2 in thick, or open discontinuities 0.05 to 0.2 in. |  |  |  |  |  |  |
| Very Poor   | Soft gouge greater than 0.2 in thick, or open discontinuities greater than 0.2 in.                   |  |  |  |  |  |  |

Fracture Frequency (FF) is the average number of fractures per 1 ft of core. This does not include mechanical breaks caused by drilling or handling.

Datum:

NAD 83/91 HARN = North American Datum of 1983/1991 High Accuracy Reference Network NAVD88 = North American Vertical Datum of 1988 SPN (ft) = State Plane North (ft)

SPS (ft) = State Plane South (ft)



Job No. XL-4653

Component Fill Wall 05.85L

#### LOG OF TEST BORING

Elevation 210.2 ft

Start Card <u>SE-61806 / AE-</u>42502

HOLE No. R2B-10-17

Sheet \_\_1\_\_ of \_\_2\_\_

Driller Henderson, Danny Lic# 2742

Project\_I-405 Renton to Bellevue - ETL - Envir & Traff

SR

405

Inspector Harvey, Thomas #2599

Start April 12, 2017 Completion April 12, 2017 Well ID# N/A Equipment CME 45C (9A4-7)

Station SB405 5617+28.003 Offset 54.4 feet left Hole Dia 4 Historical SPT Efficiency 88.4%

Northing 189137.226 Easting 1303059.157 Collected by Region Survey Crew Method Casing Advancer

 Lat
 47.5103052
 Long
 -122.1984486
 Datum
 NAD 83/91 HARN, NAVD88, SPN (ft)
 Drill Fluid
 Bentonite

| Depth (ft)         | Elevation (ft)                                | Profile | <ul> <li>⇒ SPT Efficiency</li> <li>→ Field SPT (N)</li> <li>→ Moisture Content</li> <li>☑ RQD</li> <li>20 40 60 80</li> </ul>  | Blows/6"<br>(N)<br>and/or<br>RQD<br>FF     | Sample Type | Sample No.<br>(Tube No.) | Lab<br>Tests   | Description of Material  | Groundwater | Instrument |
|--------------------|---|---------|--|--|-------------|--------------------------|----------------|--|-------------|------------|
| 5-                 | -210.0<br>                                    |         | •  | 26<br>27<br>24<br>(51)                     |             | D-1                      |                | Silty SAND, very dense, brown, moist, homogeneous.<br>HCl not tested.<br>Recovered: 1.0 ft Retained: 1.0 ft  | -           |            |
| -<br>-<br>-<br>10- |   |         | •  | 4<br>8<br>8<br>(16)<br>4<br>5<br>7<br>(12) | X           | D-2<br>D-3               | MC<br>GS<br>AL | SM, MC=19%, LL=19 Silty SAND with organics, medium dense, grayish brown, moist, stratified. HCl not tested. Recovered: 1.5 ft Retained: 1.5 ft Silty SAND, medium dense, gray, moist, homogeneous. HCl not tested. Recovered: 1.5 ft Retained: 1.5 ft            | -           |            |
| 5— 5— 10—          | -<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>195.0 |         | <ul> <li>Image: Control of the c</li></ul> | 2<br>3<br>5<br>(8)<br>4<br>6<br>15<br>(21) | X           | D-4                      | MC<br>LOI      | MC=33%, LOI=7.2% Sandy SILT with organics, loose, gray, moist, homogeneous. HCl not tested. Recovered: 1.0 ft Retained: 1.0 ft  Silty SAND with gravel, sub-rounded, medium dense, brown, moist, homogeneous. HCl not tested. Recovered: 1.0 ft Retained: 1.0 ft | -           |            |
| - 20 —             | -<br>-  |         | •  | 20<br>24                                   | X           | D-6                      |                | Silty SAND with gravel, sub-rounded, dense, brown, moist, homogeneous. HCl not tested.   | -           |            |





Job No\_XL-4653

SR <u>405</u>

Elevation 210.2 ft

HOLE No. R2B-10-17

Sheet \_\_2\_\_ of \_\_2\_\_

Project I-405 Renton to Bellevue - ETL - Envir & Traff

Driller Henderson, Danny

| Depth (ft)     | Elevation (ft)                                 | Profile | <ul><li>♣ SPT Efficit</li><li>♦ Field SPT</li><li>♣ Moisture</li><li>☑ RQD</li><li>20 40</li></ul> | 「(N) | Blows/6"<br>(N)<br>and/or<br>RQD<br>FF | Sample Type | Sample No.<br>(Tube No.) | Lab<br>Tests | Description of Material   | Groundwater      | lactrimont |
|----------------|--|---------|--|------|--|-------------|--------------------------|--------------|---|------------------|------------|
| -              | — 190<br>-<br>-                                |         |  |      | 24<br>(48)                             | X           |                          |              | Recovered: 1.0 ft Retained: 1.0 ft  | -                |            |
| -<br>25 —<br>- | -<br>-<br>-<br>-<br>-<br>-<br>-<br>-           |         | •  |      | 16<br>18<br>17<br>(35)                 | X           | D-7                      | MC<br>GS     | MC=18% Silty SAND, dense, brown, moist, homogeneous. HCl not tested. Recovered: 1.5 ft Retained: 1.5 ft   | -                |            |
| 30 —           | -<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>- |         |  |      | 15<br>24<br>26<br>(50)                 | X           | D-8                      |              | Silty SAND, dense, brown, moist, stratified. HCl not tested. Recovered: 1.5 ft Retained: 1.5 ft   | -<br>-<br>-<br>- |            |
| 35—            | -<br>-<br>-<br>175                             |         |  |      |  |             |                          |              | The implied accuracy of the borehole location information displayed on this boring log is typically sub-meter in (X,Y) when collected by the HQ Geotech Office and sub-centimeter in (X,Y,Z) when collected by the Region Survey Crew.  | -                |            |
| -<br>40 —<br>- | -<br>-<br>-<br>-<br>-<br>-<br>-<br>-<br>-      |         |  |      |  |             |                          |              | End of test hole boring at 30.5 ft below ground elevation. This is a summary Log of Test Boring. Soil/Rock descriptions are derived from visual field identifications and laboratory test data. Note: REF = SPT Refusal  Bail/Recharge test: Hole Diameter: 4 inches Depth of boring during bail test: 30.5 ft. Depth of casing during bail test: 24 ft. Water depth before bailing: 12.7 ft. | -                |            |
| -              | _<br>-<br>-                                    |         |  |      |  |             |                          |              | Bailed bore hole water level to 20.1 ft. Recharge after 5 minutes: 20.1 ft. Recharge after 10 minutes: 20.3 ft. Recharge after 15 minutes: 20.3 ft. Recharge after 30 minutes: 20.4 ft.   | _                |            |



Job No. XL-4653

Component Fill Wall 05.85L

#### LOG OF TEST BORING

Elevation 219.2 ft

Start Card <u>SE-61806 / AE-</u>42502

HOLE No. R2B-11-17

Sheet \_\_1\_\_ of \_\_3\_\_

Driller Peterson, Trevor Lic# 3008

Project\_I-405 Renton to Bellevue - ETL - Envir & Traff

SR

405

Inspector Harvey, Thomas #2599

Start April 13, 2017 Completion April 13, 2017 Well ID# N/A Equipment CME 45C (9A4-7)

 Station
 SB405 5617+34.677
 Offset
 35.6 feet left
 Hole Dia 4 (inches)
 Historical SPT Efficiency
 88.4%

Northing 189144.191 Easting 1303075.854 Collected by Region Survey Crew Method Casing Advancer

Lat 47.5103251 Long -122.1983816 Datum NAD 83/91 HARN, NAVD88, SPN (ft) Drill Fluid Bentonite

| Depth (ft)   | Elevation (ft)            | Profile | <ul> <li>♣ SPT Efficiency</li> <li>◆ Field SPT (N)</li> <li>♣ Moisture Content</li> <li>☑ RQD</li> <li>20 40 60 80</li> </ul>   | Blows/6"<br>(N)<br>and/or<br>RQD<br>FF        | Sample Type | Sample No. | (Tube No.) | Lab<br>Tests   | Description of Material  | Groundwater | Instrument |
|--|---------------------------|---------|---|---|-------------|------------|------------|----------------|--|-------------|------------|
| 2 C C C C C C C C C C C C C C C C C C C  |                           |         | •   | 15<br>22<br>14                                | Y           | D-         | .1         |                | Silty SAND with gravel, sub-rounded, dense, brown, moist, homogeneous. HCl not tested. Recovered: 1.0 ft Retained: 1.0 ft  | -           |            |
| ENTERPRISE BORING LOG XL-5467 (OLD XL-4653) 405 RENTON TO BELLEVUE ETL ENVIRO AND TRAFF.GPJ ENTERPRISE DATA TEMPLATE.GDJ 5/11/18  01 01 01 01 01 01 01 01 01 01 01 01 01 0 | -<br>-<br>-<br>-<br>210.0 |         | ◆   | (36)  5 5 6 (11) 4 5 8 (13)                   | X           | D-         |            | MC<br>GS<br>AL | SM, MC=15%, LL=18 Silty SAND with gravel and organics, sub-rounded, medium dense, gray, moist, homogeneous. HCl not tested. Recovered: 1.0 ft Retained: 1.0 ft Silty SAND with gravel, sub-rounded, medium dense, gray, moist, homogeneous. HCl not tested. Recovered: 0.8 ft Retained: 0.8 ft                   | -           |            |
| AL-3467 (ULD AL-4633) 403 KENION IO BELLEY<br>5 1  |                           |         | <ul> <li>♣</li> <li>↓</li> <li>↓</li></ul> | 7<br>7<br>10<br>(17)<br>14<br>10<br>5<br>(15) | X           | D-         |            | MC<br>LOI      | Silty SAND with gravel and organics, sub-rounded, medium dense, gray, moist, homogeneous. HCl not tested. Recovered: 0.1 ft Retained: 0.1 ft  MC=32%, LOI=7.3% Silty SAND with gravel and organics, sub-rounded, medium dense, dark gray, moist, homogeneous. HCl not tested. Recovered: 1.0 ft Retained: 1.0 ft | -           |            |
|  | 200.0                     |         | •   | 12<br>10                                      | X           | D-         | -6         |                | SILT, medium dense, light brown, moist, homogeneous.<br>HCl not tested.  | -           |            |





<sub>Job No\_</sub>XL-4653

SR \_\_405\_\_

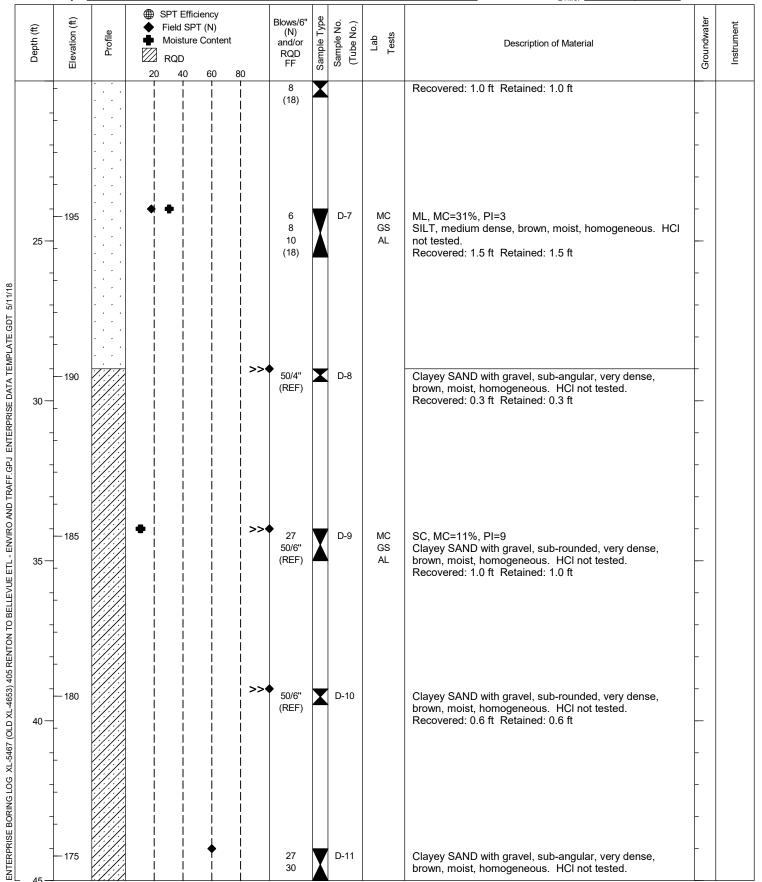
Elevation 219.2 ft

HOLE No. R2B-11-17

Sheet 2 of 3

Project I-405 Renton to Bellevue - ETL - Envir & Traff

Driller Peterson, Trevor







Job No. XL-4653 SR

Elevation 219.2 ft

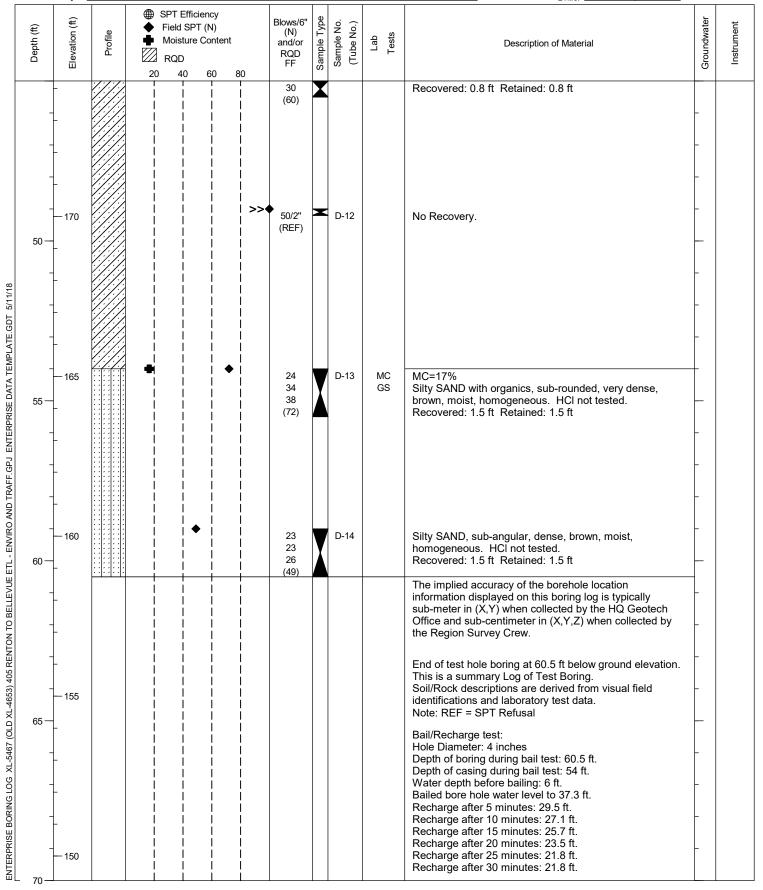
HOLE No. R2B-11-17

Sheet \_\_3\_\_ of \_\_3\_\_

Project I-405 Renton to Bellevue - ETL - Envir & Traff

405

Driller Peterson, Trevor



|                       | S.H  | S.R  | 405 SECTIO            | ON Sunset Blvd. to Factoria I/C Job No. C-2637                         |
|-----------------------|--|--|-----------------------|--|
| Hole                  | No1_   |  | Sub Section           | Cont. Sec. <u>1744</u>   |
| Station <u>377+44</u> |  |  |                       | Offset 109.0' Lt. © Ground El. 197.0'                                  |
|                       |  |  | Wash Boring           | Casing 3" x 14.0" W.T. El. See bottom of log.                          |
|                       |  |  |                       | Date <u>January 18, 1985</u> Sheet <u>1</u> of <u>2</u>                |
| DEPTH                 | BLOWS<br>PER FT.                                 | PROFILE                                      | SAMPLE<br>TUBE NOS.   | DESCRIPTION OF MATERIAL  |
|                       |  | 1  |                       | Brown, fine to coarse, sandy GRAVEL.                                   |
|                       |  | 1  | 1 STD                 | Very loose, brown, moist, gravelly, silty, fine to coarse SAND. (Fill) |
|                       | 4  | <b>↑</b> •                                   | 2 PEN<br>2 1          | Retained 0.7'.   |
|                       | <del> </del>                                     | <del> </del>                                 | 2 STD                 | Loose, brown, moist, gravelly, silty, fine to coarse SAND. (Fill)      |
|                       | 8  | 1 1  | 4 PEN                 | Retained 0.6'.   |
| 5                     | }  | <del></del>                                  | 4   2  <br>4   V      |  |
| <u>-</u>              |  | 1 1  | 1 A STD               | Very loose, brown, moist, gravelly, very silty, fine to coarse SAND    |
|                       | 3  | -  | 2 PEN 3               | with pieces of embers. Retained 0.5'.                                  |
| <del></del>           |  | 4 1  | 1                     |  |
|                       |  |  | 2 STD                 | Very loose, brown, moist, gravelly, very silty, fine to coarse SAND.   |
|                       |  | 1  | 3 PEN                 | Retained 1.2'.   |
|                       | 4  | 1  | 1 4                   |  |
| 10                    |  | 4 1  | 6 0000                |  |
|                       | 10   | ] ]  | 6 A STD<br>5 PEN      | Loose, brown, moist, silty, gravelly, fine to coarse SAND. Retained 1. |
|                       | 10   | ]  | 5 5                   |  |
|                       |  | 1  | 4                     |  |
|                       | ļ <u>.</u>                                       | 4  | 2 A STD<br>4 PEN      | Y have see sites Give CIND. Detained 0.71                              |
|                       | 9  | ]  | 5 6                   | Loose, brown, wet, very silty, fine SAND. Retained 0.7'.               |
| 15                    |  |  | 6                     | •  |
| 15                    |  | <b>│                                    </b> | 3 STD                 |  |
| <del> </del>          | 118/11"  | 1  | 18   PEN   100/ 7   7 | Very dense, brown, moist, silty, gravelly, fine to coarse SAND.        |
|                       | <u> </u>   | ]  | 5"                    | Retained 1.1'.   |
|                       |  |  | 45 <b>A</b> STD       |  |
| <del></del>           | <del>                                     </del> | 1  | 97 <b>L</b> PEN       | Very dense, brown, moist, silty, gravelly, fine to coarse SAND.        |
|                       | 197/9"   | -  | 100/ ▼ 8<br>3"        | Retained 0.8'.   |
| 20                    |  |  | ,                     |  |
|                       |  |  |                       | Original to Materials Engineer   |

Original to Materials Engineer Copy to Bridge Engineer Copy to District Administrator

Copy to

| DEPTH | BLOWS<br>PER FT. | PROFILE | SAMPLE<br>TUBE NOS.         | DESCRIPTION OF MATERIAL  |
|-------|------------------|---------|-----------------------------|--|
|       | 100/3"           |         | 100/ \$ STD<br>3" PEN       | Very dense, brown, moist, silty, gravelly, fine to coarse SAND. Retained 3".   |
|       |                  |         | 9                           |  |
|       |                  |         |                             |  |
|       | _                |         |                             |  |
| 25    | 100/4"           |         | 100/ STD<br>4" \$ PEN<br>10 | Very dense, brown, moist, silty, gravelly, fine to coarse SAND.  Retained 4".  |
|       |                  |         |                             |  |
|       |                  |         |                             | End of boring 25.0' below ground elevation. Water elevation undetermined.  |
|       |                  |         | ,                           | Note: Did not encounter any loss of drilling fluid until the depth of  |
|       |                  |         |                             | -24.0', then only slight loss.   |
|       |                  |         |                             | Note: Installed piezometer to a depth of -25.0'. Overall length of piezometer 27.5'. Piezometer slotted at -10.0' to -12.0' and -22.0' |
|       |                  |         |                             | to -24.0'.   |
|       |                  |         | <del> </del>                | Note: Samples appeared disturbed to -13.0'.  |
|       |                  | •       |                             | January 18, 1985 with 14.0' of casing; filled casing with water, no  |
|       |                  |         |                             | drop by January 21, 1985   |
|       |                  |         | -                           | This is a summary Log of Test Boring. Soil/Rock descriptions are derived from visual field identifications and laboratory test data.   |
|       |                  |         |                             |  |
|       |                  |         |                             |  |
|       |                  |         |                             |  |
|       |                  |         |                             |  |
|       |                  |         |                             | · · · · · · · · · · · · · · · · · · ·  |
|       |                  |         |                             | · · · · · · · · · · · · · · · · · · ·  |
|       |                  | •       |                             |  |
|       |                  |         |                             |  |
|       |                  |         |                             | ·  |
|       |                  |         |                             |  |
|       |                  |         | <u> </u>                    | ;<br>  |
|       |                  |         |                             |  |
|       |                  |         | 1                           | •  |

# Piezometer Readings

| CONTRACT No | . <u>C Z637</u> |                 | Total Lengti<br>Elevation To<br>Ground Eleva                       | 27.5'<br>199.5<br>197.0'              |             |
|-------------|-----------------|-----------------|--|---------------------------------------|-------------|
|             | 4 Offset 109.01 | LT              |  | ipe above Ground                      | 2.5         |
| DATE        | Water Reading   | Water Elevation |  | Remarks                               |             |
| 1-29-85     | -15.5           |                 | 84.0   | INITIAL RE                            | 9 DID 9     |
| i-30-85     | -12.0           |                 | 187.5'   |                                       | or '0.01 69 |
| 2-1-85      | - 12.0          |                 | 187.51   | 13.0' AND                             | 22.0' 70    |
| 2 -19 -85   | 9.8             |                 | 189.7  | 24.01                                 |             |
| 2-21-85     | 10.0            | <u> </u>        | 189,51   |                                       |             |
|             |                 |                 |  |                                       |             |
|             |                 |                 |  |                                       | •           |
|             |                 |                 |  |                                       |             |
|             |                 |                 |  |                                       |             |
| <u> </u>    | ,               |                 |  |                                       |             |
|             |                 |                 | ng again ng angga 1 hain at an |                                       |             |
|             |                 |                 |  |                                       |             |
|             |                 |                 |  |                                       | -           |
|             |                 |                 |  |                                       |             |
|             |                 |                 |  |                                       |             |
|             |                 |                 |  |                                       |             |
|             | ·               |                 |  | ,                                     | -           |
| -           |                 |                 |  | · · · · · · · · · · · · · · · · · · · |             |
|             |                 |                 |  |                                       |             |
|             |                 |                 |  | <del></del>                           |             |
| L           | <u> </u>        |                 |  |                                       |             |

| S.H              | S.R      | 405                    | SECTIO     | ON <u>Sunset</u> | t Blvd. to F      | actoria I/C           |                | _   | C-26   | 37  |
|------------------|----------|------------------------|------------|------------------|-------------------|-----------------------|----------------|---|--|---|
| No               | 2        | Sub Sec                | tion       |                  |                   |                       | · · ·          | _ Cont. Sec   | 1744   |   |
|                  |          |                        |            |                  |                   |                       | •              |   |  |   |
| of Boring_       | Wash     | Borin                  | ġ          |                  | Casing 3" x 20.0' |                       |                | W.T. EI. §  | See bo   | ttom of log.  |
| ctor             | <u> </u> |                        |            |                  |                   |                       | 1985           | _ Sheet   | 1  | of ·_2  |
| BLOWS<br>PER FT. | PROFILE  | SAI                    | MPLE       |                  |                   |                       | TION OF MATE   | RIAL  |  |   |
|                  | 1        | 1.                     |            | MUCK             |                   |                       |                | <del></del>   |  |   |
|                  |          | 4 4                    |            | Loose, br        | rown, moist       | , silty, grav         | elly, fine to  | coarse SA   | AND W  | vith wood   |
| 7                | ]        | 3                      | 1          | 11agment         | ts and coobs      | cs. Retain            |                |   |  | ······································  |
|                  | 1        | 5<br>8                 |            |                  |                   | n, moist, gi          | ravelly, ver   | y silty, fin  | e to c   | oarse SAND  |
| 17-              | 1 1      | 9                      | 2          |                  |                   |                       |                |   |  | <del></del>   |
|                  |          | 5<br>5                 |            | Medium o         | dense, brow       | n, moist, gr          | ravelly, silt  | y, fine to c  | oarse  | SAND  |
| 13               |          | 8<br>8                 | 3          |                  |                   |                       |                |   |  |   |
|                  |          | 7                      | STD        |                  |                   |                       | ···            |   |  |   |
| 20               | ]        | 9<br>11                | PEN<br>4   |                  |                   | n, moist, gi          | avelly, silt   | y, fine to c  | oarse  | SAND.   |
|                  |          | 10                     |            |                  |                   |                       |                |   |  | ·   |
|                  |          | 6                      | PEN        |                  |                   | , gravelly, s         | silty, fine to | coarse SA   | ND.  |   |
| •                |          | 5                      | 5          |                  |                   | ·                     |                |   |  |   |
|                  |          | 5                      | · STD      |                  |                   |                       |                |   |  |   |
| 7                |          | 3                      | PEN<br>6   | No recove        | ery.              | ····                  |                |   |  |   |
|                  |          | 3                      | ·          |                  |                   |                       |                |   |  |   |
| 7                |          | 6<br>3                 | STD<br>PEN |                  |                   | , gravelly, v         | ery silty, f   | ine to coar   | se SA  | ND.   |
|                  |          | 4                      | 7          |                  |                   |                       |                |   |  |   |
|                  |          | 6                      | STD        |                  |                   |                       |                |   | .,   |   |
| 20               | 1        | 9                      | PEN<br>8   |                  |                   |                       | velly, very    | silty, fine   | to coa   | rse SAND  |
|                  |          | 9                      |            |                  |                   | <u> </u>              |                |   |  |   |
|                  | No       | No2 on376+35 of Boring | No 2       | No               | No                | No.   2   Sub Section | No             | of Boring Wash Boring Casing 3" x 20.0'  ctor Date January 23, 1985  BLOWS PER FT. PROFILE TUBE NOS. DESCRIPTION OF MATE  MUCK  4 STD Loose, brown, moist, silty, gravelly, fine to fragments and cobbles. Retained 0.6'.  5 STD Medium dense, brown, moist, gravelly, ver Retained 1.0'.  8 PEN Retained 1.0'.  9 PEN Medium dense, brown, moist, gravelly, silt with wood fragments. Retained 1.0'.  13 8 3  7 STD PEN Medium dense, brown, moist, gravelly, silt with wood fragments. Retained 1.0'.  8 STD Loose, brown, moist, gravelly, silty, fine to Retained 0.2'.  5 STD Loose, brown, moist, gravelly, silty, fine to Retained 0.2'.  6 STD Loose, brown, moist, gravelly, silty, fine to Retained 0.2'.  6 STD Loose, brown, moist, gravelly, very silty, f Retained 1.0'.  9 PEN No recovery.  3 6 STD Loose, brown, moist, gravelly, very silty, f Retained 1.0'.  9 PEN Medium dense, brown, wet, gravelly, very silty, f Retained 1.0'. | No. 2 Sub Section Cont. Section 376+35  of Boring Wash Boring Casing 3" x 20.0' W.T. Et. Storm Bate January 23, 1985 Sheet  SLOWS PER FT. PROFILE TUBE NOS. DESCRIPTION OF MATERIAL  MUCK  SLOWS PER FT. PROFILE TUBE NOS. DESCRIPTION OF MATERIAL  MUCK  4 STD Upose, brown, moist, silty, gravelly, fine to coarse SA Fragments and cobbles. Retained 0.6'.  5 STD Medium dense, brown, moist, gravelly, very silty, fine to coarse SA STD With wood fragments. Retained 1.0'.  8 3 3  7 STD Wedium dense, brown, moist, gravelly, silty, fine to coarse SA STD Medium dense, brown, moist, gravelly, silty, fine to coarse SA STD Medium dense, brown, moist, gravelly, silty, fine to coarse SA STD Medium dense, brown, moist, gravelly, silty, fine to coarse SA STD Medium dense, brown, moist, gravelly, silty, fine to coarse SA STD Medium dense, brown, moist, gravelly, silty, fine to coarse SA STD Medium dense, brown, moist, gravelly, silty, fine to coarse SA STD Medium dense, brown, moist, gravelly, silty, fine to coarse SA STD Medium dense, brown, moist, gravelly, very silty, fine to coarse SA STD Medium dense, brown, moist, gravelly, very silty, fine to coarse SA STD Medium dense, brown, wet, gravelly, very silty, fine to coarse SA STD Medium dense, brown, wet, gravelly, very silty, fine to coarse SA STD Medium dense, brown, wet, gravelly, very silty, fine to coarse SA STD Medium dense, brown, wet, gravelly, very silty, fine to coarse SA STD Medium dense, brown, wet, gravelly, very silty, fine to coarse SA STD Medium dense, brown, wet, gravelly, very silty, fine to coarse SA STD Medium dense, brown, wet, gravelly, very silty, fine to coarse SA STD Medium dense, brown, wet, gravelly, very silty, fine to coarse SA STD Medium dense, brown, wet, gravelly, very silty, fine to coarse SA STD Medium dense, brown, wet, gravelly, very silty, fine to coarse SA STD Medium dense, brown, wet, gravelly, very silty, fine to coarse SA STD Medium dense, brown, wet, gravelly, very silty, fine to coarse SA STD Medium dense, brown, wet, gravelly, very silty, | No. 2 Sub Section Cont. Sec. 1744  on 376+35 Offset 115.0' Lt. Ground El. 182.  of Boring Wash Boring Casing 3" x 20.0' W.T. El. See be Letor Date January 23, 1985 Sheet 1  BLOWS PER FT. PROFILE TUBE NOS. DESCRIPTION OF MATERIAL  ### STD Lioose, brown, moist, silty, gravelly, fine to coarse SAND we fragments and cobbles. Retained 0.6'.  5 STD Medium dense, brown, moist, gravelly, very silty, fine to coarse Not with wood fragments. Retained 1.0'.  9 2 7 7 8 STD Medium dense, brown, moist, gravelly, silty, fine to coarse with wood fragments. Retained 1.0'.  8 9 PEN Medium dense, brown, moist, gravelly, silty, fine to coarse with wood fragments. Retained 1.0'.  8 11 4 Retained 1.1'.  10 4 PEN Retained 0.2'.  6 STD Loose, brown, moist, gravelly, silty, fine to coarse SAND. Retained 0.2'.  7 A STD PEN Retained 0.2'.  6 STD Loose, brown, moist, gravelly, silty, fine to coarse SAND. Retained 1.0'.  8 PEN Retained 1.0'.  9 PEN Retained 1.0'.  9 PEN Retained 1.0'. |

. . . .

DOT FORM 351-003 REVISED 12/79 Original to Materials Engineer Copy to Bridge Engineer Copy to District Administrator

Copy to

|              | No2  |          | 7   | Sunset Blvd. to Factoria I/C Sheet 2 of 2  |
|--------------|--|----------|---|--|
| DEPTH        | BLOWS<br>PER FT.                                 | PROFILE  | SAMPLE<br>TUBE NOS.                               | DESCRIPTION OF MATERIAL  |
|              | ]  |          | 5 A STD   | Loose, brown, moist, gravelly, very silty, fine to coarse SAND.  |
|              | 10-  |          | 5 PEN   | Retained 1.0'.   |
|              |  |          | 5 9   |  |
|              |  |          |   |  |
|              |  |          | 4 STD   | The second section with the second section of the second section of the second section |
|              | 7  |          | 2 PEN<br>5 10                                     | Loose, brown, moist, gravelly, very silty, fine to coarse SAND. Retained 2.0'.   |
| 0.5          |  |          | 5   |  |
| 25           |  |          | 17 <b>A</b> STD                                   | Medium dense, brown, moist, gravelly, very silty, fine to coarse SAND  |
|              |  |          | 8 PEN   | Retained 2.0'.   |
|              | 18   |          | 10 11   |  |
|              | ļ <u>-</u>                                       |          | 9   | <del></del>  |
|              |  |          | 8 A STD   | \$   |
|              |  |          | 8 PEN   | Medium dense, brown, wet, fine to medium sandy SILT. Retained 1.1'.  |
|              | 17   |          | 9 12  |  |
| 30           |  |          | 7   | $rac{d}{dt}$  |
|              |  | ŀ        | 4 STD   | Medium dense, brown, wet, fine sandy SILT. Retained 1.2'.  |
|              | 11   |          | 4 PEN 7 13  |  |
|              |  |          | <b> </b>   <sup>7</sup> / <sub>7</sub> <b>   </b> |  |
|              |  |          |   |  |
|              |  |          | 8  STD PEN  | Medium dense, brown, wet, very silty, fine SAND. Retained 1.4'.  |
|              | 21   | .        | 11 14   |  |
| 35           |  |          | 11  |  |
| <u> </u>     | <u> </u>   |          | 9 STD   | Medium dense, brown, moist, gravelly, very silty, fine to coarse SAND  |
|              | 16-  |          | 8 PEN   | Retained 1.5'.   |
|              | *  |          | 8 15  |  |
|              |  |          | 9   |  |
|              |  | <u> </u> | 9 A STD   |  |
|              |  | <b>A</b> | 22 PEN  | Very dense, brown, moist, silty, gravelly, fine to coarse SAND.  Retained 1.0'.  |
|              | 71_  | ¥        | 49 16<br>54 <b>V</b>                              | Retained 1.0.  |
| 40           |  |          |   |  |
|              |  |          |   | End of hosing 20 fl below ground aloyation   |
| <del></del>  |  |          |   | End of boring 39.5' below ground elevation.  |
|              |  |          |   | Note: January 29, 1985: With 20.0' of casing ground - water level was  |
|              |  |          |   | 23.0' below ground elevation.  |
| <del> </del> | <del>                                     </del> |          |   | This is a summary Log of Test Boring. Soil/Rock descriptions are   |
|              |  | ļ        |   | derived from visual field identifications and laboratory test data.  |
|              |  |          |   |  |
|              | L  | L        |   |  |

DOT FORM 351-003 REVISED 12/79

| S.H         |                  | S.R          | 405 SECTI  | ON Sunset Blvd. to Factoria I/C Job No. C-2637                           |
|-------------|------------------|--------------|--|--|
| Hole        | No               | 3            | Sub Section  | Cont. Sec. <u>1744</u>   |
|             |                  | 50           | •  | Offset 70.0' Lt. © Ground El.212.4'                                      |
| Type        | of Boring_       |              | Wash   | Boring Casing 22.5' x 3" W.T. El. See bottom of log.                     |
| Inspe       | ctor             | <del> </del> | · ·  | Date January 30, 1985 Sheet 1 of 2                                       |
| DEPTH       | BLOWS<br>PER FT. | PROFILE      | SAMPLE   | DESCRIPTION OF MATERIAL  |
|             |                  | 4            |  |  |
|             |                  | 1            | 1 STD<br>1 PEN   |  |
|             | 5 .              |              | 4 1  |  |
|             |                  | 1            | 1 STD<br>1 PEN   |  |
| <b>E</b>    | 3                | 1            | 2 2  |  |
|             |                  | 1            | 4 STD<br>2 PEN   |  |
| <del></del> | 5                | 1 1          | $\frac{2}{3}$ $\frac{1}{3}$ $\frac{1}{3}$                              | counies, (Pin) Retained 0.0.   |
|             | <u> </u>         | 1            | 5 A STD  |  |
| ·           |                  | 1            | 4 PEN<br>7 4   | Medium dense, brown, moist, slightly silty, gravelly, fine to coarse SAl |
| <del></del> | 11               | 1 1          | 4  | with cobbles. (Fill) Retained 0.6'.                                      |
| 10          |                  | 1            | 3 STD  | ,  |
|             | - 5              |              | $\begin{array}{c c} 2 & \hline PEN \\ \hline 3 & \hline 5 \end{array}$ | Retained 0.4'.   |
|             |                  | <b> </b>     | 3  | Note: Filled casing with water evening of January 30, 1985; no loss of   |
| •           |                  | 4            | 5 STD<br>5 PEN   | water noted morning of January 31, 1985.                                 |
|             | 8                | ]            | 3 6  | of organic. Retained 0.5'.   |
| 15          |                  |              | 4  |  |
|             |                  |              | 5 STD<br>3 PEN   |  |
|             | 0                |              | 3 <b>7</b> 5   |  |
|             |                  |              | 7 A STD  | · · · · · · · · · · · · · · · · · · ·                                    |
|             | 11               |              | 5 PEN<br>6 8   |  |
| 20          |                  |              | 9  |  |

27.5

Original to Materials Engineer Copy to Bridge Engineer Copy to District Administrator

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| Hole 1                                | No               | 3            | Sub Section  | Sunset Blvd. to Factoria I/C Sheet 2 of 2  |
|---------------------------------------|------------------|--------------|--|--|
| DEPTH                                 | BLOWS<br>PER FT. | PROFILE      | SAMPLE<br>TUBE NOS.                                  | DESCRIPTION OF MATERIAL  |
|                                       | 19               |              | 7 STD<br>9 PEN<br>10 _9                              |  |
|                                       |                  |              | 14   | Gray, wet, slightly sandy, slightly gravelly SILT.   |
|                                       | 110              |              | 25 A STD<br>48 PEN                                   |  |
| 25                                    | 118              |              | 70 <b>1</b> 0 10 10 10 10 10 10 10 10 10 10 10 10 10 | Retained 1:7.  Note: Filled casing with water evening of January 31, 1985; water elevation -9.7 morning of February 1, 1985.         |
|                                       | 153              |              | 45 A STD<br>59 PEN                                   | Very dense, brown, moist, silty, gravelly, fine to coarse SAND.  Retained 1.1'.  |
|                                       |                  |              | 94 11<br>100 V                                       |  |
|                                       |                  |              | , .  | End boring 27.0' below ground elevation.   |
|                                       |                  | <u> </u><br> | ,  |  |
| 30                                    |                  |              |  |  |
|                                       |                  |              |  | Note: Water-bearing gravel from -7.5' to -11.5'. Experienced slight loss of drilling fluid upper 11.0'.                              |
|                                       |                  |              |  | Note: Drilled dry from -0.0' to -7.5'.  Washed bored hole from -7.5' to -27.0'   |
|                                       |                  |              |  | Note: Piezometer installed February 4, 1985.  Overall length of piezometer 18.0'. Piezometer in ground 15.0'.                        |
|                                       |                  |              |  | Slotted from -14.0' to -12.0'.  Water elevation undetermined at this time.  Top 3.0' of piezometer sealed with bentonite.            |
|                                       |                  |              |  | 10p 3,0 or piezometer sealed with bentonite.   |
|                                       |                  |              |  | This is a summary Log of Test Boring. Soil/Rock descriptions are derived from visual field identifications and laboratory test data. |
|                                       |                  |              |  |  |
|                                       |                  |              |  |  |
|                                       |                  | •            |  |  |
|                                       |                  |              |  |  |
|                                       |                  |              |  |  |
|                                       |                  |              |  |  |
| · · · · · · · · · · · · · · · · · · · | ·                |              |  |  |
|                                       | L                | -            | <u> </u>   |  |

# Piezometer Readings

| CONTRACT No.  Hole No. 3  Station 377+50 |                      | ( t | Total Length Elevation To Ground Eleve Length of Pi | op of Pipe                    | 18.0°<br>215.4°<br>212.4°<br>3.0° |
|--|----------------------|-----|---|-------------------------------|-----------------------------------|
| DATE                                     | Water Reading        | Wat | er Elevation  | Remarks                       |                                   |
| 2-8-1985<br>Z-19-1985<br>Z-21-1985       | 10.0<br>9.0'<br>9.0' | Z   | 205.4<br>206.4<br>206.4                             | Juital Feadin<br>PIPE Shotter |                                   |
|  |                      |     |   |                               |                                   |
|  |                      |     |   |                               |                                   |
|  |                      |     |   |                               |                                   |
|  |                      |     |   |                               |                                   |
|  |                      |     |   |                               |                                   |







In Association with

### Appendix B **Laboratory Test Results**

| 7-                         |                     | Ŧ                      |                         |                        | 4VITY            |    | ATTERBERG<br>LIMITS (%) |    |          |        |         | NOI                         |   |
|----------------------------|---------------------|------------------------|-------------------------|------------------------|------------------|----|-------------------------|----|----------|--------|---------|-----------------------------|---|
| EXPLORATION<br>DESIGNATION | TOP DEPTH<br>(feet) | BOTTOM DEPTH<br>(feet) | MOISTURE<br>CONTENT (%) | ORGANIC<br>CONTENT (%) | SPECIFIC GRAVITY | LL | PL                      | PI | % GRAVEL | % SAND | % FINES | ASTM SOIL<br>CLASSIFICATION | SAMPLE DESCRIPTION                                  |
| W-201-20,S-3               | 7.5                 | 9.0                    | 15.2                    |                        |                  | 30 | 21                      | 9  | 1.7      | 34.3   | 64.0    | CL                          | Light olive-brown, sandy lean CLAY                  |
| W-201-20,S-5               | 15.0                | 16.5                   | 20.7                    |                        |                  |    |                         |    |          | 22.0   | 78.0    | ML                          | Light olive-brown, SILT with sand                   |
| W-201-20,S-6               | 20.0                | 21.5                   | 25.7                    |                        |                  | 37 | 24                      | 13 |          | 1.2    | 98.8    | CL                          | Gray, lean CLAY                                     |
| W-201-20,S-8               | 30.0                | 31.5                   | 23.4                    |                        |                  | 38 | 26                      | 12 | 0.5      | 9.6    | 90.0    | ML                          | Grayish-brown, SILT                                 |
| W-201-20,S-9               | 35.0                | 36.5                   | 11.2                    |                        |                  |    |                         |    |          | 44.7   | 55.3    | ML                          | Light olive-brown, sandy SILT                       |
| W-201-20,S-11              | 45.0                | 46.5                   | 12.6                    |                        |                  |    |                         |    |          | 38.1   | 61.9    | ML                          | Light olive-brown, sandy SILT                       |
| W-201-20,S-14              | 60.0                | 61.5                   | 22.7                    |                        |                  |    |                         |    | 0.4      | 84.8   | 14.8    | SM                          | Dark olive-gray, silty SAND                         |
| W-203-20,S-1               | 2.5                 | 4.0                    | 2.8                     |                        |                  |    |                         |    | 56.5     | 38.5   | 5.0     | GP-GM                       | Olive-gray, poorly graded GRAVEL with silt and sand |
| W-203-20,S-2               | 5.0                 | 6.5                    | 5.7                     |                        |                  |    |                         |    | 36.7     | 44.6   | 18.8    | SM                          | Olive-brown, silty SAND with gravel                 |
| W-203-20,S-3               | 7.5                 | 9.0                    | 10.5                    |                        |                  |    |                         |    |          |        | 29.5    | SM                          | Olive-gray, silty SAND                              |
| W-203-20,S-4               | 10.0                | 11.5                   | 12.2                    |                        |                  |    |                         |    |          |        | 24.1    | SM                          | Dark gray, silty SAND                               |
| W-203-20,S-5               | 15.0                | 16.5                   | 11.9                    |                        |                  |    |                         |    |          |        | 22.9    | SM                          | Dark olive-gray, silty SAND                         |
| W-203-20,S-6               | 20.0                | 21.5                   | 9.9                     |                        |                  |    |                         |    | 13.0     | 76.0   | 11.0    | SW-SM                       | Dark gray, well-graded SAND with silt               |
| W-203-20,S-7               | 25.0                | 26.5                   | 11.5                    |                        |                  | 19 | 17                      | 2  | 27.2     | 42.7   | 30.1    | SM                          | Olive-brown, silty SAND with gravel                 |
| W-207-20,S-2               | 5.0                 | 6.5                    | 10.8                    |                        |                  |    |                         |    | 13.9     | 49.0   | 37.2    | SM                          | Olive-brown, silty SAND                             |
| W-207-20,S-4               | 10.0                | 11.5                   | 10.0                    |                        |                  |    |                         |    | 15.0     | 53.6   | 31.4    | SM                          | Olive-brown, silty SAND with gravel                 |
| W-207-20,S-5               | 15.0                | 16.5                   | 17.0                    |                        |                  | 28 | 20                      | 8  | 16.1     | 33.8   | 50.1    | CL                          | Olive-brown, sandy lean CLAY with gravel            |
| W-207-20,S-8               | 30.0                | 31.5                   | 14.5                    |                        |                  |    |                         |    | 8.1      | 64.2   | 27.6    | SM                          | Olive-brown, silty SAND                             |
| W-208-20,S-1               | 2.5                 | 4.0                    | 9.8                     |                        |                  |    |                         |    | 8.6      | 74.4   | 17.0    | SM                          | Olive-brown, silty SAND                             |
| W-208-20,S-3               | 7.5                 | 9.0                    | 8.7                     |                        |                  |    |                         |    | 7.4      | 58.9   | 33.7    | SM                          | Grayish-brown, silty SAND                           |

- 1. This table summarizes information presented elsewhere in the report and should be used in conjunction with the report test, other graphs and tables, and the exploration logs.
- 2. The soil classifications in this table are based on ASTM D2487 and D2488 as applicable.



I-405 Renton to Bellevue Widening and Express Toll Lanes Client Project No.: PS19203160

## SUMMARY OF MATERIAL PROPERTIES

PAGE: 2 of 4

| 7-                         |                     | Ŧ                      |                         |                        | 4VITY            |    | ATTERBERG<br>LIMITS (%) |    |          |        |         | NOI                         |                                     |
|----------------------------|---------------------|------------------------|-------------------------|------------------------|------------------|----|-------------------------|----|----------|--------|---------|-----------------------------|-------------------------------------|
| EXPLORATION<br>DESIGNATION | TOP DEPTH<br>(feet) | BOTTOM DEPTH<br>(feet) | MOISTURE<br>CONTENT (%) | ORGANIC<br>CONTENT (%) | SPECIFIC GRAVITY | LL | PL                      | PI | % GRAVEL | % SAND | % FINES | ASTM SOIL<br>CLASSIFICATION | SAMPLE DESCRIPTION                  |
| W-208-20,S-5               | 15.0                | 16.5                   | 8.9                     |                        |                  |    |                         |    | 0.9      | 58.6   | 40.6    | SM                          | Olive-brown, silty SAND             |
| W-208-20,S-7               | 25.0                | 26.5                   | 12.8                    |                        |                  |    |                         |    | 3.3      | 47.5   | 49.3    | SM                          | Olive-brown, silty SAND             |
| W-208-20,S-8B              | 30.0                | 31.5                   | 29.8                    |                        |                  | 45 | 21                      | 24 | 1.3      | 20.5   | 78.2    | CL                          | Gray, lean CLAY with sand           |
| W-208-20,S-9               | 35.0                | 36.5                   | 9.5                     |                        |                  | 17 | 13                      | 4  | 10.2     | 46.9   | 42.9    | SC-SM                       | Olive-brown, silty, clayey SAND     |
| W-208-20,S-10              | 40.0                | 41.5                   | 12.0                    |                        |                  |    |                         |    | 8.2      | 62.1   | 29.8    | SM                          | Olive-brown, silty SAND             |
| W-214-20,S-1               | 2.5                 | 4.0                    | 10.1                    | 1.6                    |                  | 39 | 17                      | 22 | 7.2      | 45.5   | 47.3    | SC                          | Olive-brown, clayey SAND            |
| W-214-20,S-2               | 5.0                 | 6.5                    | 31.2                    |                        |                  |    |                         |    | 0.6      | 9.7    | 89.7    | ML                          | Grayish-brown, SILT                 |
| W-214-20,S-4               | 10.0                | 11.5                   | 11.4                    |                        |                  | 34 | 24                      | 10 | 47.5     | 38.0   | 14.5    | GM                          | Olive-brown, silty GRAVEL with sand |
| W-214-20,S-7               | 25.0                | 26.5                   | 11.2                    |                        |                  |    |                         |    | 4.9      | 59.2   | 36.0    | SM                          | Light olive-brown, silty SAND       |
| W-214-20,S-9               | 35.0                | 36.5                   | 21.3                    |                        |                  | 23 | 20                      | 3  | 0.7      | 38.6   | 60.7    | ML                          | Light olive-brown, sandy SILT       |
| W-215-20,S-1               | 2.5                 | 4.0                    | 9.6                     |                        |                  |    |                         |    | 3.5      | 66.7   | 29.8    | SM                          | Grayish-brown, silty SAND           |
| W-215-20,S-3               | 7.5                 | 9.0                    | 14.9                    |                        |                  |    |                         |    | 0.4      | 76.4   | 23.2    | SM                          | Olive-brown, silty SAND             |
| W-215-20,S-5B              | 16.0                | 16.5                   | 18.8                    |                        |                  | NP | NP                      | NP |          | 28.1   | 71.9    | ML                          | Light olive-brown, SILT with sand   |
| W-215-20,S-7               | 25.0                | 26.5                   | 17.9                    |                        |                  |    |                         |    |          | 77.5   | 22.5    | SM                          | Light olive-brown, silty SAND       |
| W-217-20,S-1               | 2.5                 | 4.0                    | 8.4                     |                        |                  |    |                         |    | 4.7      | 50.3   | 45.0    | SM                          | Grayish-brown, silty SAND           |
| W-217-20,S-3               | 7.5                 | 8.8                    | 8.8                     |                        |                  |    |                         |    |          |        | 36.8    | SM                          | Grayish-brown, silty SAND           |
| W-217-20,S-5               | 15.0                | 16.0                   | 11.8                    |                        |                  |    |                         |    |          |        | 40.3    | SM                          | Light brownish-gray, silty SAND     |
| W-217-20,S-7               | 25.0                | 26.5                   | 23.4                    |                        |                  | 48 | 30                      | 18 | 0.1      | 10.0   | 89.9    | ML                          | Gray, SILT                          |
| W-217-20,S-9               | 35.0                | 36.5                   | 24.2                    |                        |                  | 42 | 26                      | 16 |          | 8.0    | 92.0    | CL                          | Gray, lean CLAY                     |
| W-217-20,S-10              | 40.0                | 41.0                   | 15.4                    |                        |                  | 56 | 28                      | 28 | 8.5      | 18.9   | 72.5    | СН                          | Gray, fat CLAY with sand            |

- 1. This table summarizes information presented elsewhere in the report and should be used in conjunction with the report test, other graphs and tables, and the exploration logs.
- 2. The soil classifications in this table are based on ASTM D2487 and D2488 as applicable.



I-405 Renton to Bellevue Widening and Express Toll Lanes Client Project No.: PS19203160

## SUMMARY OF MATERIAL PROPERTIES

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| 7-                         |                     | ТН                    |                         |                        | GRAVITY      |    | ATTERBERG<br>LIMITS (%) |    |          |        |         | NOI                         |  |
|----------------------------|---------------------|-----------------------|-------------------------|------------------------|--------------|----|-------------------------|----|----------|--------|---------|-----------------------------|--|
| EXPLORATION<br>DESIGNATION | TOP DEPTH<br>(feet) | BOTTOM DEP'<br>(feet) | MOISTURE<br>CONTENT (%) | ORGANIC<br>CONTENT (%) | SPECIFIC GRA | LL | PL                      | PI | % GRAVEL | % SAND | % FINES | ASTM SOIL<br>CLASSIFICATION | SAMPLE DESCRIPTION                                   |
| W-217-20,S-12              | 50.0                | 50.8                  | 4.5                     |                        |              |    |                         |    | 33.2     | 55.6   | 11.2    | SW-SM                       | Grayish-brown, well-graded SAND with silt and gravel |
| W-221-20,S-2               | 5.0                 | 6.5                   | 18.8                    |                        |              |    |                         |    | 5.9      | 74.2   | 19.9    | SM                          | Dark yellowish-brown, silty SAND                     |
| W-221-20,S-3               | 7.5                 | 9.0                   | 13.0                    |                        |              | 23 | 15                      | 8  | 6.6      | 48.8   | 44.6    | SC                          | Grayish-brown, clayey SAND                           |
| W-221-20,S-4               | 10.0                | 11.5                  | 13.5                    |                        |              |    |                         |    | 11.8     | 59.6   | 28.5    | SM                          | Olive-brown, silty SAND                              |
| W-221-20,S-5               | 15.0                | 16.5                  | 23.6                    |                        |              | 50 | 28                      | 22 | 7.2      | 17.6   | 75.2    | СН                          | Grayish-brown, fat CLAY with sand                    |
| W-221-20,S-7               | 25.0                | 26.5                  | 31.2                    |                        |              | 41 | 25                      | 16 |          | 5.5    | 94.5    | CL                          | Dark gray, lean CLAY                                 |
| W-221-20,S-8               | 30.0                | 31.5                  | 37.3                    |                        |              | 34 | 23                      | 11 | 2.9      | 11.8   | 85.4    | CL                          | Dark gray, lean CLAY                                 |

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I-405 Renton to Bellevue Widening and Express Toll Lanes Client Project No.: PS19203160 SUMMARY OF MATERIAL PROPERTIES

PAGE: 4 of 4

| 7             |                     | E                      |                         |                        | WITY             |    | ATTERBERG<br>LIMITS (%) |    |          |        |         | NO                          |  |
|---------------|---------------------|------------------------|-------------------------|------------------------|------------------|----|-------------------------|----|----------|--------|---------|-----------------------------|--|
| EXPLORATION   | TOP DEPTH<br>(feet) | BOTTOM DEPTH<br>(feet) | MOISTURE<br>CONTENT (%) | ORGANIC<br>CONTENT (%) | SPECIFIC GRAVITY | LL | PL                      | PI | % GRAVEL | % SAND | % FINES | ASTM SOIL<br>CLASSIFICATION | SAMPLE DESCRIPTION                                   |
| W-206-20,S-8  | 30.0                | 31.5                   | 24.3                    |                        |                  | NP | NP                      | NP |          | 19.1   | 80.9    | ML                          | Olive, SILT with sand                                |
| W-216-20,S-1  | 2.5                 | 4.0                    | 7.9                     |                        |                  |    |                         |    | 14.4     | 56.3   | 29.3    | SM                          | Light olive-brown, silty SAND                        |
| W-216-20,S-2  | 5.0                 | 6.5                    | 12.0                    |                        |                  |    |                         |    | 1.4      | 47.1   | 51.6    | ML                          | Olive-brown, sandy SILT                              |
| W-216-20,S-4  | 10.0                | 11.0                   | 8.0                     |                        |                  |    |                         |    | 7.4      | 56.7   | 35.9    | SM                          | Light olive-brown, silty SAND                        |
| W-216-20,S-6  | 20.0                | 21.5                   | 5.0                     |                        |                  |    |                         |    |          | 89.9   | 10.1    | SP-SM                       | Grayish-brown, poorly graded SAND with silt          |
| W-218-20,S-1  | 2.5                 | 4.0                    | 2.8                     |                        |                  |    |                         |    | 38.9     | 52.0   | 9.1     | SW-SM                       | Grayish-brown, well-graded SAND with silt and gravel |
| W-218-20,S-3  | 7.5                 | 9.0                    | 15.5                    |                        |                  |    |                         |    | 9.1      | 57.9   | 33.0    | SM                          | Dark olive-brown, silty SAND                         |
| W-218-20,S-5  | 15.0                | 16.5                   | 10.6                    |                        |                  |    |                         |    | 20.3     | 38.5   | 41.2    | SM                          | Light olive-brown, silty SAND with gravel            |
| W-218-20,S-6  | 20.0                | 21.0                   | 10.0                    |                        |                  | 17 | 14                      | 3  | 17.6     | 37.1   | 45.3    | SM                          | Dark grayish-brown, silty SAND with gravel           |
| W-218-20,S-8  | 30.0                | 30.5                   | 5.3                     |                        |                  |    |                         |    | 28.1     | 36.1   | 35.8    | SM                          | Grayish-brown, silty SAND with gravel                |
| W-218-20,S-11 | 45.0                | 46.0                   | 21.8                    |                        |                  | 33 | 25                      | 8  |          | 1.9    | 98.1    | ML                          | Olive-brown, SILT                                    |
| W-218-20,S-13 | 55.0                | 56.0                   | 24.8                    |                        |                  | 36 | 23                      | 13 | 1.1      | 3.9    | 95.0    | CL                          | Very dark gray, lean CLAY                            |
| W-218-20,S-15 | 65.0                | 65.5                   | 8.0                     |                        |                  |    |                         |    | 34.2     | 50.7   | 15.1    | SM                          | Dark olive brown, silty SAND with gravel             |
| W-218-20,S-17 | 75.0                | 75.2                   | 6.4                     |                        |                  |    |                         |    | 38.1     | 37.3   | 24.6    | GM                          | Dark grayish-brown, silty GRAVEL with sand           |
| W-219-20,S-1  | 2.5                 | 4.0                    | 6.1                     |                        |                  |    |                         |    | 14.0     | 46.1   | 39.9    | SM                          | Light olive-brown, silty SAND                        |
| W-219-20,S-3  | 7.5                 | 9.0                    | 7.8                     |                        |                  |    |                         |    | 6.2      | 51.7   | 42.1    | SM                          | Olive-brown, silty SAND                              |
| W-219-20,S-5  | 15.0                | 16.5                   | 7.5                     |                        |                  |    |                         |    | 1.1      | 52.8   | 46.1    | SM                          | Olive-brown, silty SAND                              |
| W-219-20,S-7  | 25.0                | 26.5                   | 5.0                     |                        |                  |    |                         |    | 4.8      | 58.0   | 37.2    | SM                          | Dark gray, silty SAND                                |
| W-219-20,S-9  | 35.0                | 36.5                   | 6.8                     |                        |                  |    |                         |    | 17.1     | 45.1   | 37.8    | SM                          | Dark gray, silty SAND with gravel                    |
| W-220-20,S-1  | 2.5                 | 4.0                    | 3.9                     |                        |                  |    |                         |    | 2.5      | 84.8   | 12.7    | SM                          | Light yellowish-brown, silty SAND                    |

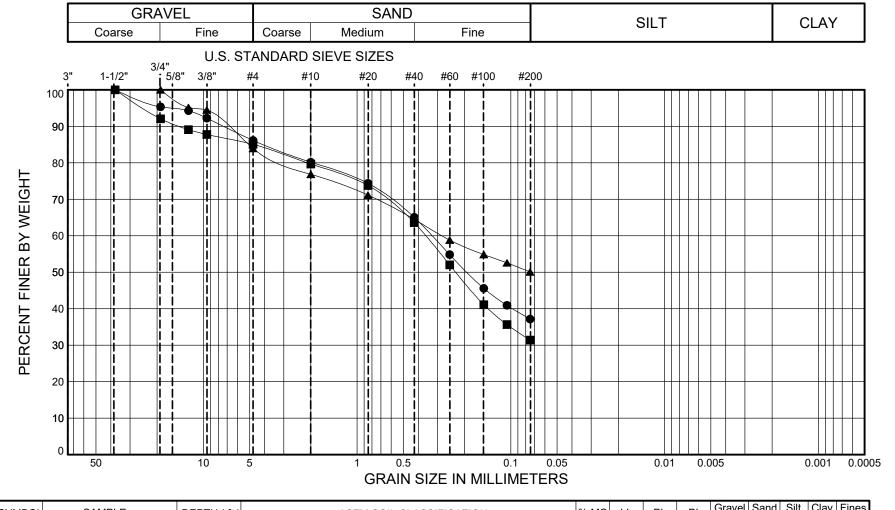
- 1. This table summarizes information presented elsewhere in the report and should be used in conjunction with the report test, other graphs and tables, and the exploration logs.
- 2. The soil classifications in this table are based on ASTM D2487 and D2488 as applicable.



I-405 Renton to Bellevue Widening and Express Toll Lanes Client Project No.: PS19203160

## SUMMARY OF MATERIAL PROPERTIES

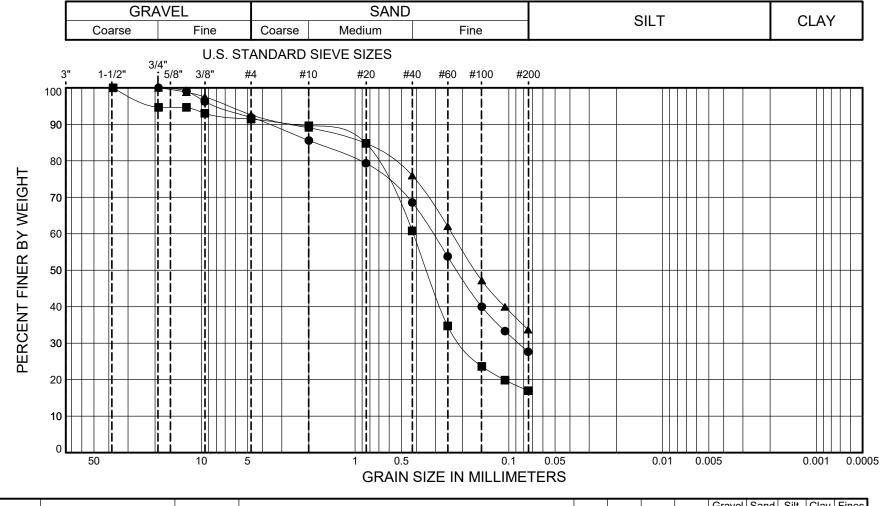
PAGE: 2 of 4



| SYMBOL   | SAMF                   | LE  | DEPTH (ft.) | ASTM SOIL CLASSIFICATION                      | % MC | LL | PL | PI | Gravel<br>% | Sand<br>% | Silt<br>% | Clay<br>% | Fines<br>% |
|----------|------------------------|-----|-------------|---|------|----|----|----|-------------|-----------|-----------|-----------|------------|
| •        | W-207-20 S-2 5.0 - 6.5 |     | 5.0 - 6.5   | (SM) Olive-brown, silty SAND                  | 11   |    |    |    | 13.9        | 49.0      |           |           | 37.2       |
|          | W-207-20               | S-4 | 10.0 - 11.5 | (SM) Olive-brown, silty SAND with gravel      | 10   |    |    |    | 15.0        | 53.6      |           |           | 31.4       |
| <b>A</b> | W-207-20               | S-5 | 15.0 - 16.5 | (CL) Olive-brown, sandy lean CLAY with gravel | 17   | 28 | 20 | 8  | 16.1        | 33.8      |           |           | 50.1       |



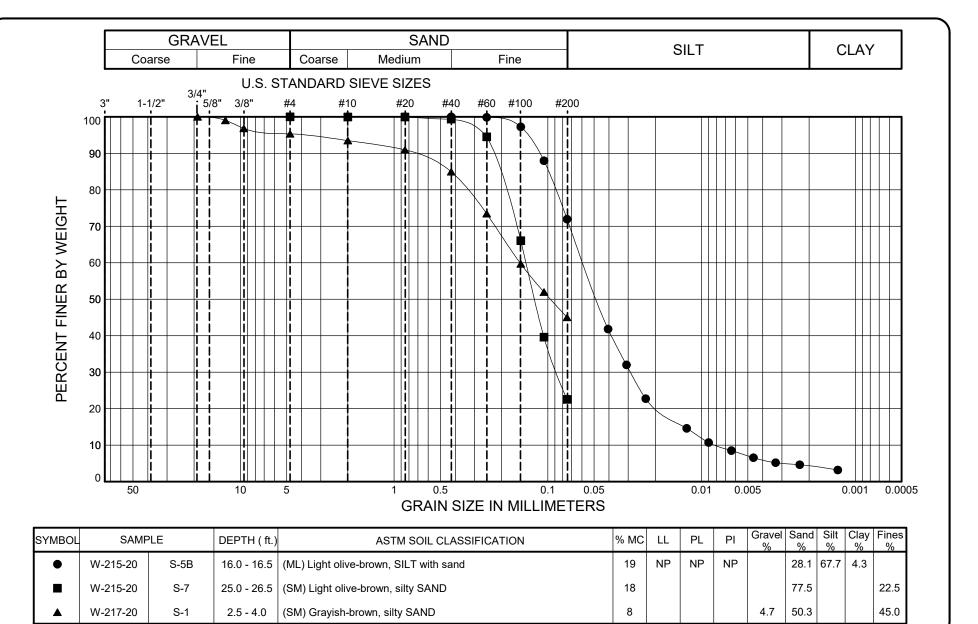
PARTICLE-SIZE ANALYSIS OF SOILS METHOD ASTM D6913



| SYMBOL   | SAMF     | LE  | DEPTH (ft.) | ASTM SOIL CLASSIFICATION       | % MC | LL | PL | PI | Gravel<br>% | Sand<br>% | Silt<br>% | Clay<br>% | Fines % |
|----------|----------|-----|-------------|--------------------------------|------|----|----|----|-------------|-----------|-----------|-----------|---------|
| •        | W-207-20 | S-8 | 30.0 - 31.5 | (SM) Olive-brown, silty SAND   | 14   |    |    |    | 8.1         | 64.2      |           |           | 27.6    |
|          | W-208-20 | S-1 | 2.5 - 4.0   | (SM) Olive-brown, silty SAND   | 10   |    |    |    | 8.6         | 74.4      |           |           | 17.0    |
| <b>A</b> | W-208-20 | S-3 | 7.5 - 9.0   | (SM) Grayish-brown, silty SAND | 9    |    |    |    | 7.4         | 58.9      |           |           | 33.7    |

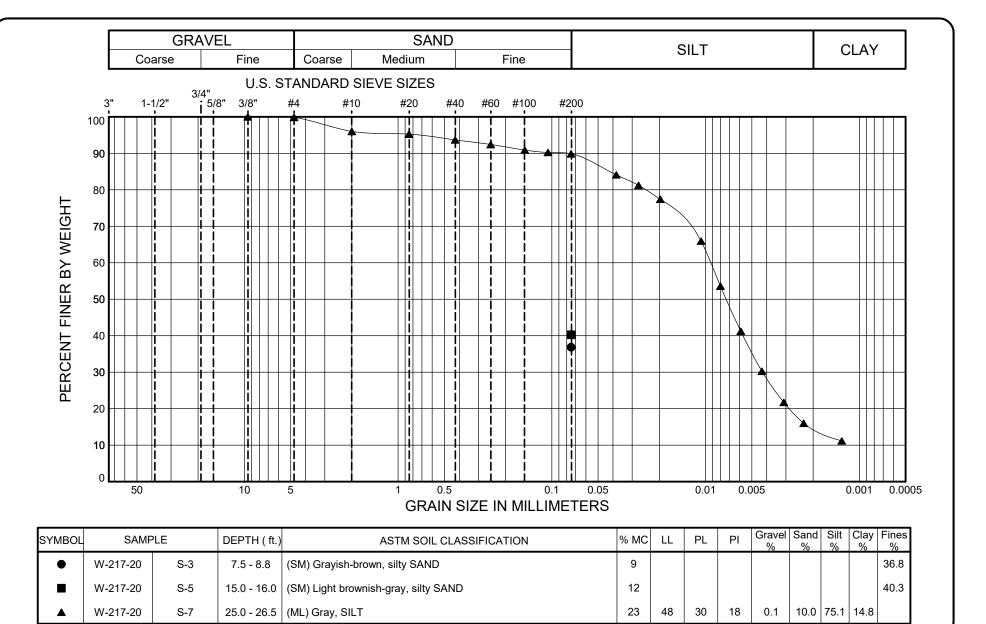


PARTICLE-SIZE ANALYSIS OF SOILS METHOD ASTM D6913



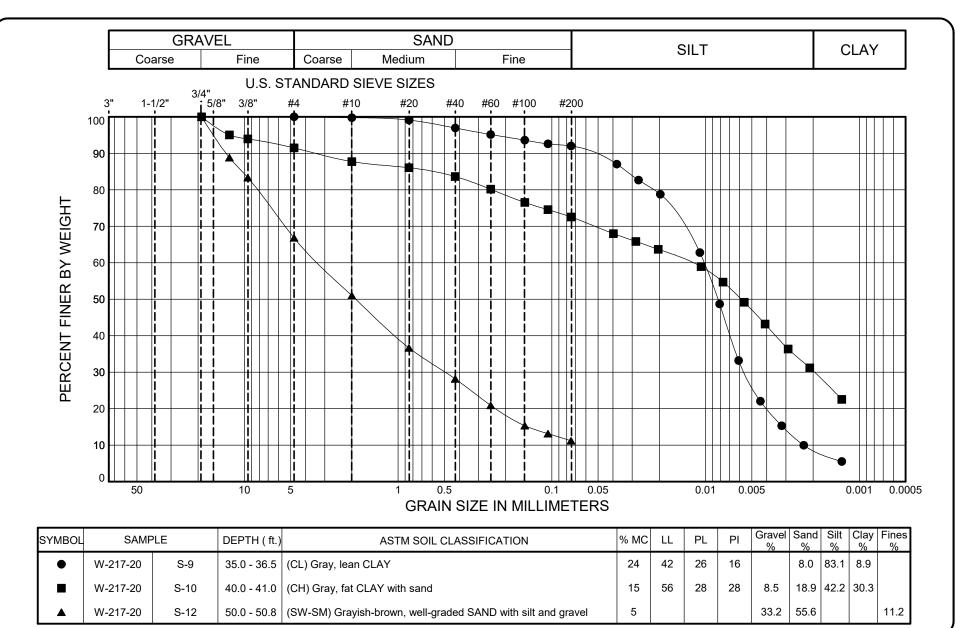


PARTICLE-SIZE ANALYSIS OF SOILS METHOD ASTM D6913



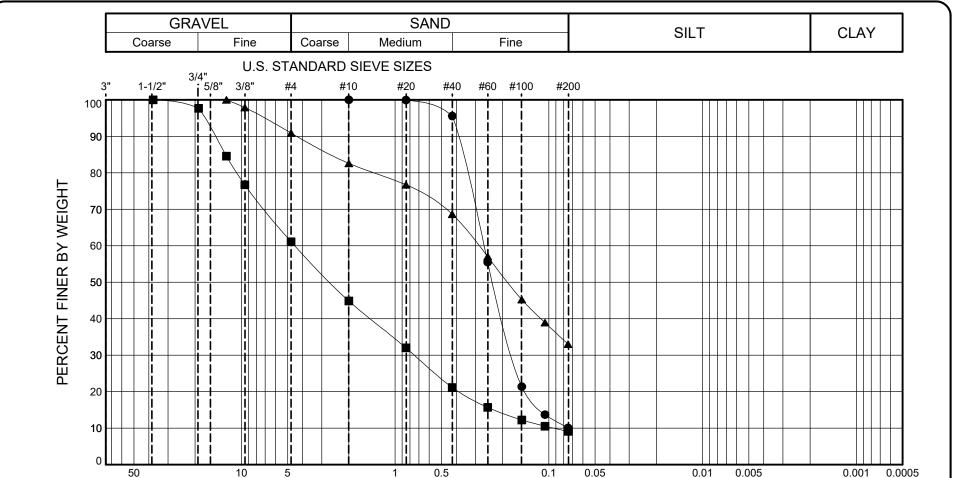


PARTICLE-SIZE ANALYSIS OF SOILS METHOD ASTM D6913





PARTICLE-SIZE ANALYSIS OF SOILS METHOD ASTM D6913



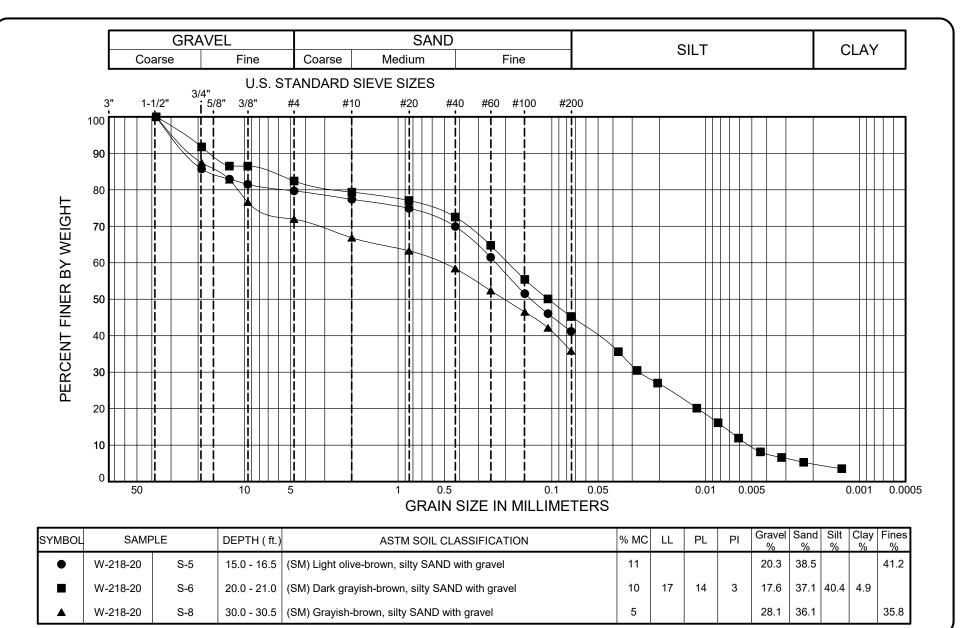
| SYMBOL   | SAMF     | LE                      | DEPTH (ft.) | ASTM SOIL CLASSIFICATION                                     | % MC | LL | PL | PI | Gravel<br>% | Sand<br>% | Silt<br>% | Clay<br>% | Fines % |
|----------|----------|-------------------------|-------------|--|------|----|----|----|-------------|-----------|-----------|-----------|---------|
| •        | W-216-20 | W-216-20 S-6 20.0 - 21. |             | (SP-SM) Grayish-brown, poorly graded SAND with silt          | 5    |    |    |    |             | 89.9      |           |           | 10.1    |
|          | W-218-20 | S-1                     | 2.5 - 4.0   | (SW-SM) Grayish-brown, well-graded SAND with silt and gravel | 3    |    |    |    | 38.9        | 52.0      |           |           | 9.1     |
| <b>A</b> | W-218-20 | S-3                     | 7.5 - 9.0   | (SM) Dark olive-brown, silty SAND                            | 15   |    |    |    | 9.1         | 57.9      |           |           | 33.0    |

**GRAIN SIZE IN MILLIMETERS** 



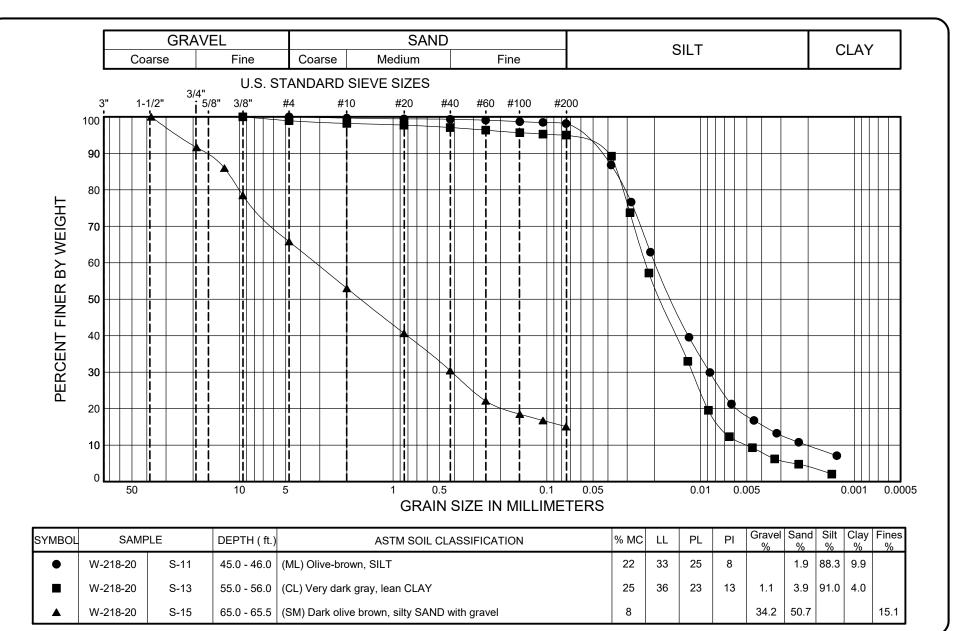
I-405 Renton to Bellevue Widening and Express Toll Lanes Client Project No.: PS19203160

PARTICLE-SIZE ANALYSIS **OF SOILS** METHOD ASTM D6913



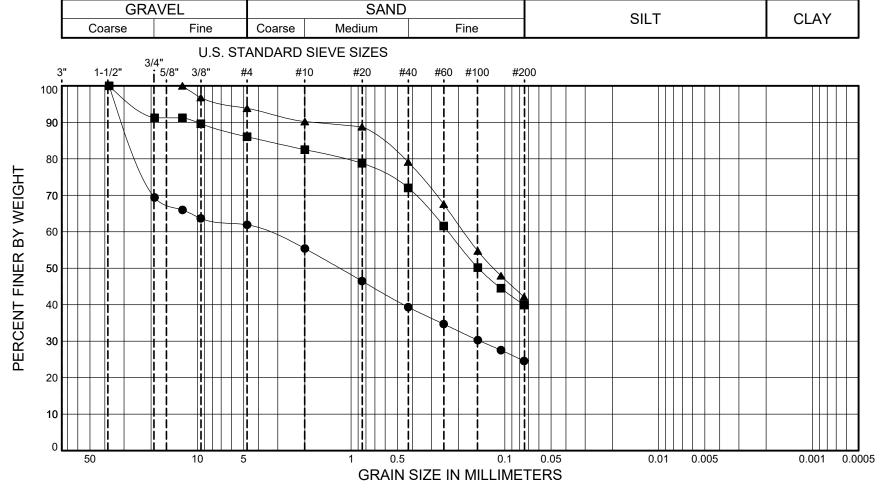


PARTICLE-SIZE ANALYSIS OF SOILS METHOD ASTM D6913





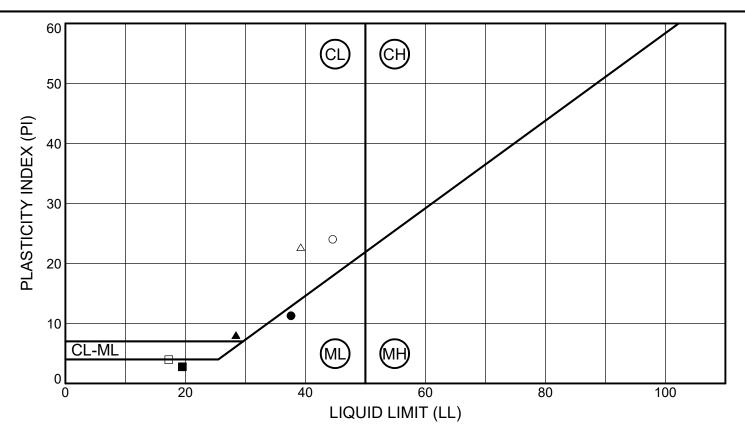
PARTICLE-SIZE ANALYSIS OF SOILS METHOD ASTM D6913



| SYMBOL   | SAMF     | LE   | DEPTH (ft.) | ASTM SOIL CLASSIFICATION                        | % MC | LL | PL | PI | Gravel<br>% | Sand<br>% | Silt<br>% | Clay<br>% | Fines<br>% |
|----------|----------|------|-------------|---|------|----|----|----|-------------|-----------|-----------|-----------|------------|
| •        | W-218-20 | S-17 | 75.0 - 75.2 | (GM) Dark grayish-brown, silty GRAVEL with sand | 6    |    |    |    | 38.1        | 37.3      |           |           | 24.6       |
|          | W-219-20 | S-1  | 2.5 - 4.0   | (SM) Light olive-brown, silty SAND              | 6    |    |    |    | 14.0        | 46.1      |           |           | 39.9       |
| <b>A</b> | W-219-20 | S-3  | 7.5 - 9.0   | (SM) Olive-brown, silty SAND                    | 8    |    |    |    | 6.2         | 51.7      |           |           | 42.1       |



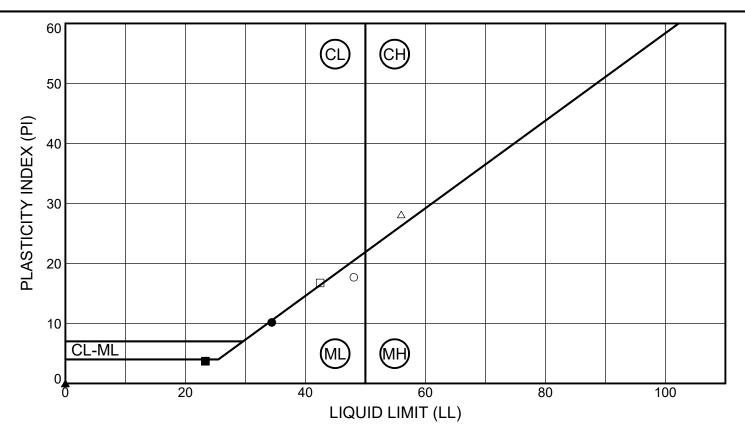
PARTICLE-SIZE ANALYSIS OF SOILS METHOD ASTM D6913



| SYMBOL   | SAMPI    | LE   | DEPTH (ft)  | CLASSIFICATION                                | % MC | LL | PL | PI | % Fines |
|----------|----------|------|-------------|---|------|----|----|----|---------|
| •        | W-201-20 | S-8  | 30.0 - 31.5 | (ML) Grayish-brown, SILT                      | 23   | 38 | 26 | 12 | 90.0    |
| ■        | W-203-20 | S-7  | 25.0 - 26.5 | (SM) Olive-brown, silty SAND with gravel      | 11   | 19 | 17 | 2  | 30.1    |
| <b>A</b> | W-207-20 |      |             | (CL) Olive-brown, sandy lean CLAY with gravel | 17   | 28 | 20 | 8  | 50.1    |
| 0        | W-208-20 | S-8B | 30.0 - 31.5 | (CL) Gray, lean CLAY with sand                | 30   | 45 | 21 | 24 | 78.2    |
|          | W-208-20 | S-9  | 35.0 - 36.5 | (SC-SM) Olive-brown, silty, clayey SAND       | 10   | 17 | 13 | 4  | 42.9    |
| Δ        | W-214-20 | S-1  | 2.5 - 4.0   | (SC) Olive-brown, clayey SAND                 | 10   | 39 | 17 | 22 | 47.3    |



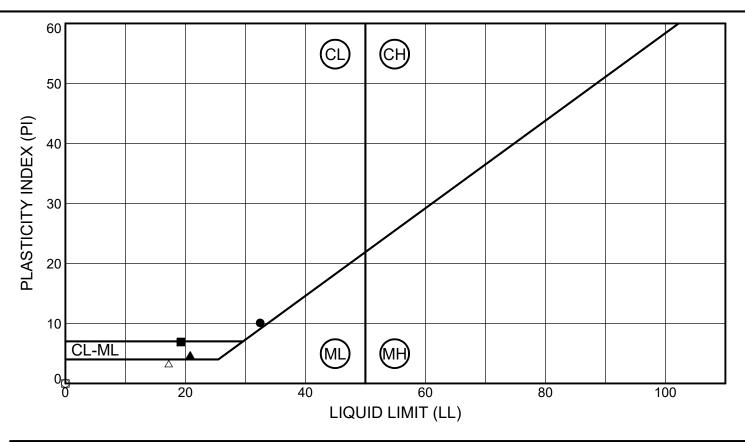
LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX OF SOILS METHOD ASTM D4318



| SYMBOL   | SAMPI    | LE   | DEPTH (ft)  | CLASSIFICATION                           | % MC | LL | PL | PI | % Fines |
|----------|----------|------|-------------|--|------|----|----|----|---------|
| •        | W-214-20 | S-4  | 10.0 - 11.5 | (GM) Olive-brown, silty GRAVEL with sand | 11   | 34 | 24 | 10 | 14.5    |
| ■        | W-214-20 | S-9  | 35.0 - 36.5 | (ML) Light olive-brown, sandy SILT       | 21   | 23 | 20 | 3  | 60.7    |
| <b>A</b> | W-215-20 |      |             | (ML) Light olive-brown, SILT with sand   | 19   | NP | NP | NP | 71.9    |
| 0        | W-217-20 | S-7  | 25.0 - 26.5 | (ML) Gray, SILT                          | 23   | 48 | 30 | 18 | 89.9    |
|          | W-217-20 | S-9  | 35.0 - 36.5 | (CL) Gray, lean CLAY                     | 24   | 42 | 26 | 16 | 92.0    |
| Δ        | W-217-20 | S-10 | 40.0 - 41.0 | (CH) Gray, fat CLAY with sand            | 15   | 56 | 28 | 28 | 72.5    |



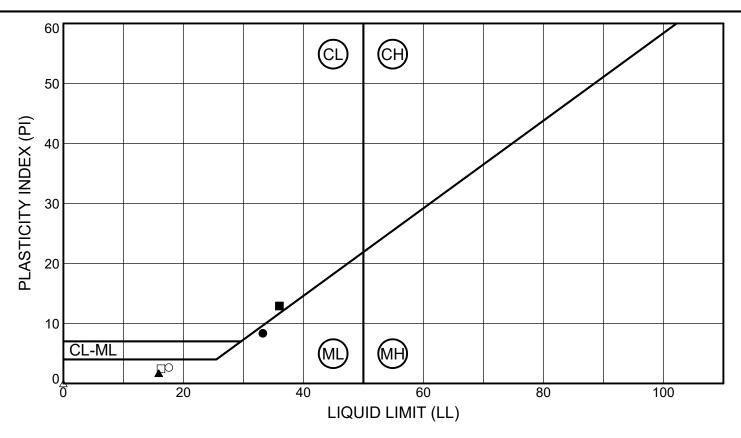
LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX OF SOILS METHOD ASTM D4318



| SYMBOL   | SAMPI    | _E                        | DEPTH (ft)  | CLASSIFICATION                                    | % MC | LL | PL | PI | % Fines |
|----------|----------|---------------------------|-------------|---|------|----|----|----|---------|
| •        | W-205-20 | S-5                       | 15.0 - 16.5 | (CL) Very dark gray, lean CLAY                    | 19   | 32 | 22 | 10 | 93.0    |
| <b> </b> | W-206-20 | S-2                       | 5.0 - 6.5   | (SC-SM) Dark gray, silty, clayey SAND with gravel | 11   | 19 | 12 | 7  | 48.8    |
| <b>A</b> | W-206-20 | W-206-20 S-4B 10.0 - 11.0 |             | (CL-ML) Gray, sandy silty CLAY                    | 12   | 21 | 16 | 5  | 59.6    |
| 0        | W-206-20 | S-7A                      | 25.0 - 26.5 | (SM) Dark grayish-brown, silty SAND               | 22   | NP | NP | NP | 36.8    |
|          | W-206-20 | S-8                       | 30.0 - 31.5 | (ML) Olive, SILT with sand                        | 24   | NP | NP | NP | 80.9    |
| Δ        | W-218-20 | S-6                       | 20.0 - 21.0 | (SM) Dark grayish-brown, silty SAND with gravel   | 10   | 17 | 14 | 3  | 45.3    |



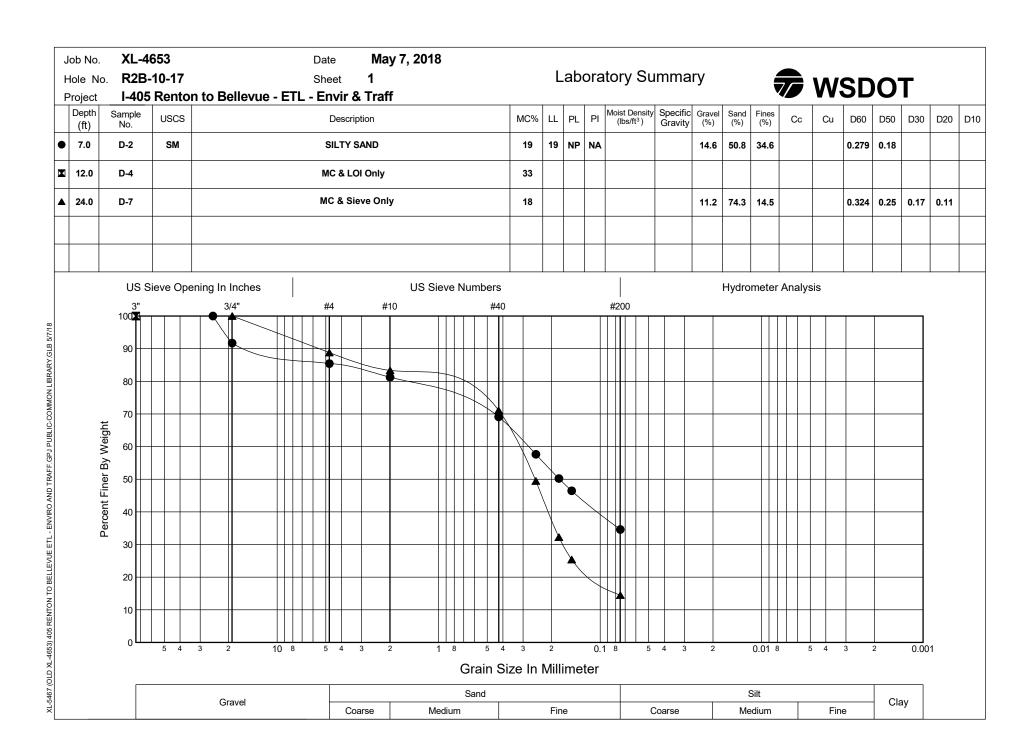
LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX OF SOILS METHOD ASTM D4318

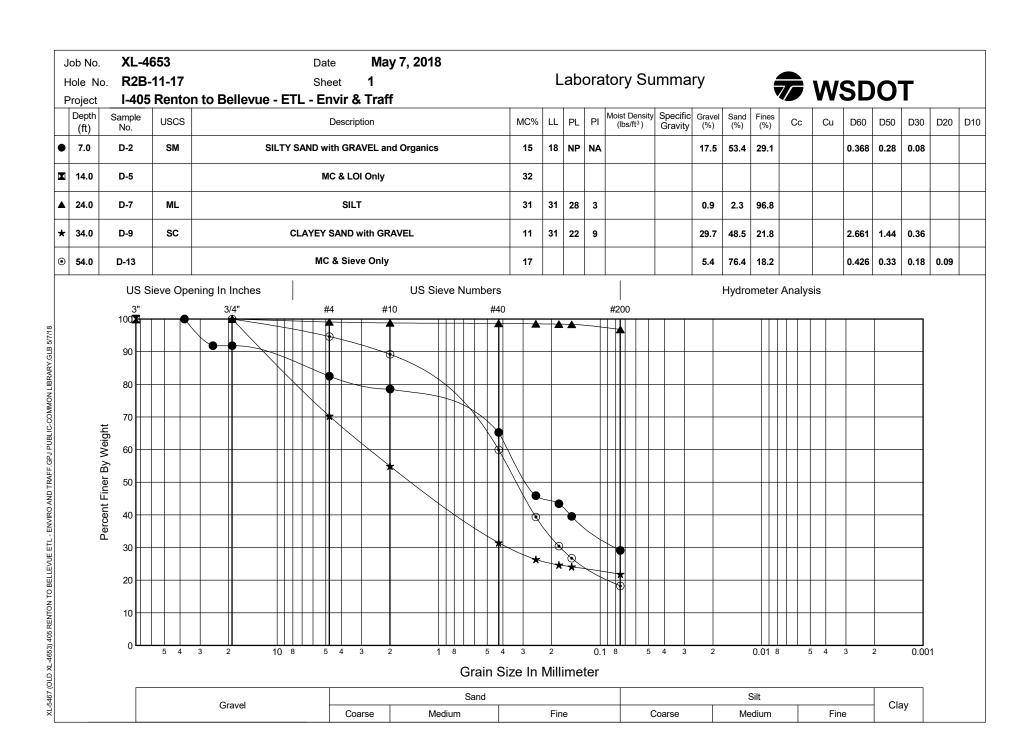


| SYMBOL   | SAMPI    | E    | DEPTH (ft)  | CLASSIFICATION                    | % MC | LL | PL | PI | % Fines |
|----------|----------|------|-------------|-----------------------------------|------|----|----|----|---------|
| •        | W-218-20 | S-11 | 45.0 - 46.0 | (ML) Olive-brown, SILT            | 22   | 33 | 25 | 8  | 98.1    |
| -        | W-218-20 | S-13 | 55.0 - 56.0 | (CL) Very dark gray, lean CLAY    | 25   | 36 | 23 | 13 | 95.0    |
| <b>A</b> | W-220-20 | S-3  | 7.5 - 9.0   | (SM) Dark olive-brown, silty SAND | 8    | 16 | 14 | 2  | 36.7    |
| 0        | W-222-20 | S-12 | 50.0 - 51.0 | (ML) Olive-brown, sandy SILT      | 15   | 18 | 15 | 3  | 61.1    |
|          | W-222-20 | S-13 | 55.0 - 55.5 | (SM) Dark gray, silty SAND        | 14   | 16 | 14 | 2  | 44.4    |
| Δ        | W-222-20 | S-17 | 75.0 - 76.0 | (ML) Dark gray, sandy SILT        | 21   | NP | NP | NP | 51.3    |



LIQUID LIMIT, PLASTIC LIMIT AND PLASTICITY INDEX OF SOILS METHOD ASTM D4318





# Washington State Department of Transportation State Materials Laboratory PO Box 47365 Olympia WA 98504 / 1655 S. 2nd Ave Tumwater WA 98512

#### Miscellaneous Report

**Work Order**: XL4653 **Sample ID**: 0000012011e

Section: I-405/Renton To Bellevue-Express Toll Lanes-Envir&Traff

State Route No: Lab Number: MC0170045

Project Engineer: Jason Qiu Bid Item No:

Org Code: 412335 Date Received: 5/25/2017

**Local Agency No:** 

Material: Soils

Contractor: Pit Number: R2B-10-17
Supplier Name: Date Sampled: 5/24/2017
Acceptance No: Date Received: 5/25/2017
Sampled Location: 12.0' to 13.5' Sampled By: Drill Crew

Make: IAS Sample No : D-4

Manufacturer: Lot Number:

Test Name Test Result Test Specifications

AASHTO T267 Determination of Organic Content in Soils by 7.23% AASHTO T267

Loss on Ignition

Result Code: Informational

**Remarks:** Boring: R2B-10-17 State Materials Engineer

Sample: D-4 Katharine Dafoe By:\_\_\_\_\_

Depth: 12.0' to 13.5'
Lab #: G-1408

Traditative Bales By: \_\_\_\_\_
Chemistry Laboratory Supervisor

Date: 5/30/2017 Phone: (360) 709-5537

Kurt R. Williams, P.E.

**Billing Code** 

T2D1 - 1

T2M6 - 1

# Washington State Department of Transportation State Materials Laboratory PO Box 47365 Olympia WA 98504 / 1655 S. 2nd Ave Tumwater WA 98512

#### Miscellaneous Report

Work Order: XL4653 Sample ID: 0000012013e

Section: I-405/Renton To Bellevue-Express Toll Lanes-Envir&Traff

State Route No: Lab Number: MC0170046

Project Engineer: Jason Qiu Bid Item No:

Org Code: 412335 Date Received: 5/25/2017

**Local Agency No:** 

Kurt R. Williams, P.E.

Material: Soils

Contractor: Pit Number: R2B-11-17
Supplier Name: Date Sampled: 5/24/2017
Acceptance No: Date Received: 5/25/2017
Sampled Location: 14.0' to 15.5' Sampled By: Drill Crew

Make: IAS Sample No: D-5

Manufacturer: Lot Number:

Test Name Test Result Test Specifications

AASHTO T267 Determination of Organic Content in Soils by 7.32% AASHTO T267

Loss on Ignition

Result Code: Informational

**Remarks:** Boring: R2B-11-17 State Materials Engineer

Sample: D-5
Depth: 14.0' to 15.5'
Lab #: G-1409

Katharine Dafoe By:\_\_\_\_\_
Chemistry Laboratory Supervisor

Report Revised to correct the Boring/Pit number. Date: 6/1/2017

Phone: (360) 709-5537

**Billing Code** 

T2D1 - 1

T2M6 - 1

### WASHINGTON STATE EPARTMENT OF TRANSPORTATION

MATERIALS ENGINEER
Materials Laboratory
P. O. Box 167, Olympia, WA 98504 (Mailing Address)
1655 So. 2nd Ave.
Tumwater, Washington 98504 (Shipping Address)

| Place | Seattle     |        |
|-------|-------------|--------|
|       | •           |        |
| Date  | February 25 | . 1985 |

Dear Sir:

DISTURBED

I have forwarded by today's Hand Carried ...... the following Foundation Samples.

Section Sunset Blvd. to Factoria Station 109'LT 6 377+44 & Offset Hole # Tube **Position** Lab No. Drive # Clas. Description Depth in Sampler P-1 -1.01 5M 1/20= to 5991-1 -3.01 12.3 P-2 -3.01 SM H20= to - 2 12.8 -5.01 P-3 -5.01 1/20= SIA to 16.2 -7.01 P-4 -7.51 HZO= 5M to -9.51 18.7 P-5 -10.01 5M 1/20= to 15.7 -12.0' P-6 -12.5' H20= 5M to 43,1 -14.51 P-7 -15.01 H20 = to 1011 -16.51 50 P-8 -17.51 H20= to 24.3 -1819" P-9 -20.01 LK5881-8 to -201311

1 copy with samples 1 copy to addressee

Yours very truly,

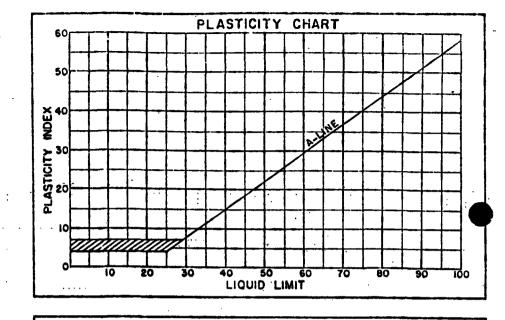
KEW (RMM)

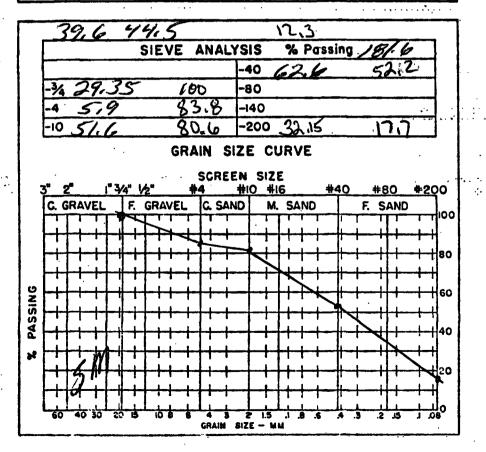
## WASHINGTON STATE EPARTMENT OF TRANSPORTATION

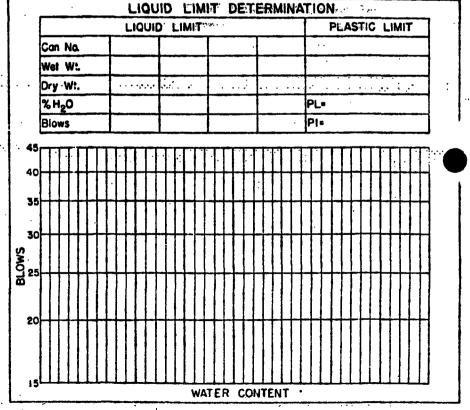
| MATERIALS<br>Materials Labo<br>P. O. Box 167 | огаtory        | •            | (Mailing Addı                         | ess)         |                                       | Plac                                    | e <u>Seatt</u>                        | le .                                  | · · ·      |
|--|----------------|--------------|---------------------------------------|--------------|---------------------------------------|---|---------------------------------------|---------------------------------------|------------|
| 1655 So. 2nd A                               | Ave.           |              |                                       |              |                                       | Date                                    | Febru                                 | ary 25, 198                           | 5          |
| Tumwater, Wa  Dear Sir:                      | isnington 9    | 6304 (Snipp  | ing Address)                          |              |                                       |   |                                       |                                       |            |
|  | - <b>6</b>     | 4 h a 44.    | Hand Cann                             | d od         | DISTURBE                              |   |                                       |                                       | •          |
|  | ,              | a by todays  |                                       |              | the following F                       |   |                                       |                                       | ,          |
|  | or<br>C-2637   | 7            | Section<br>SR No                      | nSui<br>o405 | nset Blvd. to<br>Sub-Section          | Factoria                                | I/C                                   |                                       |            |
| Station &<br>Offset                          | <u>377+J</u> J | 109' L       | T E                                   |              | Н                                     | ole # 1                                 | <del></del> .                         | · .                                   |            |
| E Lab No.                                    | Drive #        | Depth        | Tube<br>Position<br>in Sampler        | Clas.        |                                       |   | Description                           |                                       |            |
| 5001-10                                      | P-10           | -25.01<br>to | H20=<br>9.9                           | SP           |                                       |   |                                       |                                       |            |
|  |                | -2513"       |                                       | ļ <u>.</u>   |                                       |   |                                       |                                       | ··         |
|  |                |              |                                       |              |                                       |   |                                       |                                       |            |
|  |                |              |                                       |              |                                       |   |                                       | ,                                     |            |
|  | ,              |              |                                       |              |                                       |   |                                       |                                       |            |
|  |                |              | :                                     |              |                                       |   |                                       |                                       |            |
|  |                |              |                                       |              | ,                                     |   |                                       |                                       | •          |
|  |                |              |                                       |              |                                       |   | •                                     |                                       |            |
|  |                |              |                                       |              | <u>*-</u> -                           |   |                                       |                                       |            |
|  |                |              |                                       |              | :                                     | :                                       |                                       |                                       |            |
|  |                |              |                                       |              |                                       |   |                                       | · · · · · · · · · · · · · · · · · · · |            |
| :<br>-                                       |                |              |                                       |              |                                       |   |                                       |                                       |            |
|  |                |              |                                       |              |                                       |   | •                                     | •                                     |            |
|  |                |              | • .                                   |              |                                       |   |                                       |                                       |            |
|  |                |              | · · · · · · · · · · · · · · · · · · · |              |                                       | • |                                       |                                       |            |
|  |                |              |                                       |              |                                       | :                                       |                                       | -                                     |            |
|  | :              |              |                                       |              |                                       | · · · · · · · · · · · · · · · · · · ·   | · · · · · · · · · · · · · · · · · · · |                                       |            |
|  |                |              |                                       |              |                                       |   |                                       |                                       |            |
|  |                |              |                                       | <del></del>  | · · · · · · · · · · · · · · · · · · · |   |                                       |                                       |            |
| l copy with sar<br>I copy to addre           |                |              |                                       |              |                                       | Yours very tr                           | uly,<br>KEW (                         | omm I                                 |            |
|  |                | 1            |                                       |              |                                       |   | ,                                     |                                       | Inspector. |

DOT FORM 351-002 REVISED 2/80

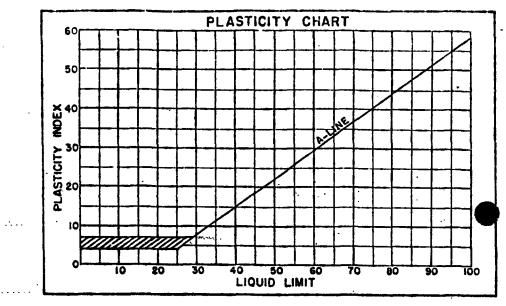
| · ···· · · · · · · · · · · · · · · · | B NO.C2637<br>Erator <i>&amp;C</i> | HOLE      | NO. /          |
|--------------------------------------|------------------------------------|-----------|----------------|
| SOIL FIELD                           |                                    | rion      |                |
| TEST                                 | SAND                               | SILT      | CLAY           |
| VISUAL                               | -                                  | ~         |                |
| DRIED CAST                           |                                    |           |                |
| DILATANCY                            |                                    |           |                |
| BITE                                 |                                    |           |                |
| TOUGHNESS                            |                                    |           |                |
| DESCRIPTION: Bu.,                    | moid, F                            | -Gravelly | Sir            |
| C'-                                  | moist, F<br>m-FSA                  | 200 7     | <del>,</del> , |

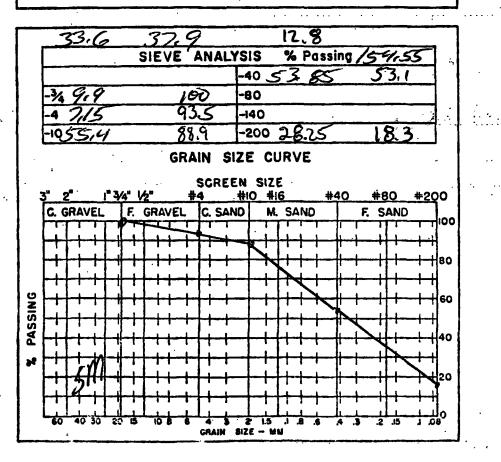


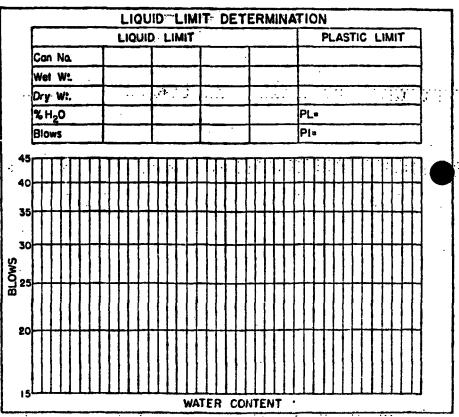




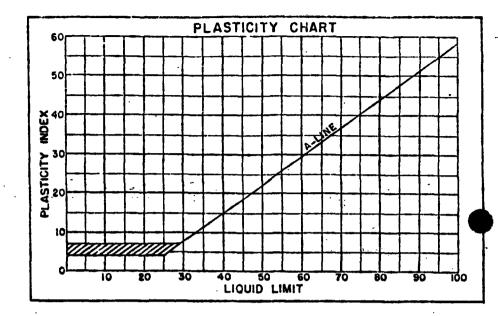
| DATE4-17-85 OF SOIL FIELD | PERATOR STILL    | FION    |          |
|---------------------------|------------------|---------|----------|
| TEST .                    | SAND             | SILT    | GLAY     |
| VISUAL                    |                  | -       |          |
| DRIED CAST                |                  |         |          |
| DILATANCY                 |                  |         |          |
| BITE                      |                  |         | <u> </u> |
| TOUGHNESS                 |                  |         |          |
| DESCRIPTION: Bu.          | mist, F<br>M-F5K | Gravele | 1.307    |

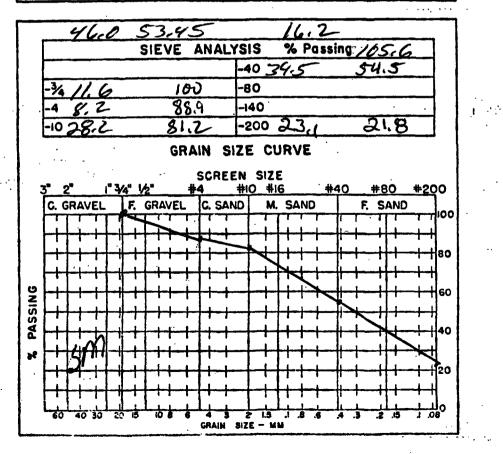


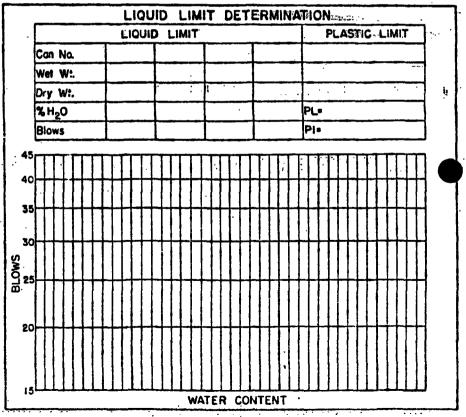




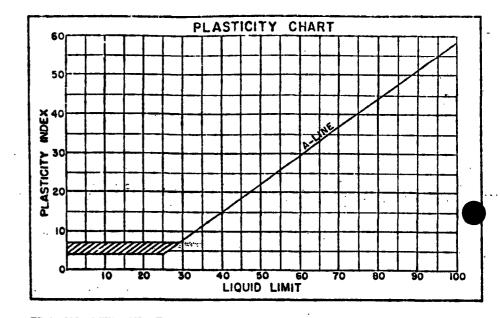
| SAMPLE NO. SER-3 JO |             | _        | NO. / |
|---------------------|-------------|----------|-------|
| DATE H1785 OP       | ERATOR SE   | <u> </u> |       |
| SOIL FIELD          | IDENTIFICAT | TION     |       |
| TEST                | SAND        | SILT     | CLAY  |
| VISUAL              | -           |          |       |
| DRIED CAST          |             |          |       |
| DILATANCY           |             |          |       |
| BITE                |             | ,        | · I   |
| TOUGHNESS           |             |          |       |
| DESCRIPTION: Bu     | moist,      | =61avell | VSUT  |
| $C^{\perp}$         | M-F3        | Ami      | //    |
| <u> </u>            | M-P3        | HMO      |       |

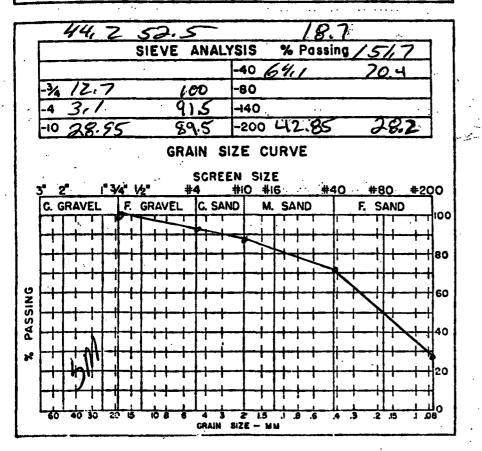


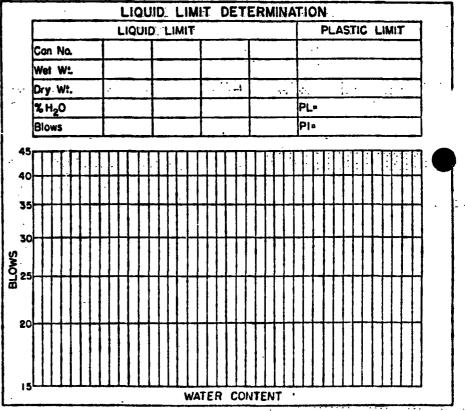




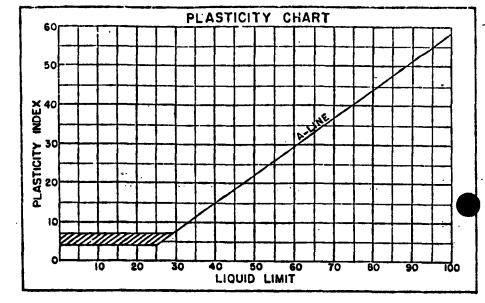
| SAMPLE NO. SEELY JO<br>DATE 4-17-85 OF | ERATOR            | >       | ,        |
|--|-------------------|---------|----------|
| SOIL FIELD                             | IDENTIFICAT       | rion    |          |
| TEST .                                 | SAND              | SILT    | GLAY     |
| VISUAL                                 |                   |         |          |
| DRIED CAST                             |                   |         |          |
| DILATANCY                              |                   |         |          |
| BITE                                   |                   |         |          |
| TOUGHNESS                              |                   |         | <u> </u> |
| DESCRIPTION: Bm.                       | moist F<br>m- F-5 | Gravell | 1. V3L   |
|  | m- 155            | Anni    | 7        |

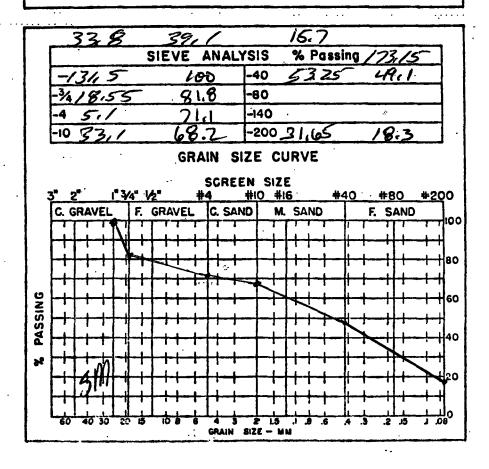


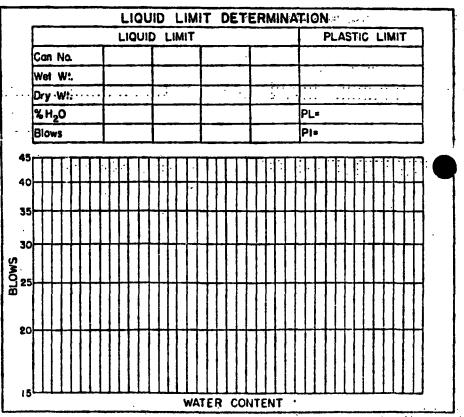




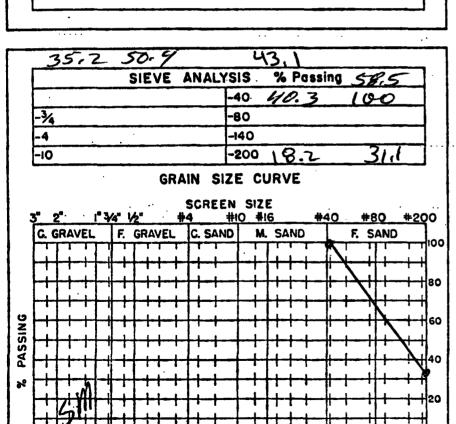
| SAMPLE NO. 586/5 JO<br>DATE4-/7-85 OP<br>SOIL FIELD | ERATOR | >            |       |
|---|--------|--------------|-------|
| TEST  | SAND   | SILT         | GLAY  |
| VISUAL  |        | -            |       |
| DRIED CAST  |        |              |       |
| DILATANCY   |        |              |       |
| BITE  |        |              |       |
| TOUGHNESS   |        |              |       |
| DESCRIPTION: BM                                     | moist, | B 503        | 7,    |
| C-F-C   | melly  | <b>智念</b> C~ | m-F5/ |



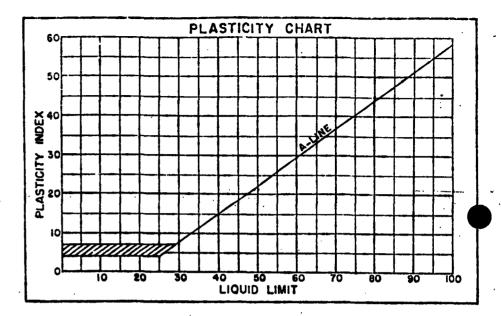


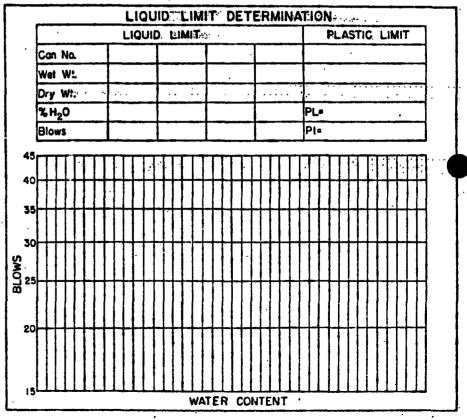


| DATE 4-17-85 OP    |        |        |      |
|--------------------|--------|--------|------|
| TEST               | SAND   | SILT   | CLAY |
| VISUAL             |        |        |      |
| DRIED CAST         |        |        |      |
| DILATANCY          |        |        |      |
| BITE               |        |        |      |
| TOUGHNESS          |        |        |      |
| DESCRIPTION: Rue 4 | vet VS | LTY. F | SANO |

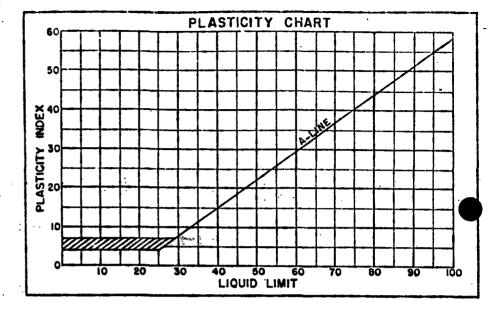


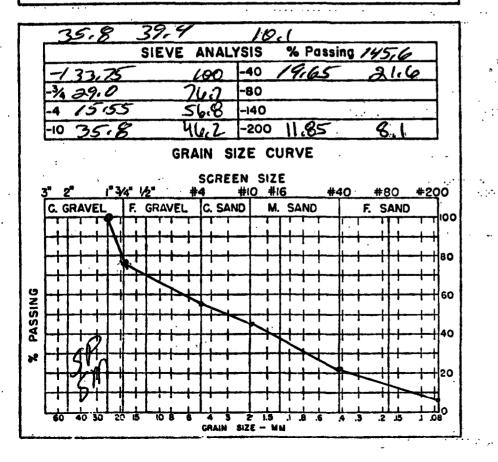
GRAIN SIZE - MM

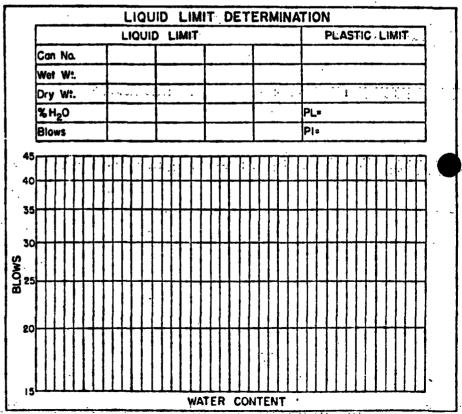




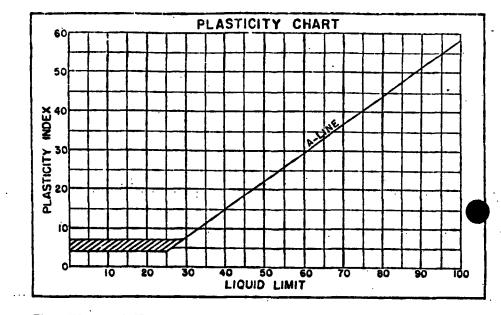
| DATE 4-17-85 OP |        | rion |        |
|-----------------|--------|------|--------|
| TEST            | SAND   | SILT | CLAY   |
| VISUAL .        |        | سر   |        |
| DRIED CAST      |        |      |        |
| DILATANCY       |        |      |        |
| BITE            |        |      |        |
| TOUGHNESS       |        |      |        |
| DESCRIPTION: Bu | moist, | SLTY | C-FGIA |

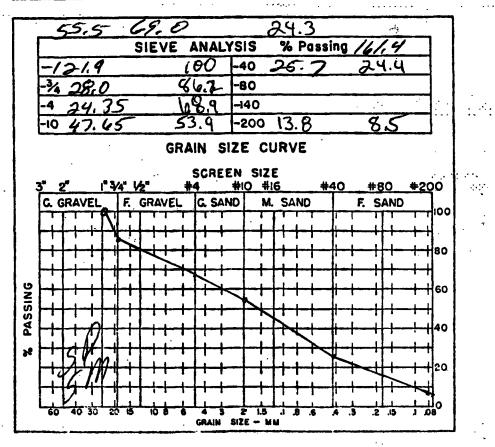


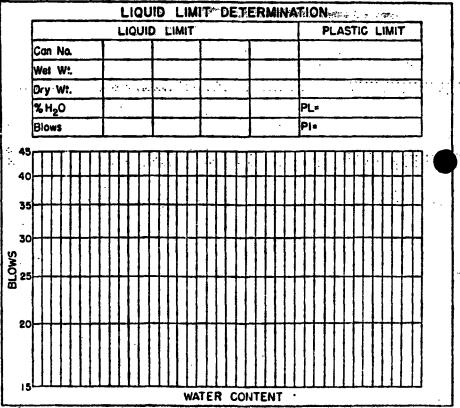




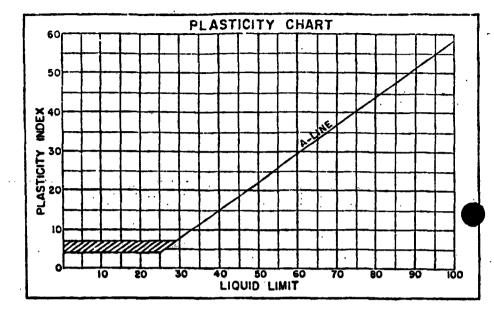
| SOIL FIELD       | ERATOR A |      | <del></del> |
|------------------|----------|------|-------------|
| TEST             | SAND     | SILT | CLAY        |
| VISUAL           | U        | ~    |             |
| DRIED CAST       |          |      |             |
| DILATANCY        |          |      |             |
| BITE             |          | • -  |             |
| TOUGHNESS        |          |      |             |
| DESCRIPTION: Ben | mist     | 547  | C-Flore     |

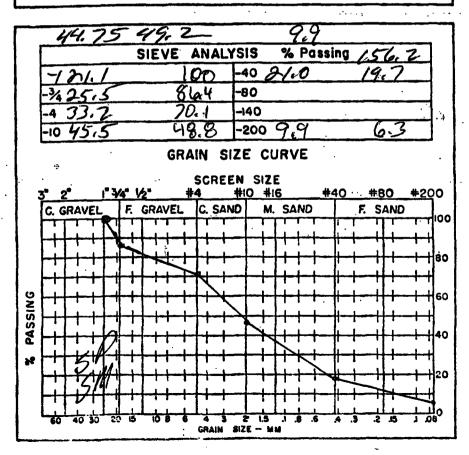


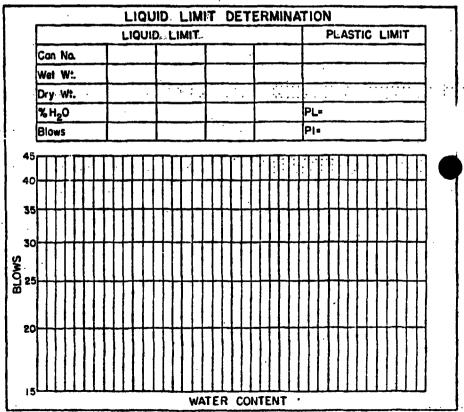




| SAMPLE NOSSOUD JO<br>DATE 4-17-85 OF<br>SOIL FIELD | PERATOR A |        |         |
|--|-----------|--------|---------|
| TEST   | SAND      | SILT   | CLAY    |
| VISUAL   |           |        |         |
| DRIED CAST   |           |        |         |
| DILATANCY  |           |        |         |
| BITE   |           |        |         |
| TOUGHNESS  |           |        |         |
| DESCRIPTION: Br.                                   | Dun SLT   | Y.C-F. | 6 ravel |
| C-m-F  | -dann     | 6      |         |







#### **WASHINGTON STATE** EPÄRTMENT OF TRANSPORTA

**MATERIALS ENGINEER** Materials Laboratory P. O. Box 167, Olympia, WA 98504 (Mailing Address) 1655 So. 2nd Ave.

Tumwater, Washington 98504 (Shipping Address)

Place Seattle

Date February 25,1985

Dear Sir:

DISTURBED

 $y_{ij}$ 

I have forwarded by today's Hand Carried the following Foundation Samples.

Contract or Job No. ..... Section Sunset Blvd. to Factoria I/C

SR No. 405 Sub-Section

| Station 376+35 115 LT & Offset |              |                        |                                |       | Hole #      |  |  |
|--------------------------------|--------------|------------------------|--------------------------------|-------|-------------|--|--|
| E Lab No.                      | Drive #      | Depth                  | Tube<br>Position<br>in Sampler | Clas. | Description |  |  |
| 5990-1                         | P <b>-1</b>  | -1.0'<br>to<br>-3.0'   | HZ0=                           | SM    |             |  |  |
| - 2                            | P-2          | -3.01<br>to<br>-5.01   | H20=<br>9.7                    | SM    |             |  |  |
| -3                             | P=3          | -5.0'<br>to<br>-7.0'   | HZO=<br>12.4                   | 5M    |             |  |  |
| -4                             | P-4          | -7.5'<br>to<br>-9.5'   | HZO=<br>11.7                   | 5M    |             |  |  |
| -5                             | P <b>-</b> 5 | -10.0'<br>to<br>-12.0' | H20=<br>11.1                   | 5111  |             |  |  |
| -6                             | P <b>-7</b>  | -15.0'<br>to<br>-17.0' | H20=<br>19.3                   | 5/11  |             |  |  |
| -7                             | P-8          | -17.5'<br>to<br>-19.5' | HZO=<br>34.3                   | sm    |             |  |  |
| -8                             | P <b>-9</b>  | -20.01<br>to<br>-22.01 | H20=                           | SM    |             |  |  |
| -9                             | P-10         | -22.51<br>to<br>-24.51 | H20=<br>1714                   | sm    |             |  |  |

I copy with samples

I copy to addressee

Yours very truly,

Inspector.



## WASHINGTON STATE EPARTMENT OF TRANSPORTATION

MATERIALS ENGINEER
Materials Laboratory
P. O. Box 167, Olympia, WA 98504 (Mailing Address)
1655 So. 2nd Ave.
Tumwater, Washington 98504 (Shipping Address)

376+35 115'LT 6

Place Seattle

Date February 25, 1985

Dear Sir:

Station

I have forwarded by today's Hand Carried the following Foundation Samples.

Contract or Section Sunset Blvd. to Factoria I/C

Job No. C-2637 SR No. 405 Sub-Section

& Offset Hole # E Lab No. Tube Position Drive # Depth Description Clas. in Sampler -25.01 P-11 911 HRO= to 59*90-*10 26.2 -27.01 P-12 -27.51 HOI ML to 28.8 -30.01 P-13 -30.01 ML HZO= to -12 29.0 -32.01 P-14 2.51 HZO= 5111 -13 to 27.3 -34.51 P-15 -35.01 Mu= 5101 to 21.2 -37.01 SPM P-16 -37.51 H20 to 10.6 -39.51

I copy with samples I copy to addressee

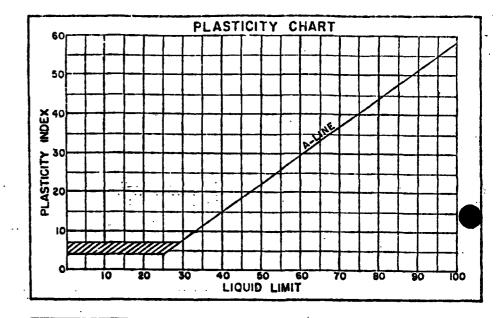
Yours very truly,

KEW (RMM)

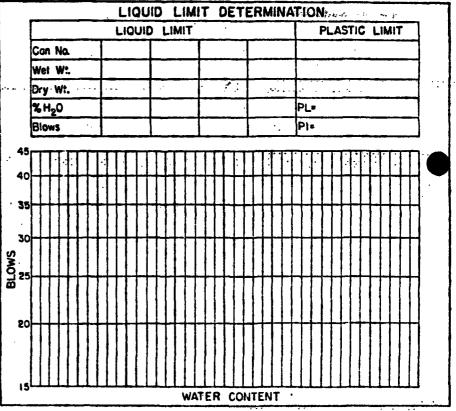
Inspector.



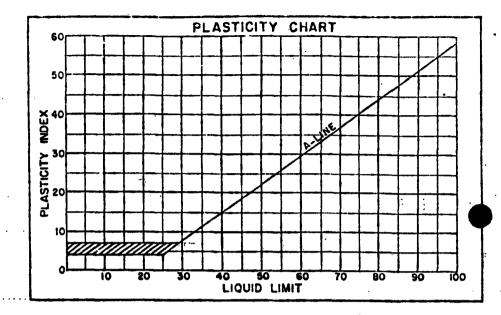
| 37770            | B NO.2437<br>PERATOR SO | HOLE   | NO. 2   |
|------------------|-------------------------|--------|---------|
| SOIL FIELD       | IDENTIFICAT             | ION    |         |
| TEST             | SAND                    | SILT   | CLAY    |
| VISUAL           | · ·                     |        |         |
| DRIED CAST       |                         |        |         |
| DILATANCY        |                         |        |         |
| BITE             |                         |        | :       |
| TOUGHNESS        |                         |        |         |
| DESCRIPTION: Bm. | noist &                 | BC74.0 | C-F610W |
| c-m              | -E 5A                   | not    |         |

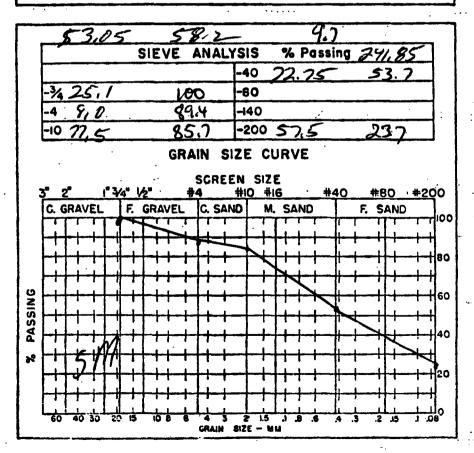


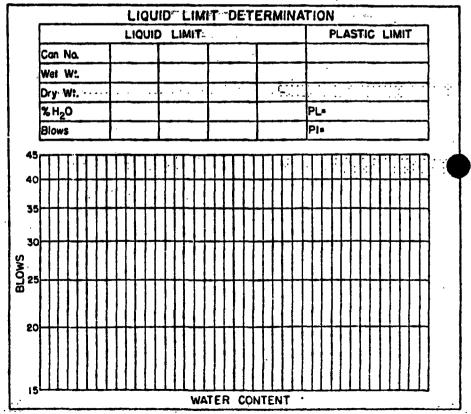
| · ·  |  |   |   |
|--|--|---|---|
| 39,15 45   |  | 16.7  |   |
| SIE  | E ANALYS   |   | ng 23417  |
| 1/8.0  |  | 0 66.35   | 43.7  |
| -3/4 35,75   | 92,4 -8  |   |   |
| -4 17,05   | 77,2 -1  |   |   |
| -10 Cel.55   | 69.9 -2  | 00 <u>36.</u> 0                                   | 15.4  |
|  | GRAIN SIZE                                       | CURVE   |   |
|  | SCREEN   | SIZE  | •   |
| 3" 2" 1" 3/4" 1/2"                                 |  |   | 0 #80 #200  |
| C. GRAVEL F. GRAV                                  | VEL C. SAND                                      | M. SAND   | F. SAND   |
|  | <del>╽╸</del> ╏ <del>╏</del> ╏╸┡╺╌┤              | <del>-                                     </del> | <del>                                     </del>  |
| <del></del>  |  | <del></del>                                       | <del> - -  </del> 80                              |
| <del>┠┼╏╏╍╂╊╣╏╇</del> ╸                            |  | <del>_                                     </del> | <del>                                     </del>  |
| SNS  | <del>┞┈╽</del> ┤┼┼┼╌┤                            |   | <del> - -  -    </del> 60                         |
| \$\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\\            | <del></del>                                      |   | <del> </del>                                      |
| A I I I I I I I I I I I I I I I I I I I            | <del>╎╸┪╸</del> ╏╶╂╸╸┪                           | <del></del>                                       | 1 1 1 40  |
| » <del>                                     </del> | <del>                                     </del> | <del>-                                     </del> | <del>                                      </del> |
| <del>                                      </del>  | <del>╿╌╏</del> ╏                                 | <del>-       + + -  </del>                        | 1-1-1-1-20  |
| <del>┡┤┧┤╌╎</del> ┪ <del>╏</del> ┼┿                | <del>╏╸┇┋</del> ╅╼╁╼┤                            | <del>-                                     </del> | <del>    - </del>                                 |
| 60 40 30 20 15 10                                  | 6 4 3 2  |   | 90. 1 21 5. 8.                                    |
|  | GRAIN SIZI                                       | E - WN  |   |



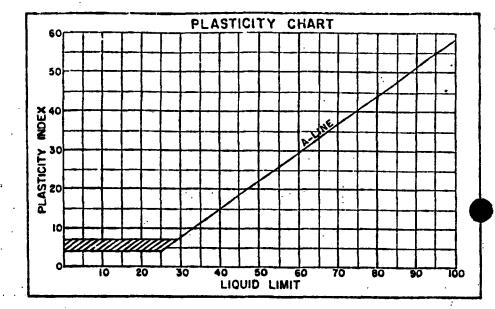
| DATE 4-17-85 OP<br>SOIL FIELD |         |        |      |
|-------------------------------|---------|--------|------|
| TEST .                        | SAND    | SILT   | CLAY |
| VISUAL                        | v       |        |      |
| DRIED CAST                    |         |        |      |
| DILATANCY                     |         |        |      |
| BITE                          |         |        |      |
| TOUGHNESS                     |         |        |      |
| DESCRIPTION: Bn,              | Duy, FG | welly, | USLT |

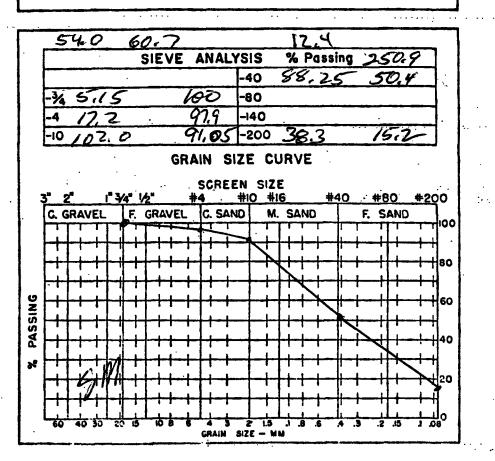


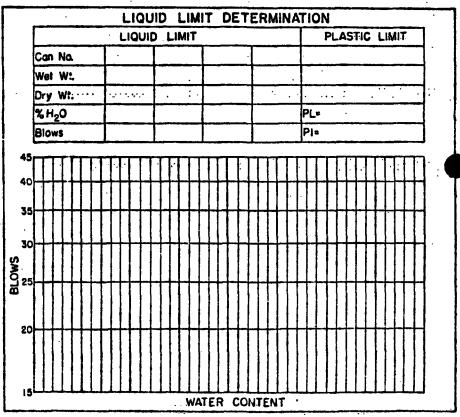




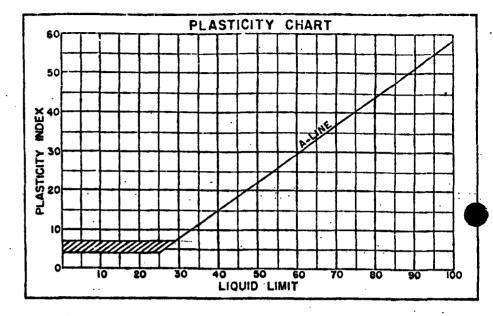
| DATE 4-17-85 OP<br>SOIL FIELD |         | ION     |         |
|-------------------------------|---------|---------|---------|
| TEST .                        | SAND    | SILT    | CLAY    |
| VISUAL                        | V       | 6       |         |
| DRIED CAST                    |         |         |         |
| DILATANCY                     |         |         |         |
| BITE                          |         |         |         |
| TOUGHNESS                     |         |         |         |
| DESCRIPTION: Br.              | mist, F | -6 mill | 2. Sitt |

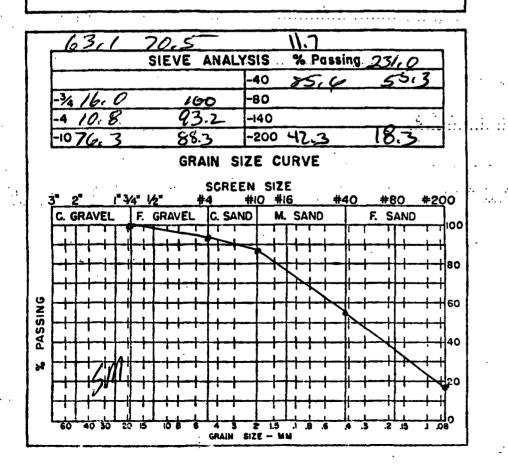


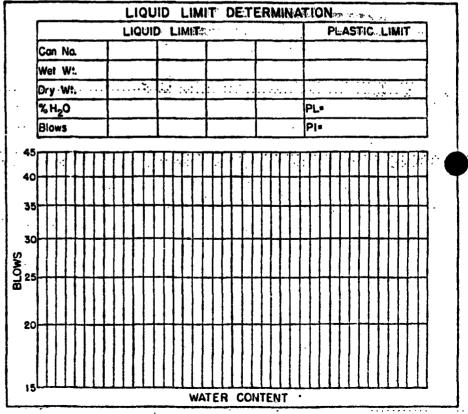




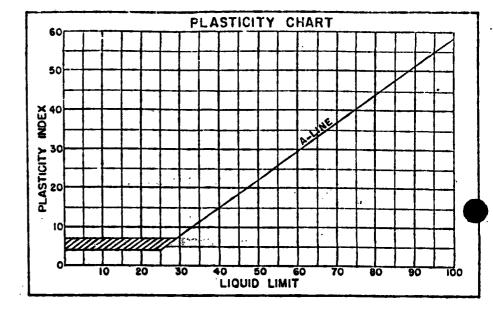
| SAMPLE NO. 5886-4 JO<br>DATE 4-17-85 OP<br>SOIL FIELD | ERATOR AL | <u> </u> | <del></del> |
|---|-----------|----------|-------------|
| TEST  | SAND      | SILT     | CLAY        |
| VISUAL  |           |          |             |
| DRIED CAST  |           |          |             |
| DILATANCY   |           |          |             |
| BITE  | -         | ·        | •           |
| TOUGHNESS   |           |          |             |
| DESCRIPTION: Bry,                                     | moid F    | Growely  | SLTY        |

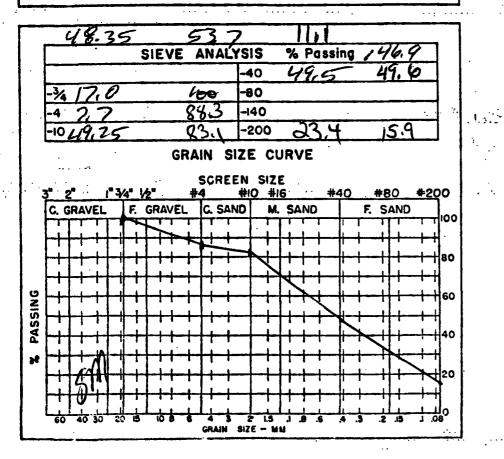


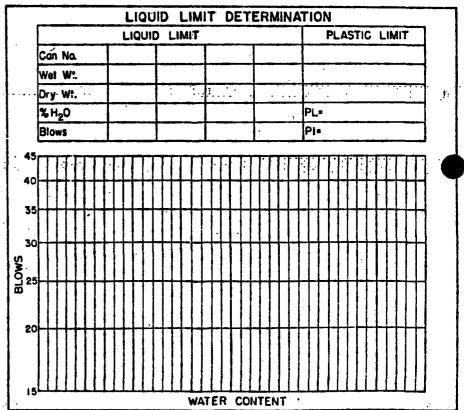




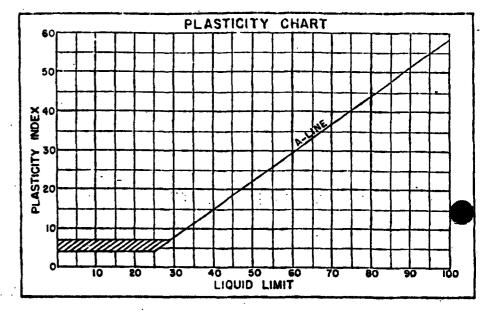
|                | PERATOR SOLUTION TO THE PERATO |          |        |
|----------------|--|----------|--------|
| TEST           | SAND   | SILT     | CLAY   |
| VISUAL         |  |          |        |
| DRIED CAST     |  |          |        |
| DILATANCY      |  |          |        |
| BITE           |  | 7        | Ĭ      |
| TOUGHNESS      |  |          |        |
| DESCRIPTION: 3 | 4, Mois  | \$ . F 6 | ravely |

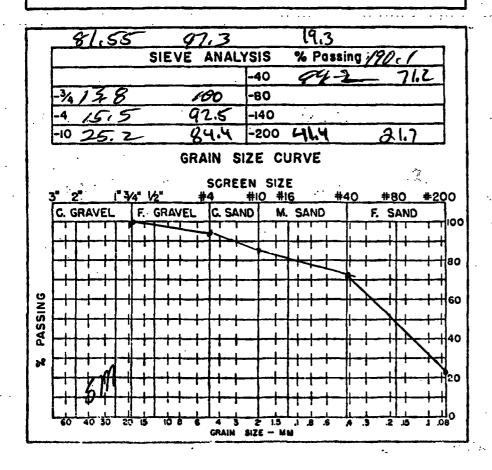


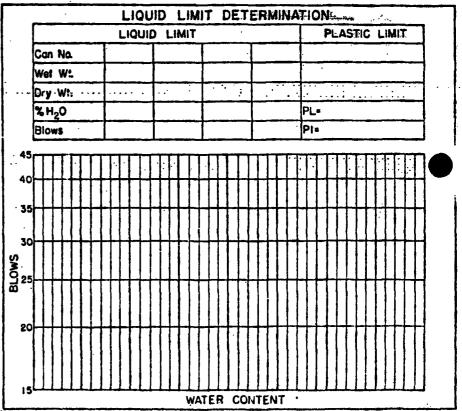




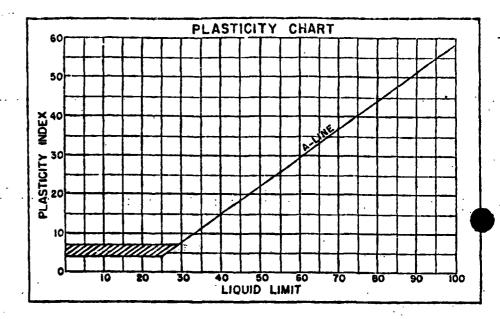
|                  | ERATOR      | )      | <del></del> |
|------------------|-------------|--------|-------------|
| SOIL FIELD       | IDENTIFICAT | TION   |             |
| TEST             | SAND        | SILT   | CLAY        |
| VISUAL           | <u> </u>    | -      |             |
| DRIED CAST       |             |        |             |
| DILATANCY        |             |        |             |
| BITE             |             |        | 1           |
| TOUGHNESS        |             |        |             |
| DESCRIPTION: Bu. | moust F     | Grovel | h           |
| VSB              | M C-W       | 1-1-6  | NO.         |

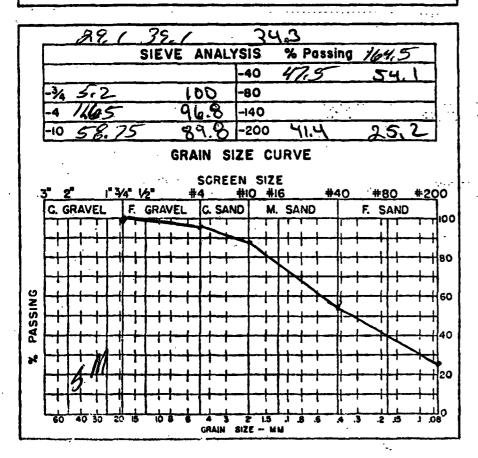


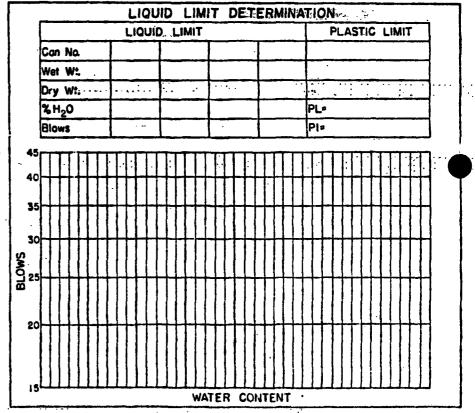




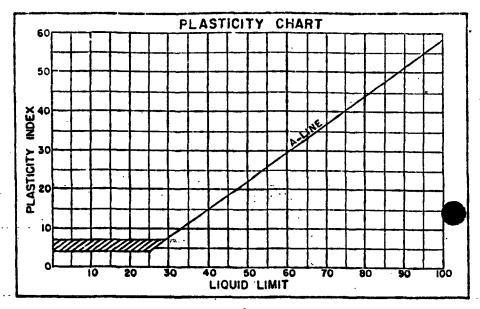
| SAMPLE NO. 5880-7 JOE | _          |         | NO. Z    |
|-----------------------|------------|---------|----------|
| DATE 4-17-85 OPI      | ERATOR     | ,<br>   |          |
| SOIL FIELD            | DENTIFICAT | ION     |          |
| TEST                  | SAND       | SILT    | CLAY     |
| VISUAL                |            |         |          |
| DRIED CAST            |            |         |          |
| DILATANCY             |            |         |          |
| BITE                  | •          |         |          |
| TOUGHNESS             |            |         |          |
| DESCRIPTION: Bx       | . Low.     | F6raull | u VSU    |
|                       | 102 = E    | SAMA    | <b>₹</b> |

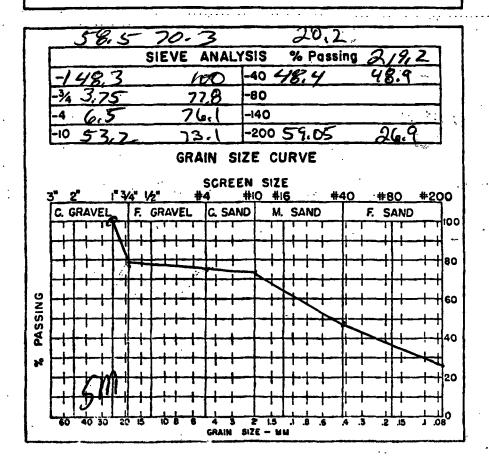


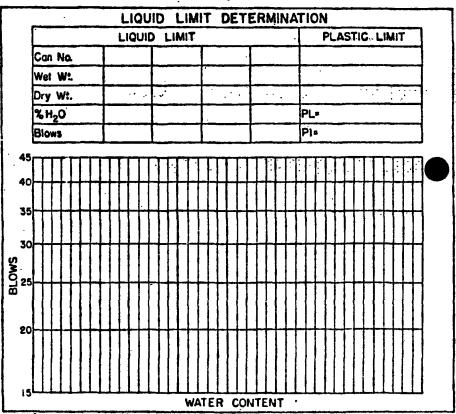




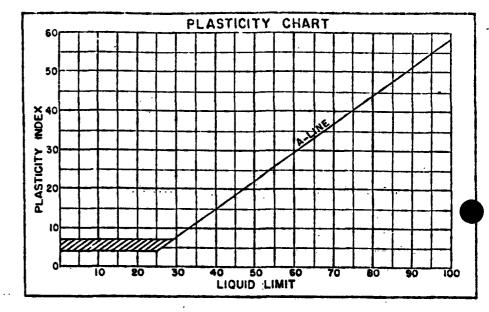
| DATE 4-16-85 OF SOIL FIELD |        |      | <del></del> |
|----------------------------|--------|------|-------------|
| TEST .                     | SAND   | SILT | CLAY        |
| VISUAL                     | V      | V    |             |
| DRIED CAST                 |        |      | 1           |
| DILATANCY                  |        |      |             |
| BITE                       |        |      |             |
| TOUGHNESS                  |        |      |             |
| DESCRIPTION: Bm.           | moist. | SLTY |             |

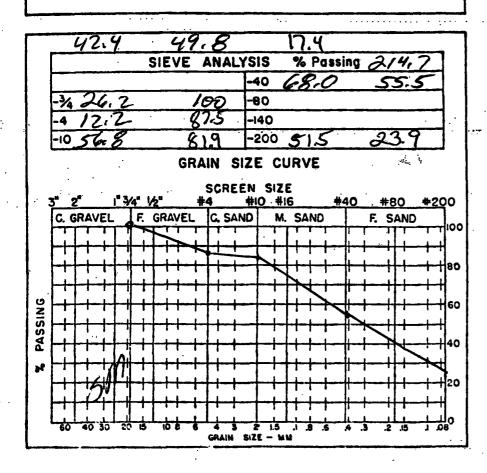


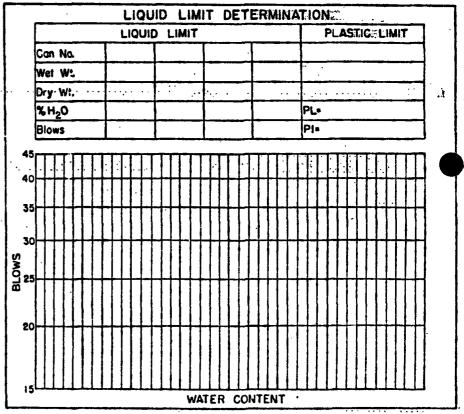




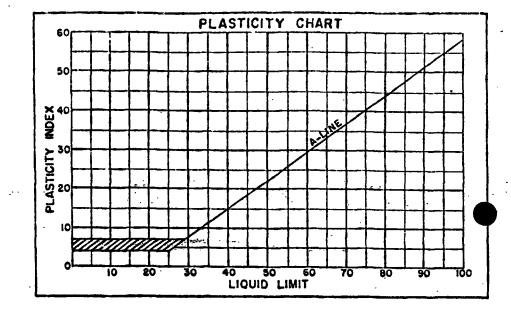
| SAMPLE NO.5880-9 |       |          | HOLE     | NO. 2 |
|------------------|-------|----------|----------|-------|
|                  |       | TOR 10   |          |       |
| SOIL FIEL        | D IDE | NTIFICAT | ION      |       |
| TEST             |       | SAND     | SILT     | CLAY  |
| VISUAL           |       |          | -        |       |
| DRIED CAST       |       |          |          |       |
| DILATANCY        |       |          |          |       |
| BITE             |       |          |          |       |
| TOUGHNESS        |       |          |          |       |
| DESCRIPTION: Bu  | mo    | Ct. F    | bravelly | VSLTY |
| (-               | m-    | -1551    | 911/51   |       |

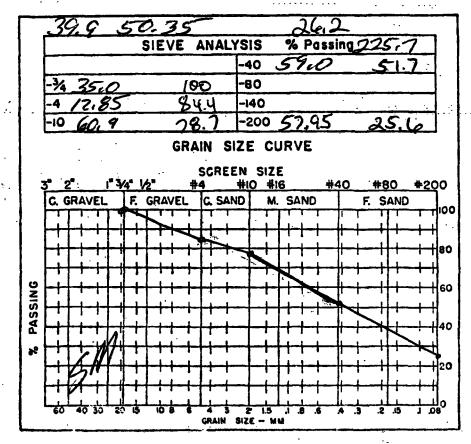


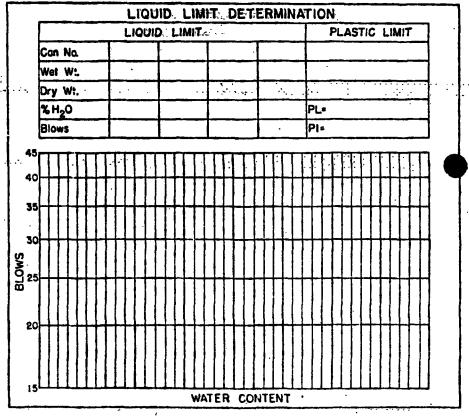




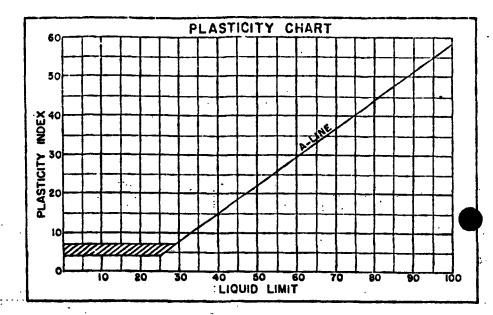
| SAMPLE NO.SESOYO JO      | ERATOR           |        |               |
|--------------------------|------------------|--------|---------------|
| DATE4-1785 OF SOIL FIELD |                  |        | <del></del> - |
| TEST                     | SAND             | SILT   | CLAY          |
| VISUAL                   |                  |        |               |
| DRIED CAST               |                  |        |               |
| DILATANCY                |                  |        |               |
| BITE                     |                  |        |               |
| TOUGHNESS                |                  |        |               |
| DESCRIPTION: Bu.         | mist, F<br>M-FSH | Gravel | 4. USC        |
| Q-r                      | n-FSH            | mo     | 7             |

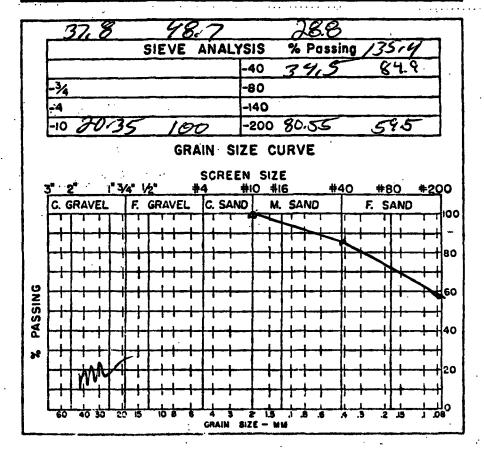


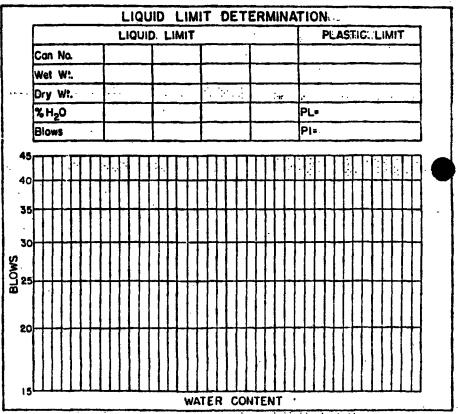




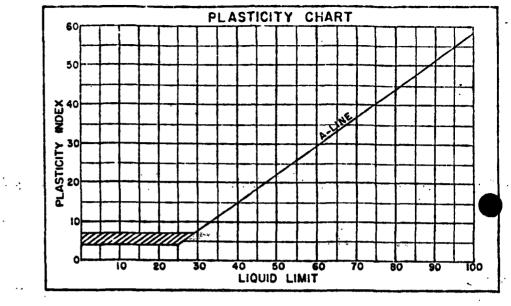
| SAMPLE NO. SOSO-11 JO<br>DATE 4-17-85 OP<br>SOIL FIELD | IDENTIFICAT | TION  |        |
|--|-------------|-------|--------|
| TEST   | SAND        | SILT  | CLAY   |
| VISUAL   |             |       |        |
| DRIED CAST   |             |       |        |
| DILATANCY  |             |       |        |
| BITE   |             |       | ] -    |
| TOUGHNESS  |             |       |        |
| DESCRIPTION: BM.                                       | noist, M    | -FSAI | MDY SL |

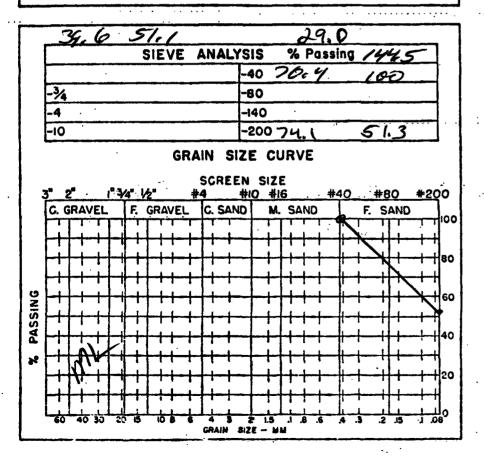


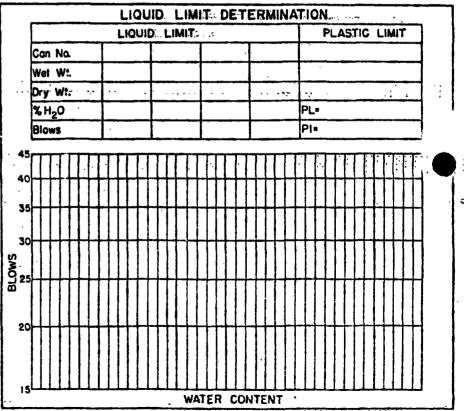




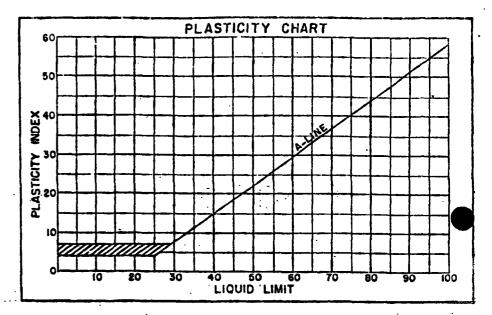
| DATE 1-17-85 OF |          |       |      |
|-----------------|----------|-------|------|
| TEST            | SAND     | SILT  | CLAY |
| VISUAL          |          |       |      |
| DRIED CAST      |          |       |      |
| DILATANCY       |          |       |      |
| BITE            |          |       |      |
| TOUGHNESS       |          |       |      |
| DESCRIPTION: BM | moist, 7 | SANDY | SLT  |

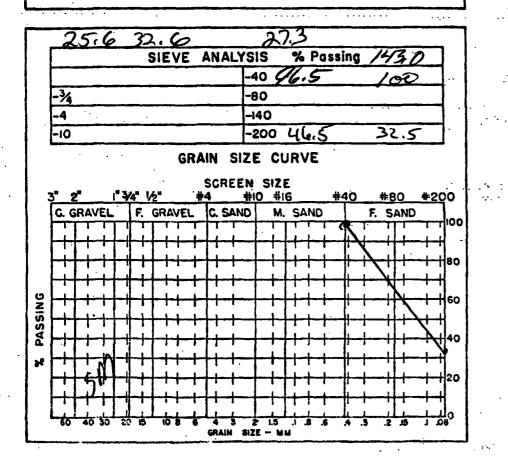


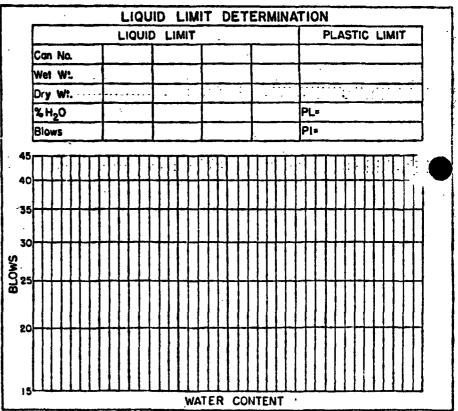




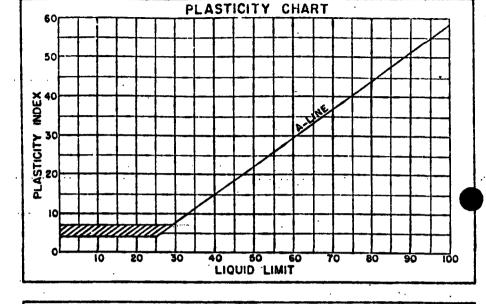
| DATE4-17-85 OP<br>SOIL FIELD | ERATOR IDENTIFICAT | ION  |       |
|------------------------------|--------------------|------|-------|
| TEST                         | SAND               | SILT | CLAY  |
| VISUAL                       |                    |      |       |
| DRIED CAST                   |                    |      |       |
| DILATANCY                    |                    |      |       |
| BITE                         | ·                  |      | 1     |
| TOUGHNESS                    |                    |      |       |
| DESCRIPTION: Bm.             | moist, v           | SLTY | ESANI |

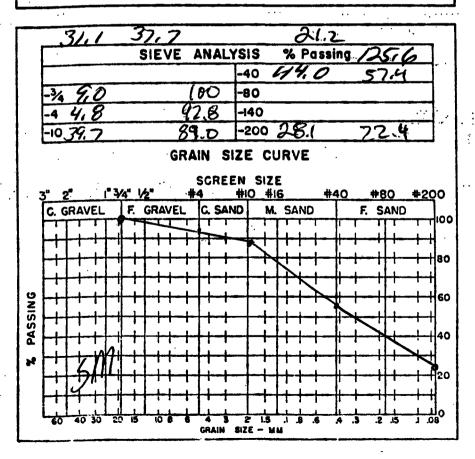


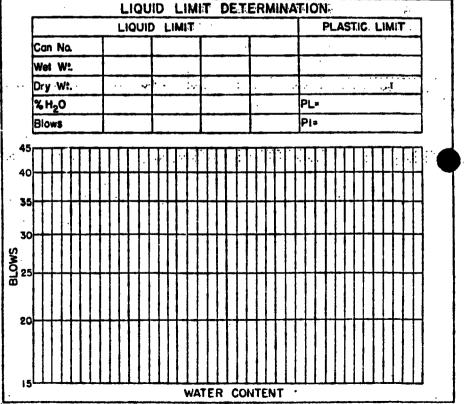




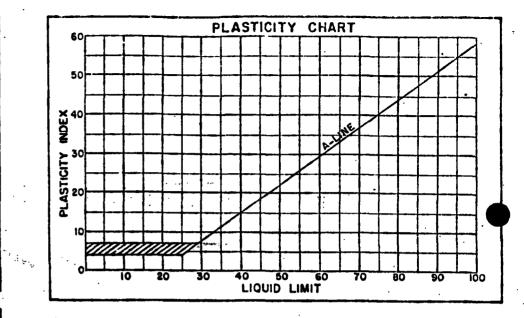
| SAMPLE NO.5EBO-14 JOE<br>DATE 4-17-85 OPI<br>SOIL FIELD I | ERATOR |        |      |
|---|--------|--------|------|
| TEST  | SAND   | SILT   | GLAY |
| VISUAL  | V      | V      |      |
| DRIED CAST  |        |        |      |
| DILATANCY   |        |        |      |
| BITE  |        |        |      |
| TOUGHNESS   |        |        |      |
| DESCRIPTION: Bry  | mout.  | -6rave | UL.  |
|   | 0==6-  |        | CANA |

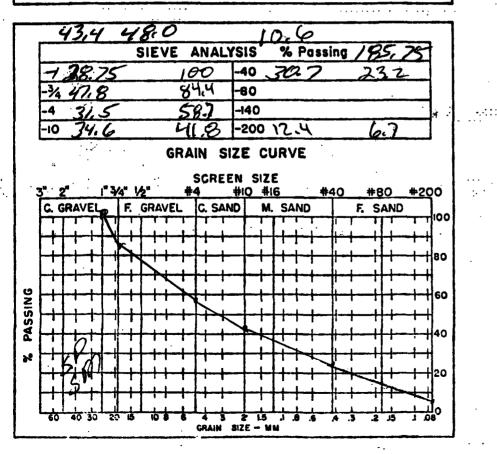


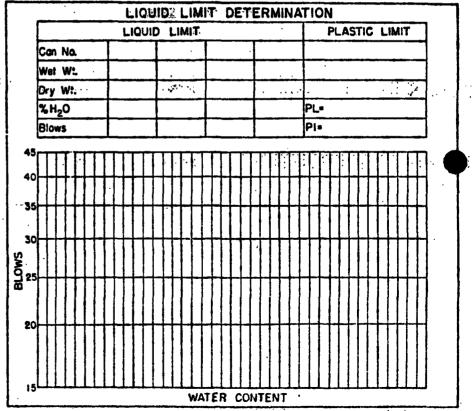




| DATE 4-17-85 OF SOIL FIELD | PERATOR SE | rion    |         |
|----------------------------|------------|---------|---------|
| TEST                       | SAND       | SILT    | CLAY    |
| VISUAL                     | 7          | 4       |         |
| DRIED CAST                 |            |         |         |
| DILATANCY                  |            |         |         |
| BITE                       | ·          | 16.7    |         |
| TOUGHNESS                  |            |         |         |
| DESCRIPTION: But.          | nout.      | SLIT, C | F6vrve) |
| C-1                        | MUFS       |         |         |







#### **WASHINGTON STATE** EPARTMENT OF TRANSPOR

| _ | _ |
|---|---|
| 4 |   |
| - |   |

MATERIALS ENGINEER Materials Laboratory P. O. Box 167, Olympia, WA 98504 (Mailing Address) 1655 So. 2nd Ave. Tumwater, Washington 98504 (Shipping Address)

| Place | Seattle | <br> |    |
|-------|---------|------|----|
|       |         |      | ٠. |

Date February 25, 1985

Dear Sir:

I have forwarded by today's ... Hand Carried ... the following Foundation Samples.

Section Sunset Blvd. to Factoria I/C Job No. .... C-2637... SR No. 1405 Sub-Section

| Station<br>&<br>Offset | 377+50       | 70'LT                | <u>e                                     </u> |          | Hole #_         | 3         | ·   | · · · · · · · · · · · · · · · · · · · |
|------------------------|--------------|----------------------|---|----------|-----------------|-----------|-----|---------------------------------------|
| Lab No.                | Drive #      | Depth                | - Tube<br>Position<br>in Sampler              | Clas.    |                 | Descripti | on  | · ·                                   |
| 5979-1                 | P <b>-1</b>  | -1.0'<br>to          | H20=<br>5,3                                   | SP       |                 | ,         |     |                                       |
|                        |              | -3.01                | 3/2   | ļ        |                 | ••        |     | ·                                     |
| 2                      | P-2          | -3.01<br>to<br>-5.01 | H20=  | 5P       | ··.             |           |     |                                       |
|                        |              | <u> </u>             | 4.4   | <u> </u> |                 | ·         | •   |                                       |
|                        | P=3          | -5.01<br>to          | mo=   | SP       |                 | ·         |     |                                       |
| -3                     |              | -7.01                | 1011  |          | . <del>``</del> |           |     |                                       |
|                        | P-4          | -7.51<br>to          | H20=  | SM       |                 |           |     |                                       |
| -4                     |              | -9.51                | 11.7  |          |                 |           |     |                                       |
|                        | P <b>-</b> 5 | -10.0'               |   |          | LK5879          | -4        |     |                                       |
| -5                     |              | -12.01               |   |          | ···;            |           |     |                                       |
| -6                     | P-6          | -12.5'<br>to         | H20=  | SEM      |                 |           |     |                                       |
| (4)                    |              | -14.51               | 11.7  |          | :               | ÷         |     | •                                     |
|                        | P-7          | -15.0'<br>to         |   |          | LK5879-         | 6         |     |                                       |
| -7                     |              | -17.01               |   |          | <u> </u>        |           | • ( |                                       |
| 0                      | P-8          | -17.51<br>to         | H20=  | SMI      |                 |           |     |                                       |
| -8                     |              | -19.51               | 17.1  |          |                 | :         |     |                                       |
|                        | P-9          | -20.0                |   |          | LK5879-9        | 3         |     |                                       |
| -9                     |              | to<br>-22.01         |   |          |                 |           |     |                                       |

| 1 | copy | with  | samples  |
|---|------|-------|----------|
| 1 | CODV | to ac | ldressee |

Yours very truly, KEW (RMM)

# WASHINGTON STATE EPARTMENT OF TRANSPORTATION

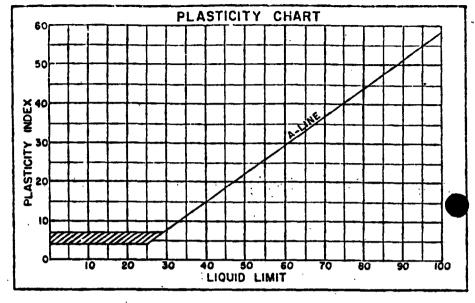
| MATERIALS<br>Materials Labo<br>P. O. Box 167, | ratory                                 | •                      | Mailing Addr                          | ess)        | Place Seattle                          |
|---|--|------------------------|---------------------------------------|-------------|--|
| 1655 So. 2nd A<br>Tumwater, Was               | ve.                                    |                        | ` ,                                   | :           | DateFebruary_25, 1985                  |
| Dear Sir:                                     |  |                        |                                       |             | DISMID DE D                            |
| I have  | forwarded                              | i by today's           | :                                     |             | the following Foundation Samples.      |
| Contract o                                    | c-263                                  | 7                      | Section<br>SR No                      | Suns<br>405 | set Blvd. to Factoria I/C Sub-Section  |
| Station<br>&<br>Offset                        | <u> 37<b>7</b>+5</u> 0                 | 70'LT                  | <u>E -</u>                            |             | Hole #                                 |
| E Lab No.                                     | Drive #                                | Depth                  | Tube<br>Position<br>in Sampler        | Clas.       | Description                            |
| 5979-10                                       | P <b>-1</b> 0                          | -22.5'                 | HZO=<br>8.8                           | 35M         |  |
| $\infty$ 7 .0                                 |  | -2319"                 | 0,0                                   |             | ;<br>                                  |
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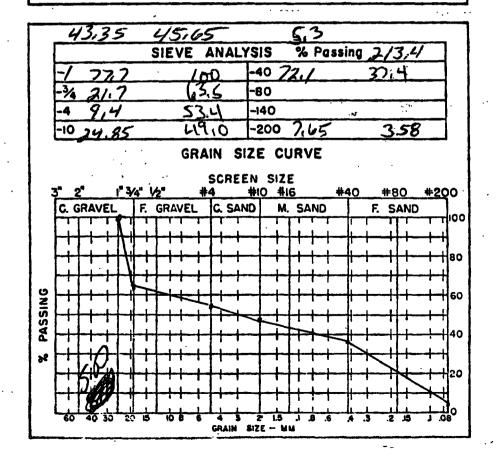
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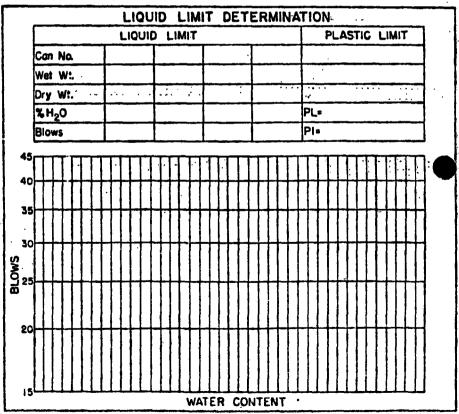
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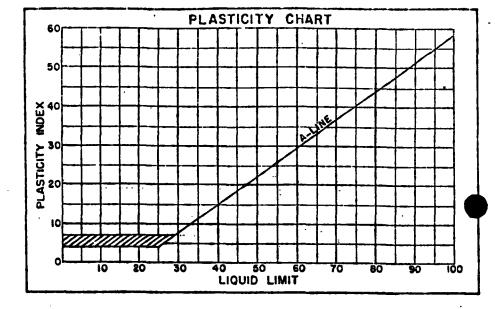
| SAMPLE NO. 5874-1 JO |             |          | NO. 3   |
|----------------------|-------------|----------|---------|
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| SOIL FIELD           | IDENTIFICAT | TION     | <u></u> |
| TEST                 | SAND        | SILT     | CLAY    |
| VISUAL               |             | 1        |         |
| DRIED CAST           |             |          |         |
| DILATANCY            |             |          |         |
| BITE                 |             |          |         |
| TOUGHNESS            |             |          |         |
| DESCRIPTION: Bu,     | Duy , 564.  | SUTY, C- | FGrove  |
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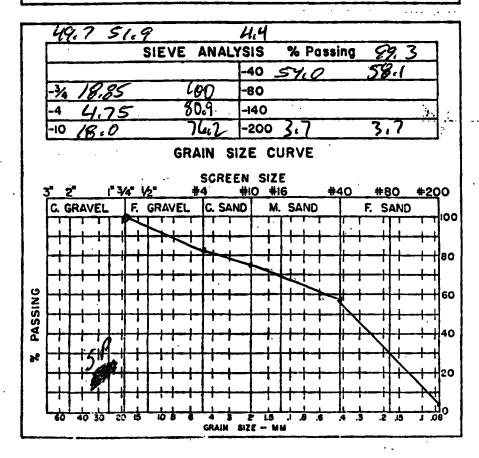


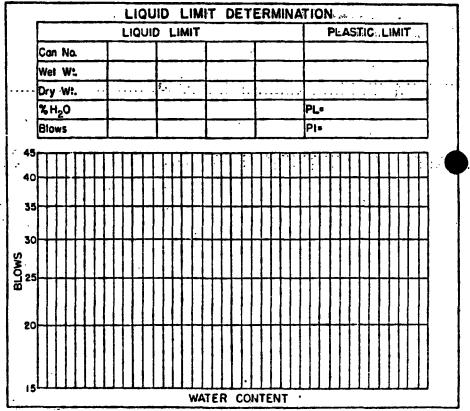




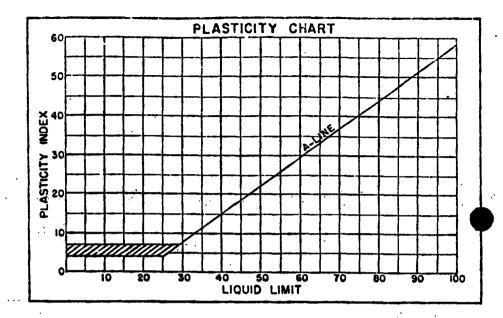
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|--|-----------|-----------|--------|
| SOIL FIELD                             |           |           |        |
| TEST                                   | SAND      | SILT      | CLAY   |
| VISUAL                                 |           | V         |        |
| DRIED CAST                             |           |           |        |
| DILATANCY                              |           |           |        |
| BITE                                   |           |           |        |
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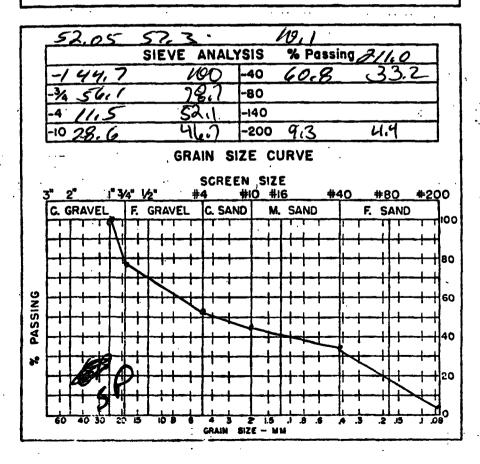


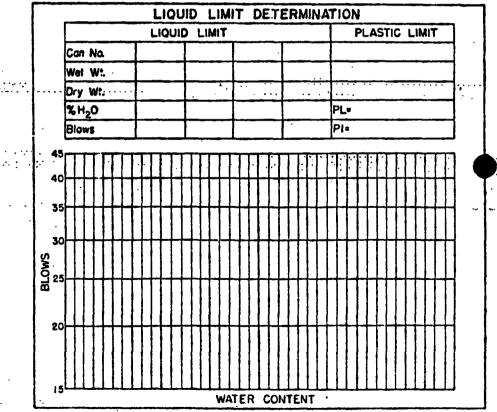




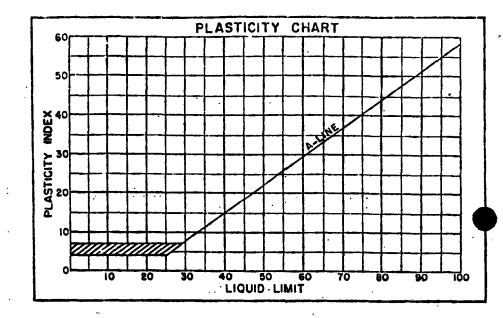
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|---|------------|---------|--------|
| SOIL FIELD I                              | DENTIFICAT | TION    |        |
| TEST                                      | SAND       | SILT    | CLAY   |
| VISUAL                                    |            |         |        |
| DRIED CAST                                |            |         |        |
| DILATANCY                                 |            |         |        |
| BITE                                      |            | ٠,      |        |
| TOUGHNESS                                 |            |         |        |
| DESCRIPTION: Ber.                         | moist, 5   | LYSLTY. | C-FGIV |

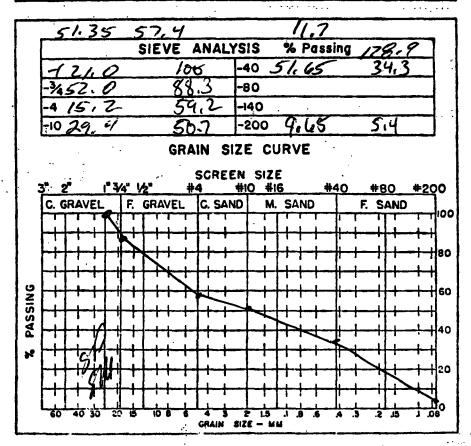


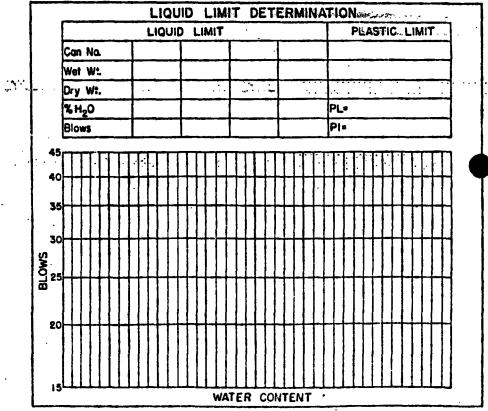




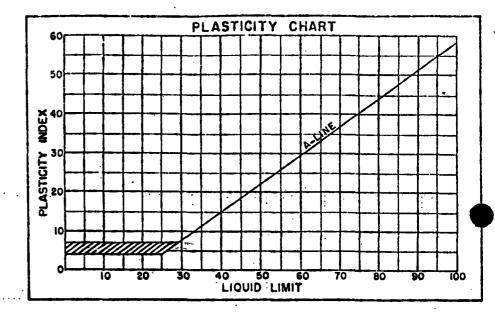
|                 | ERATOR      |       | <del></del> |
|-----------------|-------------|-------|-------------|
| SOIL FIELD      | IDENTIFICAT | TION  | <del></del> |
| TEST .          | SAND        | SILT  | CLAY        |
| VISUAL ,        | V           | -     |             |
| DRIED CAST      |             |       |             |
| DILATANCY       |             |       |             |
| BITE            |             | -     | i           |
| TOUGHNESS       |             |       |             |
| DESCRIPTION: Bm | moist       | 36456 | 79          |
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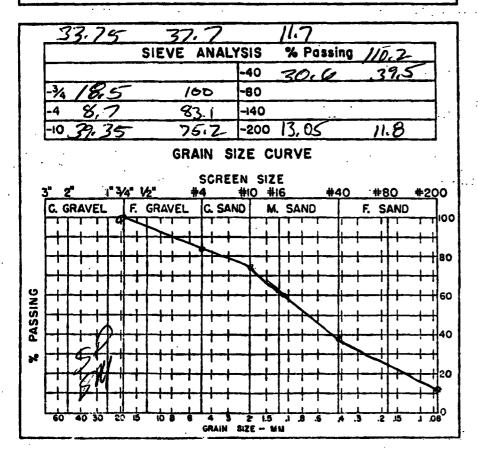


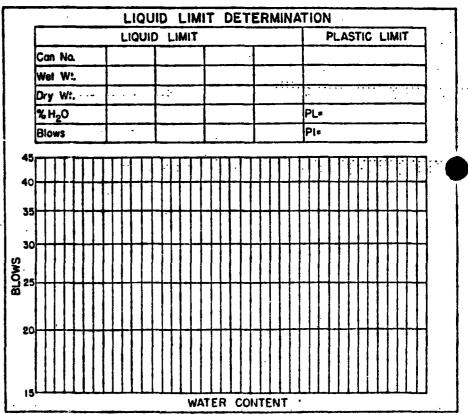




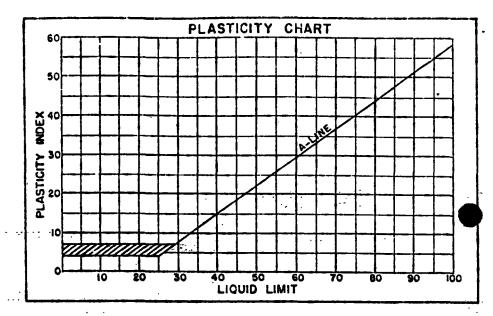
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| TEST                      | SAND    | SILT   | CLAY        |
| VISUAL                    |         |        |             |
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| DILATANCY                 |         |        |             |
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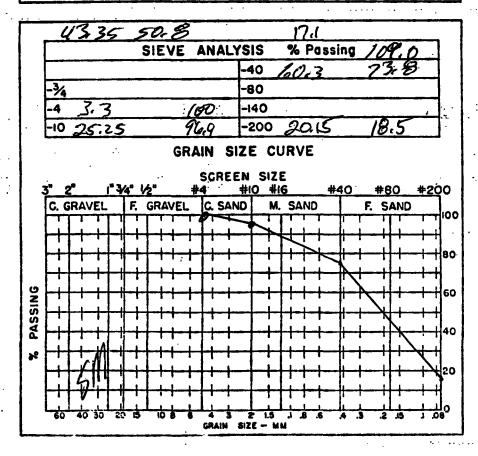


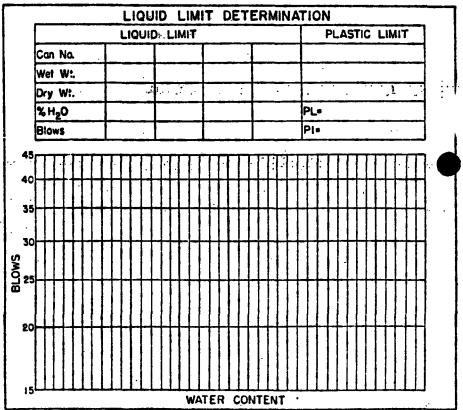




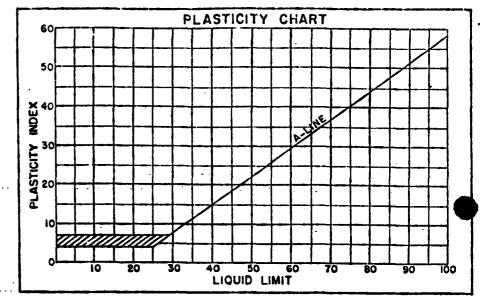
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|----------------------------|-------------|--------|---------|
| TEST                       | SAND        | SILT   | CLAY    |
| VISUAL                     |             |        |         |
| DRIED CAST                 |             |        |         |
| DILATANCY                  |             |        |         |
| BITE                       |             |        |         |
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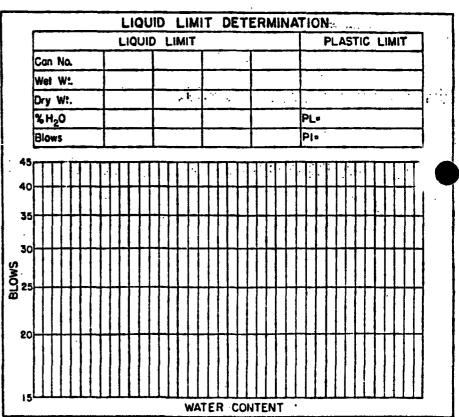




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| TEST            | SAND  | SILT   | CLAY   |
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In Association with

# **Appendix C Grade Separation Barrier 05.33R Calculations**







In Association with

#### APPENDIX C - GRADE SEPARATION BARRIER 05.33R CALCULATIONS

#### General

This appendix presents geotechnical calculations for Grade Separation Barrier 05.33R including:

- **ESU Soil Properties**
- Seismic Hazard Analysis
- Lateral Earth Pressures
- Coefficients of Friction for Sliding
- Bearing Resistance and Elastic Settlement
- Global Stability

#### **ESU Soil Properties**

Design soil properties were developed in accordance with the Project GDM, AASHTO LRFD, and FHWA. We calculated the average, geometric mean, and standard deviation within each ESU. We verified the reliability of the ESU data set by comparing the COV of each calculated geometric mean value to measured and interpreted values presented in Sabatini et al. (2002) Table 52.

A detailed description of the soil property development is presented in Section 7.1 of this geotechnical engineering report. Supporting calculations are provided in this appendix.

#### **Seismic Hazard Analysis**

We selected a representative site class for the barrier from the site class evaluation of nearby borings. We evaluated the site class of each boring using a spreadsheet developed by GeoEngineers in accordance with AASHTO LRFD Section 3.10.3.1.

We developed seismic design parameters using the WSDOT Bridge Engineering Software BEToolbox/BridgeLink in accordance with the WSDOT BDM based on the projected ground motion at the project site that has a 7 percent (SEE) probability of exceedance in a 75-year period (approximate 1,000-year return period).

We used a mean earthquake magnitude at the PGA period of 7.0 for the SEE based on the Hart Crowser design report "I-405 R2B Segment 1a Site-Specific Hazard Analysis RFU," dated March 25, 2021.

We evaluated the FS against liquefaction and liquefaction-induced settlement of saturated, loose to medium dense soils in accordance with the Project GDM Chapter 6 using a spreadsheet developed by GeoEngineers. The FSs against liquefaction at Grade Separation Barrier 05.33R were greater than 1.2 for all soil analyzed; per Project GDM Section 6-4.2.3, soils with liquefaction potential are defined as those with FSs against liquefaction less than 1.2.

Detailed descriptions of our seismic hazard analysis methodology and the results are presented in Section 7.2 and Section 8.1, respectively, of this report. Site class calculations, WSDOT BDM software outputs, and liquefaction analyses are provided in this appendix.

#### **Lateral Earth Pressures**

Active lateral pressure coefficients and active lateral earth pressures for imported common borrow, select borrow, and gravel borrow were calculated in accordance with AASHTO LRFD Section 3.11.5 using a 4H:21V barrier back face batter, the proposed 3.2H:1V backslope behind the wall, and a horizontal foreslope in front of the wall. Lateral earth pressures shall be applied using a triangular distribution. An LRFD load factor of 1.5 shall be applied to the active earth pressures in accordance with AASHTO LRFD Table 3.4.1-2. Due to negligible embedment of the wall, passive lateral earth pressures shall be ignored.

Surcharge loads and appropriate load factors from AASHTO LRFD Tables 3.4.1-1 and 3.4.1-2 shall be applied to evaluate barrier stability.







#### In Association with

A detailed description of our analysis methodology and the calculated results are presented in Section 7.3 and Section 8.2, respectively. Supporting calculations are provided in this appendix.

#### Coefficients of Friction for Sliding

Coefficients of friction for sliding on surficial native soils, common borrow, select borrow, and gravel borrow were calculated using AASHTO LRFD equation 10.6.3.4-2.

A detailed description of our analysis methodology and the results are presented in Section 7.4 and Section 8.3, respectively, of this report. Supporting calculations are provided in this appendix.

#### **Bearing Resistance and Elastic Settlement**

We estimated the bearing resistance and elastic settlement of the barrier using a spreadsheet developed by GeoEngineers in accordance with AASHTO LRFD Section 10.6.3. We estimated elastic settlement from procedures outlined in AASHTO LRFD and Section 10.6.2.4. Sliding and overturning are being evaluated by the design-build team's wall designers and will be submitted under separate cover.

A detailed description of our analysis methodology and the results are presented in Section 7.5 and Section 8.4, respectively, of this report. Supporting calculations are provided in this appendix.

#### **Global Stability**

We performed global stability analyses for the following critical design section:

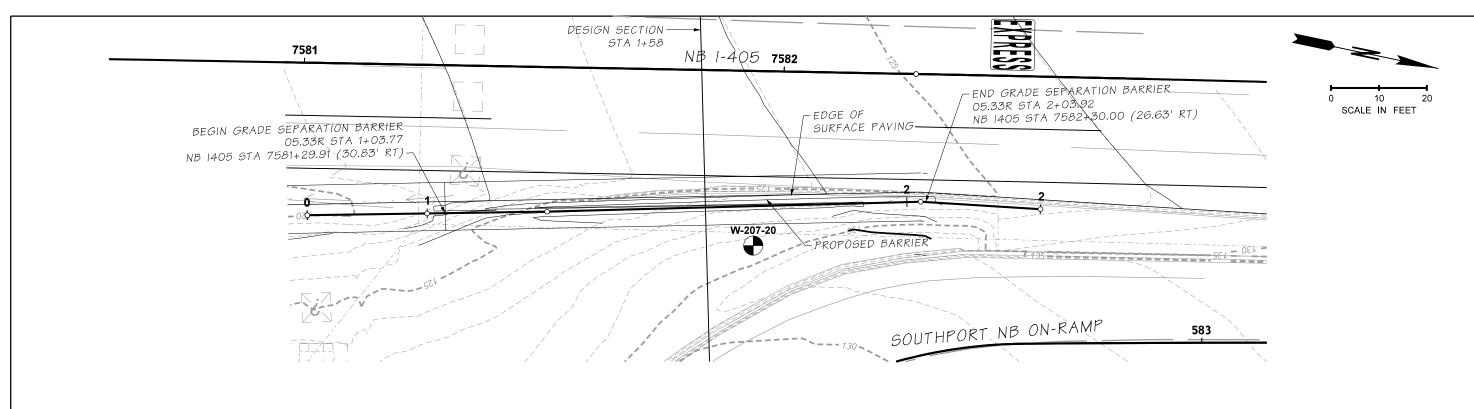
Section Sta. 1+58 – Maximum overall slope height

Global stability was evaluated using limit equilibrium analysis methodology outlined in the Project GDM using the computer design software Slope/W (Geo Slope International, Ltd. 2020). We analyzed FSs using Spencer's method and Morgenstern-Price for a circular failure surface.

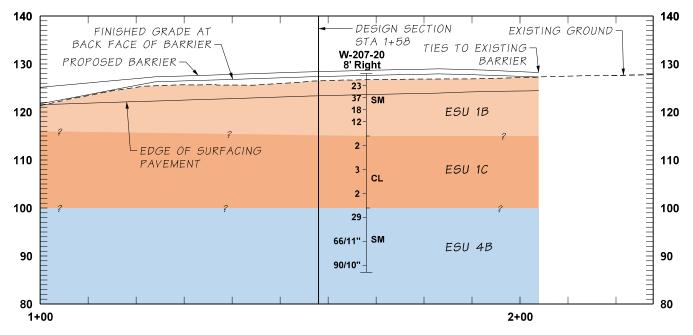
Grade Separation Barrier 05.33R will be designed in accordance with WSDOT BDM Section 10.3.1 for differential grade concrete barriers of 4 feet or less and will follow procedures in Project GDM Chapter 9 for embankments to evaluate global stability. Per Project GDM Section 9.2.3.1, seismic global stability analyses are not required for the barrier since it will not support or potentially impact structures.

Detailed descriptions of our global stability analysis methodology and the results of our analyses are presented in Section 7.8 and Section 8.6, respectively, of this report. Global stability models showing FS for critical failures at the design section are provided in this appendix. Slope/W reports are provided in Appendix J.

# Appendix C.1 - Grade Separation Barrier 05.33R Plan, Profile and Sections



#### PLAN - GRADE SEPARATION BARRIER 05.33R



DATE

REFLECTIVE ELEVATION - GRADE SEPARATION BARRIER 05.33R

THE ESU STRATIFICATION HAVE BEEN INTERPRETED, INTERPOLATED BETWEEN EXPLORATIONS, AND EXTRAPOLATED BEYOND EXPLORATIONS FOR ENGINEERING DESIGN PURPOSES, THE STRATA MAY NOT REPRESENT ACTUAL SUBSURFACE CONDITIONS, SEE THE EXPLORATION LOGS FOR DETAILED SUBSURFACE CONDITIONS AT THE LOCATION EXPLORED.

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I-405; RENTON TO BELLEVUE WIDENING AND EXPRESS TOLL LANES PROJECT

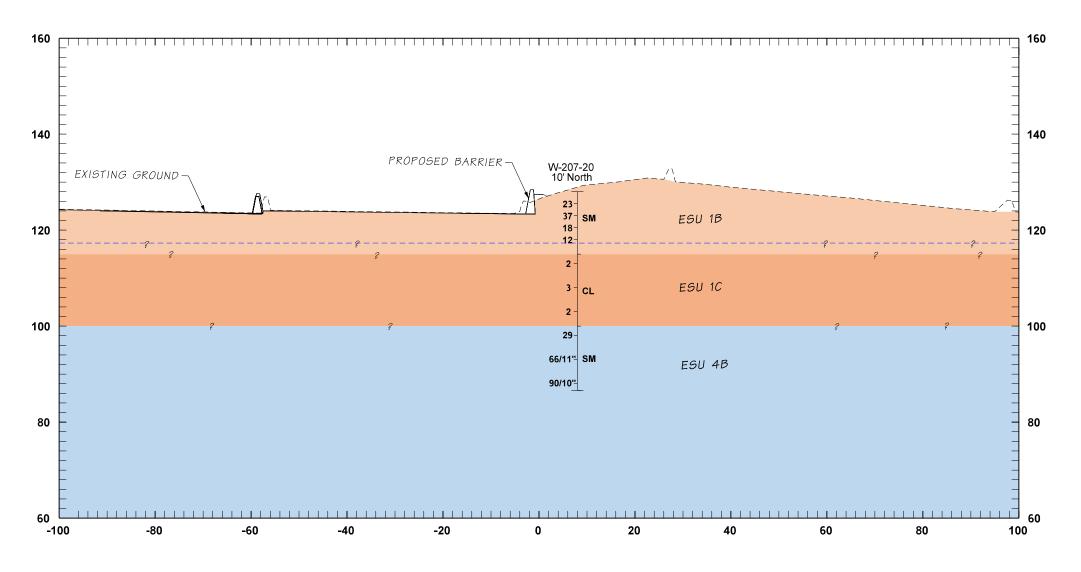
RETAINING WALL PLAN AND ELEVATION GRADE SEPARATION BARRIER 05.33R

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GRADE SEPARATION BARRIER 05.33R STATION 1+58

THE ESU STRATIFICATION HAVE BEEN INTERPRETED, INTERPOLATED BETWEEN EXPLORATIONS, AND EXTRAPOLATED BEYOND EXPLORATIONS FOR ENGINEERING DESIGN PURPOSES, THE STRATA MAY NOT REPRESENT ACTUAL SUBSURFACE CONDITIONS, SEE THE EXPLORATION LOGS FOR DETAILED SUBSURFACE CONDITIONS AT THE LOCATION EXPLORED.

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# Appendix C.2 - Grade Separation Barrier 05.33R ESU Soil Property Calculations

05.33R Soil Properties Summary

| ESU  | Description  | Samples PI (%) |    | Effective<br>Angle, φ | h (dog) | l Sottened |       | Residual<br>φ' <sup>k</sup> (deg) | Residual Shear<br>Strength, Sr (psf) | Undrain<br>Strength | ed Shear<br>, Su (psf) |                  |       |                  |       |       |       |       |       |     |
|------|--|----------------|----|-----------------------|---------|------------|-------|-----------------------------------|--------------------------------------|---------------------|------------------------|------------------|-------|------------------|-------|-------|-------|-------|-------|-----|
|      |  |                |    | Value                 | Value   | Value      | Value | COV <sup>a</sup>                  | Value                                | COV <sup>a</sup>    | Value                  | COV <sup>a</sup> | Value | COV <sup>a</sup> | Value | Value | Value | Value | Value | COV |
| 1 1B | Medium Dense to Very Dense<br>Coarse-Grained Fill                  | 3              | SM | 34                    | -       | 17         | 23    | 25%                               | 33                                   | 39%                 | 120                    | 6%               | 36    | 4%               | -     | -     | -     | -     | -     | -   |
| 10   | Very Soft to Medium Stiff/Very<br>Loose to Loose Fine-Grained Fill | 3              | CL | 50                    | 8       | 2          | 4     | 25%                               | 4                                    | 25%                 | 115                    | 0%               | 27    | 4%               | 1     | 1     | -     | -     | -     | -   |
| 4B   | Dense to Very Dense Sand/Gravel                                    | 2              | SM | 28                    | -       | 93         | 145   | 19%                               | 136                                  | 17%                 | 130                    | 0%               | 43    | 2%               | -     | -     | -     | -     | -     | -   |
|      |  |                |    |                       |         |            |       |                                   |                                      |                     |                        |                  |       |                  |       |       |       |       |       |     |

#### Notes:

- a. Coefficient of Variation (COV) percentage calculated to verify the variability and reliability of sample data within ESU (WSDOT GDM Section 5.11.2 (2015)). Calculated COV percentage compared to ranges presented in Table 52 (Sabatini et al. 2002) (below).
- b. Number of samples excludes outliers.
- c. Predominant USCS classification of all samples in ESU. Sandstone, where encountered, denoted as (SS).
- d. Fines content percentage calculated as the geometric mean of all samples, whose values were determined through lab testing or estimated from field classification.
- e. For coarse-grained ESUs, the plasticity index was estimated from the fine-grained portion of the soil. For fine-grained ESUs, if lab data is limited, the plasticity index may not be representative of the overall soil unit.
- f. Corrected blow counts ( $N_{60}$  and ( $N_{1}$ )<sub>60</sub>) were calculated following WSDOT GDM Section 5.5 (2015).
- g. Individual sample unit weights were correlated using CALTRANS Geotechnical Manual (2014), verified with applicable ranges presented in Codotu (2001), as specified in WOOD SPM. The geometric mean of the unit weights was rounded to the nearest 5pcf, as specified in WOOD SPM. Unit weight data variability and quality were evaluated by comparing the calculated COV percentage to the applicable Sabatini range.
- h. Design friction angles were selected by considering fines content. Friction angle data variability and quality were evaluated by comparing the calculated COV percentage to the applicable Sabatini range.
- i. Where applicable, fully softened friction angle was estimated following WSDOT GDM, Figure 5-7 (After Stark and Hussain, 2013).
- j. Where applicable, effective cohesion was calculated using Equations 6 through 8 in the WOOD Geotechnical SPM.
- k. Where applicable, residual friction angle (to be used for slope stability evaluation) was estimated following WSDOT GDM, Figure 5-5 (After NAVFAC, 1971).

| Measured or interpreted parameter value                 | Coefficient of Variation, V (%) |
|---|---------------------------------|
| Unit weight, γ  | 3 to 7 %                        |
| Buoyant unit weight, γ <sub>b</sub>                     | 0 to 10 %                       |
| Effective stress friction angle, φ'                     | 2 to 13 %                       |
| Undrained shear strength, su                            | 13 to 40 %                      |
| Undrained strength ratio $(s_u/\sigma_v')$              | 5 to 15 %                       |
| Compression index, C <sub>c</sub>                       | 10 to 37 %                      |
| Preconsolidation stress, σ <sub>p</sub> '               | 10 to 35 %                      |
| Hydraulic conductivity of saturated clay, k             | 68 to 90 %                      |
| Hydraulic conductivity of partly-saturated clay, k      | 130 to 240 %                    |
| Coefficient of consolidation, cv                        | 33 to 68 %                      |
| Standard penetration blowcount, N                       | 15 to 45 %                      |
| Electric cone penetration test, q <sub>c</sub>          | 5 to 15 %                       |
| Mechanical cone penetration test, q <sub>c</sub>        | 15 to 37 %                      |
| Vane shear test undrained strength, $s_{\mathrm{uVST}}$ | 10 to 20 %                      |

Source: Table 52 (Sabatini et al. 2002)

|           | ESU Name: |                 | ESU 1                           | LB - Medium | Dense to V  | ery Dense Co          | oarse-Graine         | ESU 1B - Medium Dense to Very Dense Coarse-Grained Fill |             |             |  |  |  |  |  |  |  |  |  |
|-----------|-----------|-----------------|---------------------------------|-------------|-------------|-----------------------|----------------------|---|-------------|-------------|--|--|--|--|--|--|--|--|--|
|           | N         | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub> | %F          | PI<br>(Lab) | ф'<br>(high)<br>(deg) | φ'<br>(low)<br>(deg) | Sat. Unit<br>Weight                                     | Su<br>(psf) | Sr<br>(psf) |  |  |  |  |  |  |  |  |  |
| GeoMean:  | 17        | 23              | 33                              | 34          | -           | 41                    | 36                   | 120   | -           | -           |  |  |  |  |  |  |  |  |  |
| Average:  | 18        | 23              | 34                              | 34          | -           | 41                    | 36                   | 120   | -           | -           |  |  |  |  |  |  |  |  |  |
| St. Dev.: | 5.5       | 5.9             | 13.5                            | -           | -           | 1.7                   | 1.7                  | 7.6   | -           | -           |  |  |  |  |  |  |  |  |  |
| cov:      | 0.31      | 0.25            | 0.39                            | -           | -           | 0.04                  | 0.05                 | 0.06  | -           | -           |  |  |  |  |  |  |  |  |  |

|  | COV.      | 0.31 | 0.23   | 0.35                            |                 |             | 0.04                  | 0.03                 | 0.00                | _           | _                        |      |   |
|--|-----------|------|--|---------------------------------|-----------------|-------------|-----------------------|----------------------|---------------------|-------------|--------------------------|------|---|
| Boring   | Elevation | N    | N <sub>60</sub>                                  | (N <sub>1</sub> ) <sub>60</sub> | %F <sup>3</sup> | PI<br>(Lab) | φ'<br>(high)<br>(deg) | φ'<br>(low)<br>(deg) | Sat. Unit<br>Weight | Su<br>(psf) | Sr <sup>4</sup><br>(psf) | USCS | Explanation for Sample Removal              |
| W-207-20   | 125.7     | 23   | 29   | 49                              | 37              | -           | 42                    | 37                   | 130                 | -           | =                        | SM   |   |
| W-207-20   | 123.2     |      |  |                                 |                 |             |                       |                      |                     |             |                          |      | rock in barrel, SPT may be artifically high |
| W-207-20   | 120.7     | 18   | 24   | 32                              | 34              | =           | 41                    | 36                   | 120                 | -           | =                        | SM   |   |
| W-207-20   | 118.2     | 12   | 17   | 22                              | 31              | -           | 39                    | 34                   | 115                 | -           | =                        | SM   |   |
|  |           |      |  |                                 |                 |             |                       |                      |                     |             |                          |      |   |
|  |           |      |  |                                 |                 |             |                       |                      |                     |             |                          |      |   |
|  |           |      |  |                                 |                 |             |                       |                      |                     |             |                          |      |   |
|  |           |      |  |                                 |                 |             |                       |                      |                     |             |                          |      |   |
|  |           |      |  |                                 |                 |             |                       |                      |                     |             |                          |      |   |
|  |           |      |  |                                 |                 |             |                       |                      |                     |             |                          |      |   |
| ļ  |           |      |  |                                 |                 |             |                       |                      |                     |             |                          |      |   |
| ļ  |           |      |  |                                 |                 |             |                       |                      |                     |             |                          |      |   |
| <b></b>  |           |      |  |                                 |                 |             |                       |                      |                     |             |                          |      |   |
| <b></b>  |           |      |  |                                 |                 |             |                       |                      |                     |             |                          |      |   |
| <b>-</b>   |           |      |  |                                 |                 |             |                       |                      |                     |             |                          |      |   |
| <b></b>  |           |      |  |                                 |                 |             |                       |                      |                     |             |                          |      |   |
| <b>-</b>   |           |      |  |                                 |                 |             |                       |                      |                     |             |                          |      |   |
| <del>                                     </del> |           |      | 1  |                                 |                 |             |                       |                      |                     |             |                          |      |   |
| <del>                                     </del> |           |      | <del>                                     </del> |                                 |                 |             |                       |                      |                     | -           |                          |      |   |
| <del>                                     </del> |           |      | <del>                                     </del> |                                 |                 |             |                       |                      |                     | -           |                          |      |   |
| <del>                                     </del> |           |      | 1  |                                 |                 |             |                       |                      |                     |             |                          |      |   |
| Notos:   |           |      | l  |                                 |                 | l           |                       | l                    | l                   |             |                          | l    |   |

#### Notes:

- 1. Highlighted cells in yellow if shown represent samples that were removed as outliers.
- 2. Friction angle, unit weight, and corrected blow count values were correlated using specified methodology in the WOOD Geotechnical SPM. Where applicable, undrained shear strength of fine grained ESUs were determined using Equation 9 in the WOOD Geotechnical SPM.
- 3. Fines content percentages determined through laboratory testing are highlighted in orange if shown. Non-highlighted values have been estimated from sample field classifications, applying the fines content of a lab tested sample with similar properties or using the average of two tested samples
- 4. Where applicable, residual strength is calculated using the existing relationships and weighting scheme per the GDM (section 6-2.2) to determine residual strengths for samples with (N1)60cs less than or equal to 20. Per Kramer 2008, samples that triggered liquefaction (FoS<1.2) but also has an (N1)60cs>20, uses the residual strength value for a soil with (N1)60cs=20, effectively capping the residual strength calculation at (N1)60cs=20.

#### 1. Check N160 COV is between 15 and 45%

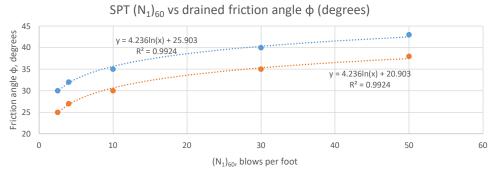
| Selected Design N160:           | 33   |
|---------------------------------|------|
| Coefficient of Variation (COV): | 0.39 |

<sup>\* 15</sup> and 45% come from GEC 5 Sabatini (2002)

#### 2. Check Phi' is between 2 to 13%

| (N <sub>1</sub> ) <sub>60</sub> (blows per foot) | Friction angle φ<br>(degrees) |
|--|-------------------------------|
| 2.5  | 25                            |
| 2.5  | 30                            |
| 4  | 27                            |
| 4  | 32                            |
| 10   | 30                            |
| 10   | 35                            |
| 30   | 35                            |
| 30   | 40                            |
| 50   | 38                            |
| 50   | 43                            |

WSDOT GDM Table 5-1



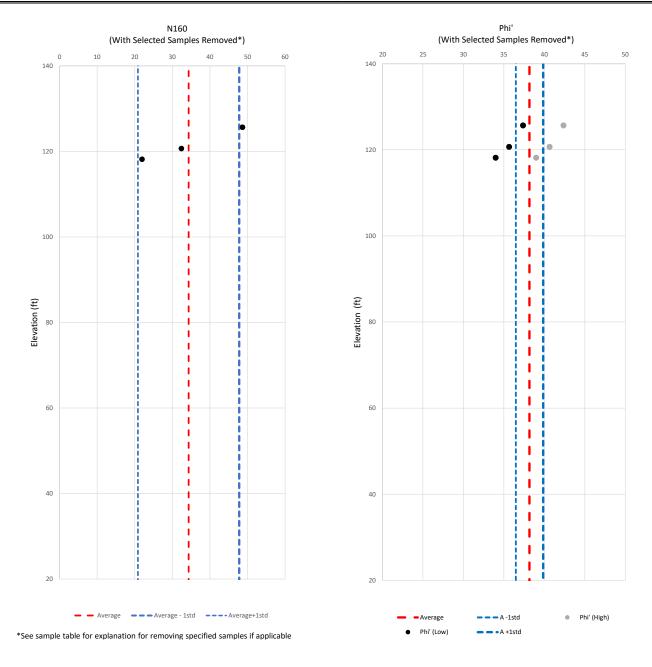
|          | φ (high) | φ (low) | ф (avg) | φ' cov |
|----------|----------|---------|---------|--------|
| GeoMean: | 41       | 36      | 38      | 0.04   |

| Selected Design Phi' (deg): | 36                 |  |
|-----------------------------|--------------------|--|
| Notes on Selection:         | The estimated fine | es content is 34% (geomean). The high fines content supports the use of the lower bound of the friction angle range. |

| Pick Representative USCS:        | SM  | *Using Predominant USCS Classification  |
|----------------------------------|-----|---|
| Pick Representative Unit Weight: | 120 |   |
| Notes on Selection:              | •   | unit weights were correlated using CALTRANS Geotechnical Manual (2014), verified with applicable ranges presented in Codotu d in WOOD SPM. The geometric mean of the unit weights was rounded to the nearest 5pcf, as specified in WOOD SPM. Data set |

<sup>\*</sup> Phi' Developed from WSDOT Correlation

<sup>\* 2</sup> to 13% comes from GEC 5 Sabatini (2002)



|          | Ī         | ESU Name: |                 | ESU 1C - Very Soft to Medium Stiff/Very Loose to Loose Fine-Grained Fill |                 |             |                       |                      |                     |              |                          |      |                                |
|----------|-----------|-----------|-----------------|--|-----------------|-------------|-----------------------|----------------------|---------------------|--------------|--------------------------|------|--------------------------------|
|          |           | N         | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub>  | %F              | PI<br>(Lab) | φ'<br>(high)<br>(deg) | ф'<br>(low)<br>(deg) | Sat. Unit<br>Weight | Su<br>(psf)  | Sr<br>(psf)              |      |                                |
|          | GeoMean:  | 2         | 4               | 4  | 50              | 8           | 32                    | 27                   | 115                 | -            | -                        |      |                                |
|          | Average:  | 2         | 4               | 4  | 50              | 8           | 32                    | 27                   | 115                 | -            | -                        |      |                                |
|          | St. Dev.: | 0.6       | 0.9             | 1.0  | -               | =           | 1.0                   | 1.0                  | 0.0                 | -            | -                        |      |                                |
|          | COV:      | 0.25      | 0.25            | 0.25   | -               | =           | 0.03                  | 0.04                 | 0.00                | =            | -                        |      |                                |
| Boring   | Elevation | N         | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub>  | %F <sup>3</sup> | PI<br>(Lab) | ф'<br>(high)<br>(deg) | ф'<br>(low)<br>(deg) | Sat. Unit<br>Weight | Su<br>(psf)  | Sr <sup>4</sup><br>(psf) | uscs | Explanation for Sample Removal |
| W-207-20 | 113.2     | 2         | 3               | 4  | 50              | 8           | 32                    | 27                   | 115                 | -            | -                        | CL   |                                |
| W-207-20 | 108.2     | 3         | 5               | 5  | 50              | -           | 33                    | 28                   | 115                 | -            | -                        | CL   |                                |
| W-207-20 | 103.2     | 2         | 3               | 3  | 50              | -           | 31                    | 26                   | 115                 | -            | -                        | CL   |                                |
|          |           |           |                 |  |                 |             |                       |                      |                     |              |                          |      |                                |
|          |           |           |                 |  |                 |             |                       |                      |                     |              |                          |      |                                |
|          |           |           |                 |  |                 |             |                       |                      |                     |              |                          |      |                                |
|          |           |           |                 |  |                 |             |                       |                      |                     |              |                          |      |                                |
|          |           |           |                 |  |                 |             |                       |                      |                     |              |                          |      |                                |
|          |           |           |                 |  |                 |             |                       |                      |                     |              |                          |      |                                |
|          |           |           |                 |  |                 |             |                       |                      |                     |              |                          |      |                                |
|          |           |           |                 |  |                 |             |                       |                      |                     |              |                          |      |                                |
|          |           |           |                 |  |                 |             |                       |                      |                     |              |                          |      |                                |
|          |           |           |                 | <del> </del>   | <del> </del>    |             |                       |                      |                     | <del> </del> |                          |      |                                |
|          |           |           |                 | <del> </del>   | <del> </del>    |             | 1                     |                      |                     | <del> </del> |                          |      |                                |
|          |           |           |                 | İ  | 1               |             |                       |                      |                     | 1            |                          |      |                                |
|          |           |           |                 |  |                 |             |                       |                      |                     |              |                          |      |                                |
|          |           |           |                 |  |                 |             |                       |                      |                     |              |                          |      |                                |

Notes:

<sup>1.</sup> Highlighted cells in yellow if shown represent samples that were removed as outliers.

<sup>2.</sup> Friction angle, unit weight, and corrected blow count values were correlated using specified methodology in the WOOD Geotechnical SPM. Where applicable, undrained shear strength of fine grained ESUs were determined using Equation 9 in the WOOD Geotechnical SPM.

<sup>3.</sup> Fines content percentages determined through laboratory testing are highlighted in orange if shown. Non-highlighted values have been estimated from sample field classifications, applying the fines content of a lab tested sample with similar properties or using the average of two tested samples

<sup>4.</sup> Where applicable, residual strength is calculated using the existing relationships and weighting scheme per the GDM (section 6-2.2) to determine residual strengths for samples with (N1)60cs less than or equal to 20. Per Kramer 2008, samples that triggered liquefaction (FoS<1.2) but also has an (N1)60cs>20, uses the residual strength value for a soil with (N1)60cs=20, effectively capping the residual strength calculation at (N1)60cs=20.

#### 1. Check N160 COV is between 15 and 45%

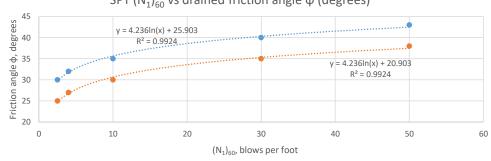
| Selected Design N160:           | 4    |
|---------------------------------|------|
| Coefficient of Variation (COV): | 0.25 |

<sup>\* 15</sup> and 45% come from GEC 5 Sabatini (2002)

#### 2. Check Phi' is between 2 to 13%

| (N <sub>1</sub> ) <sub>60</sub> (blows per foot) | Friction angle φ<br>(degrees) |
|--|-------------------------------|
| 2.5  | 25                            |
| 2.5  | 30                            |
| 4  | 27                            |
| 4  | 32                            |
| 10   | 30                            |
| 10   | 35                            |
| 30   | 35                            |
| 30   | 40                            |
| 50   | 38                            |
| 50   | 43                            |

# WSDOT GDM Table 5-1 SPT $(N_1)_{60}$ vs drained friction angle $\varphi$ (degrees)



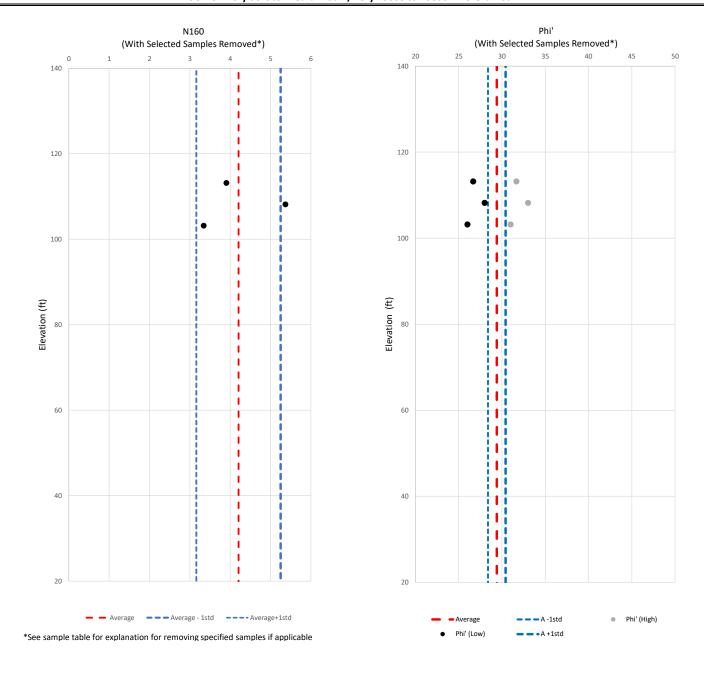
|          | φ (high) | ф (low) | ф (avg) | φ' cov |
|----------|----------|---------|---------|--------|
| GeoMean: | 32       | 27      | 29      | 0.04   |

| Selected Design Phi' (deg): | 27                 |  |
|-----------------------------|--------------------|--|
| Notes on Selection:         | The estimated fine | es content is 50% (geomean). The high fines content supports the use of the lower bound of the friction angle range. |

| Pick Representative USCS:        | CL  | *Using Predominant USCS Classification  |
|----------------------------------|-----|---|
| Pick Representative Unit Weight: | 115 |   |
| Notes on Selection:              | •   | unit weights were correlated using CALTRANS Geotechnical Manual (2014), verified with applicable ranges presented in Codotu d in WOOD SPM. The geometric mean of the unit weights was rounded to the nearest 5pcf, as specified in WOOD SPM. Data set |

<sup>\*</sup> Phi' Developed from WSDOT Correlation

<sup>\* 2</sup> to 13% comes from GEC 5 Sabatini (2002)



|           | ESU Name: |                 | ESU 4B - Dense to Very Dense Sand/Gravel |    |             |                       |                      |                     |             |             |
|-----------|-----------|-----------------|--|----|-------------|-----------------------|----------------------|---------------------|-------------|-------------|
|           | N         | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub>          | %F | PI<br>(Lab) | φ'<br>(high)<br>(deg) | φ'<br>(low)<br>(deg) | Sat. Unit<br>Weight | Su<br>(psf) | Sr<br>(psf) |
| GeoMean:  | 93        | 145             | 136                                      | 28 | -           | 47                    | 42                   | 130                 | -           | -           |
| Average:  | 96        | 147             | 137                                      | 28 | -           | 47                    | 42                   | 130                 | -           | -           |
| St. Dev.: | 27.6      | 28.3            | 23.3                                     | -  | -           | 0.7                   | 0.7                  | 0.0                 | -           | -           |
| cov:      | 0.29      | 0.19            | 0.17                                     | -  | -           | 0.02                  | 0.02                 | 0.00                | -           | -           |

| Boring   Berlation   N  |          | COV. 0.25 0.19 0.17 0.02 0.02 0.00 |     |                 |                                 |                 |   |        |       |     |   |   |      |  |
|---|----------|------------------------------------|-----|-----------------|---------------------------------|-----------------|---|--------|-------|-----|---|---|------|--|
| W-207-20 93.2 76 127 121 28 - 46 41 130 - 5 5M W-207-20 88.2 115 167 154 28 - 47 42 130 - 5 5M  W-207-20 88.2 115 167 154 28 - 47 42 130 - 5 5M  W-207-20 88.2 115 167 154 28 - 47 42 130 - 5 5M  W-207-20 88.2 115 167 154 28 - 47 42 130 - 5 5M  W-207-20 88.2 115 167 154 28 - 47 42 130 - 5 5M  W-207-20 88.2 115 167 154 28 - 47 42 130 - 5 5M  W-207-20 88.2 115 167 154 28 - 47 42 130 - 5 5M  W-207-20 88.2 115 167 154 28 - 47 42 130 - 5 5M  W-207-20 88.2 115 167 154 28 - 5 47 42 130 - 5 5M  W-207-20 88.2 115 167 154 28 - 5 47 42 130 - 5 5M  W-207-20 88.2 115 167 154 28 - 5 47 42 130 - 5 5M  W-207-20 88.2 115 167 154 28 - 5 47 42 130 - 5 5M  W-207-20 88.2 115 167 154 28 - 5 47 42 130 - 5 5M  W-207-20 88.2 115 167 154 28 - 5 47 42 130 - 5 5M  W-207-20 88.2 115 167 154 28 - 5 47 42 130 - 5 5M  W-207-20 88.2 115 167 154 28 - 5 47 42 130 - 5 5M  W-207-20 88.2 115 167 154 28 - 5 47 42 130 - 5 5M  W-207-20 88.2 115 167 154 28 - 5 47 42 130 - 5 5M  W-207-20 88.2 115 167 154 28 - 5 47 42 130 - 5 5M  W-207-20 88.2 115 167 154 28 - 5 47 42 130 - 5 5M  W-207-20 88.2 115 167 154 28 - 5 47 42 130 - 5 5M  W-207-20 88.2 115 167 154 28 - 5 47 42 130 - 5 5M  W-207-20 88.2 115 167 154 28 - 5 47 42 130 - 5 5M  W-207-20 88.2 115 167 154 28 - 5 47 42 130 - 5 5M  W-207-20 88.2 115 167 154 28 1 154 144 144 144 144 144 144 144 144 1 | Boring   | Elevation                          | N   | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub> | %F <sup>3</sup> |   | (high) | (low) |     |   |   | USCS | Explanation for Sample Removal                       |
| W-207-20 88.2 115 167 154 28 - 47 42 130 - SM   | W-207-20 | 98.2                               |     |                 |                                 |                 |   |        |       |     |   |   |      | Transition from fill above, underestimate blowcounts |
|   | W-207-20 | 93.2                               | 76  | 127             | 121                             | 28              | - | 46     | 41    | 130 | - | - | SM   |  |
|   | W-207-20 | 88.2                               | 115 | 167             | 154                             | 28              | - | 47     | 42    | 130 | - | - | SM   |  |
|   |          |                                    |     |                 |                                 |                 |   |        |       |     |   |   |      |  |
|   |          |                                    |     |                 |                                 |                 |   |        |       |     |   |   |      |  |
|   |          |                                    |     |                 |                                 |                 |   |        |       |     |   |   |      |  |
|   |          |                                    |     |                 |                                 |                 |   |        |       |     |   |   |      |  |
|   |          |                                    |     |                 |                                 |                 |   |        |       |     |   |   |      |  |
|   |          |                                    |     |                 |                                 |                 |   |        |       |     |   |   |      |  |
|   |          |                                    |     |                 |                                 |                 |   |        |       |     |   |   |      |  |
|   |          |                                    |     |                 |                                 |                 |   |        |       |     |   |   |      |  |
|   |          |                                    |     |                 |                                 |                 |   |        |       |     |   |   |      |  |
|   |          |                                    |     |                 |                                 |                 |   |        |       |     |   |   |      |  |
|   |          |                                    |     |                 |                                 |                 |   |        |       |     |   |   |      |  |
|   |          |                                    |     |                 |                                 |                 |   |        |       |     |   |   |      |  |
|   |          |                                    |     |                 |                                 |                 |   |        |       |     |   |   |      |  |
|   |          |                                    |     |                 |                                 | •               |   |        |       |     |   |   |      |  |
|   |          |                                    |     |                 |                                 |                 |   |        |       |     |   |   |      |  |
|   |          |                                    |     |                 |                                 |                 |   |        |       |     |   |   |      |  |
|   |          |                                    |     |                 |                                 |                 |   |        |       |     |   |   |      |  |
|   | Notes:   |                                    |     |                 |                                 |                 |   |        |       |     |   |   |      |  |

#### Notes:

- 1. Highlighted cells in yellow if shown represent samples that were removed as outliers.
- 2. Friction angle, unit weight, and corrected blow count values were correlated using specified methodology in the WOOD Geotechnical SPM. Where applicable, undrained shear strength of fine grained ESUs were determined using Equation 9 in the WOOD Geotechnical SPM.
- 3. Fines content percentages determined through laboratory testing are highlighted in orange if shown. Non-highlighted values have been estimated from sample field classifications, applying the fines content of a lab tested sample with similar properties or using the average of two tested samples
- 4. Where applicable, residual strength is calculated using the existing relationships and weighting scheme per the GDM (section 6-2.2) to determine residual strengths for samples with (N1)60cs less than or equal to 20. Per Kramer 2008, samples that triggered liquefaction (FoS<1.2) but also has an (N1)60cs>20, uses the residual strength value for a soil with (N1)60cs=20, effectively capping the residual strength calculation at (N1)60cs=20.

#### 1. Check N160 COV is between 15 and 45%

| Selected Design N160:           | 136  |
|---------------------------------|------|
| Coefficient of Variation (COV): | 0.17 |

<sup>\* 15</sup> and 45% come from GEC 5 Sabatini (2002)

#### 2. Check Phi' is between 2 to 13%

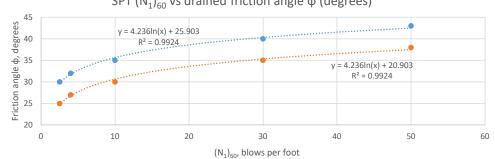
| (N <sub>1</sub> ) <sub>60</sub> (blows per foot) | Friction angle φ |
|--|------------------|
| (11760 (516115 per 1665)                         | (degrees)        |
| 2.5  | 25               |
| 2.5  | 30               |
| 4  | 27               |
| 4  | 32               |
| 10   | 30               |
| 10   | 35               |
| 30   | 35               |
| 30   | 40               |
| 50   | 38               |
| 50   | 43               |

<sup>\*</sup> Phi' Developed from WSDOT Correlation \* 2 to 13% comes from GEC 5 Sabatini (2002)

|          | φ (high) | ф (low) | ф (avg) |
|----------|----------|---------|---------|
| GeoMean: | 47       | 42      | 44      |



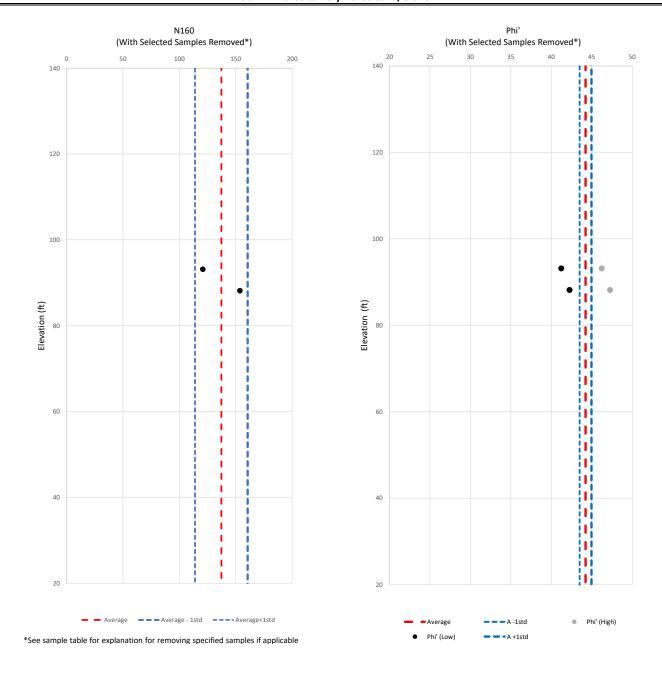




| _ |        |
|---|--------|
|   | φ' cov |
|   | 0.02   |

| Selected Design Phi' (deg): | 43 |   |
|-----------------------------|----|---|
| Notes on Selection:         |    | omean fines content is 28% (geomean). The friction angle is taken as the upper bound and capped at 43 degrees for glacially erial with fines content less than 70%. |

| Pick Representative USCS:        | SM  | *Using Predominant USCS Classification  |
|----------------------------------|-----|---|
| Pick Representative Unit Weight: | 130 |   |
| Notes on Selection:              | •   | unit weights were correlated using CALTRANS Geotechnical Manual (2014), verified with applicable ranges presented in Codotu d in WOOD SPM. The geometric mean of the unit weights was rounded to the nearest 5pcf, as specified in WOOD SPM. Data set |



The coefficient of consolidation,  $c_{\nu_{t}}$ , should be determined from the results of onedimensional consolidation tests. The variability in laboratory determination of  $\emph{c}_{\emph{V}}$  results should be considered in the final selection of the value of  $c_V$  to be used for design.

Where evaluation of elastic settlement is critical to the design of the foundation or selection of the foundation type, in-situ methods such as PMT or *DMT* for evaluating the modulus of the stratum should be used.

ESU 1B Medium Dense to Very Dense Coarse-Grained Fill Es = 725 ksf = 5.03 ksiPoisson's Ratio = 0.35

A profile of  $\sigma_{\sigma'}$ , or OCR =  $\sigma_{\sigma'}/\sigma_{\sigma'}$ , with depth should be developed for the site for design applications where the stress history could have a significant impact on the design properties selected and the performance of the foundation. As with consolidation properties, an upper and lower bound profile should be developed based on laboratory tests and plotted with a profile based on particular in-situ test(s), if used. It is particularly important to accurately compute preconsolidation stress values for relatively shallow depths where in-situ effective stresses are low. An underestimation of the preconsolidation stress at shallow depths will result in overly conservative estimates of settlement for shallow soil layers.

Due to the numerous simplifying assumptions associated with conventional consolidation theory, on which the coefficient of consolidation is based, it is unlikely that even the best estimates of  $c_{\nu}$  from high-quality laboratory tests will result in predictions of time rate of settlement in the field that are significantly better than a prediction within one order of magnitude. In general, the in-situ value of  $c_{
u}$  is larger than the value measured in the laboratory test. Therefore, a rational approach is to select average, upper, and lower bound values for the appropriate stress range of concern for the design application. These values should be compared to values obtained from previous work performed in the same soil deposit. Under the best-case conditions, these values should be compared to values computed from measurements of excess pore pressures or settlement rates during construction of other structures.

 $\ensuremath{\textit{CPTu}}$  tests in which the pore pressure dissipation rate is measured may be used to estimate the field coefficient of consolidation.

For preliminary analyses or where accurate prediction of settlement is not critical. values obtained from correlations to index properties presented in Sabatini et al. (2002)

For preliminary design or for final design where the prediction of deformation is not critical to structure performance, i.e., the structure design can tolerate the potential inaccuracies inherent in the correlations. The elastic properties  $(E_{sr}, \nu)$  of a soil may be estimated from empirical relationships presented in Table C10.4.6.3-1.

The specific definition of  $E_s$  is not always consistent for the various correlations and methods of in-situ measurement. See Sabatini et al. (2002) for additional details regarding the definition and determination of  $E_s$ .

An alternative method of evaluating the equivalent elastic modulus using measured shear wave velocities is presented in Sabatini et al. (2002).

Table C10.4.6.3-1—Elastic Constants of Various Soils (modified after U.S. Department of the Navy, 1982; Bowles, 1988)

| Soil Type                        | Typical Range of Young's Modulus Values, $E_s$ (ksi) | Poisson's Ratio, $\nu$ (dim)   |
|----------------------------------|--|--------------------------------|
| Clay:                            |  |                                |
| Soft sensitive                   |  |                                |
| Medium stiff to stiff            | 0.347-2.08   | 0.4–0.5 (undrained)            |
|                                  | 2.08-6.94  |                                |
| Very stiff                       | 6.94–13.89   |                                |
| Loess                            | 2.08-8.33  | 0.1-0.3                        |
| Silt                             | 0.278–2.78   | 0.3-0.35                       |
| Fine Sand:                       |  |                                |
| Loose                            | 1.11–1.67  | 0.25                           |
| Medium dense                     | 1.67–2.78  |                                |
| Dense                            | 2.78–4.17  |                                |
| Sand:                            |  |                                |
| Loose                            | 1.39–4.17  | 0.20-0.36                      |
| Medium dense                     | 4.17–6.94  |                                |
| Dense                            | 6.94–11.11   | 0.30-0.40                      |
| Gravel:                          |  |                                |
| Loose                            | 4.17–11.11   | 0.20-0.35                      |
| Medium dense                     | 11.11–13.89  |                                |
| Dense                            | 13.89–27.78  | 0.30-0.40                      |
| Estimating E <sub>s</sub> from S | SPT N Value  |                                |
|                                  | Soil Type  | $E_s$ (ksi)                    |
| Silts, sandy silts, slig         | htly cohesive mixtures                               | 0.056 N <sub>160</sub>         |
| Clean fine to mediun             | n sands and slightly silty sands                     | 0.097 N <sub>160</sub>         |
| Coarse sands and sa              | nds with little gravel                               | 0.139 <i>N</i> 1 <sub>60</sub> |
| Sandy gravel and gra             | avels  | 0.167 <i>N</i> 1 <sub>60</sub> |
| Estimating $E_s$ from $q$        | c (static cone resistance)                           |                                |
| Sandy soils                      |  | 0.028 <i>qc</i>                |
|                                  |  |                                |

The modulus of elasticity for normally consolidated granular soils tends to increase with depth. An alternative method of defining the soil modulus for granular soils is to assume that it increases linearly with depth starting at zero at the ground surface in accordance with the following equation:

$$E_s = nh \times z \tag{C10.4.6.3-1}$$

where:

# Appendix C.3 - Grade Separation Barrier 05.33R Design Calculations

### **AASHTO Average Blowcount in Upper 30'**

|       |                    |   | W-2   | 207-20               |                                |                                      |                  |       |                    |   |                                 |         |             |                |         |
|-------|--------------------|---|---|----------------------|--------------------------------|--------------------------------------|------------------|-------|--------------------|---|---------------------------------|---------|-------------|----------------|---------|
| Depth | Field<br>Blowcount | Energy<br>Corrected<br>Blowcount,<br>N <sub>i</sub> | Layer<br>thickness d <sub>i</sub><br>(feet) | Sum(d <sub>i</sub> ) | d <sub>i</sub> /N <sub>i</sub> | Sum(d <sub>i</sub> /N <sub>i</sub> ) | N <sub>ave</sub> | Depth | Field<br>Blowcount | Energy<br>Corrected<br>Blowcount,<br>N <sub>i</sub> | Layer<br>thickness<br>di (feet) | Sum(di) | di/Ni       | Sum(di/Ni)     | Nave    |
| 2.5   | 23                 | 33  | 3.75  | 100                  | 0.11                           | 5.8620                               | 17.1             |       |                    |   |                                 | 0       | End of Data | 0.0            | #DIV/0! |
| 5     | 37                 | 54  | 2.5   |                      | 0.05                           |                                      |                  |       |                    |   |                                 |         | End of Data |                |         |
| 7.5   | 18                 | 26  | 2.5   |                      | 0.10                           |                                      |                  |       |                    |   |                                 |         | End of Data |                |         |
| 10    | 12                 | 17  | 3.75  |                      | 0.22                           |                                      |                  |       |                    |   |                                 |         | End of Data |                |         |
| 15    | 2                  | 3   | 5   |                      | 1.72                           | Driving Energy                       | 87%              |       |                    |   |                                 |         | End of Data | Driving Energy | 60%     |
| 20    | 3                  | 4   | 5   |                      | 1.15                           |                                      |                  |       |                    |   |                                 |         | End of Data |                |         |
| 25    | 2                  | 3   | 5   |                      | 1.72                           |                                      |                  |       |                    |   |                                 |         | End of Data |                |         |
| 30    | 29                 | 42  | 5   |                      | 0.12                           |                                      |                  |       |                    |   |                                 |         | End of Data |                |         |
| 35    | 76                 | 100   | 5   |                      | 0.05                           |                                      |                  |       |                    |   |                                 |         | End of Data |                |         |
| 40    | 115                | 100   | 62.5  |                      | 0.63                           |                                      |                  |       |                    |   |                                 |         | End of Data |                |         |
|       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |         |
|       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |         |
|       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |         |
|       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |         |
|       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |         |
|       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |         |
|       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |         |
|       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |         |
|       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |         |
|       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |         |
|       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |         |
|       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |         |
|       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |         |
|       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |         |
|       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |         |
|       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |         |

| Soil Profile Type | v <sub>s</sub> (fps)         | N          |
|-------------------|------------------------------|------------|
| S <sub>A</sub>    | >5000                        | N/A        |
| S <sub>B</sub>    | 2,500 to 5,000               | IN/A       |
| S <sub>c</sub>    | 1,200 to 2,500               | >50        |
| S <sub>D</sub>    | 600 to 1,200                 | 15≤N≤50    |
| S <sub>E</sub>    | <600                         | <15        |
| Table 20.3-1 Site | Classifcation from ASCE Star | ndard 7-10 |

| Name     | Nave | Soil Profile Type |
|----------|------|-------------------|
| W-207-20 | 17.1 | D                 |

#### Note

Blowcount Percent (Energy is input BC/60). This spreadsheet approximates the layer thickness based on a function with depth, however, depending on the layering of the log, it may be necessary for the user to input their own layer thicknesses (i.e., clay layer extends at 7.5 ft and the blowcounts need to be weighted to reflect that thickness).

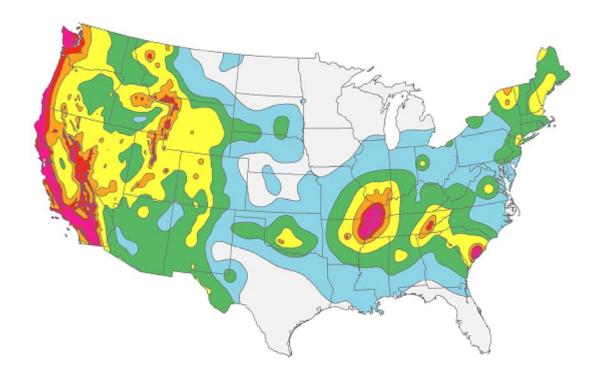
Spreadsheet based on Section 3.10.3.1 of American Association of State Highway and Transportation Officials (AASHTO).

AASHTO Average Blowcount 05.33R Site Class - AASHTO.xlsx

# $\textbf{BEToolbox}^{^{\text{TM}}}$

Spectra
Copyright © 2021, WSDOT, All Rights Reserved

Version 6.0.0.6 BETA - Built on Jan 7 2021



# 05.33R

WSDOT Bridge Design Manual 2014 Seismic Hazard Map, 7% probability of exceedance in 75 years

Site Coordinates (Latitude,Longitude): 47.5021° N, 122.196° W Site Soil Classification: Site Class D - Stiff Soil

Seismic hazard maps are for sites at the boundary of Site Classes B and C, which is  $\overline{v}_s$  = 2500 ft/s (760 m/s). Adjustments for

other Site Classes are made as needed.

| Period<br>(sec) | Sa<br>(g) |  |
|-----------------|-----------|--|
| 0.0             | 0.432     | PGA - Site Class B/C Boundary            |
| 0.2             | 0.985     | S <sub>s</sub> - Site Class B/C Boundary |
| 1.0             | 0.282     | S <sub>1</sub> - Site Class B/C Boundary |

Values of Site Coefficient,  $F_{pqa}$ , for Peak Ground Acceleration

| Site Class | Мар       | ped Peak G | round Acc | eleration Co | efficient (F | PGA)      |
|------------|-----------|------------|-----------|--------------|--------------|-----------|
|            | PGA≤ 0.10 | PGA= 0.20  | PGA= 0.30 | PGA= 0.40    | PGA= 0.50    | PGA≥ 0.60 |
| Α          | 0.8       | 0.8        | 0.8       | 8.0          | 0.8          | 8.0       |
| В          | 0.9       | 0.9        | 0.9       | 0.9          | 0.9          | 0.9       |
| С          | 1.3       | 1.2        | 1.2       | 1.2          | 1.2          | 1.2       |
| D          | 1.6       | 1.4        | 1.3       | 1.2          | 1.1          | 1.1       |
| Ē          | 2.4       | 1.9        | 1.6       | 1.4          | 1.2          | 1.1       |

For Site Class D,  $F_{pga} = 1.168$ 

Values for Site Coefficient, Fa, for 0.2 sec Period Spectral Acceleration

| Site Class | Mapped S              | pectral Acc           | celeration (          | Coefficient           | at Period 0           | .2 sec (S <sub>s</sub> ) |
|------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|--------------------------|
|            | S <sub>s</sub> ≤ 0.25 | S <sub>s</sub> = 0.50 | S <sub>s</sub> = 0.75 | S <sub>s</sub> = 1.00 | S <sub>s</sub> = 1.25 | S <sub>s</sub> ≥ 1.50    |
| Α          | 0.8                   | 0.8                   | 0.8                   | 0.8                   | 8.0                   | 0.8                      |
| В          | 0.9                   | 0.9                   | 0.9                   | 0.9                   | 0.9                   | 0.9                      |
| С          | 1.3                   | 1.3                   | 1.2                   | 1.2                   | 1.2                   | 1.2                      |
| D          | 1.6                   | 1.4                   | 1.2                   | 1.1                   | 1.0                   | 1.0                      |
| Е          | 2.4                   | 1.7                   | 1.3                   | 1.0                   | 0.9                   | 0.9                      |

For Site Class D,  $F_a = 1.106$ 

Values of Site Coefficient, F<sub>v</sub>, for 1.0 sec Period Spectral Acceleration

| Site Class | Mapped S             | pectral Acc          | eleration (          | Coefficient          | at Period 1          | .0 sec (S <sub>1</sub> ) |
|------------|----------------------|----------------------|----------------------|----------------------|----------------------|--------------------------|
|            | S <sub>1</sub> ≤ 0.1 | S <sub>1</sub> = 0.2 | S <sub>1</sub> = 0.3 | S <sub>1</sub> = 0.4 | S <sub>1</sub> = 0.5 | S <sub>1</sub> ≥ 0.6     |
| Α          | 0.8                  | 0.8                  | 0.8                  | 0.8                  | 0.8                  | 0.8                      |
| В          | 0.8                  | 0.8                  | 0.8                  | 0.8                  | 8.0                  | 0.8                      |
| С          | 1.5                  | 1.5                  | 1.5                  | 1.5                  | 1.5                  | 1.4                      |
| D          | 2.4                  | 2.2                  | 2.0                  | 1.9                  | 1.8                  | 1.7                      |
| Е          | 4.2                  | 3.3                  | 2.8                  | 2.4                  | 2.2                  | 2.0                      |

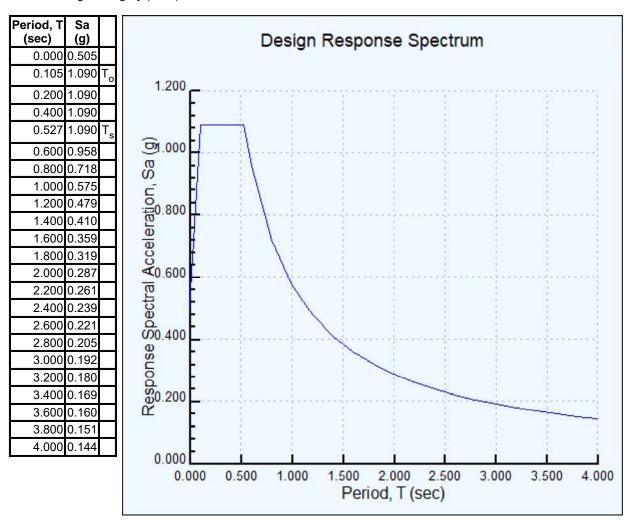
For Site Class D,  $F_v = 2.036$ 

$$\begin{split} & A_{\rm S} = F_{\rm pga} \; {\rm PGA} = (\; 1.168)(\; 0.432g) = 0.505g \\ & S_{\rm DS} = F_{\rm a} \; S_{\rm s} = (\; 1.106)(\; 0.985g) = 1.090g \\ & S_{\rm D1} = F_{\rm v} \; S_{\rm 1} = (\; 2.036)(\; 0.282g) = 0.575g \\ & T_{\rm o} = 0.2T_{\rm s} = (0.2)(\; 0.527) = 0.105 \; {\rm sec} \\ & T_{\rm s} = S_{\rm D1}/S_{\rm DS} = (\; 0.575)/(\; 1.090) = 0.527 \; {\rm sec} \end{split}$$

Partitions for Seismic Design Categories A, B, C, and D

| S <sub>D1</sub>          | SDC |
|--------------------------|-----|
| S <sub>D1</sub> < 0.15   | Α   |
| $0.15 \le S_{D1} < 0.30$ | В   |
| $0.30 \le S_{D1} < 0.50$ | С   |
| 0.50 ≤ S <sub>D1</sub>   | D   |

Seismic Design Category (SDC) = D



|                     | General Information                        |
|---------------------|--|
| Project:            | I-405/Renton to Bellevue Corridor Widening |
| Project Location:   | King County, Washington                    |
| Job Number:         | 00180-366-00                               |
| Boring Designation: | W-207-20                                   |
| Analysis by:        | ΥΠ   |
| Date Analyzed:      | 2/22/2021                                  |
| Checked by:         | ТВ   |
| Date Checked:       | 3/9/2021                                   |

| ]               |      | Sampling Information  |
|-----------------|------|---|
| GW estimated    | 10.9 | Depth to Groundwater (ft):                                  |
| from H-3-65 ATD | No   | SPT Liner (Yes/No):   |
|                 | 87   | Hammer Energy, %:   |
|                 | 5    | Distance from sample hammer to ground/mudline surface (ft): |
|                 | 8    | Rorehole Diameter (in)                                      |

| Earthquake Information | on    |
|------------------------|-------|
| Max Acceleration (g):  | 0.505 |
| Earthquake Magnitude:  | 7.0   |

| 1       | Fitle Block Information                    |
|---------|--|
| Line 1: | I-405/Renton to Bellevue Corridor Widening |
| Line 2: | King County, Washington                    |

| gIN                                 | NT Collection Information |
|-------------------------------------|---------------------------|
| P-Drive File Path to gINT database: |                           |
| Boring Selected from<br>Database:   |                           |

| Residual Strength Weighting                       |     |  |  |  |  |  |  |  |  |  |
|---|-----|--|--|--|--|--|--|--|--|--|
| Olsen & Stark (2002):                             | 0.2 |  |  |  |  |  |  |  |  |  |
| Idriss & Boulanger Void Redistribution (2007):    | 0.2 |  |  |  |  |  |  |  |  |  |
| Idriss & Boulanger No Void Redistribution (2007): | 0.0 |  |  |  |  |  |  |  |  |  |
| Kramer, Wang Hybrid (2008):                       | 0.4 |  |  |  |  |  |  |  |  |  |
| Idriss et al. (1998):                             | 0.2 |  |  |  |  |  |  |  |  |  |

| Collect Data From gINT | Automate %F from USCS |
|------------------------|-----------------------|
|                        |                       |
| uto %F from WSDOT GDM  | COMPUTE               |

User Input

gINT or User Input

| Fine -Grain Soil Susceptibi | ility |
|-----------------------------|-------|
| PI Cutoff Value:            | 12    |

| You must hit "COMPUTE" again anytime you change any of the          |
|---|
| plue or purple inputs. If the output tab is blank or has errors hit |
| COMPUTE" again.   |

| SPT Sample Number | Depth<br>(ft) | Measured N | USCS | Fines Content<br>(%) | Geologic Unit/<br>ESU | Unit Weight (pcf) | PI<br>(%) | Non-liquefiable (i.e.<br>"unstaturated",<br>"cohesive",etc) | User Override*  |
|-------------------|---------------|------------|------|----------------------|-----------------------|-------------------|-----------|---|-----------------|
|                   | 2.5           | 23         | SM   | 37                   | ESU 1B                | 130               |           | Unsaturated   |                 |
|                   | 5             | 37         | SM   | 37                   | ESU 1B                | 130               |           | Unsaturated   |                 |
|                   | 7.5           | 18         | SM   | 34                   | ESU 1B                | 120               |           | Unsaturated   |                 |
|                   | 10            | 12         | SM   | 31                   | ESU 1B                | 115               |           |   |                 |
|                   | 15            | 2          | CL   | 50                   | ESU 1C                | 115               |           | Cohesive  |                 |
|                   | 20            | 3          | CL   | 50                   | ESU 1C                | 115               |           | Cohesive  |                 |
|                   | 25            | 2          | CL   | 50                   | ESU 1C                | 115               |           | Cohesive  |                 |
|                   | 30            | 29         | SM   | 28                   | ESU 4B                | 130               |           | Non-Liquefiable   | Non-Liquefiable |
|                   | 35.0          | 76         | SM   | 28                   | ESU 4B                | 130               |           | Non-Liquefiable   | Non-Liquefiable |
|                   | 40.0          | 115        | SM   | 28                   | ESU 4B                | 130               |           | Non-Liquefiable   | Non-Liquefiable |
|                   | 1010          | 110        | O.W. | 20                   | 200 15                | 200               |           | Non Elquonablo  | Inquestions     |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |

Site Class D SEE

\*User Override column is **NOT** required to be filled out, unless needed. See "Read Me" tab.

|                      |               |                    |               |                         |                              |                                   |  | Liqu                              | efaction Analy      | /sis                        |                         |                         |   |                         |                                   | Residual S   | hear Stren              | gth Analysis   | <b>5</b>                         |                                   |                         |
|----------------------|---------------|--------------------|---------------|-------------------------|------------------------------|-----------------------------------|--|-----------------------------------|---------------------|-----------------------------|-------------------------|-------------------------|---|-------------------------|-----------------------------------|--------------|-------------------------|--|----------------------------------|-----------------------------------|-------------------------|
|                      |               |                    |               |                         | N <sub>1</sub>               | 1,60                              | =  | on Factor of<br>fety              | Liquefact           | ion-Induced Settle          | ement (in)              | LDI<br>(ft)             |   | N <sub>1,60</sub>       |                                   |              |                         | Residual Shea<br>(ps   | r Strength, Sr                   |                                   |                         |
| SPT Sample<br>Number | Depth<br>(ft) | Measured N         | USCS          | Fines<br>Content<br>(%) | Youd and<br>Idriss<br>(2001) | Idriss and<br>Boulanger<br>(2008) | Youd and<br>Idriss<br>(2001)                       | Idriss and<br>Boulanger<br>(2014) | Tokimatsu &<br>Seed | Ishihara &<br>Yoshimine     | Idriss and<br>Boulanger | Idriss and<br>Boulanger | Idriss &<br>Boulanger<br>Void<br>Distribution<br>(2007) | Olsen & Stark<br>(2002) | Kramer &<br>Wang Hybrid<br>(2008) | WSDOT        | Olsen & Stark<br>(2002) | Idriss &   | Idriss &<br>Boulanger<br>No Void | Kramer &<br>Wang Hybrid<br>(2008) | Idriss et al.<br>(1998) |
|                      | 2.5           | 23                 | SM            | 37                      | 47                           | 47                                | 2.00   | 2.00                              | 0.0                 | 0.0                         | 0.1                     | 0.0                     | 47.1  | 48.9                    | 46.3                              | n.a.         | n.a.                    | n.a.   | n.a.                             | n.a.                              | n.a.                    |
|                      | 5.0<br>7.5    | 37<br>18           | SM<br>SM      | 37<br>34                | 72<br>32                     | 67<br>31                          | 2.00   | 2.00                              | 0.0                 | 0.0                         | 0.1                     | 0.0                     | 67.3<br>31.0  | 83.9<br>35.8            | 68.0<br>30.0                      | n.a.<br>n.a. | n.a.<br>n.a.            | n.a.<br>n.a.   | n.a.<br>n.a.                     | n.a.<br>n.a.                      | n.a.<br>n.a.            |
|                      | 10.0          | 12                 | SM            | 31                      | 21                           | 21                                | 1.57   | 1.27                              | 0.0                 | 0.0                         | 0.1                     | 0.0                     | 21.0  | 22.2                    | 19.8                              | n.a.         | n.a.                    | n.a.   | n.a.                             | n.a.                              | n.a.                    |
|                      | 15.0          | 2                  | CL            | 50                      | 4                            | 4                                 | 2.00   | 2.00                              | 0.0                 | 0.0                         | 0.0                     | 0.0                     | 3.7   | 3.7                     | 3.4                               | 122          | 90                      | 119  | 123                              | 114                               | 175                     |
|                      | 20.0          | 2                  | CL            | 50<br>50                | 5<br>3                       | 5<br>3                            | 2.00   | 2.00                              | 0.0                 | 0.0                         | 0.0                     | 0.0                     | 5.1<br>3.2  | 5.1<br>3.2              | 4.9<br>3.1                        | 158<br>135   | 125<br>112              | 155<br>151   | 165<br>155                       | 145<br>126                        | 219<br>160              |
|                      | 30.0          | 29                 | SM            | 28                      | 45                           | 47                                | 2.00   | 2.00                              | 0.0                 | 0.0                         | 0.0                     | 0.0                     | 46.7  | 45.2                    | 45.4                              | n.a.         | n.a.                    | n.a.   | n.a.                             | n.a.                              | n.a.                    |
|                      | 35.0          | 76                 | SM            | 28                      | 111                          | 118                               | 2.00   | 2.00                              | 0.0                 | 0.0                         | 0.0                     | 0.0                     | 118.2   | 111.0                   | 113.3                             | n.a.         | n.a.                    | n.a.   | n.a.                             | n.a.                              | n.a.                    |
|                      | 40.0          | 115                | SM            | 28                      | 138                          | 151                               | 2.00   | 2.00                              | 0.0                 | 0.0                         | 0.0                     | 0.0                     | 173.5   | 158.5                   | 164.1                             | n.a.         | n.a.                    | n.a.   | n.a.                             | n.a.                              | n.a.                    |
|                      |               |                    |               |                         |                              |                                   |  |                                   |                     |                             |                         |                         |   |                         |                                   |              |                         |  |                                  |                                   |                         |
|                      |               |                    |               |                         |                              |                                   |  |                                   |                     |                             |                         |                         |   |                         |                                   |              |                         |  |                                  |                                   |                         |
|                      |               |                    |               |                         |                              |                                   |  |                                   |                     |                             |                         |                         | 1   |                         |                                   |              |                         |  |                                  |                                   |                         |
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|                      |               |                    |               |                         |                              |                                   |  |                                   |                     |                             |                         |                         | 1   |                         |                                   |              |                         |  |                                  |                                   |                         |
|                      |               |                    |               |                         |                              |                                   |  |                                   |                     |                             |                         |                         |   |                         |                                   |              |                         |  |                                  |                                   |                         |
|                      |               |                    |               |                         |                              |                                   |  |                                   |                     |                             |                         |                         |   |                         |                                   |              |                         |  |                                  |                                   |                         |
|                      |               |                    |               |                         |                              |                                   |  |                                   |                     |                             |                         |                         |   |                         |                                   |              |                         |  |                                  |                                   |                         |
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|                      |               |                    |               |                         |                              |                                   |  |                                   |                     |                             |                         |                         |   |                         |                                   |              |                         |  |                                  |                                   |                         |
|                      |               |                    |               |                         |                              |                                   |  |                                   |                     |                             |                         |                         |   |                         |                                   |              |                         |  |                                  |                                   |                         |
|                      |               |                    |               |                         |                              |                                   |  |                                   |                     |                             |                         |                         |   |                         |                                   |              |                         |  |                                  |                                   |                         |
|                      |               |                    |               |                         |                              |                                   |  |                                   |                     |                             |                         |                         |   |                         |                                   |              |                         |  |                                  |                                   |                         |
|                      |               |                    |               |                         |                              |                                   |  |                                   |                     |                             |                         |                         |   |                         |                                   |              |                         |  |                                  |                                   |                         |
|                      |               |                    |               |                         |                              |                                   |  |                                   |                     |                             |                         |                         | 1   |                         |                                   |              |                         | -  |                                  |                                   |                         |
|                      |               |                    |               |                         |                              |                                   |  |                                   |                     |                             |                         |                         |   |                         |                                   |              |                         |  |                                  |                                   |                         |
|                      |               |                    |               |                         |                              |                                   |  |                                   |                     |                             |                         |                         |   |                         |                                   | _            |                         |  |                                  |                                   |                         |
|                      |               | <u> </u>           |               |                         |                              |                                   |  |                                   |                     |                             |                         |                         |   |                         |                                   |              |                         | <del>                                     </del>                   |                                  |                                   |                         |
|                      |               |                    |               |                         |                              |                                   |  |                                   |                     |                             |                         |                         |   |                         |                                   |              |                         |  |                                  |                                   |                         |
|                      |               |                    |               |                         |                              |                                   |  |                                   |                     |                             |                         |                         |   |                         |                                   |              |                         |  |                                  |                                   |                         |
|                      |               |                    |               |                         |                              |                                   |  |                                   |                     |                             |                         |                         |   |                         |                                   |              |                         |  |                                  |                                   |                         |
|                      |               |                    |               |                         |                              |                                   |  |                                   |                     |                             |                         |                         |   |                         |                                   |              |                         |  |                                  |                                   |                         |
|                      |               |                    |               |                         |                              |                                   |  |                                   |                     |                             |                         |                         |   |                         |                                   |              |                         |  |                                  |                                   |                         |
|                      |               | -                  |               |                         |                              |                                   |  |                                   |                     |                             |                         |                         |   |                         |                                   |              |                         |  |                                  |                                   |                         |
|                      |               |                    |               |                         |                              |                                   |  |                                   |                     |                             |                         |                         |   |                         |                                   |              |                         |  |                                  |                                   |                         |
|                      |               |                    |               |                         |                              |                                   |  |                                   |                     |                             |                         |                         |   |                         |                                   |              |                         |  |                                  |                                   |                         |
|                      |               |                    | . –           |                         | <br>1                        |                                   |  | Residu                            | al Strength Wei     |                             |                         |                         |   |                         |                                   |              |                         |  |                                  |                                   |                         |
|                      |               | Seis<br>Max Accele | eration (g) : | <b>eters</b><br>0.505   |                              |                                   |  |                                   | Olsei               | WSDOT:<br>n & Stark (2002): |                         |                         |   |                         |                                   |              | Liquefa                 |  | esidual Sh<br>sults, W-20        |                                   | gth Analysis            |
|                      |               | Earthquake         | Magnitude:    | 7.00                    |                              |                                   | Idriss & Boulanger Void Redistribution (2007): 0.2 |                                   |                     |                             |                         |                         |   |                         |                                   |              |                         | I-405/Renton to Bellevue Corridor Widening King County, Washington |                                  |                                   |                         |

Idriss & Boulanger No Void Redistribution (2007):

Kramer, Wang Hybrid (2008):

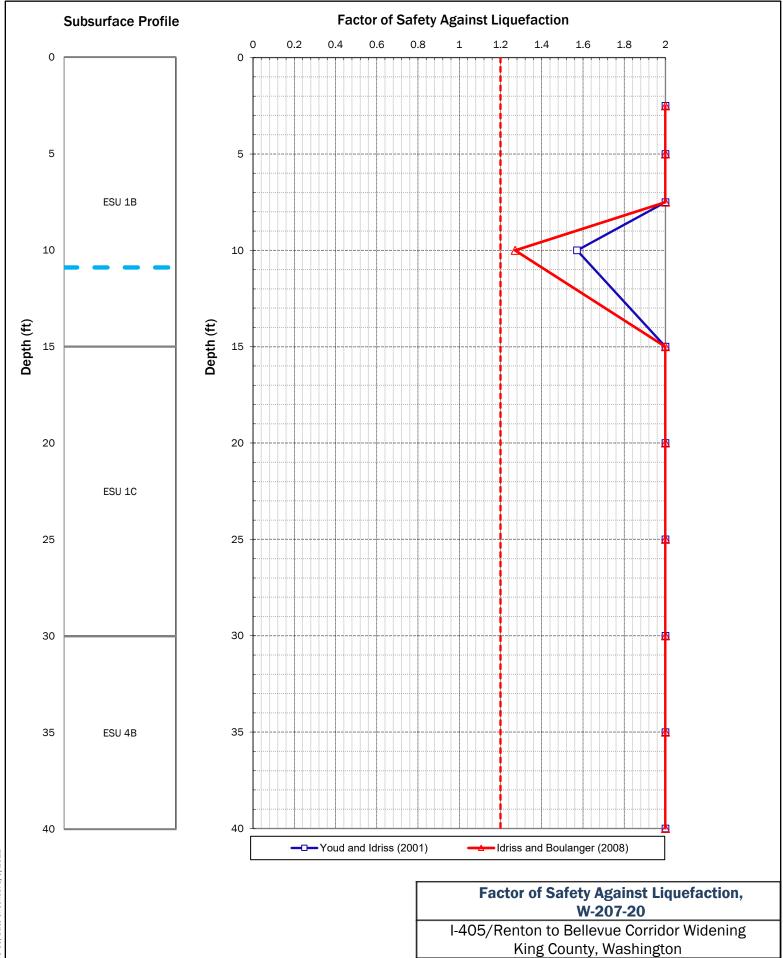
Idriss et al. (1998):

0.4

0.2

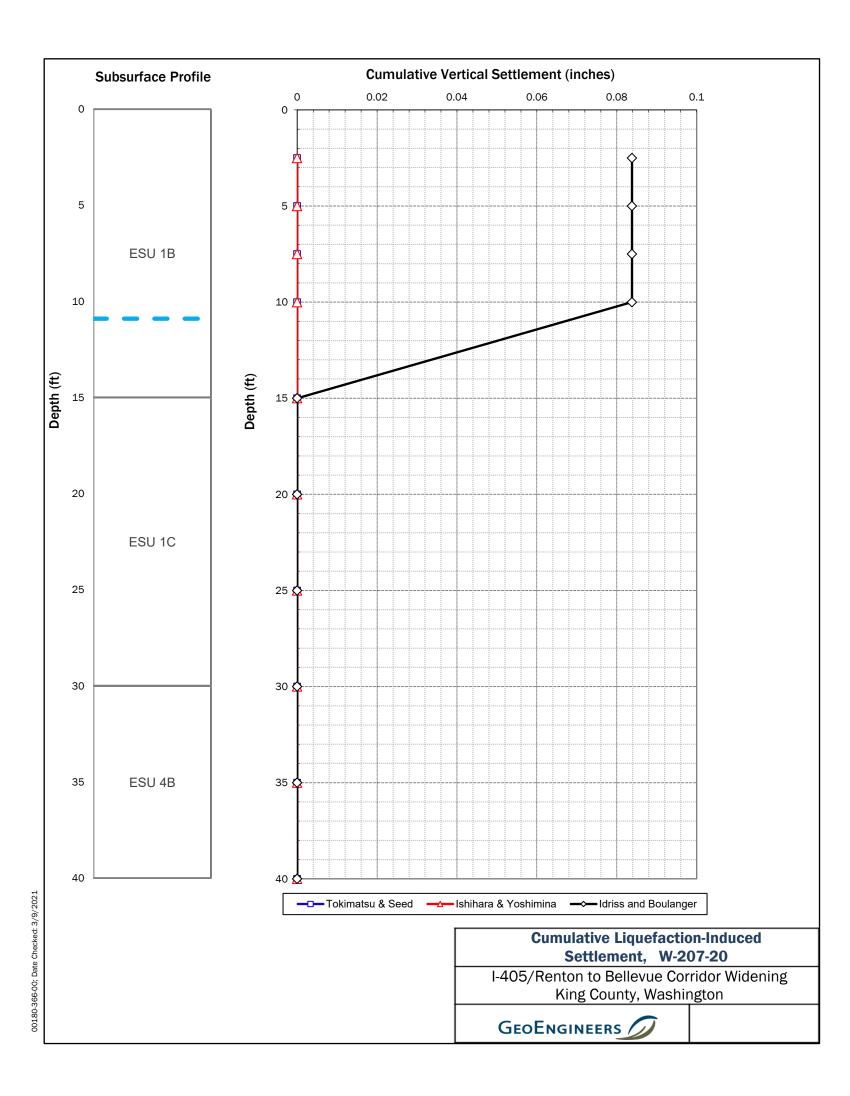
King County, Washington

GEOENGINEERS



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00180-366-00; Date Checked: 3/9/2021



# **Lateral Earth Pressures for Cohesionless Soils**

#### **Project Information**

| Project:     | I-405/Renton to Bellevue Corridor Widening |
|--------------|--|
| Owner:       | WSDOT                                      |
| Job Number:  | 00180-366-01                               |
| Analysis by: | YTT  |
| Date/Time:   | 1/18/2022 9:30 AM                          |
| Checked by:  | ТВ   |

#### **Input Parameters**

| Material      | φ<br>Friction Angle<br>(deg) | Friction Angle Foreslope Ba |               | δ<br>Wall Friction - Active<br>(deg) | δ<br>Wall Friction - Passive<br>(deg) | β<br>Wall Batter<br>(deg) | γ <sub>m</sub><br>(pcf) | γ <sub>b</sub> (pcf) | Passive<br>Factor of<br>Safety | k <sub>h</sub><br>(g) | k <sub>v</sub><br>(g) |
|---------------|------------------------------|-----------------------------|---------------|--------------------------------------|---------------------------------------|---------------------------|-------------------------|----------------------|--------------------------------|-----------------------|-----------------------|
| Common Borrow | 32                           | 0                           | (deg)<br>17.5 | 0                                    | 0                                     | 10.8                      | 120                     | 57.6                 | 1                              | 0.253                 | 0                     |
| Select Borrow | 36                           | 0                           | 17.5          | 0                                    | 0                                     | 10.8                      | 125                     | 62.6                 | 1                              | 0.253                 | 0                     |
| Gravel Borrow | 38                           | 0                           | 17.5          | 0                                    | 0                                     | 10.8                      | 130                     | 67.6                 | 1                              | 0.253                 | 0                     |
|               |                              |                             |               |                                      |                                       |                           |                         |                      |                                |                       |                       |
|               |                              |                             |               |                                      |                                       |                           |                         |                      |                                |                       |                       |
|               |                              |                             |               |                                      |                                       |                           |                         |                      |                                |                       |                       |
|               |                              |                             |               |                                      |                                       |                           |                         |                      |                                |                       |                       |
|               |                              |                             |               |                                      |                                       |                           |                         |                      |                                |                       |                       |

#### **Lateral Earth Pressures**

#### Output

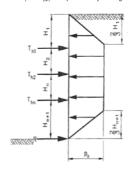
|               |                | Active                  |                          |                |                              | Pa                            | ssive                         |                                |                | At Rest                 |              |                             | EP Trapezoid                           |                 | <u>s</u>                 | eismic                    |          | Seismic Pressure -       |
|---------------|----------------|-------------------------|--------------------------|----------------|------------------------------|-------------------------------|-------------------------------|--------------------------------|----------------|-------------------------|--------------|-----------------------------|--|-----------------|--------------------------|---------------------------|----------|--------------------------|
| Material      | K <sub>a</sub> | γ <sub>a</sub><br>(pcf) | γ' <sub>a</sub><br>(pcf) | K <sub>p</sub> | γ <sub>p(all)</sub><br>(pcf) | γ' <sub>p(all)</sub><br>(pcf) | γ <sub>pe(all)</sub><br>(pcf) | γ' <sub>pe(all)</sub><br>(pcf) | K <sub>o</sub> | γ <sub>o</sub><br>(pcf) | γ'。<br>(pcf) | Single Tieback<br>(psf * H) | Mult. Tiebacks <sup>1</sup> , <b>X</b> | K <sub>ae</sub> | γ <sub>ae</sub><br>(pcf) | γ' <sub>ae</sub><br>(pcf) | $K_{pe}$ | Rectangular<br>(psf * H) |
| Common Borrow | 0.49           | 58.74                   | 28.19                    | 2.68           | 321.39                       | 154.27                        | 571.32                        | 274.23                         | 0.47           | 56.41                   | 27.08        | 58.74                       | 58.74                                  | 1.04            | 125.11                   | 60.05                     | 4.76     | 33.19                    |
| Select Borrow | 0.42           | 52.25                   | 26.17                    | 3.07           | 383.26                       | 191.94                        | 801.00                        | 401.14                         | 0.41           | 51.53                   | 25.80        | 52.25                       | 52.25                                  | 0.76            | 95.22                    | 47.68                     | 6.41     | 21.48                    |
| Gravel Borrow | 0.39           | 50.18                   | 26.09                    | 3.29           | 427.31                       | 222.20                        | 978.48                        | 508.81                         | 0.38           | 49.96                   | 25.98        | 50.18                       | 50.18                                  | 0.69            | 89.66                    | 46.62                     | 7.53     | 19.74                    |
|               |                |                         |                          |                |                              |                               |                               |                                |                |                         |              |                             |  |                 |                          |                           |          |                          |
|               |                |                         |                          |                |                              |                               |                               |                                |                |                         |              |                             |  |                 |                          |                           |          |                          |
|               |                |                         |                          |                |                              |                               |                               |                                |                |                         |              |                             |  |                 |                          |                           |          |                          |
|               |                |                         |                          |                |                              |                               |                               |                                |                |                         |              |                             |  |                 |                          |                           |          |                          |
|               |                |                         |                          |                |                              |                               |                               |                                |                |                         |              |                             |  |                 |                          |                           |          |                          |
|               |                |                         |                          |                |                              |                               |                               |                                |                |                         |              |                             |  |                 |                          |                           |          |                          |
|               |                |                         |                          |                |                              |                               |                               |                                |                |                         |              |                             |  |                 |                          |                           |          |                          |
|               |                |                         |                          |                |                              |                               |                               |                                |                |                         |              |                             |  |                 |                          |                           |          |                          |
|               |                |                         |                          |                |                              |                               |                               |                                |                |                         |              |                             |  |                 |                          |                           |          |                          |
|               |                |                         |                          |                |                              |                               |                               |                                |                |                         |              |                             |  |                 |                          |                           |          |                          |
|               |                |                         |                          |                |                              |                               |                               |                                |                |                         |              |                             |  |                 |                          |                           |          |                          |
|               |                |                         |                          |                |                              |                               |                               |                                |                |                         |              |                             |  |                 |                          |                           |          |                          |
|               |                |                         |                          |                |                              |                               |                               |                                |                |                         |              |                             |  |                 |                          |                           |          |                          |
|               |                |                         |                          |                |                              |                               |                               |                                |                |                         |              |                             |  |                 |                          |                           |          |                          |
|               |                |                         |                          |                |                              |                               |                               |                                |                |                         |              |                             |  |                 |                          |                           |          |                          |
|               |                |                         |                          |                |                              |                               |                               |                                |                |                         |              |                             |  |                 |                          |                           |          |                          |

Notes:

1 "X" to be used in the following equation:

$$\frac{X \cdot H^2}{1.5H - 0.5H_1 - 0.5H_{n+1}}$$

where  $H_1$  and  $H_{n+1}$  are represented by this diagram:





Recommended Lateral Earth Pressures

|               |    | Sliding Friction Coefficient |          |  |  |  |  |
|---------------|----|------------------------------|----------|--|--|--|--|
| Soil Type     | ان | Cast-In-Place                | Precast  |  |  |  |  |
| Soil Type     | φ' | Concrete                     | Concrete |  |  |  |  |
| Common Borrow | 32 | 0.62                         | 0.50     |  |  |  |  |
| Select Borrow | 36 | 0.73                         | 0.58     |  |  |  |  |
| Gravel Borrow | 38 | 0.78                         | 0.63     |  |  |  |  |
| ESU 1B        | 36 | 0.73                         | 0.58     |  |  |  |  |

Notes:

Sliding coefficients calculated according to AASHTO Equation 10.6.3.4-2

#### **Cast-In-Place Concrete Coefficient of Friction:**

Coefficient of friction = 1.0\*tan(Phi')

#### **Precast Concrete Coefficient of Friction:**

Coefficient of friction = 0.8\*tan(Phi')

#### **AASHTO 10.6.3.4**:

$$R_{\tau} = CV \tan \phi_f \qquad (10.6.3.4-2)$$

for which:

C = 1.0 for concrete cast against soil

= 0.8 for precast concrete footing

where:

 $\phi_f$  = internal friction angle of drained soil

(degrees)

V = total vertical force (kips)

#### LRFD Foundation Design

#### Spreadsheet Reference Section 10.6.3.1.2 of The 2014 AASHTO LRFD Bridge Design Specifications

| Date/Time:    | 1/11/22 10:24 AM                           |
|---------------|--|
| Project Name: | I-405/Renton to Bellevue Corridor Widening |
| Project No.:  | 00180-366-01                               |

| Foundation Soil Cond                      | litions |
|---|---------|
| Unit Weight, γ (pcf)                      | 120     |
| Friction angle, Φ (degrees)               | 36      |
| Friction angle, Φ (rad)                   | 0.628   |
| Cohesion, C (psf)                         | 0       |
| Embedment, D <sub>f</sub> (ft)            | 0       |
| Depth to Groundwater, D <sub>w</sub> (ft) | 10.9    |
| Footing Length, L (ft)                    | 85      |
| Footing Width, B (ft)                     | 1       |
| Poissons Ration, v                        | 0.35    |
| Young's Modulus, E <sub>s</sub> (ksf)     | 725     |

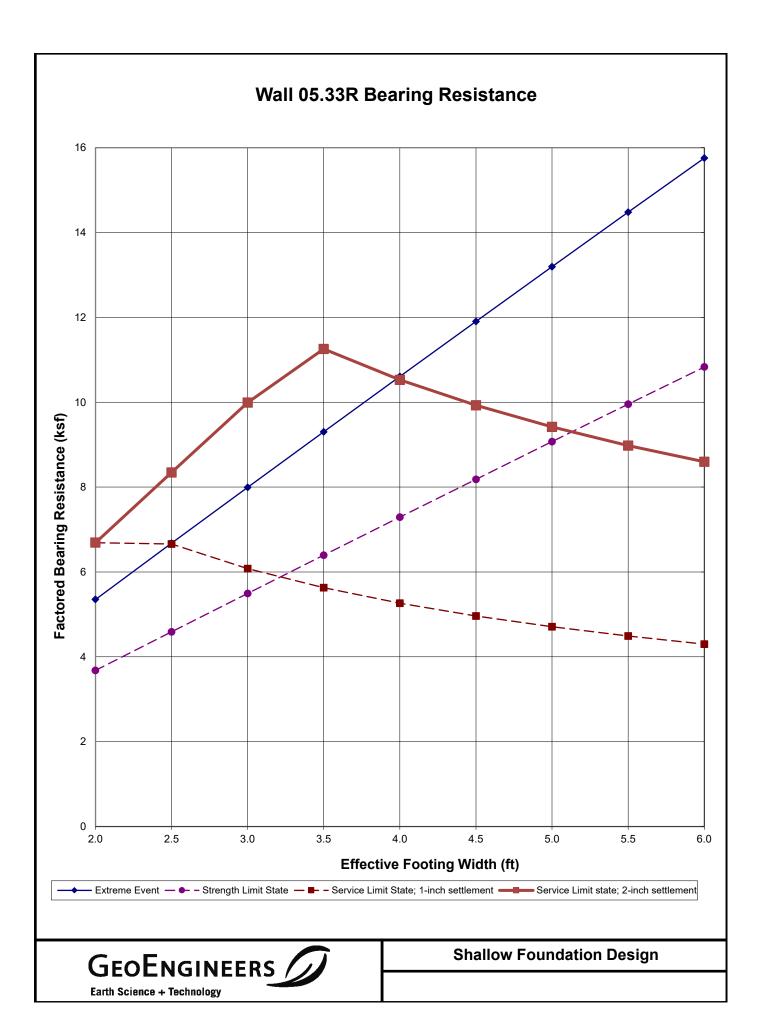
(ESU 1B, Dense SM)

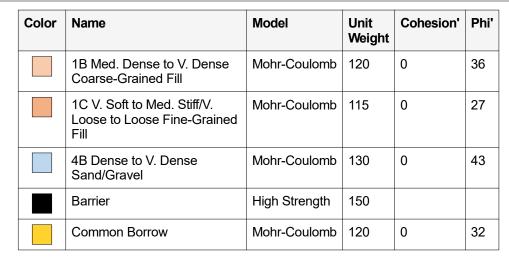
(approx wall length)

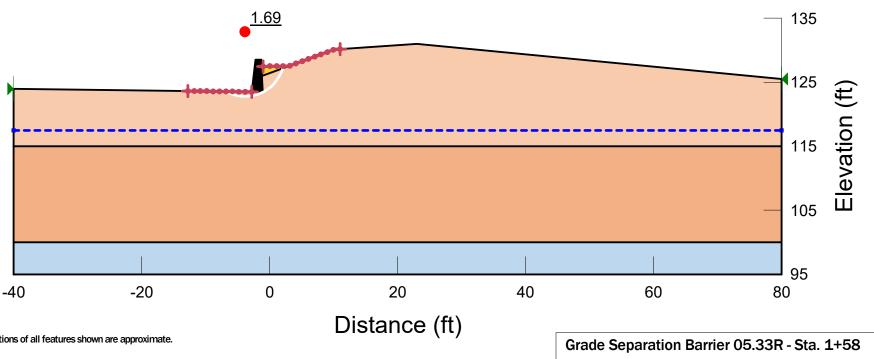
| Bearing Capacity Factors |    |  |  |  |  |  |  |  |  |
|--------------------------|----|--|--|--|--|--|--|--|--|
| $N_{\gamma}$             | 56 |  |  |  |  |  |  |  |  |
| N <sub>c</sub>           | 51 |  |  |  |  |  |  |  |  |
| $N_q$                    | 38 |  |  |  |  |  |  |  |  |

|                            | water Depth Factors Shape Factors Unfactored |                  | Extreme Event Resistance | Working Bearing Resistance | Deflection from Elastic<br>Settlement Spreadsheet | Deflection from Elastic<br>Settlement Spreadsheet |   |   |               |               |
|----------------------------|--|------------------|--------------------------|----------------------------|---|---|---|---|---------------|---------------|
| Effective Footing Width, B | Cwq  | C <sub>w-y</sub> | <u>Sc</u>                | <u>S</u> <sub>Y</sub>      | <u>Sq</u>   | Bearing<br>Resistance                             | Resistance Factor (0.8) for gravity and semigravity walls (Section 11.5.8 AASHTO) | Resistance Factor (0.55) for gravity and semigravity walls (Table 11.5.7-1) | 1" Deflection | 2" Deflection |
| (ft)                       |  |                  |                          |                            |   | (ksf)   | (ksf)   | (ksf)   | (ksf)         | (ksf)         |
| 2.0                        | 1.0  | 1.0              | 1.02                     | 0.99                       | 1.02  | 6.7   | 5.4   | 3.7   | 6.7           | 6.7           |
| 2.5                        | 1.0  | 1.0              | 1.02                     | 0.99                       | 1.02  | 8.3   | 6.7   | 4.6   | 6.7           | 8.3           |
| 3.0                        | 1.0  | 1.0              | 1.03                     | 0.99                       | 1.03  | 10.0  | 8.0   | 5.5   | 6.1           | 10.0          |
| 3.5                        | 1.0  | 1.0              | 1.03                     | 0.98                       | 1.03  | 11.6  | 9.3   | 6.4   | 5.6           | 11.3          |
| 4.0                        | 1.0  | 1.0              | 1.04                     | 0.98                       | 1.03  | 13.3  | 10.6  | 7.3   | 5.3           | 10.5          |
| 4.5                        | 1.0  | 1.0              | 1.04                     | 0.98                       | 1.04  | 14.9  | 11.9  | 8.2   | 5.0           | 9.9           |
| 5.0                        | 1.0  | 1.0              | 1.04                     | 0.98                       | 1.04  | 16.5  | 13.2  | 9.1   | 4.7           | 9.4           |
| 5.5                        | 1.0  | 1.0              | 1.05                     | 0.97                       | 1.05  | 18.1  | 14.5  | 10.0  | 4.5           | 9.0           |
| 6.0                        | 1.0  | 1.0              | 1.05                     | 0.97                       | 1.05  | 19.7  | 15.8  | 10.8  | 4.3           | 8.6           |
|                            |  |                  |                          |                            |   |   |   |   |               |               |
|                            |  |                  |                          |                            |   |   |   |   |               |               |

Note: Depth and inclination modifier were taken as 1 because the load is applied axially and during construction the soils above the footing are to be excavated.







1. The locations of all features shown are approximate.

- 2. This drawing is for information purposes. It is intended to assist in showing features discussed in an attached document
- 3. GeoEngineers, Inc. cannot guarantee the accuracy and context of electronic files. The master files is stored by GeoEngineers, Inc. and will serve as the official record of this communication

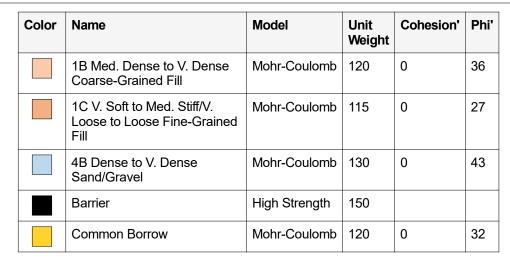
**Static Global Stability (Spencer)** 

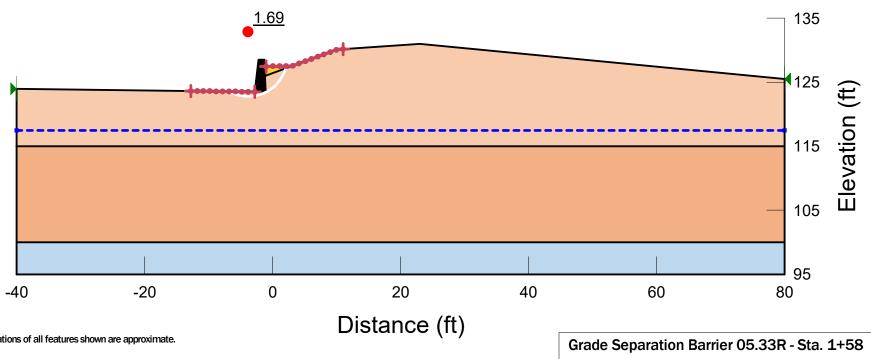
I-405/ Renton to Bellevue Corridor Widening King County, Washington



000180-366-01 Date Exported: 08/06/21

Notes:





1. The locations of all features shown are approximate.

Notes:

000180-366-01 Date Exported: 08/06/21

2. This drawing is for information purposes. It is intended to assist in showing features discussed in an attached document

3. GeoEngineers, Inc. cannot guarantee the accuracy and context of electronic files. The master files is stored by GeoEngineers, Inc. and will serve as the official record of this communication

Static Global Stability (M-P)

I-405/ Renton to Bellevue Corridor Widening King County, Washington









In Association with

# **Appendix D** Wall 05.55L Calculations







In Association with

### APPENDIX D - WALL 05.55L CALCULATIONS

#### General

This appendix presents geotechnical calculations for Wall 05.55L including:

- **ESU Soil Properties**
- Seismic Hazard Analysis
- Lateral Earth Pressures
- Coefficients of Friction for Sliding
- Bearing Resistance and Elastic Settlement
- Global Stability

#### **ESU Soil Properties**

Design soil properties were developed in accordance with the Project GDM, AASHTO LRFD, and FHWA. We calculated the average, geometric mean, and standard deviation within each ESU. We verified the reliability of the ESU data set by comparing the COV of each calculated geometric mean value to measured and interpreted values presented in Sabatini et al. (2002) Table 52.

A detailed description of the soil property development is presented in Section 7.1 of this geotechnical engineering report. Supporting calculations are provided in this appendix.

#### **Seismic Hazard Analysis**

We selected a representative site class for the wall from the site class evaluation of nearby borings. We evaluated the site class of each boring using a spreadsheet developed by GeoEngineers in accordance with AASHTO LRFD Section 3.10.3.1.

We developed seismic design parameters using the WSDOT Bridge Engineering Software BEToolbox/BridgeLink in accordance with the WSDOT BDM based on the projected ground motion at the project site that has a 7 percent (SEE) probability of exceedance in a 75-year period (approximate 1,000-year return period).

We used a mean earthquake magnitude at the PGA period is 7.0 for the SEE based on the Hart Crowser seismic design report "I-405 R2B Segment 1a Site-Specific Hazard Analysis RFU," dated March 25, 2021.

The soil samples at Wall 05.55L are unsaturated and calculated N160 values are greater than 25 blows per foot. By inspection, liquefaction potential is low. We confirmed our low liquefaction risk assumptions by evaluating liquefaction potential using a spreadsheet developed by GeoEngineers in accordance with Project GDM Chapter 6. The FSs against liquefaction at Wall 05.55L were greater than 1.2 for all soil analyzed; per Project GDM Section 6-4.2.3, soils with liquefaction potential are defined as those with FSs against liquefaction less than 1.2.

Detailed descriptions of our seismic hazard analysis methodology and the results are presented in Section 7.2 and Section 8.1, respectively, of this report. Site class calculations, WSDOT BDM software outputs, and liquefaction analyses are provided in this appendix.

#### **Lateral Earth Pressures**

Active lateral pressure coefficients and active lateral earth pressures for imported common borrow, select borrow, and gravel borrow were calculated in accordance with AASHTO LRFD Sections 3.11.5 and 11.6.5.3 using the proposed horizontal backslope behind the wall, and the 3.7H:1V foreslope in front of the wall. Lateral earth pressures shall be applied using a triangular distribution. An LRFD load factor of 1.5 shall be applied to the active earth pressures in accordance with AASHTO LRFD Table 3.4.1-2. Due to negligible embedment of the wall and a foreslope condition, passive lateral earth pressures shall be ignored.

Surcharge loads, such as traffic loading, and appropriate load factors shall be applied to evaluate the wall stability. All surcharges shall apply load factors in accordance with AASHTO LRFD Tables 3.4.1-1 and 3.4.1-2.

A detailed description of our analysis methodology and the calculated results are presented in Section 7.3 and Section 8.2, respectively. Supporting calculations are provided in this appendix.







#### In Association with

#### Coefficients of Friction for Sliding

Coefficients of friction for sliding on surficial native soils, common borrow, select borrow, and gravel borrow were calculated using AASHTO LRFD equation 10.6.3.4-2.

A detailed description of our analysis methodology and the results are presented in Section 7.4 and Section 8.3, respectively, of this report. Supporting calculations are provided in this appendix.

#### Bearing Resistance and Elastic Settlement

We estimated the bearing resistance and elastic settlement of the wall using a spreadsheet developed by GeoEngineers in accordance with AASHTO LRFD Section 10.6.3. We estimated elastic settlement from procedures outlined in AASHTO LRFD and Section 10.6.2.4. Sliding and overturning are being evaluated by the design-build team's wall designers and will be submitted under separate cover.

A detailed description of our analysis methodology and the results are presented in Section 7.5 and Section 8.4, respectively, of this report. Supporting calculations are provided in this appendix.

#### Global Stability

We performed global stability analyses for the following critical design section:

Section Sta. 1+50 – Maximum overall wall height

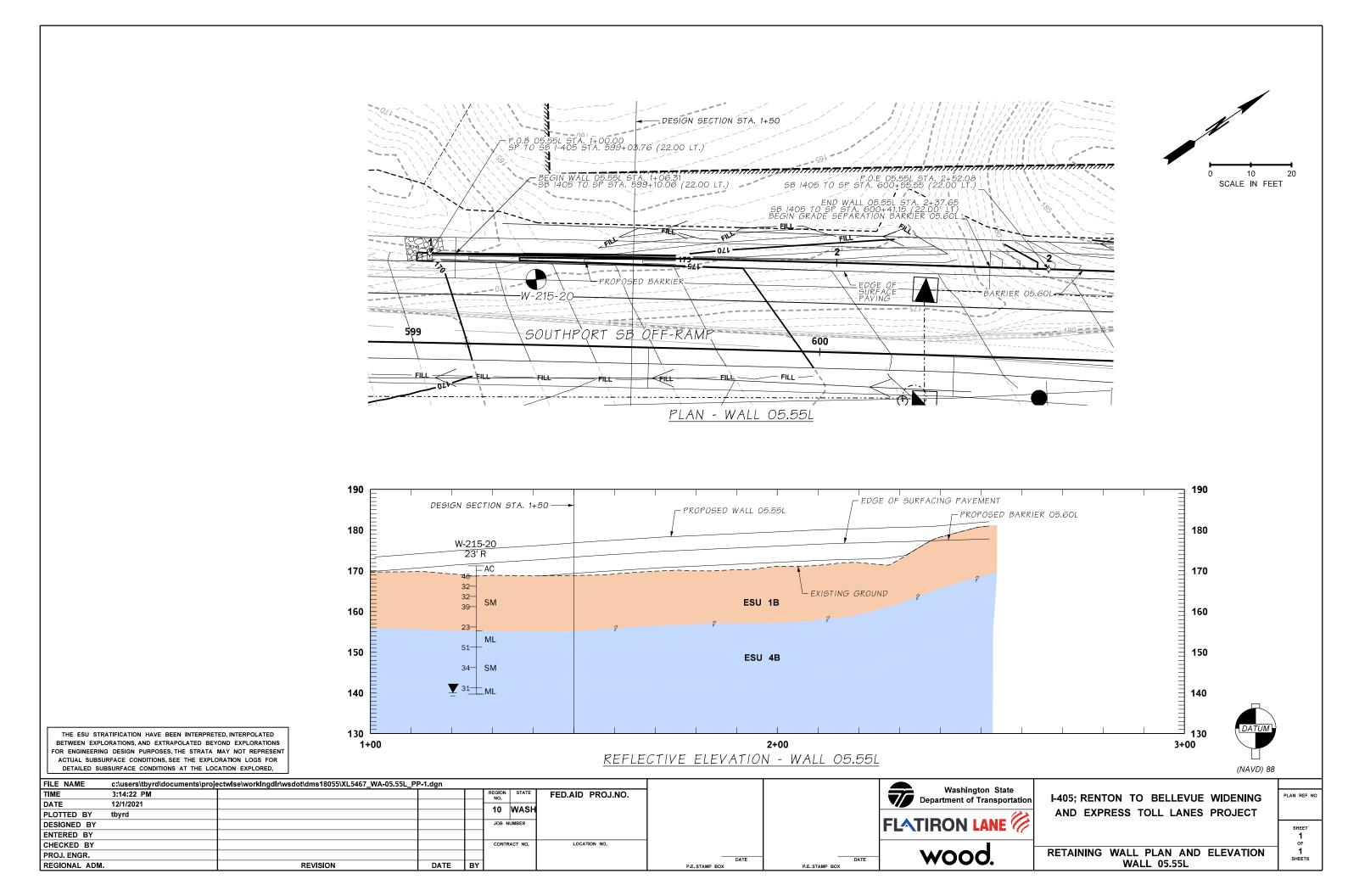
Global stability was evaluated using limit equilibrium analysis methodology outlined in the Project GDM using the computer design software Slope/W (Geo Slope International, Ltd. 2020). We analyzed FSs using Spencer's method and Morgenstern-Price for a circular failure surface.

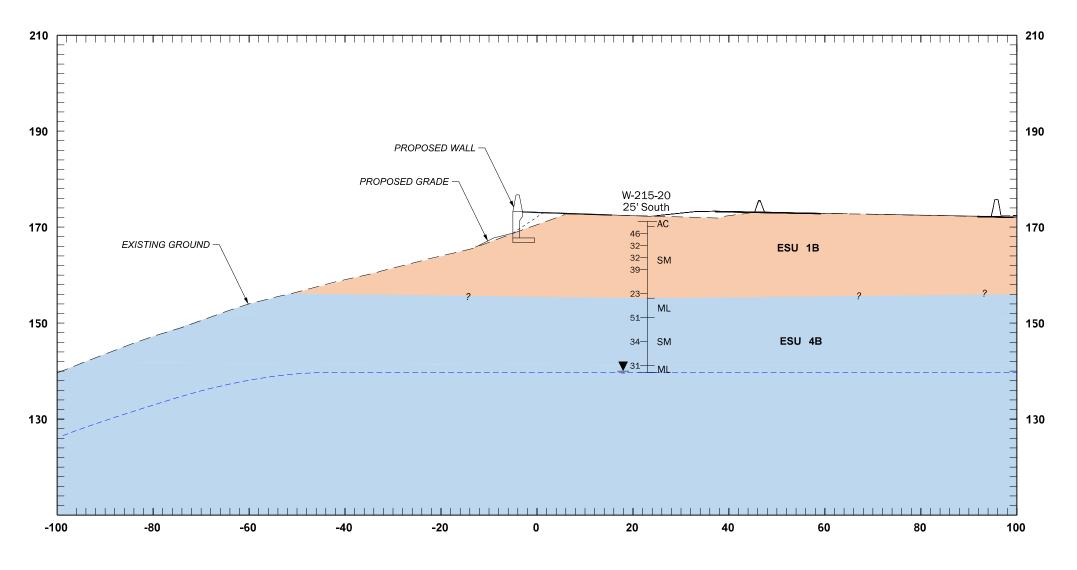
A traffic surcharge of 250 psf was applied at the top of the wall for the static global stability analysis.

Based on criteria outlined in the Hart Crowser RFU geotechnical letter "Design Requirements and Geotechnical Assessment of Retaining Walls" dated January 26, 2021, the MADTL for Wall 05.55L is less than the distance between the wall and the travel lane, and therefore additional improvements are not required since seismic failure of the wall will not severely impact the traveled way or compromise the life safety of the public. Accordingly, we did not analyze seismic stability of Wall 05.55L.

Detailed descriptions of our global stability analysis methodology and the results of our analyses are presented in Section 7.8 and Section 8.6, respectively, of this report. Global stability models showing FS for critical failures at the design section are provided in this appendix. Slope/W reports are provided in Appendix J.

# Appendix D.1 - Wall 05.55L Plan, Profile and Sections





WALL 05.55L STATION 1+50

THE ESU STRATIFICATION HAVE BEEN INTERPRETED, INTERPOLATED BETWEEN EXPLORATIONS, AND EXTRAPOLATED BEYOND EXPLORATIONS FOR ENGINEERING DESIGN PURPOSES, THE STRATA MAY NOT REPRESENT ACTUAL SUBSURFACE CONDITIONS, SEE THE EXPLORATION LOGS FOR DETAILED SUBSURFACE CONDITIONS AT THE LOCATION EXPLORED.

| FILE NAME    | c:\users\tbyra\aocuments\proj | ectwise\workingair\wsaot\ams18055\XL5467_WA-05.55L_X | (S.agn |    |              |                  |                |                | 14/2 - 12/2 - 14 - 12 - 04 - 4 -               |                                    |             |   |
|--------------|-------------------------------|--|--------|----|--------------|------------------|----------------|----------------|--|------------------------------------|-------------|---|
| TIME         | 3:17:52 PM                    |  |        |    | REGION STATE | FED.AID PROJ.NO. |                |                | Washington State  Department of Transportation | I-405: RENTON TO BELLEVUE WIDENING | PLAN REF NO | 1 |
| DATE         | 12/1/2021                     |  |        |    | 10 WASH      | <u> </u>         |                |                | Department of Transportation                   | •                                  |             | ı |
| PLOTTED BY   | tbyrd                         |  |        |    | I IU WASI    | ]                |                |                |  | AND EXPRESS TOLL LANES PROJECT     |             |   |
| DESIGNED BY  |                               |  |        |    | JOB NUMBER   |                  |                |                | FLATIRON LANE 🥢                                |                                    | SHEET       | 1 |
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| CHECKED BY   |                               |  |        |    | CONTRACT NO. | LOCATION NO.     |                |                |  |                                    | OF          | ı |
| PROJ. ENGR.  |                               |  |        |    | 1            |                  | DATE           | DATE           | WOOD.  | WALL 05.55L                        | 1<br>SHEETS |   |
| REGIONAL ADM |                               | REVISION   | DATE   | BY |              |                  | P.E. STAMP BOX | P.E. STAMP BOX | <b>******</b>                                  | DESIGN SECTION AT STA. 1+50        | 1           | Т |

# Appendix D.2 - Wall 05.55L ESU Soil Property Calculations

05.55L Soil Properties Summary

| ESU  | Description                                       | Total No. of<br>Samples <sup>b</sup> | USCS <sup>c</sup> | Fines <sup>d</sup><br>(%) | Plasticity<br>Index,<br>PI <sup>e</sup> (%) | Raw N<br>(bpf) | N <sub>e</sub> |                  | (N <sub>1</sub> | ) <sub>60</sub> <sup>f</sup><br>pf) | Tota<br>Weigh |                  | Effective<br>Angle, φ | h (doa)          | Softened | Effective<br>c' <sup>j</sup> (psf) |       | Residual Shear<br>Strength, Sr (psf) |       | ed Shear<br>, Su (psf) |
|------|---|--------------------------------------|-------------------|---------------------------|---|----------------|----------------|------------------|-----------------|-------------------------------------|---------------|------------------|-----------------------|------------------|----------|------------------------------------|-------|--------------------------------------|-------|------------------------|
|      |   |                                      |                   | Value                     | Value                                       | Value          | Value          | COV <sup>a</sup> | Value           | COV <sup>a</sup>                    | Value         | COV <sup>a</sup> | Value                 | COV <sup>a</sup> | Value    | Value                              | Value | Value                                | Value | COV                    |
| I IK | Medium Dense to Very Dense<br>Coarse-Grained Fill | 4                                    | SM                | 26                        | -   | 37             | 49             | 16%              | 66              | 27%                                 | 130           | 0%               | 40                    | 3%               | -        | -                                  | -     | -                                    | -     | -                      |
| 4B   | Dense to Very Dense Sand/Gravel                   | 4                                    | SM                | 40                        | -   | 33             | 54             | 33%              | 51              | 33%                                 | 120           | 10%              | 43                    | 3%               | 1        | -                                  | -     | -                                    | -     | -                      |
|      |   |                                      |                   |                           |   |                |                |                  |                 |                                     |               |                  |                       |                  |          |                                    |       |                                      |       |                        |

#### Notes:

- a. Coefficient of Variation (COV) percentage calculated to verify the variability and reliability of sample data within ESU (WSDOT GDM Section 5.11.2 (2015)). Calculated COV percentage compared to ranges presented in Table 52 (Sabatini et al. 2002) (below).
- b. Number of samples excludes outliers.
- c. Predominant USCS classification of all samples in ESU. Sandstone, where encountered, denoted as (SS).
- d. Fines content percentage calculated as the geometric mean of all samples, whose values were determined through lab testing or estimated from field classification.
- e. For coarse-grained ESUs, the plasticity index was estimated from the fine-grained portion of the soil. For fine-grained ESUs, if lab data is limited, the plasticity index may not be representative of the overall soil unit.
- f. Corrected blow counts ( $N_{60}$  and ( $N_{1}$ )<sub>60</sub>) were calculated following WSDOT GDM Section 5.5 (2015).
- g. Individual sample unit weights were correlated using CALTRANS Geotechnical Manual (2014), verified with applicable ranges presented in Codotu (2001), as specified in WOOD SPM. The geometric mean of the unit weights was rounded to the nearest 5pcf, as specified in WOOD SPM. Unit weight data variability and quality were evaluated by comparing the calculated COV percentage to the applicable Sabatini range.
- h. Design friction angles were selected by considering fines content. Friction angle data variability and quality were evaluated by comparing the calculated COV percentage to the applicable Sabatini range.
- i. Where applicable, fully softened friction angle was estimated following WSDOT GDM, Figure 5-7 (After Stark and Hussain, 2013).
- j. Where applicable, effective cohesion was calculated using Equations 6 through 8 in the WOOD Geotechnical SPM.
- k. Where applicable, residual friction angle (to be used for slope stability evaluation) was estimated following WSDOT GDM, Figure 5 -5 (After NAVFAC, 1971).

| Measured or interpreted parameter value               | Coefficient of Variation, V<br>(%) |  |  |  |  |  |
|---|------------------------------------|--|--|--|--|--|
| Unit weight, γ  | 3 to 7 %                           |  |  |  |  |  |
| Buoyant unit weight, γ <sub>b</sub>                   | 0 to 10 %                          |  |  |  |  |  |
| Effective stress friction angle, φ'                   | 2 to 13 %                          |  |  |  |  |  |
| Undrained shear strength, su                          | 13 to 40 %                         |  |  |  |  |  |
| Undrained strength ratio $(s_u/\sigma_v')$            | 5 to 15 %                          |  |  |  |  |  |
| Compression index, C <sub>c</sub>                     | 10 to 37 %                         |  |  |  |  |  |
| Preconsolidation stress, $\sigma_p'$                  | 10 to 35 %                         |  |  |  |  |  |
| Hydraulic conductivity of saturated clay, k           | 68 to 90 %                         |  |  |  |  |  |
| Hydraulic conductivity of partly-saturated clay, k    | 130 to 240 %                       |  |  |  |  |  |
| Coefficient of consolidation, c <sub>v</sub>          | 33 to 68 %                         |  |  |  |  |  |
| Standard penetration blowcount, N                     | 15 to 45 %                         |  |  |  |  |  |
| Electric cone penetration test, q <sub>c</sub>        | 5 to 15 %                          |  |  |  |  |  |
| Mechanical cone penetration test, q <sub>c</sub>      | 15 to 37 %                         |  |  |  |  |  |
| Vane shear test undrained strength, s <sub>uVST</sub> | 10 to 20 %                         |  |  |  |  |  |

Source: Table 52 (Sabatini et al. 2002)

|           | ESU Name: |                 | ESU 1B - Medium Dense to Very Dense Coarse-Grained Fill |    |                          |                       |                      |                     |             |             |  |  |  |  |
|-----------|-----------|-----------------|---|----|--------------------------|-----------------------|----------------------|---------------------|-------------|-------------|--|--|--|--|
|           | N         | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub>                         | %F | PI <sup>3</sup><br>(Lab) | φ'<br>(high)<br>(deg) | φ'<br>(low)<br>(deg) | Sat. Unit<br>Weight | Su<br>(psf) | Sr<br>(psf) |  |  |  |  |
| GeoMean:  | 37        | 49              | 66  | 26 | -                        | 44                    | 39                   | 130                 | -           | -           |  |  |  |  |
| Average:  | 37        | 50              | 67  | 26 | -                        | 44                    | 39                   | 130                 | -           | -           |  |  |  |  |
| St. Dev.: | 6.7       | 8.0             | 18.3  | -  | -                        | 1.1                   | 1.1                  | 0.0                 | -           | =           |  |  |  |  |
| cov:      | 0.18      | 0.16            | 0.27  | -  | -                        | 0.02                  | 0.03                 | 0.00                | -           | -           |  |  |  |  |

| Boring   | Elevation | N  | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub> | %F <sup>4</sup> | PI<br>(Lab) | φ'<br>(high)<br>(deg) | φ'<br>(low)<br>(deg) | Sat. Unit<br>Weight | Su<br>(psf) | Sr <sup>5</sup><br>(psf) | USCS | Explanation for Sample Removal |
|----------|-----------|----|-----------------|---------------------------------|-----------------|-------------|-----------------------|----------------------|---------------------|-------------|--------------------------|------|--------------------------------|
| W-215-20 | 168.7     | 46 | 58              | 94                              | 30              | -           | 45                    | 40                   | 130                 | -           | -                        | SM   |                                |
| W-215-20 | 166.2     | 32 | 43              | 59                              | 27              | -           | 43                    | 38                   | 130                 | -           | -                        | SM   |                                |
| W-215-20 | 163.7     | 32 | 43              | 53                              | 23              | -           | 43                    | 38                   | 130                 | -           | -                        | SM   |                                |
| W-215-20 | 161.2     | 39 | 55              | 64                              | 23              | -           | 43                    | 38                   | 130                 | -           | -                        | SM   |                                |
|          |           |    |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |    |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |    |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |    |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |    |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |    |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |    |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |    |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |    |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |    |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |    |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |    |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |    |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |    |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |    |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |    |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |    |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
| Notes:   | -         | ļ  | 1               | 1                               | 1               |             |                       | ļ                    | 1                   |             |                          |      |                                |

- ${\bf 1.} \ Highlighted \ cells \ in \ yellow \ if \ shown \ represent \ samples \ that \ were \ removed \ as \ outliers.$
- 2. Friction angle, unit weight, and corrected blow count values were correlated using specified methodology in the WOOD Geotechnical SPM. Where applicable, undrained shear strength of fine grained ESUs were determined using Equation 9 in the WOOD Geotechnical SPM.
- 3. Fines content percentages determined through laboratory testing are highlighted in orange if shown. Non-highlighted values have been estimated from sample field classifications, applying the fines content of a lab tested sample with similar properties or using the average of two tested samples.
- 4. Where applicable, residual strength is calculated using the existing relationships and weighting scheme per the GDM (section 6-2.2) to determine residual strengths for samples with (N1)60cs less than or equal to 20. Per Kramer 2008, samples that triggered liquefaction (FoS<1.2) but also has an (N1)60cs>20, uses the residual strength value for a soil with (N1)60cs=20, effectively capping the residual strength calculation at (N1)60cs=20.

#### 1. Check N160 COV is between 15 and 45%

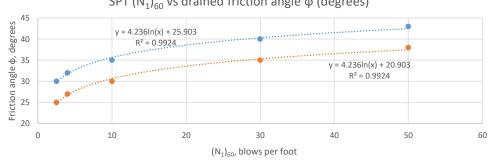
| Selected Design N160:           | 66   |
|---------------------------------|------|
| Coefficient of Variation (COV): | 0.27 |

<sup>\* 15</sup> and 45% come from GEC 5 Sabatini (2002)

#### 2. Check Phi' is between 2 to 13%

| (N <sub>1</sub> ) <sub>60</sub> (blows per foot) | Friction angle φ<br>(degrees) |  |  |  |  |  |
|--|-------------------------------|--|--|--|--|--|
| 2.5  | 25                            |  |  |  |  |  |
| 2.5  | 30                            |  |  |  |  |  |
| 4  | 27                            |  |  |  |  |  |
| 4  | 32                            |  |  |  |  |  |
| 10   | 30                            |  |  |  |  |  |
| 10   | 35                            |  |  |  |  |  |
| 30   | 35                            |  |  |  |  |  |
| 30   | 40                            |  |  |  |  |  |
| 50   | 38                            |  |  |  |  |  |
| 50   | 43                            |  |  |  |  |  |





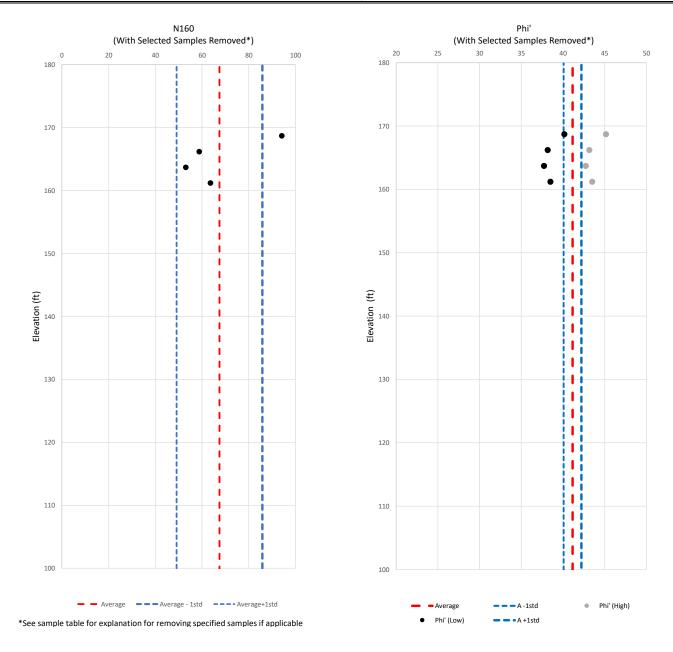
|          | φ (high) | φ (low) | ф (avg) | φ' cov |
|----------|----------|---------|---------|--------|
| GeoMean: | 44       | 39      | 41      | 0.03   |

| Selected Design Phi' (deg): | 40                 |   |
|-----------------------------|--------------------|---|
| Notes on Selection:         | The fines content  | test data is representative of the ESU. The estimated fines content is 26% (geomean). The friction angle is interpolated based on |
| Notes on Selection.         | fines content (phi | (high) at 5% fines, and phi' (low) at 30% fines).   |

| Pick Representative USCS:        | SM  | *Using Predominant USCS Classification  |
|----------------------------------|-----|---|
| Pick Representative Unit Weight: | 130 |   |
| Notes on Selection:              | •   | unit weights were correlated using CALTRANS Geotechnical Manual (2014), verified with applicable ranges presented in Codotu d in WOOD SPM. The geometric mean of the unit weights was rounded to the nearest 5pcf, as specified in WOOD SPM. Data set |

<sup>\*</sup> Phi' Developed from WSDOT Correlation

<sup>\* 2</sup> to 13% comes from GEC 5 Sabatini (2002)



|          | ESU Name: |                 | ESU 4B - Dense to Very Dense Sand/Gravel |    |             |                       |                      |                     |             |             |
|----------|-----------|-----------------|--|----|-------------|-----------------------|----------------------|---------------------|-------------|-------------|
|          | N         | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub>          | %F | PI<br>(Lab) | ф'<br>(high)<br>(deg) | ф'<br>(low)<br>(deg) | Sat. Unit<br>Weight | Su<br>(psf) | Sr<br>(psf) |
| GeoMean  | 33        | 54              | 51                                       | 40 | -           | 43                    | 38                   | 120                 | -           | -           |
| Average  | 35        | 56              | 52                                       | 47 | -           | 43                    | 38                   | 120                 | -           | -           |
| St. Dev. | 11.8      | 18.4            | 17.5                                     | -  | =           | 1.3                   | 1.3                  | 11.5                | =           | -           |
| COV      | 0.34      | 0.33            | 0.33                                     | -  | =           | 0.03                  | 0.03                 | 0.10                | =           | -           |
|          |           |                 |  |    |             |                       |                      |                     |             |             |

|          |           | 0.5 1 | 0.55            | 0.55                            |                 |             | 0.05                  | 0.05                 | 0.10                |             |                          |      |                                |
|----------|-----------|-------|-----------------|---------------------------------|-----------------|-------------|-----------------------|----------------------|---------------------|-------------|--------------------------|------|--------------------------------|
| Boring   | Elevation | N     | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub> | %F <sup>3</sup> | PI<br>(Lab) | ф'<br>(high)<br>(deg) | ф'<br>(low)<br>(deg) | Sat. Unit<br>Weight | Su<br>(psf) | Sr <sup>4</sup><br>(psf) | USCS | Explanation for Sample Removal |
| W-215-20 | 156.2     | 23    | 36              | 38                              | 72              | -           | 41                    | 36                   | 110                 | -           | =                        | ML   |                                |
| W-215-20 | 151.2     | 51    | 81              | 78                              | 23              | -           | 44                    | 39                   | 130                 | -           | -                        | SM   |                                |
| W-215-20 | 146.2     | 34    | 54              | 49                              | 23              | -           | 42                    | 37                   | 130                 | -           | ÷                        | SM   |                                |
| W-215-20 | 141.2     | 31    | 52              | 45                              | 70              | -           | 42                    | 37                   | 110                 | -           | -                        | ML   |                                |
|          |           |       |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |       |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |       |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |       |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |       |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |       |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |       |                 |                                 |                 |             |                       |                      |                     |             | -                        |      |                                |
|          |           |       |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |       |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |       |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |       |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |       |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |       |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |       |                 |                                 |                 |             |                       |                      |                     | 1           | <del> </del>             |      |                                |
|          |           |       |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
|          |           |       |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |
| Notes:   |           |       |                 |                                 |                 |             |                       |                      |                     |             |                          |      |                                |

#### Notes:

- 1. Highlighted cells in yellow if shown represent samples that were removed as outliers.
- 2. Friction angle, unit weight, and corrected blow count values were correlated using specified methodology in the WOOD Geotechnical SPM. Where applicable, undrained shear strength of fine grained ESUs were determined using Equation 9 in the WOOD Geotechnical SPM.
- 3. Fines content percentages determined through laboratory testing are highlighted in orange if shown. Non-highlighted values have been estimated from sample field classifications, applying the fines content of a lab tested sample with similar properties or using the average of two tested samples
- 4. Where applicable, residual strength is calculated using the existing relationships and weighting scheme per the GDM (section 6-2.2) to determine residual strengths for samples with (N1)60cs less than or equal to 20. Per Kramer 2008, samples that triggered liquefaction (FoS<1.2) but also has an (N1)60cs>20, uses the residual strength value for a soil with (N1)60cs=20, effectively capping the residual strength calculation at (N1)60cs=20.

#### 1. Check N160 COV is between 15 and 45%

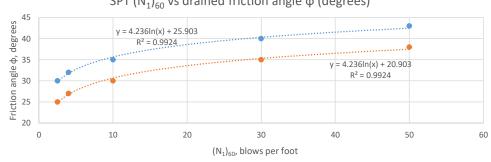
| Selected Design N160:           | 51   |
|---------------------------------|------|
| Coefficient of Variation (COV): | 0.33 |

<sup>\* 15</sup> and 45% come from GEC 5 Sabatini (2002)

#### 2. Check Phi' is between 2 to 13%

| (N <sub>1</sub> ) <sub>60</sub> (blows per foot) | Friction angle ф<br>(degrees) |  |  |  |
|--|-------------------------------|--|--|--|
| 2.5  | 25                            |  |  |  |
| 2.5  | 30                            |  |  |  |
| 4  | 27                            |  |  |  |
| 4  | 32                            |  |  |  |
| 10   | 30                            |  |  |  |
| 10   | 35                            |  |  |  |
| 30   | 35                            |  |  |  |
| 30   | 40                            |  |  |  |
| 50   | 38                            |  |  |  |
| 50   | 43                            |  |  |  |

WSDOT GDM Table 5-1 SPT  $(N_1)_{60}$  vs drained friction angle  $\varphi$  (degrees)



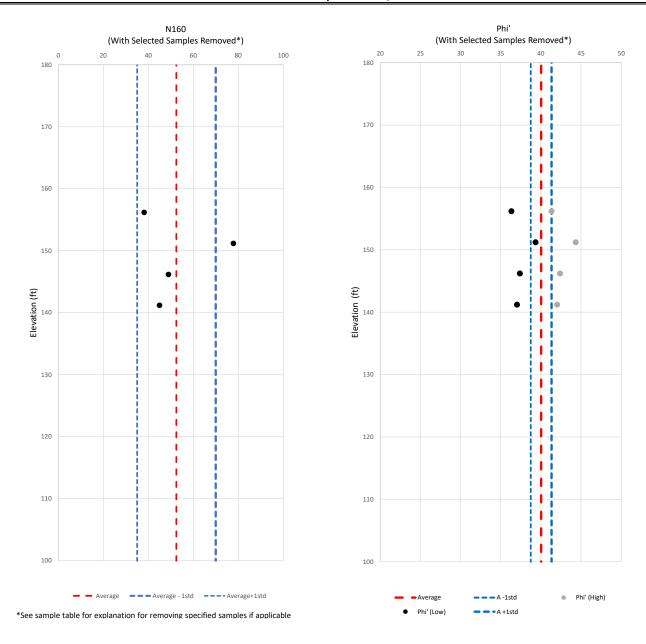
|          | φ (high) | ф (low) | ф (avg) | φ' cov |
|----------|----------|---------|---------|--------|
| GeoMean: | 43       | 38      | 40      | 0.03   |

| Selected Design Phi' (deg): | 43                |   |
|-----------------------------|-------------------|---|
| Notes on Selection:         | The estimated ged | omean fines content is 40% (geomean). The friction angle is taken as the upper bound and capped at 43 degrees for glacially |
| Notes on Selection.         | consolidated mate | erial with fines content less than 70%.   |

| Pick Representative USCS:        | SM  | *Using Predominant USCS Classification  |
|----------------------------------|-----|---|
| Pick Representative Unit Weight: | 120 |   |
| Notes on Selection:              | •   | unit weights were correlated using CALTRANS Geotechnical Manual (2014), verified with applicable ranges presented in Codotu d in WOOD SPM. The geometric mean of the unit weights was rounded to the nearest 5pcf, as specified in WOOD SPM. Data set |

<sup>\*</sup> Phi' Developed from WSDOT Correlation

<sup>\* 2</sup> to 13% comes from GEC 5 Sabatini (2002)



The coefficient of consolidation,  $c_{\nu_{t}}$ , should be determined from the results of onedimensional consolidation tests. The variability in laboratory determination of  $\emph{c}_{\emph{V}}$  results should be considered in the final selection of the value of  $c_V$  to be used for design.

Where evaluation of elastic settlement is critical to the design of the foundation or selection of the foundation type, in-situ methods such as PMT or *DMT* for evaluating the modulus of the stratum should be used.

ESU 1B Medium Dense to Very Dense Coarse-Grained Fill Es = 800 ksf = 5.56 ksiPoisson's Ratio = 0.40

A profile of  $\sigma_{\sigma'}$ , or OCR =  $\sigma_{\sigma'}/\sigma_{\sigma'}$ , with depth should be developed for the site for design applications where the stress history could have a significant impact on the design properties selected and the performance of the foundation. As with consolidation properties, an upper and lower bound profile should be developed based on laboratory tests and plotted with a profile based on particular in-situ test(s), if used. It is particularly important to accurately compute preconsolidation stress values for relatively shallow depths where in-situ effective stresses are low. An underestimation of the preconsolidation stress at shallow depths will result in overly conservative estimates of settlement for shallow soil layers.

Due to the numerous simplifying assumptions associated with conventional consolidation theory, on which the coefficient of consolidation is based, it is unlikely that even the best estimates of  $c_{\nu}$  from high-quality laboratory tests will result in predictions of time rate of settlement in the field that are significantly better than a prediction within one order of magnitude. In general, the in-situ value of  $c_{
u}$  is larger than the value measured in the laboratory test. Therefore, a rational approach is to select average, upper, and lower bound values for the appropriate stress range of concern for the design application. These values should be compared to values obtained from previous work performed in the same soil deposit. Under the best-case conditions, these values should be compared to values computed from measurements of excess pore pressures or settlement rates during construction of other structures.

 $\ensuremath{\textit{CPTu}}$  tests in which the pore pressure dissipation rate is measured may be used to estimate the field coefficient of consolidation.

For preliminary analyses or where accurate prediction of settlement is not critical. values obtained from correlations to index properties presented in Sabatini et al. (2002)

For preliminary design or for final design where the prediction of deformation is not critical to structure performance, i.e., the structure design can tolerate the potential inaccuracies inherent in the correlations. The elastic properties  $(E_{sr}, \nu)$  of a soil may be estimated from empirical relationships presented in Table C10.4.6.3-1.

The specific definition of  $E_s$  is not always consistent for the various correlations and methods of in-situ measurement. See Sabatini et al. (2002) for additional details regarding the definition and determination of  $E_s$ .

An alternative method of evaluating the equivalent elastic modulus using measured shear wave velocities is presented in Sabatini et al. (2002).

Table C10.4.6.3-1—Elastic Constants of Various Soils (modified after U.S. Department of the Navy, 1982; Bowles, 1988)

| Soil Type                         | Typical Range of Young's Modulus Values, $E_s$ (ksi) | Poisson's Ratio, $\nu$ (dim) |
|-----------------------------------|--|------------------------------|
| Clay:                             |  |                              |
| Soft sensitive                    |  |                              |
| Medium stiff to stiff             | 0.347-2.08   | 0.4–0.5 (undrained)          |
|                                   | 2.08-6.94  |                              |
| Very stiff                        | 6.94–13.89   |                              |
| Loess                             | 2.08-8.33  | 0.1-0.3                      |
| Silt                              | 0.278-2.78   | 0.3-0.35                     |
| Fine Sand:                        |  |                              |
| Loose                             | 1.11–1.67  | 0.25                         |
| Medium dense                      | 1.67-2.78  |                              |
| Dense                             | 2.78-4.17  |                              |
| Sand:                             |  |                              |
| Loose                             | 1.39-4.17  | 0.20-0.36                    |
| Medium dense                      | 4.17–6.94  |                              |
| Dense                             | 6.94–11.11   | 0.30-0.40                    |
| Gravel:                           |  |                              |
| Loose                             | 4.17–11.11   | 0.20-0.35                    |
| Medium dense                      | 11.11-13.89  |                              |
| Dense                             | 13.89–27.78  | 0.30-0.40                    |
| Estimating E <sub>s</sub> from Si | PT N Value   |                              |
|                                   | Soil Type  | $E_s$ (ksi)                  |
| Silts, sandy silts, sligh         | ntly cohesive mixtures                               | 0.056 M <sub>160</sub>       |
| Clean fine to medium              | 0.097 M <sub>160</sub>                               |                              |
| Coarse sands and sar              | nds with little gravel                               | 0.139 M <sub>160</sub>       |
| Sandy gravel and gra              | 0.167 <i>N</i> 1 <sub>60</sub>                       |                              |
| Estimating $E_s$ from $q_c$       | (static cone resistance)                             |                              |
| Sandy soils                       | •  | 0.028 <i>q</i> <sub>€</sub>  |

The modulus of elasticity for normally consolidated granular soils tends to increase with depth. An alternative method of defining the soil modulus for granular soils is to assume that it increases linearly with depth starting at zero at the ground surface in accordance with the following equation:

$$E_s = nh \times z \tag{C10.4.6.3-1}$$

where:

# Appendix D.3 - Wall 05.55L Design Calculations

### **AASHTO Average Blowcount in Upper 100 feet**

| W-215-20 |                    |   |   |                      |                                |                                      |                  |
|----------|--------------------|---|---|----------------------|--------------------------------|--------------------------------------|------------------|
| Depth    | Field<br>Blowcount | Energy<br>Corrected<br>Blowcount,<br>N <sub>i</sub> | Layer<br>thickness d <sub>i</sub><br>(feet) | Sum(d <sub>i</sub> ) | d <sub>i</sub> /N <sub>i</sub> | Sum(d <sub>i</sub> /N <sub>i</sub> ) | N <sub>ave</sub> |
| 2.5      | 46                 | 67  | 3.75  | 100                  | 0.06                           | 2.1622                               | 46.3             |
| 5        | 32                 | 46  | 2.5   |                      | 0.05                           | 2.1022                               |                  |
| 7.5      | 32                 | 46  | 2.5   |                      | 0.05                           |                                      |                  |
| 10       | 39                 | 57  | 3.75  |                      | 0.07                           |                                      |                  |
| 15       | 23                 | 33  | 5   |                      | 0.15                           | Driving Energy                       | 87%              |
| 20       | 51                 | 74  | 5   |                      | 0.07                           |                                      |                  |
| 25       | 34                 | 49  | 5   |                      | 0.10                           |                                      |                  |
| 30       | 31                 | 45  | 72.5  |                      | 1.61                           |                                      |                  |
|          |                    |   |   |                      | End of Data                    |                                      |                  |
|          |                    |   |   |                      | End of Data                    |                                      |                  |
|          |                    |   |   |                      | End of Data                    |                                      |                  |
|          |                    |   |   |                      | End of Data                    |                                      |                  |
|          |                    |   |   |                      | End of Data                    |                                      |                  |
|          |                    |   |   |                      | End of Data                    |                                      |                  |
|          |                    |   |   |                      | End of Data                    |                                      |                  |
|          |                    |   |   |                      | End of Data                    |                                      |                  |
|          |                    |   |   |                      | End of Data                    |                                      |                  |
|          |                    |   |   |                      | End of Data                    |                                      |                  |
|          |                    |   |   |                      | End of Data                    |                                      |                  |
|          |                    |   |   |                      | End of Data                    |                                      |                  |
|          |                    |   |   |                      | End of Data                    |                                      |                  |
|          |                    |   |   |                      | End of Data                    |                                      |                  |
|          |                    |   |   |                      | End of Data                    |                                      |                  |
|          |                    |   |   |                      | End of Data                    |                                      |                  |
|          |                    |   |   |                      | End of Data                    |                                      |                  |
|          |                    |   |   |                      | End of Data                    |                                      |                  |

| Soil Profile Type                                   | v <sub>s</sub> (fps) | N       |  |  |
|---|----------------------|---------|--|--|
| S <sub>A</sub>                                      | >5000                | N/A     |  |  |
| S <sub>B</sub>                                      | 2,500 to 5,000       | N/A     |  |  |
| S <sub>c</sub>                                      | 1,200 to 2,500       | >50     |  |  |
| S <sub>D</sub>                                      | 600 to 1,200         | 15≤N≤50 |  |  |
| S <sub>E</sub>                                      | <600                 | <15     |  |  |
| Table 3.10.3.1-1—Site Class Definitions from AASHTO |                      |         |  |  |

| Name     | Nave | Soil Profile Type |
|----------|------|-------------------|
| W-215-20 | 46.3 | D                 |

Blowcount Percent (Energy is input BC/60). This spreadsheet approximates the layer thickness based on a function with depth, however, depending on the layering of the log, it may be necessary for the user to input their own layer thicknesses (i.e., clay layer extends at 7.5 ft and the blowcounts need to be weighted to reflect that thickness).

Spreadsheet based on Section 3.10.3.1 of American Association of State Highway and Transportation Officials

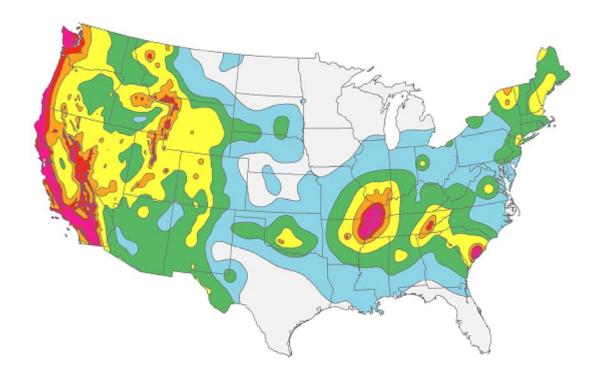
Password

Average\_Blow\_Count

## $\mathbf{BEToolbox}^{^{\mathsf{TM}}}$

Spectra
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Version 6.0.0.6 BETA - Built on Jan 7 2021



## 05.55L

WSDOT Bridge Design Manual 2014 Seismic Hazard Map, 7% probability of exceedance in 75 years

Site Coordinates (Latitude,Longitude):  $47.5054^\circ$  N,  $122.198^\circ$  W Site Soil Classification: Site Class D - Stiff Soil

Seismic hazard maps are for sites at the boundary of Site Classes B and C, which is  $\overline{v}_s$  = 2500 ft/s (760 m/s). Adjustments for

other Site Classes are made as needed.

| Period<br>(sec) | Sa<br>(g) |  |
|-----------------|-----------|--|
| 0.0             | 0.433     | PGA - Site Class B/C Boundary            |
| 0.2             | 0.986     | S <sub>s</sub> - Site Class B/C Boundary |
| 1.0             | 0.283     | S <sub>1</sub> - Site Class B/C Boundary |

Values of Site Coefficient, Fpga, for Peak Ground Acceleration

| Site Class | Мар       | Mapped Peak Ground Acceleration Coefficient (PGA) |           |           |           |           |
|------------|-----------|---|-----------|-----------|-----------|-----------|
|            | PGA≤ 0.10 | PGA= 0.20   | PGA= 0.30 | PGA= 0.40 | PGA= 0.50 | PGA≥ 0.60 |
| Α          | 0.8       | 0.8   | 0.8       | 0.8       | 0.8       | 0.8       |
| В          | 0.9       | 0.9   | 0.9       | 0.9       | 0.9       | 0.9       |
| С          | 1.3       | 1.2   | 1.2       | 1.2       | 1.2       | 1.2       |
| D          | 1.6       | 1.4   | 1.3       | 1.2       | 1.1       | 1.1       |
| E          | 2.4       | 1.9   | 1.6       | 1.4       | 1.2       | 1.1       |

For Site Class D, F<sub>pga</sub> = 1.167

Values for Site Coefficient, F<sub>a</sub>, for 0.2 sec Period Spectral Acceleration

| Site Class | Mapped S              | Mapped Spectral Acceleration Coefficient at Period 0.2 sec (S <sub>s</sub> ) |                       |                       |                       |                       |  |
|------------|-----------------------|--|-----------------------|-----------------------|-----------------------|-----------------------|--|
|            | S <sub>s</sub> ≤ 0.25 | S <sub>s</sub> = 0.50  | S <sub>s</sub> = 0.75 | S <sub>s</sub> = 1.00 | S <sub>s</sub> = 1.25 | S <sub>s</sub> ≥ 1.50 |  |
| Α          | 0.8                   | 0.8  | 0.8                   | 0.8                   | 0.8                   | 8.0                   |  |
| В          | 0.9                   | 0.9  | 0.9                   | 0.9                   | 0.9                   | 0.9                   |  |
| С          | 1.3                   | 1.3  | 1.2                   | 1.2                   | 1.2                   | 1.2                   |  |
| D          | 1.6                   | 1.4  | 1.2                   | 1.1                   | 1.0                   | 1.0                   |  |
| E          | 2.4                   | 1.7  | 1.3                   | 1.0                   | 0.9                   | 0.9                   |  |

For Site Class D,  $F_a = 1.106$ 

Values of Site Coefficient, F<sub>v</sub>, for 1.0 sec Period Spectral Acceleration

| Site Class | Mapped S             | Mapped Spectral Acceleration Coefficient at Period 1.0 sec (S <sub>1</sub> ) |                      |                      |                      |                      |  |
|------------|----------------------|--|----------------------|----------------------|----------------------|----------------------|--|
|            | S <sub>1</sub> ≤ 0.1 | S <sub>1</sub> = 0.2   | S <sub>1</sub> = 0.3 | S <sub>1</sub> = 0.4 | S <sub>1</sub> = 0.5 | S <sub>1</sub> ≥ 0.6 |  |
| Α          | 0.8                  | 0.8  | 0.8                  | 0.8                  | 0.8                  | 0.8                  |  |
| В          | 0.8                  | 0.8  | 0.8                  | 0.8                  | 0.8                  | 0.8                  |  |
| С          | 1.5                  | 1.5  | 1.5                  | 1.5                  | 1.5                  | 1.4                  |  |
| D          | 2.4                  | 2.2  | 2.0                  | 1.9                  | 1.8                  | 1.7                  |  |
| Е          | 4.2                  | 3.3  | 2.8                  | 2.4                  | 2.2                  | 2.0                  |  |

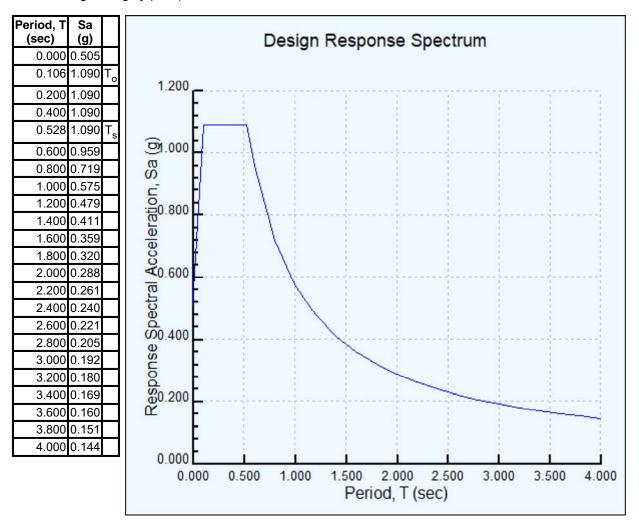
For Site Class D,  $F_v = 2.035$ 

$$\begin{split} & A_{\rm S} = F_{\rm pga} \; {\rm PGA} = (\; 1.167)(\; 0.433g) = 0.505g \\ & S_{\rm DS} = F_{\rm a} \; S_{\rm s} = (\; 1.106)(\; 0.986g) = 1.090g \\ & S_{\rm D1} = F_{\rm v} \; S_{\rm 1} = (\; 2.035)(\; 0.283g) = 0.575g \\ & T_{\rm o} = 0.2T_{\rm s} = (0.2)(\; 0.528) = 0.106 \; {\rm sec} \\ & T_{\rm s} = S_{\rm D1}/S_{\rm DS} = (\; 0.575)/(\; 1.090) = 0.528 \; {\rm sec} \end{split}$$

Partitions for Seismic Design Categories A, B, C, and D

| S <sub>D1</sub>          | SDC |
|--------------------------|-----|
| S <sub>D1</sub> < 0.15   | Α   |
| $0.15 \le S_{D1} < 0.30$ | В   |
| $0.30 \le S_{D1} < 0.50$ | С   |
| 0.50 ≤ S <sub>D1</sub>   | D   |

Seismic Design Category (SDC) = D



| General Information |  |  |  |  |
|---------------------|--|--|--|--|
| Project:            | I-405/Renton to Bellevue Corridor Widening |  |  |  |
| Project Location:   | King County, Washington                    |  |  |  |
| Job Number:         | 00180-366-01                               |  |  |  |
| Boring Designation: | W-215-20                                   |  |  |  |
| Analysis by:        | BZ   |  |  |  |
| Date Analyzed:      | 1/27/2021                                  |  |  |  |
| Checked by:         | YT   |  |  |  |
| Date Checked:       | 3/10/2021                                  |  |  |  |

| Sampling Information  | n  |
|---|----|
| Depth to Groundwater (ft):                                  | 31 |
| SPT Liner (Yes/No):   | No |
| Hammer Energy, %:   | 87 |
| Distance from sample hammer to ground/mudline surface (ft): | 5  |
| Borehole Diameter (in)                                      | 8  |

| Earthquake Information     | on    |
|----------------------------|-------|
| Max Acceleration (As) (g): | 0.505 |
| Earthquake Magnitude:      | 7.00  |

| ٦       | Fitle Block Information                    |
|---------|--|
| Line 1: | I-405/Renton to Bellevue Corridor Widening |
| Line 2: | King County, Washington                    |

| gINT Collection Information         |  |  |  |  |  |  |  |
|-------------------------------------|--|--|--|--|--|--|--|
| P-Drive File Path to gINT database: |  |  |  |  |  |  |  |
| Boring Selected from<br>Database:   |  |  |  |  |  |  |  |

| Residual Strength Weighting                       |     |  |  |  |  |  |  |
|---|-----|--|--|--|--|--|--|
| Olsen & Stark (2002):                             | 0.2 |  |  |  |  |  |  |
| Idriss & Boulanger Void Redistribution (2007):    | 0.2 |  |  |  |  |  |  |
| Idriss & Boulanger No Void Redistribution (2007): | 0.0 |  |  |  |  |  |  |
| Kramer, Wang Hybrid (2008):                       | 0.4 |  |  |  |  |  |  |
| Idriss et al. (1998):                             | 0.2 |  |  |  |  |  |  |

| Collect Data From gINT  | Automate %F from USCS |
|-------------------------|-----------------------|
|                         |                       |
| Auto % F from WSDOT GDM | COMPUTE               |

\*You must hit "COMPUTE" again anytime you change any of the blue or purple inputs. If the output tab is blank or has errors hit "COMPUTE" again.

User Input

Fine -Grain Soil Susceptibility

PI Cutoff Value:

gINT or User

Input

12

| SPT Sample Number | Depth<br>(ft) | Measured N | USCS | Fines Content<br>(%) | Geologic Unit/<br>ESU | Unit Weight (pcf) | PI<br>(%) | Non-liquefiable (i.e.<br>"unstaturated",<br>"cohesive",etc) | User Override*  |
|-------------------|---------------|------------|------|----------------------|-----------------------|-------------------|-----------|---|-----------------|
|                   | 2.5           | 46         | SM   | 30                   | ESU 1B                | 130               |           | Unsaturated   |                 |
|                   | 5.0           | 32         | SM   | 27                   | ESU 1B                | 120               |           | Unsaturated   |                 |
|                   | 7.5           | 32         | SM   | 23                   | ESU 1B                | 120               |           | Unsaturated   |                 |
|                   | 10.0          | 39         | SM   | 23                   | ESU 1B                | 125               |           | Unsaturated   |                 |
|                   | 15.0          | 23         | ML   | 72                   | ESU 4B                | 110               |           | Non-Liquefiable   | Non-Liquefiable |
|                   | 20.0          | 51         | SM   | 23                   | ESU 4B                | 130               |           | Non-Liquefiable   | Non-Liquefiable |
|                   | 25.0          | 34         | SM   | 23                   | ESU 4B                | 120               |           | Non-Liquefiable   | Non-Liquefiable |
|                   | 30.0          | 31         | ML   | 70                   | ESU 4B                | 110               |           | Non-Liquefiable   | Non-Liquefiable |
|                   |               |            |      |                      |                       |                   |           | ,   | ·               |
|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |
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|                   |               |            |      |                      |                       |                   |           |   |                 |
|                   |               |            |      |                      |                       |                   |           |   |                 |

GW observed ATD

Site Class D SEE

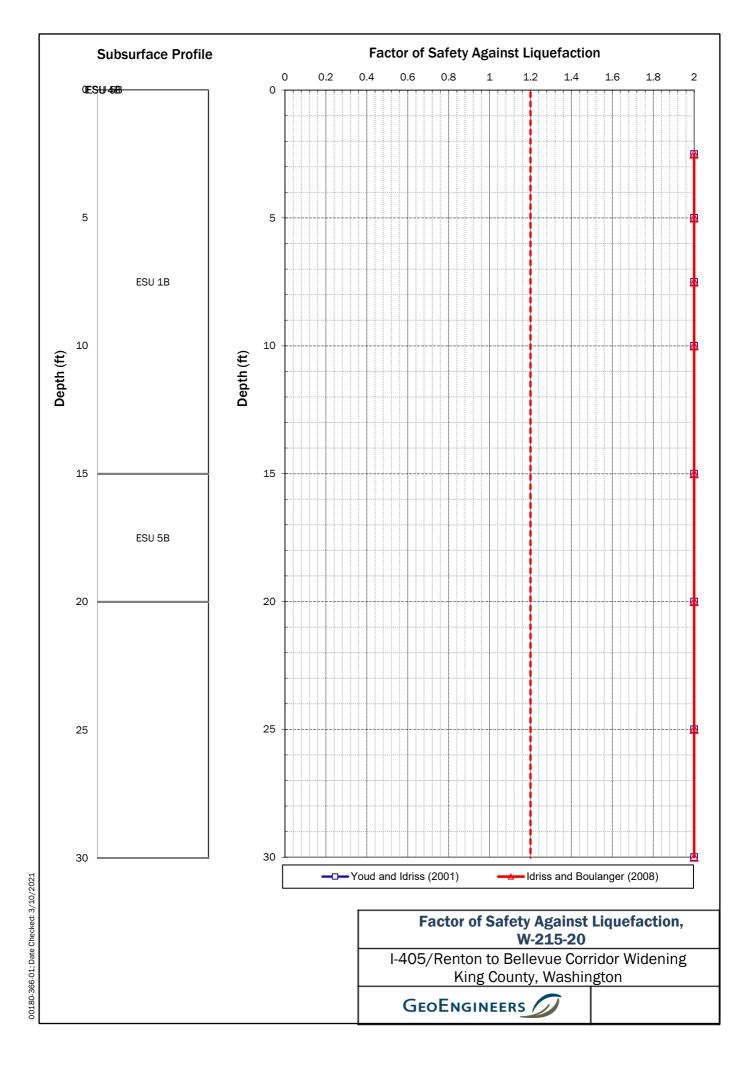
\*User Override column is *NOT* required to be filled out, unless needed. See "Read Me" tab.

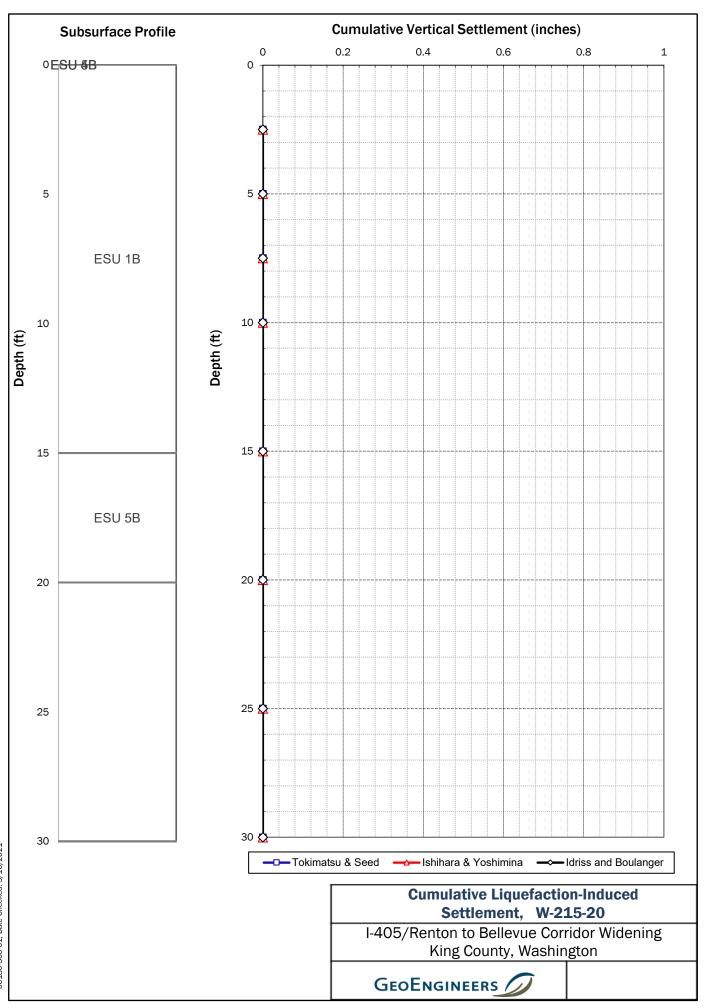
|                      |               |              |               |                         |                              |                                   |                              | Lique                             | efaction Analy      | /sis                    |                         |                         |   |                         |                                   | Residual S   | Shear Stren             | gth Analysis   |                                  |                                   |                         |
|----------------------|---------------|--------------|---------------|-------------------------|------------------------------|-----------------------------------|------------------------------|-----------------------------------|---------------------|-------------------------|-------------------------|-------------------------|---|-------------------------|-----------------------------------|--------------|-------------------------|----------------|----------------------------------|-----------------------------------|-------------------------|
|                      |               |              |               |                         | N                            | 1,60                              | =                            | on Factor of<br>ety               | Liquefacti          | on-Induced Settle       | ement (in)              | LDI<br>(ft)             |   | N <sub>1,60</sub>       |                                   |              |                         | Residual Shear | Strength, Sr                     |                                   |                         |
| SPT Sample<br>Number | Depth<br>(ft) | Measured N   | USCS          | Fines<br>Content<br>(%) | Youd and<br>Idriss<br>(2001) | Idriss and<br>Boulanger<br>(2008) | Youd and<br>Idriss<br>(2001) | Idriss and<br>Boulanger<br>(2014) | Tokimatsu &<br>Seed | Ishihara &<br>Yoshimine | Idriss and<br>Boulanger | Idriss and<br>Boulanger | Idriss &<br>Boulanger<br>Void<br>Distribution<br>(2007) | Olsen & Stark<br>(2002) | Kramer &<br>Wang Hybrid<br>(2008) | WSDOT        | Olsen & Stark<br>(2002) | Idriss &       | Idriss &<br>Boulanger<br>No Void | Kramer &<br>Wang Hybrid<br>(2008) | Idriss et al.<br>(1998) |
|                      | 2.5           | 46           | SM            | 30                      | 94                           | 94                                | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 94.2  | 97.8                    | 92.6                              | n.a.         | n.a.                    | n.a.           | n.a.                             | n.a.                              | n.a.                    |
|                      | 5.0           | 32           | SM            | 27                      | 63                           | 59                                | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 58.8  | 72.6                    | 59.4                              | n.a.         | n.a.                    | n.a.           | n.a.                             | n.a.                              | n.a.                    |
|                      | 7.5<br>10.0   | 32<br>39     | SM<br>SM      | 23                      | 57<br>68                     | 53<br>64                          | 2.00                         | 2.00<br>2.00                      | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 53.1  | 64.6                    | 53.8                              | n.a.         | n.a.                    | n.a.           | n.a.                             | n.a.                              | n.a.                    |
|                      | 15.0          | 23           | ML            | 72                      | 39                           | 38                                | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 63.7<br>38.2  | 72.3<br>39.6            | 64.3<br>37.9                      | n.a.<br>n.a. | n.a.                    | n.a.           | n.a.<br>n.a.                     | n.a.<br>n.a.                      | n.a.<br>n.a.            |
|                      | 20.0          | 51           | SM            | 23                      | 76                           | 78                                | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 77.8  | 75.3                    | 75.6                              | n.a.         | n.a.                    | n.a.           | n.a.                             | n.a.                              | n.a.                    |
|                      | 25.0          | 34           | SM            | 23                      | 45                           | 49                                | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 49.0  | 45.0                    | 46.4                              | n.a.         | n.a.                    | n.a.           | n.a.                             | n.a.                              | n.a.                    |
|                      | 30.0          | 31           | ML            | 70                      | 39                           | 45                                | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 45.0  | 39.7                    | 41.7                              | n.a.         | n.a.                    | n.a.           | n.a.                             | n.a.                              | n.a.                    |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         | 1   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         | <u> </u>  |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         | <u> </u>  |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              |               |                         | <br>1                        |                                   |                              | Residu                            | al Strength Wei     |                         |                         |                         |   |                         |                                   |              |                         |                |                                  |                                   |                         |
|                      |               |              | mic Parame    |                         | 1                            |                                   |                              |                                   |                     | WSDOT:                  |                         |                         |   |                         |                                   |              | Liquefa                 | ction and Ro   | esidual Sh                       | ear Streng                        | gth Analysis            |
|                      |               | Max Accelera | tion (As) (g) | : 0.505                 |                              |                                   |                              |                                   | Olser               | n & Stark (2002):       | 0.2                     |                         |   |                         |                                   |              |                         | Res            | sults, W-2                       | 15-20                             |                         |
|                      |               | Earthquake   | Magnitude:    | 7.00                    |                              |                                   |                              | Idriss & Bou                      | langer Void Redis   | stribution (2007).      | 0.2                     |                         |   |                         |                                   |              | I 1_                    | 405/Renton to  | Rellevue C                       | orridor Wide                      | ning                    |

Idriss & Boulanger Void Redistribution (2007): 0.2 Idriss & Boulanger No Void Redistribution (2007): Kramer, Wang Hybrid (2008): 0.4 Idriss et al. (1998): 0.2

I-405/Renton to Bellevue Corridor Widening King County, Washington







00180-366-01; Date Checked: 3/10/2021

## **Lateral Earth Pressures for Cohesionless Soils**

### **Project Information**

| Project:     | I-405/Renton to Bellevue Corridor Widening |
|--------------|--|
| Owner:       | WSDOT                                      |
| Job Number:  | 00180-366-01                               |
| Analysis by: | YTT  |
| Date/Time:   | 1/12/2022 11:40 AM                         |
| Checked by:  | ТВ   |

### **Input Parameters**

| Material      | φ<br>Friction Angle<br>(deg) | β <sub>2</sub> (-)<br>Foreslope<br>(deg) | i (+)<br>Backslope<br>(deg) | δ<br>Wall Friction - Active<br>(deg) | δ<br>Wall Friction - Passive<br>(deg) | β<br>Wall Batter<br>(deg) | γ <sub>m</sub><br>(pcf) | γ <sub>b</sub><br>(pcf) | Passive<br>Factor of<br>Safety | k <sub>h</sub><br>(g) | k <sub>v</sub> (g) |
|---------------|------------------------------|--|-----------------------------|--------------------------------------|---------------------------------------|---------------------------|-------------------------|-------------------------|--------------------------------|-----------------------|--------------------|
| Common Borrow | 32                           | -15                                      | 0                           | 21                                   | 0                                     | 0                         | 120                     | 57.6                    | 1                              | 0.253                 | 0                  |
| Select Borrow | 36                           | -15                                      | 0                           | 24                                   | 0                                     | 0                         | 125                     | 62.6                    | 1                              | 0.253                 | 0                  |
| Gravel Borrow | 38                           | -15                                      | 0                           | 25                                   | 0                                     | 0                         | 130                     | 67.6                    | 1                              | 0.253                 | 0                  |
|               |                              |  |                             |                                      |                                       |                           |                         |                         |                                |                       |                    |
|               |                              |  |                             |                                      |                                       |                           |                         |                         |                                |                       |                    |
|               |                              |  |                             |                                      |                                       |                           |                         |                         |                                |                       |                    |
|               |                              |  |                             |                                      |                                       |                           |                         |                         |                                |                       | <u> </u>           |
|               |                              |  |                             |                                      |                                       |                           |                         |                         |                                |                       |                    |
|               |                              |  |                             |                                      |                                       |                           |                         |                         |                                |                       |                    |
|               |                              |  |                             |                                      |                                       |                           |                         |                         |                                |                       | <u> </u>           |
|               |                              |  |                             |                                      |                                       |                           |                         |                         |                                |                       |                    |
|               |                              |  |                             |                                      |                                       |                           |                         |                         |                                |                       |                    |

#### **Lateral Earth Pressures**

#### Output

|               |                | Active                  |                          |       |                              | Pa                            | ssive                         |                                |                | At Rest                 |              |                             | EP Trapezoid                    |                 | <u>s</u>                 | eismic_                   |          | Seismic Pressure -       |
|---------------|----------------|-------------------------|--------------------------|-------|------------------------------|-------------------------------|-------------------------------|--------------------------------|----------------|-------------------------|--------------|-----------------------------|---------------------------------|-----------------|--------------------------|---------------------------|----------|--------------------------|
| Material      | K <sub>a</sub> | γ <sub>a</sub><br>(pcf) | γ' <sub>a</sub><br>(pcf) | $K_p$ | γ <sub>p(all)</sub><br>(pcf) | γ' <sub>p(all)</sub><br>(pcf) | γ <sub>pe(all)</sub><br>(pcf) | γ' <sub>pe(all)</sub><br>(pcf) | K <sub>o</sub> | γ <sub>o</sub><br>(pcf) | γ'。<br>(pcf) | Single Tieback<br>(psf * H) | Mult. Tiebacks <sup>1</sup> , X | K <sub>ae</sub> | γ <sub>ae</sub><br>(pcf) | γ′ <sub>ae</sub><br>(pcf) | $K_{pe}$ | Rectangular<br>(psf * H) |
| Common Borrow | 0.28           | 33.00                   | 15.84                    | 2.00  | 240.13                       | 115.26                        | 571.32                        | 274.23                         | 0.47           | 56.41                   | 27.08        | 33.00                       | 33.00                           | 0.48            | 57.47                    | 27.59                     | 4.76     | 12.23                    |
| Select Borrow | 0.23           | 29.36                   | 14.70                    | 2.30  | 287.97                       | 144.21                        | 801.00                        | 401.14                         | 0.41           | 51.53                   | 25.80        | 29.36                       | 29.36                           | 0.42            | 52.60                    | 26.34                     | 6.41     | 11.62                    |
| Gravel Borrow | 0.22           | 28.18                   | 14.65                    | 2.47  | 321.67                       | 167.27                        | 978.48                        | 508.81                         | 0.38           | 49.96                   | 25.98        | 28.18                       | 28.18                           | 0.39            | 51.33                    | 26.69                     | 7.53     | 11.58                    |
|               |                |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|               |                |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|               |                |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|               |                |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|               |                |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|               |                |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|               |                |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|               |                |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|               |                |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|               |                |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|               |                |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|               |                |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|               |                |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|               |                |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             | -                               |                 |                          |                           |          |                          |
|               |                |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |



|               |    | Sliding Friction Coefficient |
|---------------|----|------------------------------|
| Soil Type     | φ' | Cast-In-Place Concrete       |
| Common Borrow | 32 | 0.62                         |
| Select Borrow | 36 | 0.73                         |
| Gravel Borrow | 38 | 0.78                         |
| ESU 1B        | 40 | 0.84                         |

Notes:

Sliding coefficients calculated according to AASHTO Equation 10.6.3.4-2

#### **Cast-In-Place Concrete Coefficient of Friction:**

Coefficient of friction = 1.0\*tan(Phi')

#### **AASHTO 10.6.3.4:**

$$R_{\tau} = CV \tan \phi_f \qquad (10.6.3.4-2)$$

for which:

C = 1.0 for concrete cast against soil

= 0.8 for precast concrete footing

where:

φ<sub>f</sub> = internal friction angle of drained soil

(degrees)

V = total vertical force (kips)

#### LRFD Foundation Design

#### Spreadsheet Reference Section 10.6.3.1.2 of The 2014 AASHTO LRFD Bridge Design Specifications

| Date/Time:    | 1/11/22 10:25 AM   |
|---------------|--|
| Project Name: | I-405/Renton to Bellevue Corridor Widening - Wall 05.55L |
| Project No.:  | 00180-366-01   |

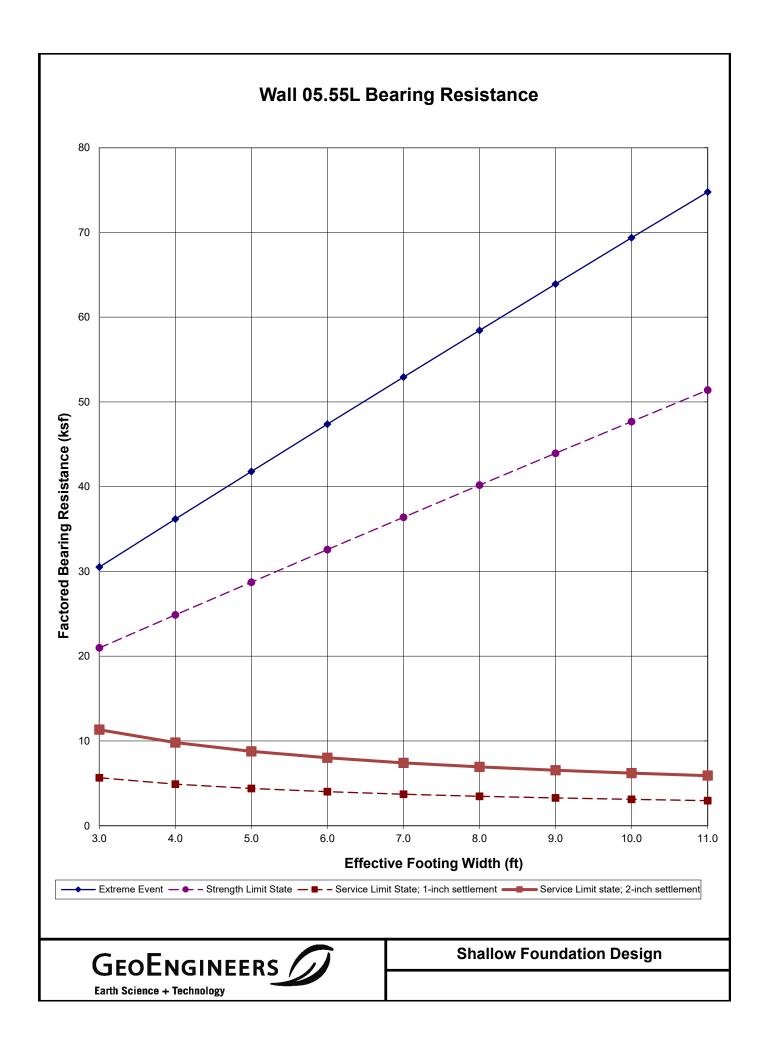
| Foundation Soil Conditions                |       |  |  |  |  |  |  |
|---|-------|--|--|--|--|--|--|
| Unit Weight, γ (pcf)                      | 130   |  |  |  |  |  |  |
| Friction angle, Φ (degrees)               | 40    |  |  |  |  |  |  |
| Friction angle, Φ (rad)                   | 0.698 |  |  |  |  |  |  |
| Cohesion, C (psf) 0                       |       |  |  |  |  |  |  |
| Embedment, D <sub>f</sub> (ft)            | 2     |  |  |  |  |  |  |
| Depth to Groundwater, D <sub>w</sub> (ft) | 26    |  |  |  |  |  |  |
| Footing Length, L (ft)                    | 130   |  |  |  |  |  |  |
| Footing Width, B (ft)                     | 1     |  |  |  |  |  |  |
| Poissons Ration, v 0.40                   |       |  |  |  |  |  |  |
| Young's Modulus, E <sub>s</sub> (ksf)     | 800   |  |  |  |  |  |  |

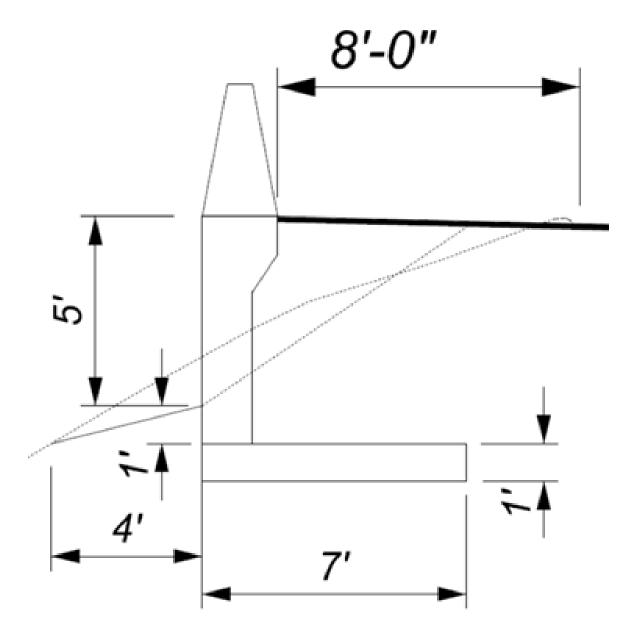
(ESU 1B)

| Bearing Capacity Factor | ors . |
|-------------------------|-------|
| N <sub>Y</sub>          | 109   |
| N <sub>c</sub>          | 75    |
| $N_q$                   | 64    |

| Effective Footing Width, B | Water Dep       | th Factors             |           | Shape Factors         |           | Unfactored<br>Bearing | Extreme Event Resistance Resistance Factor (0.8) for gravity and | Working Bearing Resistance Resistance Factor (0.55) for gravity and | Deflection from Elastic<br>Settlement Spreadsheet | Deflection from Elastic<br>Settlement Spreadsheet |
|----------------------------|-----------------|------------------------|-----------|-----------------------|-----------|-----------------------|--|---|---|---|
| Ellective Footing Width, B | C <sub>wq</sub> | <u>C<sub>w-y</sub></u> | <u>Sc</u> | <u>S</u> <sub>y</sub> | <u>Sq</u> | Resistance            | semigravity walls (Section 11.5.8 AASHTO)                        | semigravity walls (Table Table 11.5.7-1)                            | 1" Deflection                                     | 2" Deflection                                     |
| (ft)                       |                 |                        |           |                       |           | (ksf)                 | (ksf)  | (ksf)   | (ksf)   | (ksf)   |
| 3.0                        | 1.0             | 1.0                    | 1.02      | 0.99                  | 1.02      | 38.2                  | 30.5   | 21.0  | 5.7   | 11.3  |
| 4.0                        | 1.0             | 1.0                    | 1.03      | 0.99                  | 1.03      | 45.2                  | 36.2   | 24.9  | 4.9   | 9.8   |
| 5.0                        | 1.0             | 1.0                    | 1.03      | 0.98                  | 1.03      | 52.2                  | 41.8   | 28.7  | 4.4   | 8.8   |
| 6.0                        | 1.0             | 1.0                    | 1.04      | 0.98                  | 1.04      | 59.2                  | 47.4   | 32.6  | 4.0   | 8.0   |
| 7.0                        | 1.0             | 1.0                    | 1.05      | 0.98                  | 1.05      | 66.2                  | 52.9   | 36.4  | 3.7   | 7.4   |
| 8.0                        | 1.0             | 1.0                    | 1.05      | 0.98                  | 1.05      | 73.0                  | 58.4   | 40.2  | 3.5   | 6.9   |
| 9.0                        | 1.0             | 1.0                    | 1.06      | 0.97                  | 1.06      | 79.9                  | 63.9   | 43.9  | 3.3   | 6.5   |
| 10.0                       | 1.0             | 1.0                    | 1.07      | 0.97                  | 1.06      | 86.7                  | 69.4   | 47.7  | 3.1   | 6.2   |
| 11.0                       | 1.0             | 1.0                    | 1.07      | 0.97                  | 1.07      | 93.5                  | 74.8   | 51.4  | 3.0   | 5.9   |
|                            |                 |                        |           |                       |           |                       |  |   |   |   |
|                            |                 |                        |           |                       |           |                       |  |   |   |   |

Note: Depth and inclination modifier were taken as 1 because the load is applied axially and during construction the soils above the footing are to be excavated.

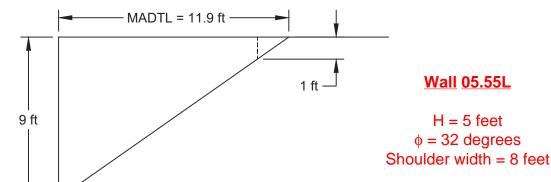




Wall 05.55L dimensions provided by Wood on November 17, 2021

#### **Cast-in-Place or Precast Wall**

#### **Assumed Deformation Profile**

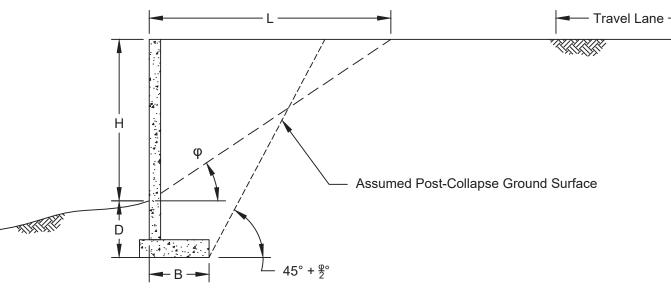


MADTL =  $(5-1)/5 * H/(tan\phi) = 6.4$  feet < 8-foot shoulder

**Wall 05.55L** 

H = 5 feet  $\phi$  = 32 degrees

#### **Assumed Failure Geometry**



MADTL = Minimum Allowable Distance to Travel Lane =  $\frac{H-1}{H}$  \*  $\frac{H}{\tan(\phi)}$ 

 $\varphi$  = Internal friction angle of wall backfill material (assume 34 degrees if unknown)

B = distance from wall face to back edge of wall footing or reinforced zone

H = exposed height of wall

NOT TO SCALE

I-405 R2B Express Toll Lanes King County, Washington

Minimum Allowable Distance to Travel Lane -**Wall Below Travel Lane** 19434-03

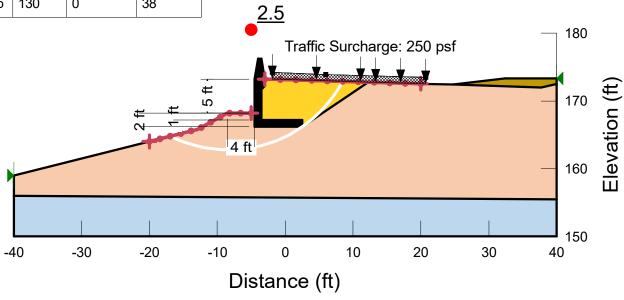


Figure **1A** 

above) is representative of an "abrupt elevation change" within the traveled way and is used to define the minimum wall offset from the traveled way.

Note: The assumed 1-foot vertical deformation (shown

| Color | Name  | Material Model | Unit<br>Weight | Effective<br>Cohesion | Effective<br>Friction<br>Angle |
|-------|---|----------------|----------------|-----------------------|--------------------------------|
|       | Barrier   | High Strength  | 150            |                       |                                |
|       | Common Borrow   | Mohr-Coulomb   | 120            | 0                     | 32                             |
|       | ESU 1B Medium Dense<br>to Very Dense<br>Coarse-Grained Fill | Mohr-Coulomb   | 130            | 0                     | 40                             |
|       | ESU 4B Dense to Very<br>Dense Sand/Gravel                   | Mohr-Coulomb   | 120            | 0                     | 43                             |
|       | Gravel Borrow   | Mohr-Coulomb   | 130            | 0                     | 38                             |



#### Notes:

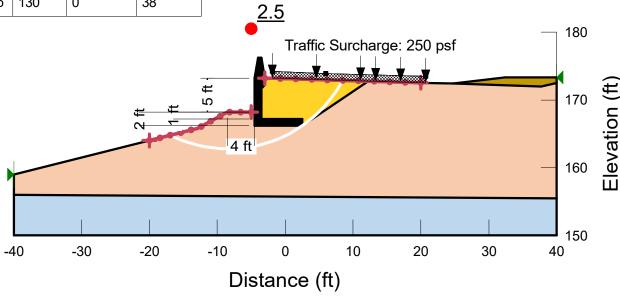
- 1. The locations of all features shown are approximate.
- This drawing is for information purposes. It is intended to assist in showing features discussed in an attached document.
- GeoEngineers, Inc. cannot guarantee the accuracy and context of electronic files. The master file is stored by GeoEngineers, Inc. and will serve as the official record of this communication.

Wall 05.55L - Sta. 1+50 Static Global Stability (Spencer)

I-405/Renton to Bellevue Corridor Widening King County, Washington



| Color | Name  | Material Model | Unit<br>Weight | Effective<br>Cohesion | Effective<br>Friction<br>Angle |
|-------|---|----------------|----------------|-----------------------|--------------------------------|
|       | Barrier   | High Strength  | 150            |                       |                                |
|       | Common Borrow   | Mohr-Coulomb   | 120            | 0                     | 32                             |
|       | ESU 1B Medium Dense<br>to Very Dense<br>Coarse-Grained Fill | Mohr-Coulomb   | 130            | 0                     | 40                             |
|       | ESU 4B Dense to Very<br>Dense Sand/Gravel                   | Mohr-Coulomb   | 120            | 0                     | 43                             |
|       | Gravel Borrow   | Mohr-Coulomb   | 130            | 0                     | 38                             |



#### Notes:

- 1. The locations of all features shown are approximate.
- This drawing is for information purposes. It is intended to assist in showing features discussed in an attached document.
- GeoEngineers, Inc. cannot guarantee the accuracy and context of electronic files. The master file is stored by GeoEngineers, Inc. and will serve as the official record of this communication.

Wall 05.55L - Sta. 1+50 Static Global Stability (M-P)

I-405/Renton to Bellevue Corridor Widening King County, Washington









## Appendix E Wall 05.85L-A Calculations







#### **APPENDIX E - WALL 05.85L-A CALCULATIONS**

#### General

This appendix presents geotechnical calculations for Wall 05.85L-A including:

- **ESU Soil Properties**
- Seismic Hazard Analysis
- Lateral Earth Pressures
- Coefficients of Friction for Sliding
- Bearing Resistance and Elastic Settlement
- Seepage Analysis
- Global Stability
- Compound Stability

#### **ESU Soil Properties**

Design soil properties were developed in accordance with the Project GDM, AASHTO LRFD, FHWA, WSDOT HRM, and the USGS. We calculated the average, geometric mean, and standard deviation within each ESU. We verified the reliability of the ESU data set by comparing the COV of each calculated geometric mean value to measured and interpreted values presented in Sabatini et al. (2002) Table 52.

A detailed description of the soil property development is presented in Section 7.1 of this geotechnical engineering report. Supporting calculations are provided in this appendix.

#### **Seismic Hazard Analysis**

We selected a representative site class for the wall from the site class evaluation of nearby borings. We evaluated the site class of each boring using a spreadsheet developed by GeoEngineers in accordance with AASHTO LRFD Section 3.10.3.1.

We developed seismic design parameters using the WSDOT Bridge Engineering Software BEToolbox/BridgeLink in accordance with the WSDOT BDM based on the projected ground motion at the project site that has a 7 percent (SEE) probability of exceedance in a 75-year period (approximate 1,000-year return period).

We used a mean earthquake magnitude at the PGA period is 7.0 for the SEE based on the Hart Crowser design report "I-405" R2B Segment 1a Site-Specific Hazard Analysis RFU," dated March 25, 2021.

We evaluated the FS against liquefaction and liquefaction-induced settlement of saturated, loose to medium dense soils in accordance with the Project GDM Chapter 6 using a spreadsheet developed by GeoEngineers. Per Project GDM Section 6-4.2.3, soils with liquefaction potential are defined as those with FSs against liquefaction less than 1.2. Our analysis shows that saturated, low-plasticity portions of ESU 2B at Wall 05.85L-A may be liquefiable. Estimated liquefaction-induced settlement at Wall 05.85L-A ranges from 2 to 4 inches, considering the full thickness of ESU 2B present at H-2-85. We estimate that differential liquefaction settlements in ESU 2B could be on the order of 1 to 2 inches. However, based on the planned base of wall elevation, we do not anticipate that a significant thickness of ESU 2B will remain below the base of the wall. In addition, based on our groundwater model, we anticipate that any ESU 2B material remaining below the wall will not be saturated. Therefore, we do not anticipate liquefaction or related settlement of soil beneath the wall. Saturated portions of ESU 2B downslope of the wall may experience liquefaction and related settlement.

Residual shear strength was calculated for liquefiable soils from existing relationships and procedures outlined in Project GDM Section 6-2.2 using a spreadsheet developed by GeoEngineers. Residual strength calculations become unconservatively high for liquefiable soils with an N160 corrected to an equivalent clean sand [N160(cs)] that is greater than 20. Using guidance presented in WSDOT Report WA-RD 668.1 (Kramer 2008), we capped N160(cs) to 20 to calculate a residual shear strength for soils exhibiting liquefaction potential (FS against liquefaction < 1.2).







Detailed descriptions of our seismic hazard analysis methodology and the results are presented in Section 7.2 and Section 8.1, respectively, of this report. Site class calculations, WSDOT BDM software outputs, liquefaction analyses, and residual shear strength calculations are provided in this appendix.

#### **Lateral Earth Pressures**

Active static lateral pressure coefficients and corresponding lateral earth pressures for ESU 2A were calculated on the back of Wall 05.85L-A in accordance with AASHTO LRFD Section 3.11.5 using the proposed 2H:1V backslope behind the wall and 2H:1V foreslope in front of the wall. Static lateral earth pressures shall be applied using a triangular distribution. An LRFD load factor of 1.5 shall be applied to the static earth pressures in accordance with AASHTO LRFD Table 3.4.1-2.

Due to relatively shallow embedment of the wall combined with a foreslope condition, passive lateral earth pressures shall be ignored.

Active static + seismic lateral pressure coefficients and static + seismic lateral earth pressures were calculated using the GLE Method in accordance with AASHTO LRFD Section A11.3.3 and NCHRP Report 611 Section 7.4. The GLE analysis was evaluated for Spencer's method using the computer design software Slope/W (Geo Slope International, Ltd. 2020). For the static + seismic earth pressures, we used a modified horizontal seismic coefficient, kh, coupling a 50 percent reduction for flexible wall displacements with a reduction for wave scattering effects. Static + seismic lateral earth pressures shall be applied using a triangular distribution. An LRFD load factor of 1.0 shall be applied to the static + seismic earth pressures in accordance with AASHTO LRFD Table 3.4.1-1.

Surcharge loads (such as traffic loading, fill loads above the wall, and forward compatible loading for future I-405 widening) and appropriate load factors shall be applied to evaluate wall stability. All surcharges shall apply load factors in accordance with AASHTO LRFD Tables 3.4.1-1 and 3.4.1-2.

A detailed description of our analysis methodology and the calculated results are presented in Section 7.3 and Section 8.2, respectively. Supporting calculations are provided in this appendix.

#### Coefficients of Friction for Sliding

Coefficients of friction for sliding on surficial native soils, common borrow, select borrow, and gravel borrow were calculated using AASHTO LRFD equation 10.6.3.4-2.

A detailed description of our analysis methodology and the results are presented in Section 7.4 and Section 8.3, respectively, of this report. Supporting calculations are provided in this appendix.

#### **Bearing Resistance and Elastic Settlement**

We estimated the bearing resistance and elastic settlement of the wall using a spreadsheet developed by GeoEngineers in accordance with AASHTO LRFD Section 10.6.3. We estimated elastic settlement from procedures outlined in AASHTO LRFD and Section 10.6.2.4. Sliding, overturning, and internal stability are being evaluated by the design-build team's wall designers and will be submitted under separate cover.

A detailed description of our analysis methodology and the results are presented in Section 7.5 and Section 8.4, respectively, of this report. Supporting calculations are provided in this appendix.

#### Seepage Analysis

We used finite element seepage modeling software, Seep/W, to estimate a steady state groundwater level at the wall. We used existing groundwater measurements from piezometers in borings H-2-85 and H-3-85, subsurface soil hydraulic conductivity properties, and precipitation data to develop a conceptual model of seepage patterns.

A detailed description of our analysis methodology is presented in Section 7.7, and discussion of the model development and conclusions is presented in Section 8.5 of this report. Steady-state seepage results are presented in this appendix. Seep/W output reports are provided in Appendix I.







#### Global Stability

We performed global stability analyses for the following critical design section:

Section Sta. 1+90 – Maximum overall slope height

Global stability was evaluated using limit equilibrium analysis methodology outlined in the Project GDM using the computer design software Slope/W (Geo Slope International, Ltd. 2020). We analyzed FSs using Spencer's method and Morgenstern-Price for a circular failure surface.

We used an apparent cohesion in the surficial native soils for pseudo-static analyses. Apparent cohesion was based on the fines content ranges presented in Table 11-2 of the FHWA Geotechnical Engineering Circular No. 3.

We evaluated post-seismic global stability using residual shear strengths for potentially liquefiable soil.

We modeled a 4-foot horizontal bench in front of the wall per AASHTO LRFD Section 11.10.2.2 and a front face embedment depth of 3 feet using criteria outlined in AASHTO LRFD Table C11.10.2.2-1.

To meet minimum FSs, we used a minimum reinforcement length of 0.8H to model the SEW. We modeled a 1.5-foot clearance between the reinforced zone and the temporary shoring, which was backfilled with imported gravel borrow. See Section 8.8.3 in this geotechnical report for discussion on temporary shoring.

We used the horizontal seismic coefficient, kh, for global stability presented in Table 8 of this geotechnical report for the pseudo-static global stability analyses. We used the residual shear strength presented in Table 5 of this geotechnical report for liquefiable soils to evaluate post-seismic global stability.

A uniform traffic surcharge of 250 psf was included in static stability analysis. A uniform traffic surcharge of 125 psf was included for the seismic (pseudo-static and post-seismic) stability analyses. In accordance with Section 15-4.12 of the Project GDM, we used a load factor of 1.0 for the static traffic surcharge because it is a non-structural load.

The groundwater level was modeled using results from the seepage analysis.

We also evaluated the global stability of the wall with a forward compatible wall for future I-405 widening. We modeled the forward compatible wall directly above the proposed SEW with the face of the forward compatible wall set back 7 feet from the face of the SEW. We modeled the backfill behind the forward compatible wall as lightweight EPS using the strength properties presented in Table 7 and truncated the EPS behind the forward compatible wall at 4 feet from the proposed edge of the traveled way. The required minimum static, pseudo-static, and post-seismic FSs were met for all forward compatible wall cases.

Detailed descriptions of our global stability analysis methodology and the results of our analyses are presented in Section 7.8 and Section 8.6, respectively, of this report. Global stability models showing FS for critical failures at the design section are provided in this appendix. Slope/W reports are provided in Appendix J.

#### Compound Stability

We used the results of the global stability analyses to model and evaluate compound stability at the critical design section using the minimum reinforcement lengths required to meet the minimum FSs from the global stability analyses. To meet minimum FSs for compound stability, we kept the upper 6 rows of reinforcing strips at a length of 0.8H (2 strips per row per panel), but for the bottom 2 rows, we increased the length of reinforcing strips to 1.0H and increased the number of reinforcing strips to 4 per row per panel.

We used the horizontal seismic coefficient, kh, for compound stability presented in Table 8 and applied the apparent cohesion presented in Table 5 for the pseudo-static analysis. We used the residual shear strength presented in Table 5 for liquefiable soils to evaluate post-seismic compound stability.

We applied a uniform traffic surcharge of 437.5 psf directly over the reinforced zone and a uniform traffic surcharge of 250 psf outside of the reinforced zone for the static compound stability analysis, and a traffic surcharge of 125psf for the seismic (pseudo-static and post-seismic) compound stability analysis.

We used the piezometric surface from the seepage analysis to model the groundwater level.



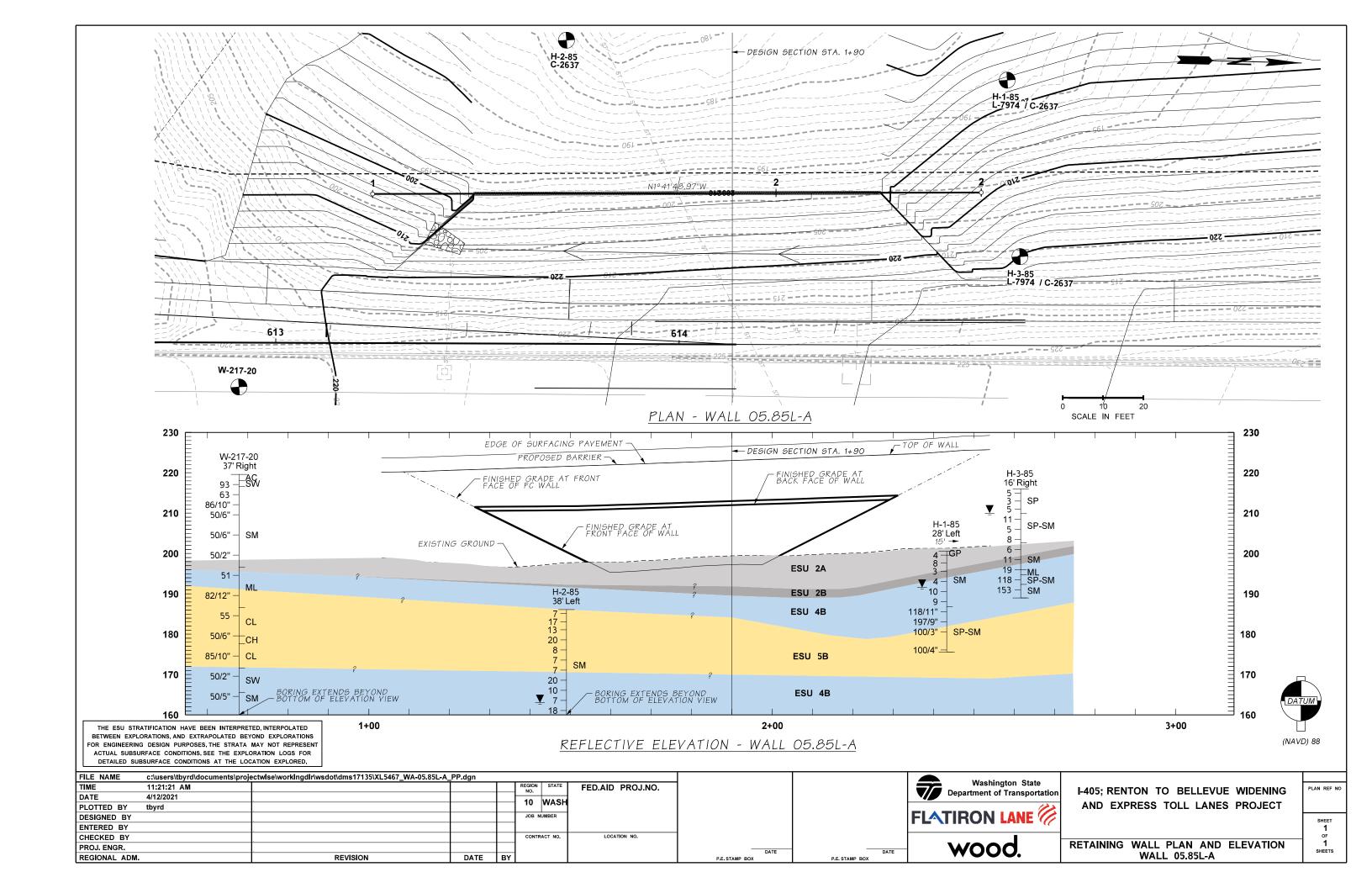


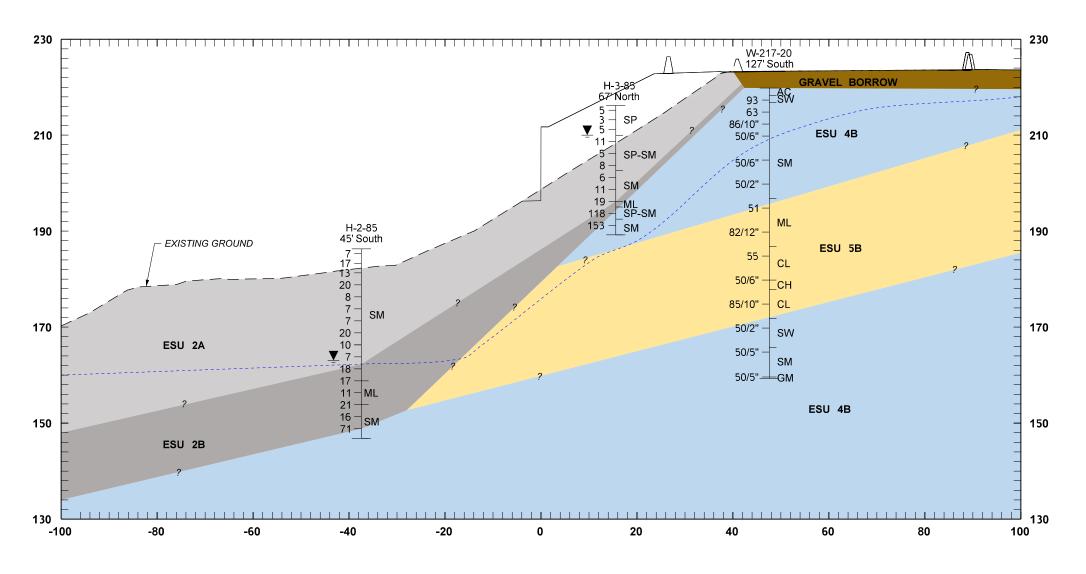


We also evaluated the compound stability of proposed Wall 05.85L-A considering forward compatible walls for future I-405 widening, using the same geometry and strength properties from the global stability analyses for the forward compatible wall. As one option to meet required compound stability minimum FSs, we modeled the backfill as lightweight EPS. We did not explore all potential options as design of the forward compatible walls is outside the scope of this project, but minimally, the option we did analyze demonstrated that future I-405 widening projects can be designed and constructed without demolition or reconstruction of Wall 05.85L-A.

Detailed descriptions of our compound stability analysis methodology and the results of our analyses are presented in Section 7.9 and Section 8.7, respectively, of this geotechnical report. Compound stability models showing FS for critical failures at the design section are provided in this appendix. Slope/W reports are provided in Appendix K.

# Appendix E.1 - Wall 05.85L-A Plan, Profile and Sections





WALL 05.85L-A STATION 1+90

THE ESU STRATIFICATION HAVE BEEN INTERPRETED, INTERPOLATED BETWEEN EXPLORATIONS, AND EXTRAPOLATED BEYOND EXPLORATIONS FOR ENGINEERING DESIGN PURPOSES, THE STRATA MAY NOT REPRESENT ACTUAL SUBSURFACE CONDITIONS, SEE THE EXPLORATION LOGS FOR DETAILED SUBSURFACE CONDITIONS AT THE LOCATION EXPLORED,

| FILE NAME    | c:\users\tbyra\aocuments\pro | jectwise\workingair\wsaot\ams1/135\XL546/_WA-U5.85L-A | _x5.agn |    |              |                  |                |                | 14/2 - 12/2 - 14 - 12 - 04 - 4 -        |                                    |             |   |
|--------------|------------------------------|---|---------|----|--------------|------------------|----------------|----------------|---|------------------------------------|-------------|---|
| TIME         | 6:09:09 PM                   |   |         |    | REGION STATE | FED.AID PROJ.NO. |                |                | Washington State                        | I-405: RENTON TO BELLEVUE WIDENING | PLAN REF NO | 1 |
| DATE         | 4/9/2021                     |   |         |    | 10 WASH      | <u></u>          |                |                | Department of Transportation            | •                                  |             | ı |
| PLOTTED BY   | tbyrd                        |   |         |    | I IU WASI    | 1                |                |                |   | AND EXPRESS TOLL LANES PROJECT     |             | ı |
| DESIGNED BY  |                              |   |         |    | JOB NUMBER   |                  |                |                | FLATIRON LANE 🥢                         |                                    | SHEET       | 1 |
| ENTERED BY   |                              |   |         |    |              |                  |                |                | , _ ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, |                                    | 1           | ı |
| CHECKED BY   |                              |   |         |    | CONTRACT NO. | LOCATION NO.     |                |                |   |                                    | OF OF       |   |
| PROJ. ENGR.  |                              |   |         |    | 1            |                  | DATE           | DATE           | WOOD.                                   | WALL 05.85L-A                      | 1<br>SHEETS | 1 |
| REGIONAL ADM | 1.                           | REVISION  | DATE    | BY | 1            |                  | P.E. STAMP BOX | P.E. STAMP BOX | <b>******</b>                           | DESIGN SECTION AT STA. 1+90        | 5.1.2.10    | ı |

# Appendix E.2 - Wall 05.85L-A ESU Soil Property Calculations

| ESU | Description  | Total No. of<br>Samples <sup>b</sup> | USCS <sup>c</sup> | Fines <sup>d</sup><br>(%) | Plasticity<br>Index,<br>PI <sup>e</sup> (%) | Raw N<br>(bpf) | N<br>(b | <sub>60</sub> <sup>f</sup><br>pf) | (N <sub>1</sub> |       |       | l Unit<br>t <sup>g</sup> (pcf) | Effective<br>Angle, φ | Friction | Fully<br>Softened<br>$\phi'^{i}$ (deg) | Effective<br>c' j (psf) |       | Residual Shear<br>Strength, Sr (psf) | Undrain<br>Strength | ed Shear<br>, Su (psf) |
|-----|--|--------------------------------------|-------------------|---------------------------|---|----------------|---------|-----------------------------------|-----------------|-------|-------|--------------------------------|-----------------------|----------|--|-------------------------|-------|--------------------------------------|---------------------|------------------------|
|     |  |                                      |                   | Value                     | Value                                       | Value          | Value   | COV a                             | Value           | COV a | Value | COV a                          | Value                 | COV a    | Value                                  | Value                   | Value | Value                                | Value               | COV                    |
| 1A  | Loose to Medium Dense Coarse-<br>Grained Fill                | 7                                    | SP-SM             | 8                         | -   | 6              | 4       | 47%                               | 7               | 44%   | 110   | 7%                             | 34                    | 6%       | -                                      | -                       | -     | -                                    | -                   | -                      |
| 2A  | Very Loose to Loose Sand/Gravel                              | 17                                   | SM                | 20                        | -   | 9              | 7       | 52%                               | 10              | 54%   | 110   | 7%                             | 32                    | 7%       | -                                      | -                       | -     | -                                    | -                   | -                      |
| 2B  | Medium Dense Sand/Gravel                                     | 6                                    | SM                | 40                        | -   | 17             | 16      | 20%                               | 14              | 22%   | 110   | 2%                             | 32                    | 3%       | -                                      | -                       | -     | 497                                  |                     | -                      |
| 4B  | Dense to Very Dense Sand/Gravel                              | 16                                   | SM                | 18                        | -   | 148            | 108     | 24%                               | 111             | 25%   | 130   | 2%                             | 43                    | 3%       | -                                      | -                       | -     | -                                    | -                   | -                      |
| 5B  | Very Stiff to Hard Silt and<br>Clay/Dense to Very Dense Silt | 5                                    | ML/CL             | 82                        | 20  | 76             | 108     | 32%                               | 99              | 29%   | 130   | 2%                             | 43                    | 3%       | -                                      | -                       | -     | -                                    | -                   | -                      |

#### Notes:

- a. Coefficient of Variation (COV) percentage calculated to verify the variability and reliability of sample data within ESU (WSDOT GDM Section 5.11.2 (2015)). Calculated COV percentage compared to ranges presented in Table 52 (Sabatini et al. 2002) (below).
- b. Number of samples excludes outliers.
- c. Predominant USCS classification of all samples in ESU. Sandstone, where encountered, denoted as (SS).
- d. Fines content percentage calculated as the geometric mean of all samples, whose values were determined through lab testing or estimated from field classification.
- e. For coarse-grained ESUs, the plasticity index was estimated on the fine-grained portion of the soil. For fine-grained ESUs, if lab data is limited, the plasticity index may not be representative of the overall soil unit.
- f. Corrected blow counts ( $N_{60}$  and ( $N_{1}$ )<sub>60</sub>) were calculated following WSDOT GDM Section 5.5 (2015).
- g. Individual sample unit weights were correlated using CALTRANS Geotechnical Manual (2014), verified with applicable ranges presented in Codotu (2001), as specified in WOOD SPM. The geometric mean of the unit weights was rounded to the nearest 5pcf, as specified in WOOD SPM. Unit weight data variability and quality were evaluated by comparing the calculated COV percentage to the applicable Sabatini range.
- h. Design friction angles were selected by considering fines content. Friction angle data variability and quality were evaluated by comparing the calculated COV percentage to the applicable Sabatini range.
- i. Where applicable, fully softened friction angle was estimated following WSDOT GDM, Figure 5-7 (After Stark and Hussain, 2013).
- j. Where applicable, effective cohesion was calculated using Equations 6 through 8 in the WOOD Geotechnical SPM.
- k. Where applicable, residual friction angle (to be used for slope stability evaluation) was estimated following WSDOT GDM, Figure 5-5 (After NAVFAC, 1971).

| Measured or interpreted parameter value                     | Coefficient of Variation, V |
|---|-----------------------------|
| Unit weight, γ  | 3 to 7 %                    |
| Buoyant unit weight, γ <sub>b</sub>                         | 0 to 10 %                   |
| Effective stress friction angle, φ'                         | 2 to 13 %                   |
| Undrained shear strength, su                                | 13 to 40 %                  |
| Undrained strength ratio (s <sub>u</sub> /σ <sub>v</sub> ') | 5 to 15 %                   |
| Compression index, C <sub>c</sub>                           | 10 to 37 %                  |
| Preconsolidation stress, σ <sub>p</sub> '                   | 10 to 35 %                  |
| Hydraulic conductivity of saturated clay, k                 | 68 to 90 %                  |
| Hydraulic conductivity of partly-saturated clay, k          | 130 to 240 %                |
| Coefficient of consolidation, c <sub>v</sub>                | 33 to 68 %                  |
| Standard penetration blowcount, N                           | 15 to 45 %                  |
| Electric cone penetration test, q <sub>c</sub>              | 5 to 15 %                   |
| Mechanical cone penetration test, q <sub>c</sub>            | 15 to 37 %                  |
| Vane shear test undrained strength, suvst                   | 10 to 20 %                  |

Source: Table 52 (Sabatini et al. 2002)

|        | ſ         | ESU Name: |                 | ES                              | SU 1A - Loos    | e to Medium | Dense Coar            | se-Grained           | Fill             |             | Ī                        |              |                                |
|--------|-----------|-----------|-----------------|---------------------------------|-----------------|-------------|-----------------------|----------------------|------------------|-------------|--------------------------|--------------|--------------------------------|
|        |           | N         | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub> | %F              | PI<br>(Lab) | φ'<br>(high)<br>(deg) | φ'<br>(low)<br>(deg) | Sat. Unit Weight | Su<br>(psf) | Sr<br>(psf)              |              |                                |
|        | GeoMean:  | 6         | 4               | 7                               | 8               | -           | 34                    | 29                   | 110              | -           | -                        |              |                                |
|        | Average:  | 6         | 5               | 8                               | 10              | -           | 34                    | 29                   | 110              | -           | -                        |              |                                |
|        | St. Dev.: | 2.7       | 2.2             | 3.5                             | -               | -           | 1.9                   | 1.9                  | 8.2              | -           | -                        |              |                                |
|        | cov:      | 0.45      | 0.47            | 0.44                            | -               | -           | 0.05                  | 0.06                 | 0.07             | -           | -                        |              |                                |
| Boring | Elevation | N         | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub> | %F <sup>3</sup> | PI<br>(Lab) | ф'<br>(high)<br>(deg) | ф'<br>(Iow)<br>(deg) | Sat. Unit Weight | Su<br>(psf) | Sr <sup>4</sup><br>(psf) | USCS         | Explanation for Sample Removal |
| H-1-85 | 199.59    | 4         | 3               | 5                               | 18              | -           | 33                    | 28                   | 95               | -           | -                        | SM           |                                |
| H-1-85 | 197.59    | 8         | 6               | 10                              | 18              | -           | 36                    | 31                   | 110              | -           | -                        | SM           |                                |
| H-2-85 | 185.09    | 7         | 5               | 9                               | 15              | -           | 35                    | 30                   | 110              | -           | -                        | SM           |                                |
| H-3-85 | 214.99    | 5         | 4               | 6                               | 4               | -           | 34                    | 29                   | 110              | -           | -                        | SP           |                                |
| H-3-85 | 212.99    | 3         | 2               | 4                               | 4               | -           | 32                    | 27                   | 105              | -           | -                        | SP           |                                |
| H-3-85 | 210.99    | 5         | 4               | 7                               | 4               | -           | 34                    | 29                   | 120              | -           | -                        | SP           |                                |
| H-3-85 | 208.49    | 11        | 9               | 14                              | 5               | -           | 37                    | 32                   | 117.5            | -           | -                        | SP-SM        |                                |
|        |           |           |                 |                                 |                 |             |                       |                      |                  |             |                          |              |                                |
|        |           |           |                 |                                 |                 |             |                       |                      |                  |             |                          |              |                                |
|        |           |           |                 |                                 |                 |             |                       |                      |                  |             |                          |              |                                |
|        |           |           |                 |                                 |                 |             |                       |                      |                  |             |                          |              |                                |
|        |           |           |                 |                                 |                 |             |                       |                      |                  |             |                          |              |                                |
|        |           |           |                 |                                 |                 |             |                       |                      | 1                |             | 1                        | 1            |                                |
|        |           |           |                 |                                 |                 |             |                       |                      |                  |             |                          |              |                                |
|        |           |           |                 |                                 |                 |             |                       |                      |                  |             |                          |              |                                |
|        |           |           |                 |                                 |                 |             |                       |                      | +                |             | <del> </del>             | <del> </del> |                                |
|        |           |           |                 |                                 |                 |             |                       |                      |                  |             | t                        | 1            |                                |

Notes

<sup>1.</sup> Highlighted cells in yellow if shown represent samples that were removed as outliers.

<sup>2.</sup> Friction angle, unit weight, and corrected blow count values were correlated using specified methodology in the WOOD Geotechnical SPM. Where applicable, undrained Shear Strength of fine grained ESUs were determined using Equation 9 in the WOOD Geotechnical SPM.

<sup>3.</sup> Fines content percentages determined through laboratory testing are highlighted in orange if shown. Non-highlighted values have been estimated from sample field classifications, applying the fines content of a lab tested sample with similar properties, or using the average of two lab tested samples.

<sup>4.</sup> Where applicable, residual strength is calculated using the existing relationships and weighting scheme per the GDM (section 6-2.2) to determine residual strengths for samples with (N1)60cs less than or equal to 20. Per Kramer 2008, samples that triggered liquefaction (FoS<1.2) but also has an (N1)60cs>20, uses the residual strength value for a soil with (N1)60cs=20, effectively capping the residual strength calculation at (N1)60cs=20.

#### 1. Check N160 COV is between 15 and 45%

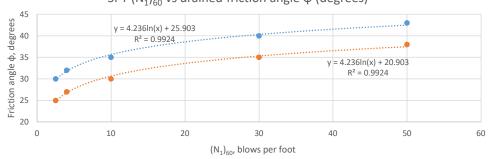
| Selected Design N160:           | 7    |
|---------------------------------|------|
| Coefficient of Variation (COV): | 0.44 |

<sup>\* 15</sup> and 45% come from GEC 5 Sabatini (2002)

#### 2. Check Phi' is between 2 to 13%

| (N <sub>1</sub> ) <sub>60</sub> (blows per foot) | Friction angle φ |
|--|------------------|
| (11760 (516115 per 1665)                         | (degrees)        |
| 2.5  | 25               |
| 2.5  | 30               |
| 4  | 27               |
| 4  | 32               |
| 10   | 30               |
| 10   | 35               |
| 30   | 35               |
| 30   | 40               |
| 50   | 38               |
| 50   | 43               |

SPT  $(N_1)_{60}$  vs drained friction angle  $\varphi$  (degrees)



|          | φ (high) | ф (low) | ф (avg) |
|----------|----------|---------|---------|
| GeoMean: | 34       | 29      | 32      |

| φ' cov |
|--------|
| 0.06   |

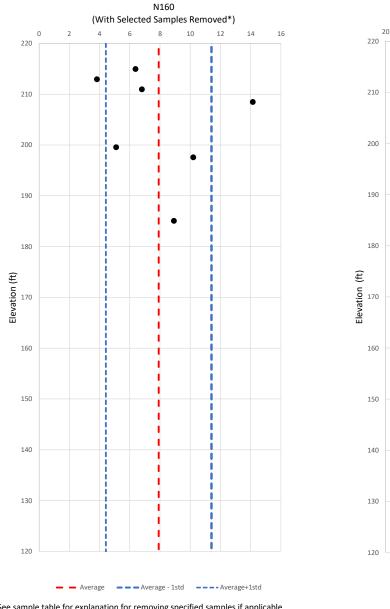
| Selected Design Phi' (deg): | 34                             |   |
|-----------------------------|--------------------------------|---|
| Notes on Selection:         | The estimated fine 30% fines). | es content is 8% (geomean). The friction angle is interpolated based on fines content (phi' (high) at 5% fines, and phi' (low) at |

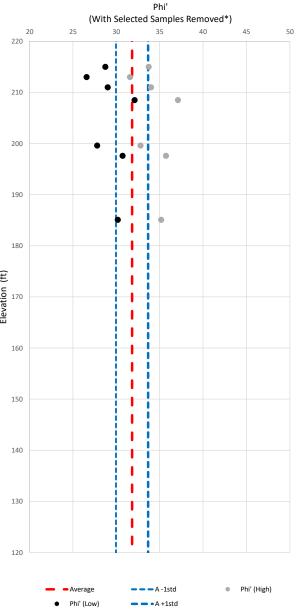
| Pick Representative USCS:        | SP-SM | *Using Predominant USCS Classification  |
|----------------------------------|-------|---|
| Pick Representative Unit Weight: | 110   |   |
| Notes on Selection:              |       | unit weights were correlated using CALTRANS Geotechnical Manual (2014), verified with applicable ranges presented in Codotu d in WOOD SPM. The geometric mean of the unit weights was rounded to the nearest 5pcf, as specified in WOOD SPM. Data set |

WSDOT GDM Table 5-1

<sup>\*</sup> Phi' Developed from WSDOT Correlation

<sup>\* 2</sup> to 13% comes from GEC 5 Sabatini (2002)





<sup>\*</sup>See sample table for explanation for removing specified samples if applicable

|           | ESU Name: |                 | ESU 2A - Very Loose to Loose Sand/Gravel |                 |             |                       |                      |                  |             |                          |  |  |  |
|-----------|-----------|-----------------|--|-----------------|-------------|-----------------------|----------------------|------------------|-------------|--------------------------|--|--|--|
| ,         | N         | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub>          | %F              | PI<br>(Lab) | ф'<br>(high)<br>(deg) | ф'<br>(low)<br>(deg) | Sat. Unit Weight | Su<br>(psf) | Sr<br>(psf)              |  |  |  |
| GeoMean:  | 9         | 7               | 10                                       | 20              | -           | 35                    | 30                   | 110              | -           | -                        |  |  |  |
| Average:  | 10        | 8               | 11                                       | 21              | -           | 36                    | 31                   | 110              | -           | -                        |  |  |  |
| St. Dev.: | 5.1       | 4.4             | 5.9                                      | -               | -           | 2.1                   | 2.1                  | 7.2              | -           | -                        |  |  |  |
| cov:      | 0.53      | 0.52            | 0.54                                     | -               | -           | 0.06                  | 0.07                 | 0.07             | -           | -                        |  |  |  |
| Elevation | N         | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub>          | %F <sup>3</sup> | PI<br>(Lab) | φ'<br>(high)<br>(deg) | φ'<br>(low)<br>(deg) | Sat. Unit Weight | Su<br>(psf) | Sr <sup>4</sup><br>(psf) |  |  |  |

| Boring | Elevation | N  | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub> | %F <sup>3</sup> | PI<br>(Lab) | φ'<br>(high)<br>(deg) | φ'<br>(low)<br>(deg) | Sat. Unit Weight | Su<br>(psf) | Sr <sup>4</sup><br>(psf) | uscs  | Explanation for Sample Removal |
|--------|-----------|----|-----------------|---------------------------------|-----------------|-------------|-----------------------|----------------------|------------------|-------------|--------------------------|-------|--------------------------------|
| H-1-85 | 195.59    | 3  | 2               | 4                               | 22              | -           | 32                    | 27                   | 90               | -           | -                        | SM    |                                |
| H-1-85 | 193.09    | 4  | 3               | 5                               | 28              | -           | 33                    | 28                   | 95               | -           | -                        | SM    |                                |
| H-1-85 | 190.59    | 10 | 9               | 12                              | 18              | -           | 36                    | 31                   | 110              | -           | -                        | SM    |                                |
| H-1-85 | 188.09    | 9  | 8               | 10                              | 31              | -           | 36                    | 31                   | 110              | -           | -                        | SM    |                                |
| H-2-85 | 183.09    | 17 | 13              | 22                              | 24              |             | 39                    | 34                   | 115              | -           | -                        | SM    |                                |
| H-2-85 | 181.09    | 13 | 10              | 18                              | 15              | -           | 38                    | 33                   | 115              | -           | -                        | SM    |                                |
| H-2-85 | 178.59    | 20 | 16              | 23                              | 18              | -           | 39                    | 34                   | 115              | -           | -                        | SM    |                                |
| H-2-85 | 176.09    | 8  | 7               | 9                               | 16              | -           | 35                    | 30                   | 110              | -           | -                        | SM    |                                |
| H-2-85 | 173.59    | 7  | 6               | 7                               | 30              | -           | 34                    | 29                   | 110              | -           | -                        | SM    |                                |
| H-2-85 | 171.09    | 7  | 7               | 8                               | 22              | -           | 34                    | 29                   | 110              | -           | -                        | SM    |                                |
| H-2-85 | 168.59    | 20 | 19              | 20                              | 25              | -           | 39                    | 34                   | 115              | -           | -                        | SM    |                                |
| H-2-85 | 166.09    | 10 | 10              | 9                               | 27              | -           | 35                    | 30                   | 110              | -           | -                        | SM    |                                |
| H-2-85 | 163.59    | 7  | 7               | 6                               | 24              | -           | 34                    | 29                   | 100              | -           | -                        | SM    |                                |
| H-3-85 | 205.99    | 5  | 4               | 6                               | 10              | -           | 34                    | 29                   | 105              | -           | -                        | SP-SM |                                |
| H-3-85 | 203.49    | 8  | 7               | 9                               | 12              | -           | 35                    | 30                   | 115              | -           | -                        | SP-SM |                                |
| H-3-85 | 200.99    | 6  | 6               | 7                               | 12              | -           | 34                    | 29                   | 110              | -           | -                        | SM    |                                |
| H-3-85 | 198.49    | 11 | 10              | 11                              | 19              | -           | 36                    | 31                   | 110              |             | -                        | SM    |                                |
|        |           |    |                 |                                 |                 |             |                       |                      |                  |             |                          |       |                                |
|        |           |    |                 |                                 |                 |             |                       |                      |                  |             |                          |       |                                |
|        |           |    |                 |                                 |                 |             |                       |                      |                  |             |                          |       |                                |
|        |           |    |                 |                                 |                 |             |                       |                      |                  |             |                          |       |                                |
|        |           |    |                 |                                 |                 |             |                       |                      |                  |             |                          |       |                                |

#### Notes:

- 1. Highlighted cells in yellow if shown represent samples that were removed as outliers.
- 2. Friction angle, unit weight, and corrected blow count values were correlated using specified methodology in the WOOD Geotechnical SPM. Where applicable, undrained Shear Strength of fine grained ESUs were determined using Equation 9 in the WOOD Geotechnical SPM.
- 3. Fines content percentages determined through laboratory testing are highlighted in orange if shown. Non-highlighted values have been estimated from sample field classifications, applying the fines content of a lab tested sample with similar properties, or using the average of two lab tested samples.
- 4. Where applicable, residual strength is calculated using the existing relationships and weighting scheme per the GDM (section 6-2.2) to determine residual strengths for samples with (N1)60cs less than or equal to 20. Per Kramer 2008, samples that triggered liquefaction (FoS<1.2) but also has an (N1)60cs>20, uses the residual strength value for a soil with (N1)60cs=20, effectively capping the residual strength calculation at (N1)60cs=20.

#### 1. Check N160 COV is between 15 and 45%

| Selected Design N160:           | 10   |
|---------------------------------|------|
| Coefficient of Variation (COV): | 0.54 |

<sup>\* 15</sup> and 45% come from GEC 5 Sabatini (2002)

#### 2. Check Phi' is between 2 to 13%

| (N <sub>1</sub> ) <sub>60</sub> (blows per foot) | Friction angle φ<br>(degrees) |
|--|-------------------------------|
| 2.5  | 25                            |
| 2.5  | 30                            |
| 4  | 27                            |
| 4  | 32                            |
| 10   | 30                            |
| 10   | 35                            |
| 30   | 35                            |
| 30   | 40                            |
| 50   | 38                            |
| 50   | 43                            |

<sup>\*</sup> Phi' Developed from WSDOT Correlation

|   | y = 4.236        | ln(x) + 25.903 |    |                                   | •                      |    |
|---|------------------|----------------|----|-----------------------------------|------------------------|----|
|   | R <sup>2</sup> = | 0.9924         |    |                                   |                        |    |
|   |                  |                |    | y = 4.236ln<br>R <sup>2</sup> = 0 | (x) + 20.903<br>0.9924 |    |
|   | ,,,,,,,,,,,,     |                |    |                                   |                        |    |
|   |                  |                |    |                                   |                        |    |
| 0 | 10               | 20             | 30 | 40                                | 50                     | 60 |

WSDOT GDM Table 5-1

|          | φ (high) | ф (low) | φ (avg) |
|----------|----------|---------|---------|
| GeoMean: | 35       | 30      | 33      |

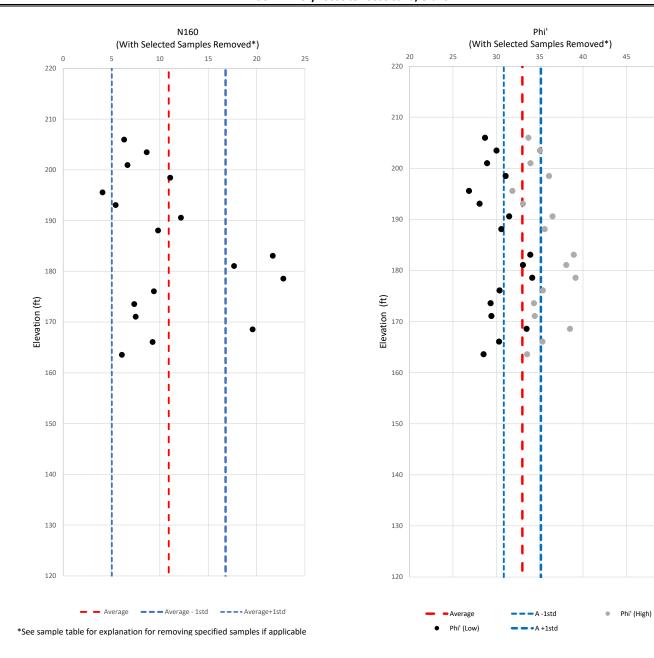
| ) | ф (avg) | φ' cov |
|---|---------|--------|
|   | 33      | 0.07   |

| Selected Design Phi' (deg): | 32                             |  |
|-----------------------------|--------------------------------|--|
| Notes on Selection:         | The estimated fine 30% fines). | es content is 20% (geomean). The friction angle is interpolated based on fines content (phi' (high) at 5% fines, and phi' (low) at |

| Pick Representative USCS:        | SM   | *Using Predominant USCS Classification  |  |  |  |  |
|----------------------------------|--|---|--|--|--|--|
| Pick Representative Unit Weight: | 110  |   |  |  |  |  |
|                                  | Individual sample  | unit weights were correlated using CALTRANS Geotechnical Manual (2014), verified with applicable ranges presented in Codotu |  |  |  |  |
| Notes on Selection:              | (2001), as specified in WOOD SPM. The geometric mean of the unit weights was rounded to the nearest 5pcf, as specified in WOOD SPM. Data set |   |  |  |  |  |
|                                  | COV was 7%.  |   |  |  |  |  |

<sup>\* 2</sup> to 13% comes from GEC 5 Sabatini (2002)

50



|           | ESU Name: |                 |                                 | FSII 21         | 3 - Medium I | Jense Sand/           | Gravel               |                  |             | 1                        |      |                                |
|-----------|-----------|-----------------|---------------------------------|-----------------|--------------|-----------------------|----------------------|------------------|-------------|--------------------------|------|--------------------------------|
|           | N         | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub> | %F              | PI<br>(Lab)  | φ' (high) (deg)       | φ'                   | Sat. Unit Weight | Su<br>(psf) | Sr<br>(psf)              |      |                                |
| GeoMean:  | 17        | 16              | 14                              | 40              | -            | 37                    | 32                   | 110              | -           | 497                      |      |                                |
| Average:  | 17        | 17              | 15                              | 44              | -            | 37                    | 32                   | 110              | -           | 514                      |      |                                |
| St. Dev.: | 3.4       | 3.3             | 3.2                             | -               | -            | 1.0                   | 1.0                  | 2.0              | -           | -                        |      |                                |
| cov:      | 0.20      | 0.20            | 0.22                            | -               | -            | 0.03                  | 0.03                 | 0.02             | -           | -                        |      |                                |
| Elevation | N         | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub> | %F <sup>3</sup> | PI<br>(Lab)  | φ'<br>(high)<br>(deg) | φ'<br>(low)<br>(deg) | Sat. Unit Weight | Su<br>(psf) | Sr <sup>4</sup><br>(psf) | USCS | Explanation for Sample Removal |
| 161.09    | 18        | 17              | 15                              | 26              | -            | 37                    | 32                   | 110              | -           | 527                      | SM   |                                |
| 158.59    | 17        | 16              | 14                              | 60              | -            | 37                    | 32                   | 110              | -           | 538                      | ML   |                                |
| 156.09    | 11        | 11              | 9                               | 51              | -            | 35                    | 30                   | 110              | -           | 331                      | ML   |                                |
| 153.59    | 21        | 21              | 18                              | 33              | -            | 38                    | 33                   | 115              | -           | 735                      | SM   |                                |
| 151.09    | 16        | 16              | 13                              | 22              | -            | 37                    | 32                   | 110              | -           | 441                      | SM   |                                |
| 195.99    | 19        | 18              | 18                              | 70              | -            | 38                    | 33                   | 110              | -           | -                        | ML   |                                |
|           |           |                 |                                 |                 |              |                       |                      |                  |             |                          |      |                                |
|           |           |                 |                                 |                 |              |                       |                      |                  |             |                          |      |                                |
|           |           |                 |                                 |                 |              |                       |                      |                  |             |                          |      |                                |
|           |           |                 |                                 |                 |              |                       |                      |                  |             |                          |      |                                |
|           |           |                 |                                 |                 |              |                       |                      |                  |             |                          |      |                                |
|           |           |                 |                                 |                 |              |                       |                      |                  |             |                          |      |                                |
|           |           |                 |                                 |                 |              |                       |                      |                  |             |                          |      |                                |
|           |           |                 |                                 |                 |              |                       |                      |                  |             |                          |      |                                |
|           |           |                 |                                 |                 |              |                       |                      |                  |             |                          |      |                                |

Notes:

H-2-85 H-2-85 H-2-85 H-2-85 H-2-85 H-3-85

 $<sup>{\</sup>bf 1.} \ Highlighted \ cells \ in \ yellow \ if \ shown \ represent \ samples \ that \ were \ removed \ as \ outliers.$ 

<sup>2.</sup> Friction angle, unit weight, and corrected blow count values were correlated using specified methodology in the WOOD Geotechnical SPM. Where applicable, undrained Shear Strength of fine grained ESUs were determined using Equation 9 in the WOOD Geotechnical SPM.

<sup>3.</sup> Fines content percentages determined through laboratory testing are highlighted in orange if shown. Non-highlighted values have been estimated from sample field classifications, applying the fines content of a lab tested sample with similar properties, or using the average of two lab tested samples.

<sup>4.</sup> Where applicable, residual strength is calculated using the existing relationships and weighting scheme per the GDM (section 6-2.2) to determine residual strengths for samples with (N1)60cs less than or equal to 20. Per Kramer 2008, samples that triggered liquefaction (FoS<1.2) but also has an (N1)60cs>20, uses the residual strength value for a soil with (N1)60cs=20, effectively capping the residual strength calculation at (N1)60cs=20.

#### 1. Check N160 COV is between 15 and 45%

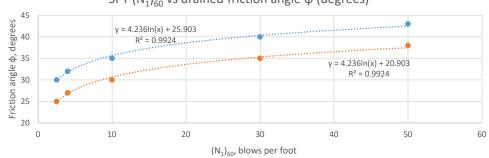
| Selected Design N160:           | 14   |
|---------------------------------|------|
| Coefficient of Variation (COV): | 0.22 |

<sup>\* 15</sup> and 45% come from GEC 5 Sabatini (2002)

#### 2. Check Phi' is between 2 to 13%

| (N <sub>1</sub> ) <sub>60</sub> (blows per foot) | Friction angle φ (degrees) |
|--|----------------------------|
| 2.5  | 25                         |
| 2.5  | 30                         |
| 4  | 27                         |
| 4  | 32                         |
| 10   | 30                         |
| 10   | 35                         |
| 30   | 35                         |
| 30   | 40                         |
| 50   | 38                         |
| 50   | 43                         |

SPT  $(N_1)_{60}$  vs drained friction angle  $\varphi$  (degrees)



|          | φ (high) | ф (low) | φ (avg) |
|----------|----------|---------|---------|
| GeoMean: | 37       | 32      | 35      |

| ф' | cov |
|----|-----|
| 0  | .03 |

| Selected Design Phi' (deg): | 32 |
|-----------------------------|----|
|                             |    |

Notes on Selection:

The estimated fines content is 40% (geomean). The high fines content supports the use of the lower bound of the friction angle range.

| Pick Representative USCS:        | SM  | *Using Predominant USCS Classification  |
|----------------------------------|-----|---|
| Pick Representative Unit Weight: | 110 |   |
| Notes on Selection:              | •   | unit weights were correlated using CALTRANS Geotechnical Manual (2014), verified with applicable ranges presented in Codotu d in WOOD SPM. The geometric mean of the unit weights was rounded to the nearest 5pcf, as specified in WOOD SPM. Data set |

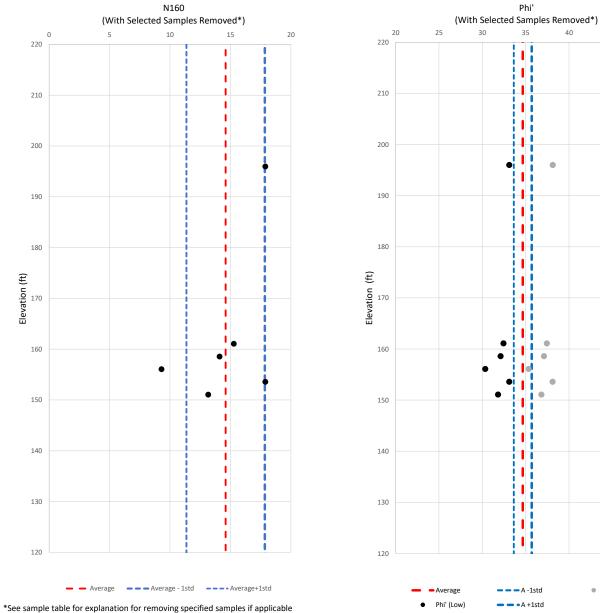
#### 4. Residual Strength (psf):

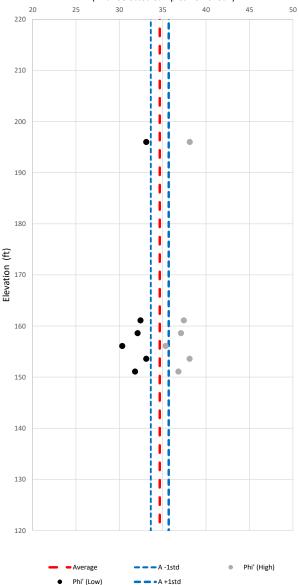
| Sr Selected:        | 497                |  |
|---------------------|--------------------|--|
| Notes on Selection: | Individual sample  | residual strength is calculated using the existing relationships and weighting scheme per the GDM (section 6-2.2) to determine |
| Notes on Selection. | residual strengths | for samples with (N1)60cs less than or equal to 20.  |

WSDOT GDM Table 5-1

<sup>\*</sup> Phi' Developed from WSDOT Correlation

<sup>\* 2</sup> to 13% comes from GEC 5 Sabatini (2002)





Phi'

|          |           | ESU Name: |                 | ESU 4B - Dense to Very Dense Sand/Gravel |                 |             |                       |                      |                  |             |                          |       |                                |
|----------|-----------|-----------|-----------------|--|-----------------|-------------|-----------------------|----------------------|------------------|-------------|--------------------------|-------|--------------------------------|
|          | 1         | N         | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub>          | %F              | PI<br>(Lab) | φ'<br>(high)<br>(deg) | φ'<br>(low)<br>(deg) | Sat. Unit Weight | Su<br>(psf) | Sr<br>(psf)              |       |                                |
|          | GeoMean:  | 148       | 108             | 111                                      | 18              | -           | 46                    | 41                   | 130              | -           | -                        |       |                                |
|          | Average:  | 174       | 111             | 114                                      | 23              | -           | 46                    | 41                   | 130              | -           | -                        |       |                                |
|          | St. Dev.: | 106.1     | 26.1            | 28.3                                     | -               | -           | 1.1                   | 1.1                  | 3.0              | -           | -                        |       |                                |
|          | cov:      | 0.61      | 0.24            | 0.25                                     | -               | -           | 0.02                  | 0.03                 | 0.02             | -           | -                        | 1     |                                |
| Boring   | Elevation | N         | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub>          | %F <sup>3</sup> | PI<br>(Lab) | φ'<br>(high)<br>(deg) | φ'<br>(low)<br>(deg) | Sat. Unit Weight | Su<br>(psf) | Sr <sup>4</sup><br>(psf) | uscs  | Explanation for Sample Removal |
| W-217-20 | 217.1     | 93        | 102             | 167                                      | 45              | -           | 48                    | 43                   | 130              | -           | -                        | SM    |                                |
| W-217-20 | 214.6     | 63        | 74              | 101                                      | 30              | -           | 45                    | 40                   | 130              | -           | -                        | SM    |                                |
| W-217-20 | 212.1     | 111       | 117             | 144                                      | 37              | -           | 47                    | 42                   | 130              | -           | -                        | SM    |                                |
| W-217-20 | 209.6     | 100       | 125             | 142                                      | 40              | -           | 47                    | 42                   | 130              | -           | -                        | SM    |                                |
| W-217-20 | 204.6     | 100       | 139             | 148                                      | 40              | -           | 47                    | 42                   | 130              | -           | -                        | SM    |                                |
| W-217-20 | 199.6     | 300       | 139             | 141                                      | 40              | =           | 47                    | 42                   | 130              | -           | -                        | SM    |                                |
| W-217-20 | 169.6     | 300       | 147             | 124                                      | 11              | -           | 46                    | 41                   | 140              | -           | -                        | SW    |                                |
| W-217-20 | 164.6     | 120       | 147             | 121                                      | 30              | -           | 46                    | 41                   | 130              | -           | -                        | SM    |                                |
| W-217-20 | 159.6     | 120       | 147             | 119                                      | 30              | -           | 46                    | 41                   | 130              | -           | -                        | GM    |                                |
| H-1-85   | 185.59    | 138       | 95              | 102                                      | 8               | -           | 46                    | 41                   | 130              | -           | -                        | SP-SM |                                |
| H-1-85   | 183.09    | 297       | 95              | 97                                       | 9               | -           | 45                    | 40                   | 130              | -           | -                        | SP-SM |                                |
| H-1-85   | 180.59    | 400       | 95              | 93                                       | 7               | -           | 45                    | 40                   | 135              | -           | -                        | SP-SM |                                |
| H-1-85   | 175.59    | 300       | 95              | 90                                       | 6               | -           | 45                    | 40                   | 135              | -           | -                        | SP-SM |                                |
| H-2-85   | 148.59    | 71        | 71              | 63                                       | 7               | -           | 43                    | 38                   | 135              | -           | -                        | SP-SM |                                |
| H-3-85   | 193.49    | 118       | 95              | 91                                       | 11              | -           | 45                    | 40                   | 130              | -           | -                        | SP-SM |                                |
| H-3-85   | 190.99    | 153       | 95              | 88                                       | 11              | -           | 45                    | 40                   | 130              | -           | -                        | SM    |                                |
|          |           |           |                 |  |                 |             |                       |                      |                  |             |                          |       |                                |
|          |           |           |                 |  |                 |             |                       |                      |                  |             |                          |       |                                |
|          |           |           |                 |  |                 |             |                       |                      |                  | •           |                          |       |                                |
|          |           |           |                 |  |                 |             |                       |                      |                  |             |                          |       |                                |
|          |           |           |                 |  |                 |             |                       |                      |                  |             |                          |       |                                |
|          |           |           |                 |  |                 |             |                       |                      |                  |             |                          |       |                                |

Notes:

 $<sup>{\</sup>bf 1.} \ Highlighted \ cells \ in \ yellow \ if \ shown \ represent \ samples \ that \ were \ removed \ as \ outliers.$ 

<sup>2.</sup> Friction angle, unit weight, and corrected blow count values were correlated using specified methodology in the WOOD Geotechnical SPM. Where applicable, undrained Shear Strength of fine grained ESUs were determined using Equation 9 in the WOOD Geotechnical SPM.

<sup>3.</sup> Fines content percentages determined through laboratory testing are highlighted in orange if shown. Non-highlighted values have been estimated from sample field classifications, applying the fines content of a lab tested sample with similar properties, or using the average of two lab tested samples.

<sup>4.</sup> Where applicable, residual strength is calculated using the existing relationships and weighting scheme per the GDM (section 6-2.2) to determine residual strengths for samples with (N1)60cs less than or equal to 20. Per Kramer 2008, samples that triggered liquefaction (FoS<1.2) but also has an (N1)60cs>20, uses the residual strength value for a soil with (N1)60cs=20, effectively capping the residual strength calculation at (N1)60cs=20.

#### 1. Check N160 COV is between 15 and 45%

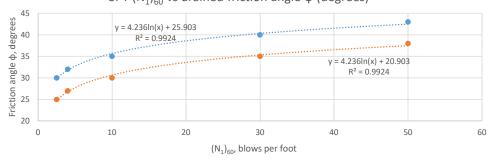
| Selected Design N160:           | 111  |
|---------------------------------|------|
| Coefficient of Variation (COV): | 0.25 |

<sup>\* 15</sup> and 45% come from GEC 5 Sabatini (2002)

#### 2. Check Phi' is between 2 to 13%

| (N <sub>1</sub> ) <sub>60</sub> (blows per foot) | Friction angle φ |
|--|------------------|
| (11760 (516115 per 1665)                         | (degrees)        |
| 2.5  | 25               |
| 2.5  | 30               |
| 4  | 27               |
| 4  | 32               |
| 10   | 30               |
| 10   | 35               |
| 30   | 35               |
| 30   | 40               |
| 50   | 38               |
| 50   | 43               |

SPT  $(N_1)_{60}$  vs drained friction angle  $\varphi$  (degrees)



|          | φ (high) | ф (low) | φ (avg) |
|----------|----------|---------|---------|
| GeoMean: | 46       | 41      | 43      |

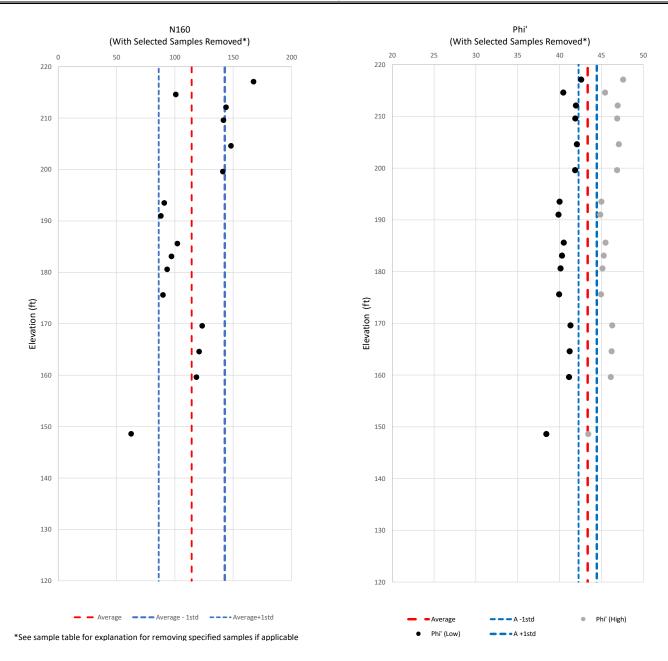
| Selected Design Phi' (deg): | 43                |   |
|-----------------------------|-------------------|---|
| Notes on Selection:         | The estimated ged | omean fines content is 18% (geomean). The friction angle is taken as the upper bound and capped at 43 degrees for glacially |
| Notes on Selection.         | consolidated mate | erial with fines content less than 70%.   |

| Pick Representative USCS:        | *Using Predominant USCS Classification   |   |  |
|----------------------------------|--|---|--|
| Pick Representative Unit Weight: | 130  |   |  |
|                                  | Individual sample  | unit weights were correlated using CALTRANS Geotechnical Manual (2014), verified with applicable ranges presented in Codotu |  |
| Notes on Selection:              | (2001), as specified in WOOD SPM. The geometric mean of the unit weights was rounded to the nearest 5pcf, as specified in WOOD SPM. Data set |   |  |
|                                  | COV was 2%.  |   |  |

WSDOT GDM Table 5-1

<sup>\*</sup> Phi' Developed from WSDOT Correlation

<sup>\* 2</sup> to 13% comes from GEC 5 Sabatini (2002)



|          |           | ESU Name: |                 | ESU 5B                          | - Very Stiff to | o Hard Silt a | nd Clay/Den           | se to Very D         | ense Silt        |             |                          |      |                                |
|----------|-----------|-----------|-----------------|---------------------------------|-----------------|---------------|-----------------------|----------------------|------------------|-------------|--------------------------|------|--------------------------------|
|          |           | N         | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub> | %F              | PI<br>(Lab)   | ф'<br>(high)<br>(deg) | ф'<br>(low)<br>(deg) | Sat. Unit Weight | Su<br>(psf) | Sr<br>(psf)              |      |                                |
|          | GeoMean:  | 76        | 108             | 99                              | 82              | 20            | 45                    | 40                   | 130              | -           | -                        |      |                                |
|          | Average:  | 80        | 113             | 102                             | 83              | 21            | 45                    | 40                   | 130              | =           | -                        |      |                                |
|          | St. Dev.: | 26.3      | 35.8            | 29.2                            | -               | -             | 1.3                   | 1.3                  | 2.2              | -           | -                        |      |                                |
|          | cov:      | 0.33      | 0.32            | 0.29                            | -               | -             | 0.03                  | 0.03                 | 0.02             | -           | -                        |      |                                |
| Boring   | Elevation | N         | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub> | %F <sup>3</sup> | PI<br>(Lab)   | φ'<br>(high)<br>(deg) | ф'<br>(low)<br>(deg) | Sat. Unit Weight | Su<br>(psf) | Sr <sup>4</sup><br>(psf) | uscs | Explanation for Sample Removal |
| W-217-20 | 194.6     | 51        | 71              | 69                              | 90              | 18            | 44                    | 39                   | 130              | -           | -                        | ML   |                                |
| W-217-20 | 189.6     | 82        | 120             | 113                             | 90              | -             | 46                    | 41                   | 130              | -           | -                        | ML   |                                |
| W-217-20 | 184.6     | 55        | 81              | 73                              | 92              | 16            | 44                    | 39                   | 130              | -           | -                        | CL   |                                |
| W-217-20 | 179.6     | 100       | 147             | 130                             | 73              | 28            | 47                    | 42                   | 125              | -           | -                        | СН   |                                |
| W-217-20 | 174.6     | 110       | 147             | 127                             | 70              | -             | 46                    | 41                   | 130              | -           | -                        | CL   |                                |
|          |           |           |                 |                                 |                 |               |                       |                      |                  |             |                          |      |                                |
|          |           |           |                 |                                 |                 |               |                       |                      |                  |             |                          |      |                                |
|          |           |           |                 |                                 |                 |               |                       |                      |                  |             |                          |      |                                |
|          |           |           |                 |                                 |                 |               |                       |                      |                  |             |                          |      |                                |
|          |           |           |                 |                                 |                 |               |                       |                      |                  |             |                          |      |                                |
|          |           |           |                 |                                 |                 |               |                       |                      |                  |             |                          |      |                                |
|          |           |           |                 |                                 |                 |               |                       |                      |                  |             |                          |      |                                |
|          |           |           |                 |                                 |                 |               |                       |                      | 1                |             |                          |      |                                |
|          |           |           |                 |                                 |                 |               |                       |                      |                  |             |                          |      |                                |
|          |           |           |                 |                                 |                 |               |                       |                      | <u> </u>         |             |                          |      |                                |
|          |           |           |                 |                                 |                 |               |                       |                      |                  |             |                          |      |                                |
|          |           |           |                 |                                 |                 |               |                       |                      |                  |             |                          |      |                                |

Notes:

<sup>1.</sup> Highlighted cells in yellow if shown represent samples that were removed as outliers.

<sup>2.</sup> Friction angle, unit weight, and corrected blow count values were correlated using specified methodology in the WOOD Geotechnical SPM. Where applicable, undrained Shear Strength of fine grained ESUs were determined using Equation 9 in the WOOD Geotechnical SPM.

<sup>3.</sup> Fines content percentages determined through laboratory testing are highlighted in orange if shown. Non-highlighted values have been estimated from sample field classifications, applying the fines content of a lab tested sample with similar properties, or using the average of two lab tested samples.

<sup>4.</sup> Where applicable, residual strength is calculated using the existing relationships and weighting scheme per the GDM (section 6-2.2) to determine residual strengths for samples with (N1)60cs less than or equal to 20. Per Kramer 2008, samples that triggered liquefaction (FoS<1.2) but also has an (N1)60cs>20, uses the residual strength value for a soil with (N1)60cs=20, effectively capping the residual strength calculation at (N1)60cs=20.

#### 1. Check N160 COV is between 15 and 45%

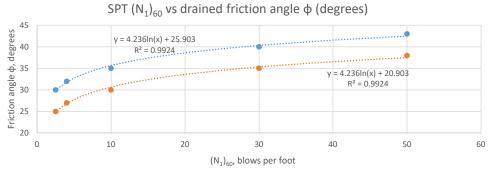
| Selected Design N160:           | 99   |
|---------------------------------|------|
| Coefficient of Variation (COV): | 0.29 |

<sup>\* 15</sup> and 45% come from GEC 5 Sabatini (2002)

#### 2. Check Phi' is between 2 to 13%

| (N <sub>1</sub> ) <sub>60</sub> (blows per foot) | Friction angle φ |
|--|------------------|
| (11760 (516115 per 1665)                         | (degrees)        |
| 2.5  | 25               |
| 2.5  | 30               |
| 4  | 27               |
| 4  | 32               |
| 10   | 30               |
| 10   | 35               |
| 30   | 35               |
| 30   | 40               |
| 50   | 38               |
| 50   | 43               |

WSDOT GDM Table 5-1



|          | φ (high) | ф (low) | ф (avg) |
|----------|----------|---------|---------|
| GeoMean: | 45       | 40      | 43      |

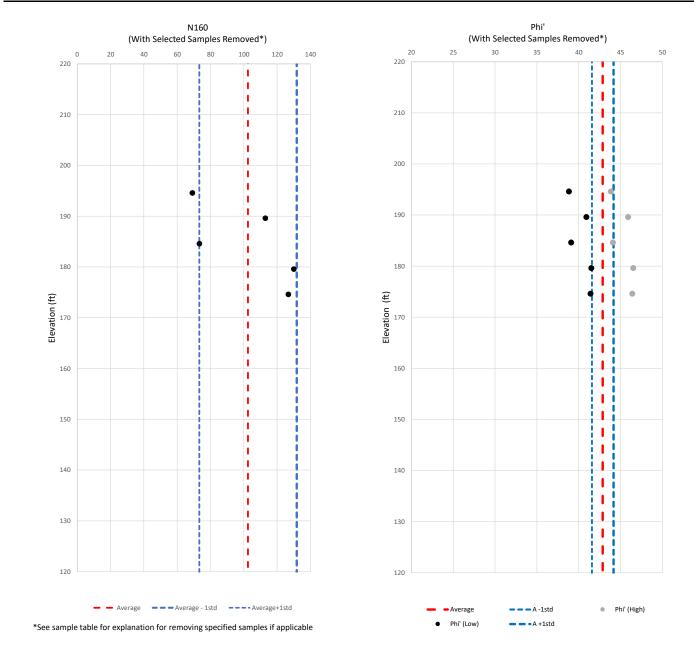
| φ' cov |
|--------|
| 0.03   |

| Selected Design Phi' (deg): | 43                 |   |
|-----------------------------|--------------------|---|
| Notes on Selection:         | The estimated ged  | omean fines content is 82% (geomean). The friction angle is taken as the average of upper bound and lower bound and capped at |
| Notes on Selection:         | 43 degrees for gla | cially consolidated material with fines content more than 70%.  |

| Pick Representative USCS:        | ML/CL *Using Predominant USCS Classification |   |
|----------------------------------|--|---|
| Pick Representative Unit Weight: | 130  |   |
| Notes on Selection:              | •  | unit weights were correlated using CALTRANS Geotechnical Manual (2014), verified with applicable ranges presented in Codotu d in WOOD SPM. The geometric mean of the unit weights was rounded to the nearest 5pcf, as specified in WOOD SPM. Data set |

<sup>\*</sup> Phi' Developed from WSDOT Correlation

<sup>\* 2</sup> to 13% comes from GEC 5 Sabatini (2002)



One of the primary shortcomings of the Mononobe-Okabe method is that it cannot consider the effect of cohesion in the backfill on the seismic active earth pressure. Even relatively small amounts of cohesion in the backfill can significantly reduce the seismic active earth pressure. Sources of cohesion in backfill soils include both true cohesion due to inter-particle bonding and apparent cohesion due to capillary forces in the backfill. The influence of cohesion on the seismic active earth pressure is a function of the normalizing parameter  $c\gamma/H$ , where  $\gamma$  is the unit weight of the backfill soil. Figure 11-14 presents a plot of the seismic active earth pressure coefficient,  $k_{AE}$ , as a function of the normalizing parameter  $c/\gamma H$  and the seismic coefficient,  $k_h$ , for a friction angle of 35° and for a uniform level backfill. An Appendix in NCHRP Report 611 presents additional plots for friction angles of 30° and 40°.

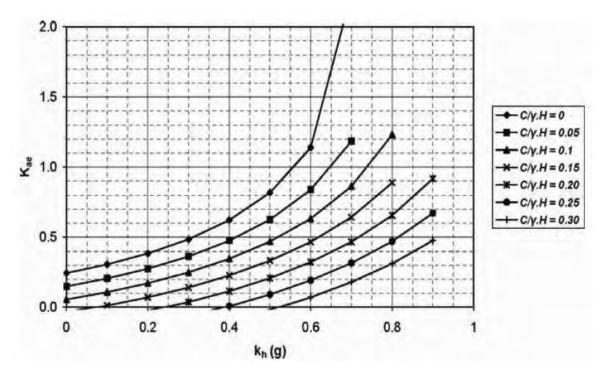


Figure 11-14 Effect of cohesion on the seismic active earth pressure coefficient for  $\phi = 35^{\circ}$  (NCHRP, 2008)

NCHRP Report 611 provides recommendations for the maximum amount of apparent cohesion that should be assumed for backfill soil as a function of the fines content of the soil. These recommendations are presented in Table 11-2.

| <b>TABLE 11-2</b> | MAXIMUM AMOUNT OF APPARENT COHESION THAT SHOULD BE |
|-------------------|--|
|                   | ASSUMED FOR BACKFILL SOILS (NCHRP, 2008)           |

% (by weight) passing #200 sieve maximum apparent cohesion

| 5 - 15  | 50 psf  |                 |
|---------|---------|-----------------|
| 15 - 25 | 100 psf | ESU 2A (FC=20%) |
| 25-50   | 200 psf | ESU 2B (FC=40%) |

## 11.3.3 Log Spiral Earth Pressure Theory

The Mononobe-Okabe and Trial Wedge methods for calculating earth pressure assume that the failure surface in the backfill is planar. It has been long recognized that when there is a significant soil-wall friction angle, the assumption of the planar failure surface is incorrect. Instead, in a homogeneous soil a logarithmic surface gives the critical values for the active and passive earth pressure in a limit equilibrium analysis. Note, however, that when there is no wall friction the logarithmic surface degenerates to a planar surface. As illustrated in Figure 11-15, or the active case the difference between the critical log spiral surface and the critical planar surface is small enough that it can be ignored, even when there is wall friction. However, as illustrated in Figure 11-15, the critical log spiral surface for the passive case differs significantly from the critical planar surface when the wall friction angle is more than one-third the value of the backfill friction angle. In these cases it is essential to consider the logarithmic surface: failure to do so can result in an unconservative assessment of the seismic passive earth pressure.

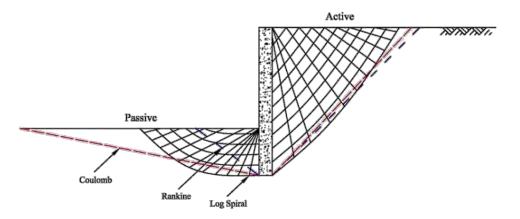


Figure 11-15 Critical Log Spiral Surfaces Compared to Planar Critical Surfaces

The log spiral method can be used to evaluate seismic passive earth pressures accounting for backfill friction and cohesion, soil-wall interface friction angle, and backslope angle. Shamsabadi et al. (2007) describe the general method that can be used to do this. The soil-wall interface friction angle is a key parameter in this approach. The soil-wall interface friction angle for static loading is often assumed to

The coefficient of consolidation,  $c_{\nu_{t}}$ , should be determined from the results of onedimensional consolidation tests. The variability in laboratory determination of  $\emph{c}_{\emph{V}}$  results should be considered in the final selection of the value of  $c_{\nu}$  to be used for design.

Where evaluation of elastic settlement is critical to the design of the foundation or selection of the foundation type, in-situ methods such as PMT or *DMT* for evaluating the modulus of the stratum should be used.

ESU 2A Very Loose to Loose Sand/ Gravel Es = 3.7 ksi = 530 ksfPoisson Ratio = 0.33

A profile of  $\sigma_{\sigma'}$ , or OCR =  $\sigma_{\sigma'}/\sigma_{\sigma'}$ , with depth should be developed for the site for design applications where the stress history could have a significant impact on the design properties selected and the performance of the foundation. As with consolidation properties, an upper and lower bound profile should be developed based on laboratory tests and plotted with a profile based on particular in-situ test(s), if used. It is particularly important to accurately compute preconsolidation stress values for relatively shallow depths where in-situ effective stresses are low. An underestimation of the preconsolidation stress at shallow depths will result in overly conservative estimates of settlement for shallow soil layers.

Due to the numerous simplifying assumptions associated with conventional consolidation theory, on which the coefficient of consolidation is based, it is unlikely that even the best estimates of  $c_{\nu}$  from high-quality laboratory tests will result in predictions of time rate of settlement in the field that are significantly better than a prediction within one order of magnitude. In general, the in-situ value of  $c_{
u}$  is larger than the value measured in the laboratory test. Therefore, a rational approach is to select average, upper, and lower bound values for the appropriate stress range of concern for the design application. These values should be compared to values obtained from previous work performed in the same soil deposit. Under the best-case conditions, these values should be compared to values computed from measurements of excess pore pressures or settlement rates during construction of other structures.

 $\ensuremath{\textit{CPTu}}$  tests in which the pore pressure dissipation rate is measured may be used to estimate the field coefficient of consolidation.

For preliminary analyses or where accurate prediction of settlement is not critical. values obtained from correlations to index properties presented in Sabatini et al. (2002)

For preliminary design or for final design where the prediction of deformation is not critical to structure performance, i.e., the structure design can tolerate the potential inaccuracies inherent in the correlations. The elastic properties  $(E_{sr}, \nu)$  of a soil may be estimated from empirical relationships presented in Table C10.4.6.3-1.

The specific definition of  $E_s$  is not always consistent for the various correlations and methods of in-situ measurement. See Sabatini et al. (2002) for additional details regarding the definition and determination of  $E_s$ .

An alternative method of evaluating the equivalent elastic modulus using measured shear wave velocities is presented in Sabatini et al. (2002).

Table C10.4.6.3-1—Elastic Constants of Various Soils (modified after U.S. Department of the Navy, 1982; Bowles, 1988)

| Department or the                | Navy, 1982; Bowles, 1988)                            |                              |
|----------------------------------|--|------------------------------|
| Soil Type                        | Typical Range of Young's Modulus Values, $E_s$ (ksi) | Poisson's Ratio, $\nu$ (dim) |
| Clay:                            |  |                              |
| Soft sensitive                   |  |                              |
| Medium stiff to stiff            | 0.347–2.08   | 0.4–0.5 (undrained)          |
|                                  | 2.08–6.94  |                              |
| Very stiff                       | 6.94–13.89   |                              |
| Loess                            | 2.08-8.33  | 0.1-0.3                      |
| Silt                             | 0.278–2.78   | 0.3-0.35                     |
| Fine Sand:                       |  |                              |
| Loose                            | 1.11–1.67  | 0.25                         |
| Medium dense                     | 1.67–2.78  |                              |
| Dense                            | 2.78–4.17  |                              |
| Sand:                            |  |                              |
| Loose                            | 1.39-4.17  | 0.20-0.36                    |
| Medium dense                     | 4.17–6.94  |                              |
| Dense                            | 6.94–11.11   | 0.30-0.40                    |
| Gravel:                          |  |                              |
| Loose                            | 4.17–11.11   | 0.20-0.35                    |
| Medium dense                     | 11.11–13.89  |                              |
| Dense                            | 13.89–27.78  | 0.30-0.40                    |
| Estimating E <sub>s</sub> from S | SPT N Value  |                              |
|                                  | $E_s$ (ksi)  |                              |
| Silts, sandy silts, slig         | 0.056 M <sub>160</sub>                               |                              |
| Clean fine to mediun             | 0.097 <i>N</i> 1 <sub>60</sub>                       |                              |
| Coarse sands and sa              | 0.139 <i>N</i> 1 <sub>60</sub>                       |                              |
| Sandy gravel and gra             | 0.167 N1 <sub>60</sub>                               |                              |
| Estimating E <sub>s</sub> from q |  |                              |
| Sandy soils                      | 0.028 <i>qc</i>                                      |                              |
|                                  |  |                              |

The modulus of elasticity for normally consolidated granular soils tends to increase with depth. An alternative method of defining the soil modulus for granular soils is to assume that it increases linearly with depth starting at zero at the ground surface in accordance with the following equation:

$$E_s = nh \times z \tag{C10.4.6.3-1}$$

where:

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# Wall 05.85L-A Soil Saturated Hydraulic Conductivity Estimates

#### References:

- Washington State Department of Transportation (WSDOT). Highway Runoff Manual.
   M31-16.05. April 2019
- Massmann, J. W. 2003. Implementation of Infiltration Ponds Research, WA-RD 578.1.
- Allen, T.M. 2017. Stormwater Infiltration in Highway Embankments Saturated Hydraulic Conductivity Estimation for Uncompacted and Compacted Soils, WSDOT Research Report WARD 872-1.
- Allen, T.M. 2018. Stormwater Infiltration in Highway Embankments Saturated Hydraulic Conductivity Estimation for Natural Low Plasticity Silts, WSDOT Research Report WA-RD 872-2.

WSDOT research has been conducted to investigate the most promising saturated hydraulic conductivity ( $K_{sat}$ ) predictive equations to assess and improve  $K_{sat}$  prediction accuracy using soils commonly encountered in WSDOT projects (Massmann 2003; Allen 2017, 2018). Based on that research, if a grain size based correlation is used,  $K_{sat}$  on WSDOT projects should be estimated using the optimized Slichter Equation as developed in Allen (2017).

Soil saturated hydraulic conductivity  $K_{sat}$  was estimated using the procedures outlined in Section 4D-4.1 of the Washington State Department of Transportation (WSDOT) Highway Runoff Manual (April 2019 updates) to estimate  $K_{sat}$  of site soil using correlations between Ksat and grain-size distribution data.

We used Equation 4D-3 in the HRM to estimate Ksat for soils based on grain-size. Equation 4D-3 is:

$$K_{sat}$$
 = 21.2  $\eta^{3.5} d_{10}^{-1.75}$ 

Where:

 $K_{sat}$  = saturated hydraulic conductivity (centimeters per second [cm/sec])

 $\eta$  = porosity

 $d_{10}$  = grain size (millimeters [mm]) at which 10 percent of the material passes by weight

For natural soil deposits, porosity can be estimated using equation 4D-4 in the HRM if measured porosities or void ratios are not available:

$$\eta = 0.4 \left(d_{10}^{-0.08}\right) \left(C_u^{-0.1}\right) \left(F_{cp}\right) + 0.0015 \left(PI\right)$$

Where:

 $C_u$  = uniformity coefficient ( $d_{60}/d_{10}$ )

 $d_{60}$  = grain size (mm) at which 60 percent of the material passes by weight

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 $F_{cp}=$  compaction factor for porosity (set equal to 1.0 for loose or un-compacted soil) PI = plasticity index

# **Example Calculations**

## **Determine:**

• Saturated hydraulic conductivity  $(K_{sat})$ 

# Given:

The following seive analysis results for consecutive samples from borings H-1-85, H-2-85, and H-3-85 which are described as being from with in the same Engineering Soil Unit ESU 2A:

|        |               | ECILOA                     | •         |       |      |
|--------|---------------|----------------------------|-----------|-------|------|
|        |               | ESU 2A                     |           |       |      |
| Boring | Sample Number | Sample Depth               | Soil Type | D10   | D60  |
| Doming | Sample Number | (feet below groundsurface) | 3011 Type | (mm)  | (mm  |
| H-1-85 | P-3           | 5 to 7                     | SM        | 0.040 | 0.58 |
| H-1-85 | P-4           | 7.5 to 9.5                 | SM        | 0.035 | 0.28 |
| H-1-85 | P-5           | 10 to 12                   | SM        | 0.047 | 1.03 |
| H-1-85 | P-6           | 12.5 to 14.5               | SM        | 0.044 | 0.16 |
| H-2-85 | P-2           | 3 to 5                     | SM        | 0.034 | 0.58 |
| H-2-85 | P-3           | 5 to 7                     | SM        | 0.058 | 0.61 |
| H-2-85 | P-4           | 7.5 to 9.5                 | SM        | 0.051 | 0.53 |
| H-2-85 | P-5           | 10 to 12                   | SM        | 0.055 | 0.69 |
| H-2-85 | P-7           | 15 to 17                   | SM        | 0.050 | 0.29 |
| H-2-85 | P-8           | 17.5 to 19.5               | SM        | 0.030 | 0.55 |
| H-2-85 | P-9           | 20 to 22                   | SM        | 0.020 | 0.86 |
| H-2-85 | P-10          | 22.5 to 24.5               | SM        | 0.035 | 0.55 |
| H-3-85 | P-6           | 12.5 to 14.5               | SP-SM     | 0.067 | 1.03 |
| H-3-85 | P-8           | 17.5 to 19.5               | SM        | 0.057 | 0.28 |

The following seive analysis results for consecutive samples from boring H-2-85 which are described as being from with in the same Engineering Soil Unit ESU 2B:

|        | ESU 2B        |                            |      |       |      |  |  |  |  |  |  |
|--------|---------------|----------------------------|------|-------|------|--|--|--|--|--|--|
| Boring | Sample Number | Sample Depth               | USGS | D10   | D60  |  |  |  |  |  |  |
|        |               | (feet below groundsurface) |      | (mm)  | (mm) |  |  |  |  |  |  |
| H-2-85 | P-11          | 25 to 27                   | SM   | 0.027 | 0.68 |  |  |  |  |  |  |
| H-2-85 | P-12          | 27.5 to 30                 | ML   | 0.003 | 0.08 |  |  |  |  |  |  |
| H-2-85 | P-13          | 30 to 32                   | ML   | 0.017 | 0.10 |  |  |  |  |  |  |
| H-2-85 | P-14          | 32.5 to 34.5               | SM   | 0.042 | 0.15 |  |  |  |  |  |  |
| H-2-85 | P-15          | 35 to 37                   | SM   | 0.041 | 0.48 |  |  |  |  |  |  |
|        | •             | Average                    |      |       |      |  |  |  |  |  |  |

# Solution:

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Find  $K_{sat}$  for sample P-3 in boring H-1-85 (other samples calculated similarly)

$$d_{10} = 0.040 \ mm$$

$$d_{60} = 0.58 \ mm$$

$$C_u = \frac{d_{60}}{d_{10}} = 14.5$$

$$F_{cp} \coloneqq 1.0$$

(Natural site soil was deposited under alluvial conditions, has not been subjected to compaction and is not overconsolidated.)

$$PI = 0.0$$

(non-plastic soil)

$$\eta := 0.4 \cdot \left( \left( \frac{d_{10}}{mm} \right)^{-0.08} \right) \cdot \left( C_u^{-0.1} \right) \cdot \left( F_{cp} \right) + 0.0015 \cdot (PI) = 0.396$$

$$K_{sat} := 21.2 \cdot (\eta^{3.5}) \cdot \left( \left( \frac{d_{10}}{mm} \right)^{1.75} \right) = 3.0 \cdot 10^{-3} \frac{cm}{s}$$

$$K_{sat} := \frac{K_{sat}}{(2.54 \cdot 12)} = 9.7 \cdot 10^{-5} \frac{ft}{s}$$

# **Results:**

The results of estimated  $K_{sat}$  values for site soil samples for which grain-size analyses were conducted are as follows:

|        |               | Saturated hydrau           | lic conductivity | (Ks) for ESU | J 2A |          |            |        |
|--------|---------------|----------------------------|------------------|--------------|------|----------|------------|--------|
|        |               | ESU 2A                     |                  |              |      | WSDOT    | 2019 HRM I | Method |
| Doring | Cample Number | Sample Depth               | Soil Tuno        | D10          | D60  | Dorositu | Ksat       | Ksa    |
| Boring | Sample Number | (feet below groundsurface) | Soil Type        | (mm)         | (mm) | Porosity | (cm/s)     | (ft/:  |
| H-1-85 | P-3           | 5 to 7                     | SM               | 0.040        | 0.58 | 0.40     | 3.0E-03    | 9.7E-  |
| H-1-85 | P-4           | 7.5 to 9.5                 | SM               | 0.035        | 0.28 | 0.43     | 3.1E-03    | 1.0E-  |
| H-1-85 | P-5           | 10 to 12                   | SM               | 0.047        | 1.03 | 0.38     | 3.3E-03    | 1.1E-  |
| H-1-85 | P-6           | 12.5 to 14.5               | SM               | 0.044        | 0.16 | 0.45     | 5.6E-03    | 1.8E-  |
| H-2-85 | P-2           | 3 to 5                     | SM               | 0.034        | 0.58 | 0.40     | 2.2E-03    | 7.2E-  |
| H-2-85 | P-3           | 5 to 7                     | SM               | 0.058        | 0.61 | 0.40     | 5.7E-03    | 1.9E-  |
| H-2-85 | P-4           | 7.5 to 9.5                 | SM               | 0.051        | 0.53 | 0.40     | 4.7E-03    | 1.6E-  |
| H-2-85 | P-5           | 10 to 12                   | SM               | 0.055        | 0.69 | 0.39     | 5.0E-03    | 1.7E-  |
| H-2-85 | P-7           | 15 to 17                   | SM               | 0.050        | 0.29 | 0.43     | 5.6E-03    | 1.9E-  |
| H-2-85 | P-8           | 17.5 to 19.5               | SM               | 0.030        | 0.55 | 0.40     | 1.8E-03    | 5.9E-  |
| H-2-85 | P-9           | 20 to 22                   | SM               | 0.020        | 0.86 | 0.38     | 7.2E-04    | 2.3E-  |
| H-2-85 | P-10          | 22.5 to 24.5               | SM               | 0.035        | 0.55 | 0.40     | 2.4E-03    | 7.7E-  |
| H-3-85 | P-6           | 12.5 to 14.5               | SP-SM            | 0.067        | 1.03 | 0.38     | 6.2E-03    | 2.0E-  |
| H-3-85 | P-8           | 17.5 to 19.5               | SM               | 0.057        | 0.28 | 0.43     | 7.4E-03    | 2.4E-  |
|        |               | Average                    |                  |              |      |          | 4.1E-03    | 1.3E-  |
|        |               |                            | 3.5E-03          | 1.1E-        |      |          |            |        |

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|        | Saturated hydraulic conductivity (Ks) for ESU 2B |                            |         |         |         |                |         |         |  |  |  |  |
|--------|--|----------------------------|---------|---------|---------|----------------|---------|---------|--|--|--|--|
|        |  | ESU 2B                     |         |         |         | WSDOT 2019 HRM |         |         |  |  |  |  |
| Boring | Sample Number                                    | Sample Depth               | USGS    | D10     | D60     | Porosity       | Ksat    | Ksat    |  |  |  |  |
|        |  | (feet below groundsurface) |         | (mm)    | (mm)    |                | (cm/s)  | (ft/s)  |  |  |  |  |
| H-2-85 | P-11   | 25 to 27                   | SM      | 0.027   | 0.68    | 0.39           | 1.3E-03 | 4.4E-05 |  |  |  |  |
| H-2-85 | P-12   | 27.5 to 30                 | ML      | 0.003   | 0.08    | 0.46           | 4.0E-05 | 1.3E-06 |  |  |  |  |
| H-2-85 | P-13   | 30 to 32                   | ML      | 0.017   | 0.10    | 0.46           | 1.2E-03 | 3.9E-05 |  |  |  |  |
| H-2-85 | P-14   | 32.5 to 34.5               | SM      | 0.042   | 0.15    | 0.45           | 5.2E-03 | 1.7E-04 |  |  |  |  |
| H-2-85 | P-15   | 35 to 37                   | SM      | 0.041   | 0.48    | 0.40           | 3.2E-03 | 1.1E-04 |  |  |  |  |
|        |  |                            |         | 2.2E-03 | 7.2E-05 |                |         |         |  |  |  |  |
|        |  |                            | 1.0E-03 | 3.3E-05 |         |                |         |         |  |  |  |  |

#### Notes:

- 1. Estimated diameter of 10 percent passing (  $d_{10} ) \, {\rm by}$  extrapolating data on grainsize curve.
- 2. mm = millimeters; cm = centimeters; ft/s = feet/second.

ESU 2A Estimated  $K_{sat}$  ranged from about 2.3E-5 ft/s to 2.4E-4 ft/s, with geomean value of about 1.1E-4 ft/s.

ESU 2B Estimated  $K_{sat}$  ranged from about 1.3E-6 ft/s to 1.7E-4 ft/s, with geomean value of about 3.3E-5 ft/s.

Geolinaneers

Table 1. Dry  $(\rho_{dry})$  and wet  $(\rho_{wet})$  densities for the units shown in Figure 1.

| Geologic Unit          | ρ <sub>dry</sub> kg/m <sup>3</sup> | $\rho_{\text{wet}}  \text{kg/m}^3$ | Source           | Reference                 |
|------------------------|------------------------------------|------------------------------------|------------------|---------------------------|
| D 1                    |                                    | 2050                               | Laboratory       | Robinson and others, 1983 |
| Recessional<br>Outwash |                                    | 1600-1920                          | Not<br>Specified | Galster and Laprade, 1991 |
|                        | 1920-2400                          | 2160-2560                          | Laboratory       | Olmstead, 1969            |
| Vashon Till            |                                    | 2080-2400                          | Not<br>Specified | Galster and Laprade, 1991 |
| Esperance Sand         | 1760                               | 1920                               | Laboratory       | Miller, 1989              |
| (Advance<br>Outwash)   |                                    | 1920-2160                          | Not<br>Specified | Galster and Laprade, 1991 |
|                        |                                    | 1890                               | Laboratory       | Robinson and others, 1983 |
| Lawton Clay            |                                    | 1600-1920                          | Not<br>Specified | Galster and Laprade, 1991 |
|                        |                                    | 1910                               | Laboratory       | Robinson and others, 1983 |
| Pre-Vashon             | 1460                               | 1920                               | Laboratory       | Miller, 1989              |
| 1 1C- v asiion         |                                    | 2080-2040                          | Not<br>Specified | Galster and Laprade, 1991 |

Table 2. Hydraulic conductivities, k, for the units shown in Figure 1.

| Geologic Unit      | k m/day                                 | Source        | Reference                  |
|--------------------|---|---------------|----------------------------|
|                    | $1x10^{-1}$ - $1x10^{2}$                | Not Specified | Laprade and Robinson, 1989 |
| Recessional        | $1x10^{-2}$ - $1x10^{2}$                | Not Specified | Galster and Laprade, 1991  |
| Outwash            | $1x10^{0}-1x10^{1}$                     | Field Tests   | Morgan and Jones, 1995     |
|                    | $1x10^{-2}$ - $1x10^{2}$                | Field Tests   | Woodward and others, 1995  |
|                    | 1x10 <sup>-5</sup> - 1x10 <sup>-2</sup> | Laboratory    | Olmstead, 1969             |
|                    | $1x10^{-5}$ - $1x10^{-2}$               | Not Specified | Laprade and Robinson, 1989 |
| Vashon Till        | 1x10 <sup>-6</sup> - 1x10 <sup>-1</sup> | Field Tests   | Mills and Cordell, 1989    |
|                    | $1x10^{-4}$ - $1x10^{0}$                | Not Specified | Galster and Laprade, 1991  |
|                    | $1x10^{-5}-1x10^{1}$                    | Field Tests   | Morgan and Jones, 1995     |
|                    | $1x10^{-2}$ - $1x10^{1}$                | Not Specified | Mills and Cordell, 1989    |
| Esperance Sand     | $1x10^{-1}$ - $1x10^{2}$                | Not Specified | Galster and Laprade, 1991  |
| (Advance Outwash)  | $1x10^{0}-1x10^{1}$                     | Field Tests   | Morgan and Jones, 1995     |
|                    | $1x10^{-3}-1x10^{1}$                    | Field Tests   | Woodward and others, 1995  |
| Transitional silt- | 1x10 <sup>-6</sup> -1x10 <sup>-1</sup>  | Field Tests   | Morgan and Jones, 1995     |
| sands              | 1x10 <sup>-1</sup> -1x10 <sup>1</sup>   | Field Tests   | Woodward and others, 1995  |
| Lawton Clay        | 1x10 <sup>-5</sup> - 1x10 <sup>-3</sup> | Not Specified | Laprade and Robinson, 1989 |
| Law ton Ciay       | 1x10 <sup>-4</sup> - 1x10 <sup>-1</sup> | Not Specified | Galster and Laprade, 1991  |
| Duo Voob on        | $1x10^{-5}$ - $1x10^{-2}$               | Not Specified | Laprade and Robinson, 1989 |
| Pre-Vashon         | 1x10 <sup>-4</sup> - 1x10 <sup>-1</sup> | Not Specified | Galster and Laprade, 1991  |

# Appendix E.3 - Wall 05.85L-A Design Calculations

# **AASHTO Average Blowcount in Upper 100 feet**

|          | Α            | В              | С                | D                  | Е               | F      | G           | Н  | I   | J | K | L | М | N         | 0            | Р |
|----------|--------------|----------------|------------------|--------------------|-----------------|--------|-------------|--|---|---|---|---|---|-----------|--------------|---|
| 30       |              | Soil Profile T | ype              | v <sub>s</sub> (fp | os)             |        | N           |  |   | • | • |   | • | •         | •            |   |
| 31       |              | S <sub>A</sub> |                  | >50                | 00              |        |             |  | Note:   |   |   |   |   |           |              |   |
| 32       |              | S <sub>B</sub> |                  | 2,500 to           | 5,000           |        | N/A         |  | Blowcount Percent (Energy is input BC/60). This spreadsheet approximates the layer thickness based on a function w    |   |   |   |   |           | unction with |   |
| 33       |              | Sc             |                  | 1,200 to           | 2,500           |        | >50         |  | depth, however, depending on the layering of the log, it may be necessary for the user to input their own layer thick |   |   |   |   |           | er thickness |   |
| 34       |              | S <sub>D</sub> |                  | 600 to             | 1,200           | 1:     | 5≤N≤50      | (i.e., clay layer extends at 7.5 ft and the blowcounts need to be weighted to reflect that thickness).  Spreadsheet based on Section 3.10.3.1 of American Association of State Highway and Transportation Office (AASHTO). |   |   |   |   |   | Officials |              |   |
| 35       |              | S <sub>E</sub> |                  | <60                | 0               |        | <15         |  |   |   |   |   |   | Unicials  |              |   |
| 36       |              |                | Table 3.10.3.1-1 | 1—Site Class Def   | initions from A | ASHTO  |             |  |   |   |   |   |   |           |              |   |
| 37       |              |                |                  |                    |                 |        |             |  |   |   |   |   |   |           |              |   |
| 38       | Name         |                |                  |                    | Nave            | Soil P | rofile Type |  |   |   |   |   |   |           |              |   |
|          | W-217-20     |                |                  |                    | 97.0            |        | С           |  |   |   |   |   |   |           |              |   |
|          | H-1-85       |                |                  |                    | 28.4            |        | D           |  |   |   |   |   |   |           |              |   |
|          | H-2-85       |                |                  |                    | 24.1            |        | D           |  |   |   |   |   |   |           |              |   |
|          | H-3-85       |                |                  |                    | 24.3            |        | D           |  |   |   |   |   |   |           |              |   |
| 43       |              |                |                  |                    |                 |        |             |  |   |   |   |   |   |           |              |   |
| 44<br>45 | <del> </del> |                |                  |                    |                 |        |             |  |   |   |   |   |   |           |              |   |
| 46       |              |                |                  |                    | 1               |        |             |  |   |   |   |   |   |           |              |   |
| 47       |              |                |                  |                    |                 |        |             |  |   |   |   |   |   |           |              |   |
| 48       |              |                |                  |                    | 1               |        |             |  |   |   |   |   |   |           |              |   |
| 49       |              |                |                  |                    |                 |        |             |  |   |   |   |   |   |           |              |   |
| 50       |              |                |                  |                    |                 |        |             |  |   |   |   |   |   |           |              |   |
| 51       |              |                |                  |                    |                 |        |             |  |   |   |   |   |   |           |              |   |
| 52       |              |                |                  |                    |                 |        |             |  |   |   |   |   |   |           |              |   |

# **AASHTO Average Blowcount in Upper 100 feet**

|    | Α     | В                  | С   | D   | Е                    | F                              | G                                    | Н                | ı     | J                  | K                                       | L                               | М       | N           | 0              | Р    |
|----|-------|--------------------|---|---|----------------------|--------------------------------|--------------------------------------|------------------|-------|--------------------|---|---------------------------------|---------|-------------|----------------|------|
| 1  |       | II.                |   | W-2   | 217-20               |                                | -                                    |                  |       |                    |   | H-                              | 1-85    |             | -              |      |
| 2  | Depth | Field<br>Blowcount | Energy<br>Corrected<br>Blowcount,<br>N <sub>i</sub> | Layer<br>thickness d <sub>i</sub><br>(feet) | Sum(d <sub>i</sub> ) | d <sub>i</sub> /N <sub>i</sub> | Sum(d <sub>i</sub> /N <sub>i</sub> ) | N <sub>ave</sub> | Depth | Field<br>Blowcount | Energy<br>Corrected<br>Blowcount,<br>N; | Layer<br>thickness<br>di (feet) | Sum(di) | di/Ni       | Sum(di/Ni)     | Nave |
| 3  | 2.5   | 93                 | 100   | 3.75  | 100                  | 0.04                           | 1.0309                               | 97.0             | 1     | 4                  | 4                                       | 2                               | 100     | 0.50        | 3.5            | 28.4 |
| 4  | 5     | 63                 | 92  | 2.5   |                      | 0.03                           |                                      |                  | 3     | 8                  | 8                                       | 2                               |         | 0.25        |                |      |
| 5  | 7.5   | 111                | 100   | 2.5   |                      | 0.03                           |                                      |                  | 5     | 3                  | 3                                       | 2.25                            |         | 0.75        |                |      |
| 6  | 10    | 100                | 100   | 3.75  |                      | 0.04                           |                                      |                  | 7.5   | 4                  | 4                                       | 2.5                             |         | 0.63        |                |      |
| 7  | 15    | 100                | 100   | 5   |                      | 0.05                           | Driving Energy                       | 88%              | 10    | 10                 | 10                                      | 2.5                             |         | 0.25        | Driving Energy | 60%  |
| 8  | 20    | 300                | 100   | 5   |                      | 0.05                           |                                      |                  | 12.5  | 9                  | 9                                       | 2.5                             |         | 0.28        |                |      |
| 9  | 25    | 51                 | 75  | 5   |                      | 0.07                           |                                      |                  | 15    | 138                | 100                                     | 2.5                             |         | 0.03        |                |      |
| 10 | 30    | 82                 | 100   | 5   |                      | 0.05                           |                                      |                  | 17.5  | 297                | 100                                     | 2.5                             |         | 0.03        |                |      |
| 11 | 35    | 55                 | 81  | 5   |                      | 0.06                           |                                      |                  | 20    | 400                | 100                                     | 3.75                            |         | 0.04        |                |      |
| 12 | 40    | 100                | 100   | 5   |                      | 0.05                           |                                      |                  | 25    | 300                | 100                                     | 77.5                            |         | 0.78        |                |      |
| 13 | 45    | 110                | 100   | 5   |                      | 0.05                           |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |
| 14 | 50    | 300                | 100   | 5   |                      | 0.05                           |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |
| 15 | 55    | 120                | 100   | 5   |                      | 0.05                           |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |
| 16 | 60    | 120                | 100   | 42.5  |                      | 0.43                           |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |
| 17 |       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |
| 18 |       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |
| 19 |       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |
| 20 |       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |
| 21 |       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |
| 22 |       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |
| 23 |       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |
| 24 |       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |
| 25 |       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |
| 26 |       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |
| 27 |       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |
| 28 |       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |

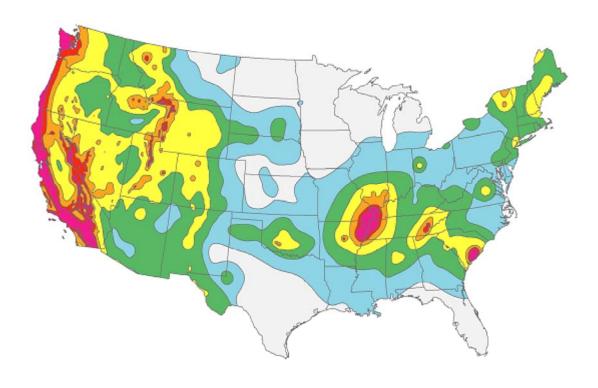
# **AASHTO Average Blowcount in Upper 100 feet**

| Depth 1 3 5 7.5 10 12.5 | Field<br>Blowcount       | Energy<br>Corrected<br>Blowcount,<br>N <sub>i</sub><br>7<br>17 | Layer<br>thickness<br>di (feet) | 2-85<br>Sum(di)          | di/Ni                    |                                    |  |       |   | Energy   | H-3-   | 85   |  |  |  |
|-------------------------|--------------------------|--|---------------------------------|--------------------------|--------------------------|------------------------------------|--|-------|---|--|--|--|--|--|--|
| 1<br>3<br>5<br>7.5      |                          | Corrected Blowcount, N <sub>i</sub> 7                          | thickness<br>di (feet)          | ` ,                      | di/Ni                    |                                    |  |       |   |  |  |  |  |  |  |
| 3<br>5<br>7.5<br>10     |                          | 17   | 2                               |                          | UI/IVI                   | Sum(di/Ni)                         | Nave   | Depth | Field<br>Blowcount  | Corrected<br>Blowcount,<br>N <sub>i</sub>  | Layer<br>thickness di<br>(feet)  | Sum(di)  | di/Ni  | Sum(di/Ni)   | Nave   |
| 5<br>7.5<br>10          |                          |  |                                 | 100                      | 0.29                     | 4.1468                             | 24.1   | 1     | 5   | 5  | 2  | 100  | 0.40   | 4.1  | 24.3   |
| 7.5<br>10               |                          | 13   | 2                               |                          | 0.12                     |                                    |  | 3     | 3   | 3  | 2  |  | 0.67   |  |  |
| 10                      |                          | 15   | 2.25                            |                          | 0.17                     |                                    |  | 5     | 5   | 5  | 2.25   |  | 0.45   |  |  |
|                         |                          | 20   | 2.5                             |                          | 0.13                     |                                    |  | 7.5   | 11  | 11   | 2.5  |  | 0.23   |  |  |
| 12.5                    |                          | 8  | 2.5                             |                          | 0.31                     | Driving Energy                     | 60%  | 10    | 5   | 5  | 2.5  |  | 0.50   | Driving Energy   | 60%  |
|                         |                          | 7  | 2.5                             |                          | 0.36                     |                                    |  | 12.5  | 8   | 8  | 2.5  |  | 0.31   |  |  |
| 15                      |                          | 7  | 2.5                             |                          | 0.36                     |                                    |  | 15    | 6   | 6  | 2.5  |  | 0.42   |  |  |
| 17.5                    |                          | 20   | 2.5                             |                          | 0.13                     |                                    |  | 17.5  | 11  | 11   | 2.5  |  | 0.23   |  |  |
| 20                      |                          | 10   | 2.5                             |                          | 0.25                     |                                    |  | 20    | 19  | 19   | 2.5  |  | 0.13   |  |  |
| 22.5                    |                          | 7  | 2.5                             |                          | 0.36                     |                                    |  | 22.5  | 118   | 100  | 2.5  |  | 0.03   |  |  |
| 25                      |                          | 18   | 2.5                             |                          | 0.14                     |                                    |  | 25    | 153   | 100  | 76.25  |  | 0.76   |  |  |
| 27.5                    |                          | 17   | 2.5                             |                          | 0.15                     |                                    |  |       |   |  |  |  | End of Data  |  |  |
|                         |                          |  |                                 |                          |                          |                                    |  |       |   |  |  |  |  |  |  |
|                         |                          |  |                                 |                          |                          |                                    |  |       |   |  |  |  |  |  |  |
|                         |                          |  |                                 |                          |                          |                                    |  |       |   |  |  |  |  |  |  |
| 37.5                    |                          | 71   | 63.75                           |                          |                          |                                    |  |       |   |  |  |  |  |  |  |
|                         |                          |  |                                 |                          |                          |                                    |  |       |   |  |  |  |  |  |  |
|                         |                          |  |                                 |                          |                          |                                    |  |       |   |  |  |  |  |  |  |
|                         |                          |  |                                 |                          |                          |                                    |  |       |   |  |  |  |  |  |  |
|                         |                          |  |                                 |                          |                          |                                    |  |       |   |  |  |  |  |  |  |
|                         |                          |  |                                 |                          |                          |                                    |  |       |   |  |  |  |  |  |  |
|                         |                          |  |                                 |                          |                          |                                    |  |       |   |  |  |  |  |  |  |
|                         |                          |  |                                 |                          |                          |                                    |  |       |   |  |  |  |  |  |  |
|                         |                          |  |                                 |                          |                          |                                    |  |       |   |  |  |  |  |  |  |
|                         |                          |  |                                 |                          |                          |                                    |  |       |   |  |  |  |  |  |  |
|                         |                          |  |                                 |                          | Liiu ol Dala T           |                                    |  |       |   |  |  |  |  |  |  |
| 3                       | 30<br>32.5<br>35<br>37.5 | 32.5<br>35   | 32.5 21<br>35 16                | 32.5 21 2.5<br>35 16 2.5 | 32.5 21 2.5<br>35 16 2.5 | 32.5 21 2.5 0.12<br>35 16 2.5 0.16 | 2.5   21   2.5   0.12   0.16   0.35   0.16   0.375   0.90   0.9 | 2.5   | 32.5 21 2.5 0.12 0.16 3.75 0.90 End of Data | 22.5   21   2.5   0.12   0.16   0.90   0.9 | 22.5   21   2.5   0.12   0.16   0.90   0.9 | 22.5   21   2.5   0.12   0.16   0.90   0.9 | 22.5   21   2.5   0.12   0.16   0.90   0.9 | 22.5   21   2.5   0.12   0.16   0.1 | 22.5   21   2.5   0.12   0.16   0.1 |

# $\textbf{BEToolbox}^{^{\text{TM}}}$

Spectra
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Version 6.0.0.6 BETA - Built on Jan 7 2021



# 05.85L-A

WSDOT Bridge Design Manual 2014 Seismic Hazard Map, 7% probability of exceedance in 75 years

Site Coordinates (Latitude,Longitude): 47.5097° N, 122.198° W Site Soil Classification: Site Class D - Stiff Soil

Seismic hazard maps are for sites at the boundary of Site Classes B and C, which is  $\overline{v}_s$  = 2500 ft/s (760 m/s). Adjustments for

other Site Classes are made as needed.

| Period (sec) | Sa<br>(g) |  |
|--------------|-----------|--|
| 0.0          | 0.433     | PGA - Site Class B/C Boundary            |
| 0.2          | 0.987     | S <sub>s</sub> - Site Class B/C Boundary |
| 1.0          | 0.283     | S <sub>1</sub> - Site Class B/C Boundary |

Values of Site Coefficient, F<sub>pga</sub>, for Peak Ground Acceleration

| Site Class | Мар       | ped Peak G | round Acc | eleration Co | efficient (F | PGA)      |
|------------|-----------|------------|-----------|--------------|--------------|-----------|
|            | PGA≤ 0.10 | PGA= 0.20  | PGA= 0.30 | PGA= 0.40    | PGA= 0.50    | PGA≥ 0.60 |
| Α          | 0.8       | 0.8        | 0.8       | 0.8          | 0.8          | 0.8       |
| В          | 0.9       | 0.9        | 0.9       | 0.9          | 0.9          | 0.9       |
| С          | 1.3       | 1.2        | 1.2       | 1.2          | 1.2          | 1.2       |
| D          | 1.6       | 1.4        | 1.3       | 1.2          | 1.1          | 1.1       |
| E          | 2.4       | 1.9        | 1.6       | 1.4          | 1.2          | 1.1       |

For Site Class D, F<sub>pga</sub> = 1.167

Values for Site Coefficient,  $\rm F_a$ , for 0.2 sec Period Spectral Acceleration

| Site Class | Mapped S              | pectral Acc           | celeration (          | Coefficient           | at Period 0           | .2 sec (S <sub>s</sub> ) |
|------------|-----------------------|-----------------------|-----------------------|-----------------------|-----------------------|--------------------------|
|            | S <sub>s</sub> ≤ 0.25 | S <sub>s</sub> = 0.50 | S <sub>s</sub> = 0.75 | S <sub>s</sub> = 1.00 | S <sub>s</sub> = 1.25 | S <sub>s</sub> ≥ 1.50    |
| Α          | 0.8                   | 0.8                   | 0.8                   | 0.8                   | 8.0                   | 0.8                      |
| В          | 0.9                   | 0.9                   | 0.9                   | 0.9                   | 0.9                   | 0.9                      |
| С          | 1.3                   | 1.3                   | 1.2                   | 1.2                   | 1.2                   | 1.2                      |
| D          | 1.6                   | 1.4                   | 1.2                   | 1.1                   | 1.0                   | 1.0                      |
| Е          | 2.4                   | 1.7                   | 1.3                   | 1.0                   | 0.9                   | 0.9                      |

For Site Class D,  $F_a = 1.105$ 

Values of Site Coefficient, F<sub>v</sub>, for 1.0 sec Period Spectral Acceleration

| Site Class | Mapped S             | Mapped Spectral Acceleration Coefficient at Period 1.0 sec (S |                      |     |     |     |  |  |  |  |  |  |  |  |  |
|------------|----------------------|---|----------------------|-----|-----|-----|--|--|--|--|--|--|--|--|--|
|            | S <sub>1</sub> ≤ 0.1 | S <sub>1</sub> = 0.5  | S <sub>1</sub> ≥ 0.6 |     |     |     |  |  |  |  |  |  |  |  |  |
| Α          | 0.8                  | 0.8   | 0.8                  | 0.8 | 0.8 | 8.0 |  |  |  |  |  |  |  |  |  |
| В          | 0.8                  | 0.8   | 0.8                  | 0.8 | 8.0 | 0.8 |  |  |  |  |  |  |  |  |  |
| С          | 1.5                  | 1.5   | 1.5                  | 1.5 | 1.5 | 1.4 |  |  |  |  |  |  |  |  |  |
| D          | 2.4                  | 2.2   | 2.0                  | 1.9 | 1.8 | 1.7 |  |  |  |  |  |  |  |  |  |
| Е          | 4.2                  | 3.3   | 2.8                  | 2.4 | 2.2 | 2.0 |  |  |  |  |  |  |  |  |  |

For Site Class D,  $F_v = 2.034$ 

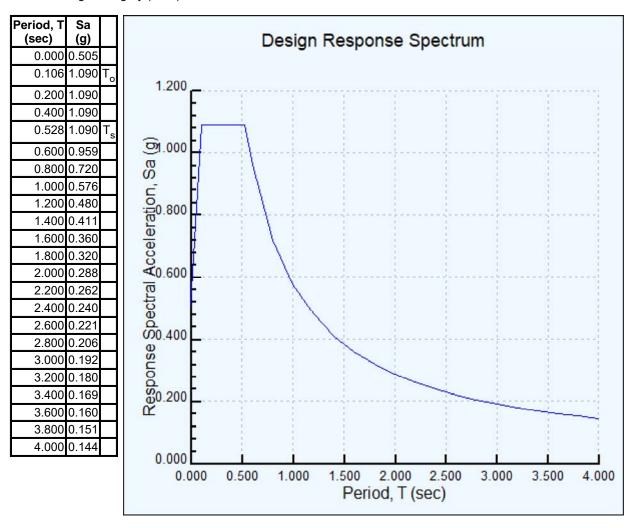
$$\begin{split} & A_{\rm S} = F_{\rm pga} \; {\rm PGA} = (\; 1.167)(\; 0.433g) = 0.505g \\ & S_{\rm DS} = F_{\rm a} \; S_{\rm s} = (\; 1.105)(\; 0.987g) = 1.090g \\ & S_{\rm D1} = F_{\rm v} \; S_{\rm 1} = (\; 2.034)(\; 0.283g) = 0.576g \\ & T_{\rm o} = 0.2T_{\rm s} = (0.2)(\; 0.528) = 0.106 \; {\rm sec} \\ & T_{\rm s} = S_{\rm D1}/S_{\rm DS} = (\; 0.576)/(\; 1.090) = 0.528 \; {\rm sec} \end{split}$$

# 05.85L-A

Partitions for Seismic Design Categories A, B, C, and D

| S <sub>D1</sub>          | SDC |
|--------------------------|-----|
| S <sub>D1</sub> < 0.15   | Α   |
| $0.15 \le S_{D1} < 0.30$ | В   |
| $0.30 \le S_{D1} < 0.50$ | С   |
| 0.50 ≤ S <sub>D1</sub>   | D   |

Seismic Design Category (SDC) = D



Project: <u>405 Renton to Bellveue</u> By: <u>YT</u> Checked By: <u>TB</u>

# <u>Calculating Wall Seismic Acceleration Considering Wave Scattering</u> Wall 05.85L-A

Per National Cooperative Highway Research Program (NCHRP) Report 611 the site class adjusted peak ground acceleration (PGA), As, can be corrected to account for vertical variations in the average ground acceleration observed behind tall retaining walls and/ or slopes greater than 20-feet in height by applying a wall height acceleration reduction factor (or  $\alpha$  coefficient) to the As.

## Site Class D

M = 7.0

Mean earthquake magnitude at the PGA period based on the Hart Crowser seismic design report "I-405 R2B Segment 1a Site-Specific Hazard Analysis RFU," dated March 25, 2021.

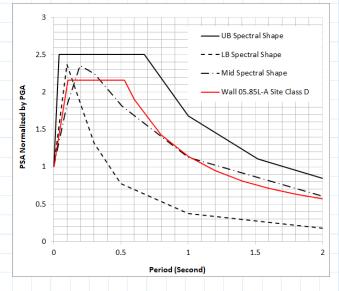
Determine response spectrum using WSDOT Bridge Engineering Software BEToolbox/BridgeLink Version 6.0.0.6 BETA in accordance with the WSDOT BDM based on the projected ground motion at the project site that has a 7 percent (SEE) probability of exceedance in a 75-year period (approximate 1,000-year return period).

$$A_s = 0.505$$
 (g)  
 $S_{D1} = 0.576$ 

Site Class Adjusted PGA

Determine the most appropriate spectral curve shape based on NCHRP Report 611 Figure 5-4.

- 1. Normalize response spectrum by the peak ground acceleration (PGA).
- 2. The peak spectral acceleration (PSA) normalized by PGA is then overlaid on the spectral shapes shown on Figure 5-4 to determine the most appropriate spectral curve shape for the design condition. Three spectral shapes shown on Figure 5-4 include an upper bound (UB), lower bound (LB), and intermediate (Mid) spectral shape.



The Mid spectral shape was selected.



Project Number: <u>00180-366-01</u>

Date: 01/11/22

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Project: 405 Renton to Bellveue
By: YT Checked By: TB

Determine wall height acceleration reduction factor (or  $\alpha$  coefficient) using wall height and the spectral shapes based on NCHRP Report 611 Figure 6-13.

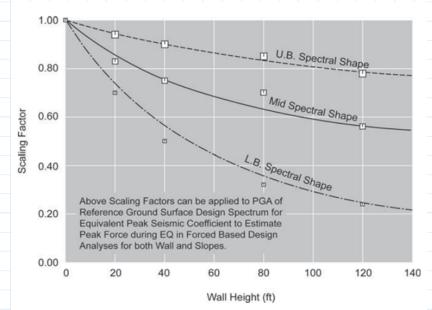


Figure 6-13. Resultant wave scattering  $\alpha$  coefficients for retaining wall design.

# Station 1+90 (Current design)

For <u>Lateral Earth Pressure</u> calculations, slope height is taken as 28.5 ft. (vertical distance between proposed ground surface prior to Forward Compatible Wall construction and SEW wall base at the back of wall heel) The wall height acceleration reduction factor selected from Figure 6-13 is:

$$\alpha = 0.815$$

Wall seismic acceleration considering wave scattering

$$PGA_a := A_s \cdot \alpha = 0.412$$

Horizontal seismic coefficient for use in pseudo-static slope stability analyses

$$k_h = \frac{PGA_a}{2} = 0.206$$

For <u>Compound Stability</u> calculations, the slope height is taken as 40.5 ft based on the height of the critical failure surface (refer to Slope/W figures). The wall height acceleration reduction factor selected from Figure 6-13 is:



$$\alpha = 0.765$$

Wall seismic acceleration considering wave scattering

$$PGA_a := A_s \cdot \alpha = 0.386$$

Horizontal seismic coefficient for use in pseudo-static slope stability analyses

$$k_h = \frac{PGA_a}{2} = 0.193$$

For <u>Global Stability</u> calculations, the slope height is taken as 44 ft based on the height of the critical failure surface (refer to Slope/W figures). The wall height acceleration reduction factor selected from Figure 6-13 is:

$$\alpha = 0.753$$

Wall seismic acceleration considering wave scattering

$$PGA_a := A_s \cdot \alpha = 0.38$$

Horizontal seismic coefficient for use in pseudo-static slope stability analyses

$$k_h = \frac{PGA_a}{2} = 0.190$$

# Station 1+90 (with Forward Compatible Wall)

For <u>Compound Stability</u> calculations, the slope height is taken as 40.5 ft based on the height of the critical failure surface (refer to Slope/W figures). The wall height acceleration reduction factor selected from Figure 6-13 is:

$$\alpha = 0.765$$

Wall seismic acceleration considering wave scattering

$$PGA_a := A_s \cdot \alpha = 0.386$$

Horizontal seismic coefficient for use in pseudo-static slope stability analyses

$$k_h = \frac{PGA_a}{2} = 0.193$$

Project: <u>405 Renton to Bellveue</u> By: <u>YT</u> Checked By: <u>TB</u> For <u>Global Stability</u> calculations, the slope height is taken as 43 ft based on the height of the critical failure surface (refer to Slope/W figures). The wall height acceleration reduction factor selected from Figure 6-13 is:

$$\alpha = 0.756$$

Wall seismic acceleration considering wave scattering

$$PGA_a := A_s \cdot \alpha = 0.382$$

Horizontal seismic coefficient for use in pseudo-static slope stability analyses

$$k_h = \frac{PGA_a}{2} = 0.191$$

| General Information |  |  |  |  |  |  |  |  |
|---------------------|--|--|--|--|--|--|--|--|
| Project:            | I-405/Renton to Bellevue Corridor Widening |  |  |  |  |  |  |  |
| Project Location:   | King County, Washington                    |  |  |  |  |  |  |  |
| Job Number:         | 00180-366-01                               |  |  |  |  |  |  |  |
| Boring Designation: | W-217-20                                   |  |  |  |  |  |  |  |
| Analysis by:        | BZ   |  |  |  |  |  |  |  |
| Date Analyzed:      | 4/12/2021                                  |  |  |  |  |  |  |  |
| Checked by:         | ТВ   |  |  |  |  |  |  |  |
| Date Checked:       | 4/12/2021                                  |  |  |  |  |  |  |  |

| Sampling Information  | n    |
|---|------|
| Depth to Groundwater (ft):                                  | 10.6 |
| SPT Liner (Yes/No):   | No   |
| Hammer Energy, %:   | 88   |
| Distance from sample hammer to ground/mudline surface (ft): | 5    |
| Borehole Diameter (in)                                      | 4    |

| Earthquake Information      | on    |
|-----------------------------|-------|
| Max Acceleration (As) (g) : | 0.505 |
| Farthquake Magnitude:       | 7.00  |

| Title Block Information |  |  |  |  |  |  |
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| Line 1:                 | I-405/Renton to Bellevue Corridor Widening |  |  |  |  |  |
| Line 2:                 | King County, Washington                    |  |  |  |  |  |

| gIN                                 | IT Collection Information |
|-------------------------------------|---------------------------|
| P-Drive File Path to gINT database: |                           |
| Boring Selected from<br>Database:   |                           |

| Residual Strength Weighting                       | 5   |
|---|-----|
| Olsen & Stark (2002):                             | 0.2 |
| Idriss & Boulanger Void Redistribution (2007):    | 0.2 |
| Idriss & Boulanger No Void Redistribution (2007): | 0.0 |
| Kramer, Wang Hybrid (2008):                       | 0.4 |
| Idriss et al. (1998):                             | 0.2 |

|                     | Collect Data From gINT | Automate %F from USCS |
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| Site Class D<br>SEE | Auto %F from WSDOT GDM | СОМРИТЕ               |

User Input

gINT or User Input

| Fine -Grain Soil Susceptib | ility |
|----------------------------|-------|
| PI Cutoff Value:           | 12    |

\*You must hit "COMPUTE" again anytime you change any of the blue or purple inputs. If the output tab is blank or has errors hit "COMPUTE" again.

| 93<br>63<br>111<br>100<br>100<br>300<br>51<br>82<br>55<br>100<br>110<br>300<br>120 | SM SM SM SM SM SM SM ML ML CL CH CH GH GH | 45<br>30<br>37<br>40<br>40<br>40<br>90<br>90<br>92<br>73<br>70<br>11<br>30 | ESU 4B ESU 4B ESU 4B ESU 4B ESU 4B ESU 4B ESU 5B ESU 5B ESU 5B ESU 5B | 130<br>130<br>130<br>130<br>130<br>130<br>130<br>130<br>130 | 18.0 | Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable | Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable |
|--|---|--|---|---|------|---|---|
| 63<br>111<br>100<br>100<br>300<br>51<br>82<br>55<br>100<br>110<br>300<br>120       | SM SM SM SM SM ML ML CL CH CL SW SM       | 30<br>37<br>40<br>40<br>40<br>90<br>90<br>92<br>73<br>70<br>11             | ESU 4B ESU 4B ESU 4B ESU 4B ESU 5B ESU 5B ESU 5B ESU 5B               | 130<br>130<br>130<br>130<br>130<br>130<br>130               |      | Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable                                 | Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable                 |
| 111<br>100<br>100<br>300<br>51<br>82<br>55<br>100<br>110<br>300<br>120             | SM SM SM SM ML ML CL CH CH SW SM          | 37<br>40<br>40<br>40<br>90<br>90<br>92<br>73<br>70<br>11                   | ESU 4B ESU 4B ESU 4B ESU 5B ESU 5B ESU 5B ESU 5B                      | 130<br>130<br>130<br>130<br>130<br>130<br>130               |      | Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable   | Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable                                 |
| 100<br>300<br>51<br>82<br>55<br>100<br>110<br>300<br>120                           | SM SM ML ML CL CH CSW SM                  | 40<br>40<br>90<br>90<br>92<br>73<br>70<br>11                               | ESU 4B ESU 4B ESU 5B ESU 5B ESU 5B ESU 5B                             | 130<br>130<br>130<br>130<br>130                             |      | Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable   | Non-Liquefiable Non-Liquefiable Non-Liquefiable Non-Liquefiable   |
| 300<br>51<br>82<br>55<br>100<br>110<br>300<br>120                                  | SM ML ML CL CH CL SW SM                   | 40<br>90<br>90<br>92<br>73<br>70<br>11                                     | ESU 4B<br>ESU 5B<br>ESU 5B<br>ESU 5B<br>ESU 5B                        | 130<br>130<br>130<br>130                                    |      | Non-Liquefiable<br>Non-Liquefiable<br>Non-Liquefiable   | Non-Liquefiable<br>Non-Liquefiable<br>Non-Liquefiable   |
| 51<br>82<br>55<br>100<br>110<br>300<br>120   | ML ML CL CH CL SW SM                      | 90<br>90<br>92<br>73<br>70<br>11   | ESU 5B<br>ESU 5B<br>ESU 5B<br>ESU 5B                                  | 130<br>130<br>130   |      | Non-Liquefiable<br>Non-Liquefiable  | Non-Liquefiable<br>Non-Liquefiable  |
| 82<br>55<br>100<br>110<br>300<br>120   | ML CL CH CL SW SM                         | 90<br>92<br>73<br>70<br>11   | ESU 5B<br>ESU 5B<br>ESU 5B  | 130<br>130  |      | Non-Liquefiable   | Non-Liquefiable   |
| 55<br>100<br>110<br>300<br>120   | CL<br>CH<br>CL<br>SW<br>SM                | 92<br>73<br>70<br>11   | ESU 5B<br>ESU 5B  | 130   | 16.0 |   |   |
| 100<br>110<br>300<br>120   | CH<br>CL<br>SW<br>SM                      | 73<br>70<br>11   | ESU 5B  |   | 16.0 | Non-Liquefiable   |   |
| 110<br>300<br>120  | CL<br>SW<br>SM                            | 70<br>11   |   |   |      |   | Non-Liquefiable   |
| 300<br>120   | SW<br>SM                                  | 11   |   | 125   | 28.0 | Non-Liquefiable   | Non-Liquefiable   |
| 120  | SM  |  | ESU 5B  | 130   |      | Non-Liquefiable   | Non-Liquefiable   |
|  |   | 20   | ESU 4B  | 140   |      | Non-Liquefiable   | Non-Liquefiable   |
| 120  | GM  |  | ESU 4B  | 130   |      | Non-Liquefiable   | Non-Liquefiable   |
|  |   | 30   | ESU 4B  | 130   |      | Non-Liquefiable   | Non-Liquefiable   |
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GW based on SEEP/W analysis

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|                      |               |            |          |                         |                              |                                   |                              | Liqu                              | efaction Anal       | ysis                    |                         | Residual Shear Strength Analysis |   |   |                                   |              |                         |  |                       |                                   |                         |
|----------------------|---------------|------------|----------|-------------------------|------------------------------|-----------------------------------|------------------------------|-----------------------------------|---------------------|-------------------------|-------------------------|----------------------------------|---|---|-----------------------------------|--------------|-------------------------|--|-----------------------|-----------------------------------|-------------------------|
|                      |               |            |          |                         | N                            | 1,60                              | Liquefactio<br>Saf           |                                   | Liquefact           | ion-Induced Settle      | ement (in)              | LDI<br>(ft)                      |   | N <sub>1,60</sub> Residual Shear Strength, Sr (psf) |                                   |              |                         |  |                       |                                   |                         |
| SPT Sample<br>Number | Depth<br>(ft) | Measured N | USCS     | Fines<br>Content<br>(%) | Youd and<br>Idriss<br>(2001) | Idriss and<br>Boulanger<br>(2008) | Youd and<br>Idriss<br>(2001) | Idriss and<br>Boulanger<br>(2014) | Tokimatsu &<br>Seed | Ishihara &<br>Yoshimine | Idriss and<br>Boulanger | Idriss and<br>Boulanger          | Idriss & Boulanger Void Distribution (2007) | Olsen & Stark<br>(2002)                             | Kramer &<br>Wang Hybrid<br>(2008) | WSDOT        | Olsen & Stark<br>(2002) | Idriss &<br>Boulanger<br>Void                    | Idriss &<br>Boulanger | Kramer &<br>Wang Hybrid<br>(2008) | Idriss et al.<br>(1998) |
|                      | 2.5           | 93         | SM       | 45                      | 166                          | 167                               | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                              | 167.5                                       | 173.9   | 164.6                             | n.a.         | n.a.                    | n.a.   | n.a.                  | n.a.                              | n.a.                    |
|                      | 5.0           | 63         | SM       | 30                      | 108                          | 101                               | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                              | 100.8                                       | 125.7   | 101.8                             | n.a.         | n.a.                    | n.a.   | n.a.                  | n.a.                              | n.a.                    |
|                      | 7.5           | 111        | SM       | 37                      | 155                          | 144                               | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                              | 159.7                                       | 191.9   | 161.8                             | n.a.         | n.a.                    | n.a.   | n.a.                  | n.a.                              | n.a.                    |
|                      | 10.0<br>15.0  | 100<br>100 | SM<br>SM | 40<br>40                | 151<br>154                   | 142<br>148                        | 2.00                         | 2.00<br>2.00                      | 0.0                 | 0.0                     | 0.0                     | 0.0                              | 141.7<br>148.2                              | 159.1<br>156.6                                      | 142.8<br>147.8                    | n.a.         | n.a.                    | n.a.   | n.a.                  | n.a.                              | n.a.                    |
|                      | 20.0          | 300        | SM       | 40                      | 142                          | 141                               | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                              | 423.5                                       | 428.5   | 417.8                             | n.a.<br>n.a. | n.a.                    | n.a.<br>n.a.                                     | n.a.<br>n.a.          | n.a.<br>n.a.                      | n.a.                    |
|                      | 25.0          | 51         | ML       | 90                      | 68                           | 69                                | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                              | 69.1  | 67.4  | 67.3                              | n.a.         | n.a.                    | n.a.   | n.a.                  | n.a.                              | n.a.                    |
|                      | 30.0          | 82         | ML       | 90                      | 107                          | 113                               | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                              | 112.9                                       | 106.7   | 108.6                             | n.a.         | n.a.                    | n.a.   | n.a.                  | n.a.                              | n.a.                    |
|                      | 35.0<br>40.0  | 55<br>100  | CH       | 92                      | 67<br>116                    | 73<br>130                         | 2.00                         | 2.00<br>2.00                      | 0.0                 | 0.0                     | 0.0                     | 0.0                              | 73.4  | 67.4  | 69.6                              | n.a.         | n.a.                    | n.a.   | n.a.                  | n.a.                              | n.a.                    |
|                      | 45.0          | 110        | CL       | 73<br>70                | 110                          | 130                               | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                              | 130.1<br>139.5                              | 116.7<br>122.4                                      | 121.8<br>128.7                    | n.a.<br>n.a. | n.a.                    | n.a.<br>n.a.                                     | n.a.<br>n.a.          | n.a.<br>n.a.                      | n.a.<br>n.a.            |
|                      | 50.0          | 300        | SW       | 11                      | 103                          | 124                               | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                              | 370.5                                       | 317.4   | 336.4                             | n.a.         | n.a.                    | n.a.   | n.a.                  | n.a.                              | n.a.                    |
|                      | 55.0          | 120        | SM       | 30                      | 98                           | 121                               | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                              | 145.1                                       | 122.0   | 129.9                             | n.a.         | n.a.                    | n.a.   | n.a.                  | n.a.                              | n.a.                    |
|                      | 60.0          | 120        | GM       | 30                      | 94                           | 119                               | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                              | 142.3                                       | 117.6   | 125.5                             | n.a.         | n.a.                    | n.a.   | n.a.                  | n.a.                              | n.a.                    |
|                      |               |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                                  |   |   |                                   |              |                         |  |                       |                                   |                         |
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|                      |               |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                                  |   |   |                                   |              |                         | <del>                                     </del> |                       |                                   |                         |
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|                      |               |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                                  |   |   |                                   |              |                         |  |                       |                                   |                         |
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|                      |               |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                                  |   |   |                                   |              |                         |  |                       |                                   |                         |
|                      |               |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                                  |   |   |                                   |              |                         |  |                       |                                   |                         |
|                      |               |            |          |                         |                              |                                   |                              | Docid                             | al Ctuanath Mais    | ahtina Eastara          |                         |                                  |   |   |                                   |              |                         |  |                       |                                   |                         |
| Seismic Parameters   |               |            |          |                         |                              | Residua                           | al Strength Wei              | WSDOT:                            | 0                   |                         |                         |                                  |   |   | Liquefac                          | tion and R   | esidual Sh              | ear Streng                                       | gth Analysis          |                                   |                         |

Seismic Parameters

Max Acceleration (As) (g): 0.505

Earthquake Magnitude: 7.00

WSDOT: 0
Olsen & Stark (2002): 0.2
Idriss & Boulanger Void Redistribution (2007): 0.2
Idriss & Boulanger No Void Redistribution (2007): 0
Kramer, Wang Hybrid (2008): 0.4

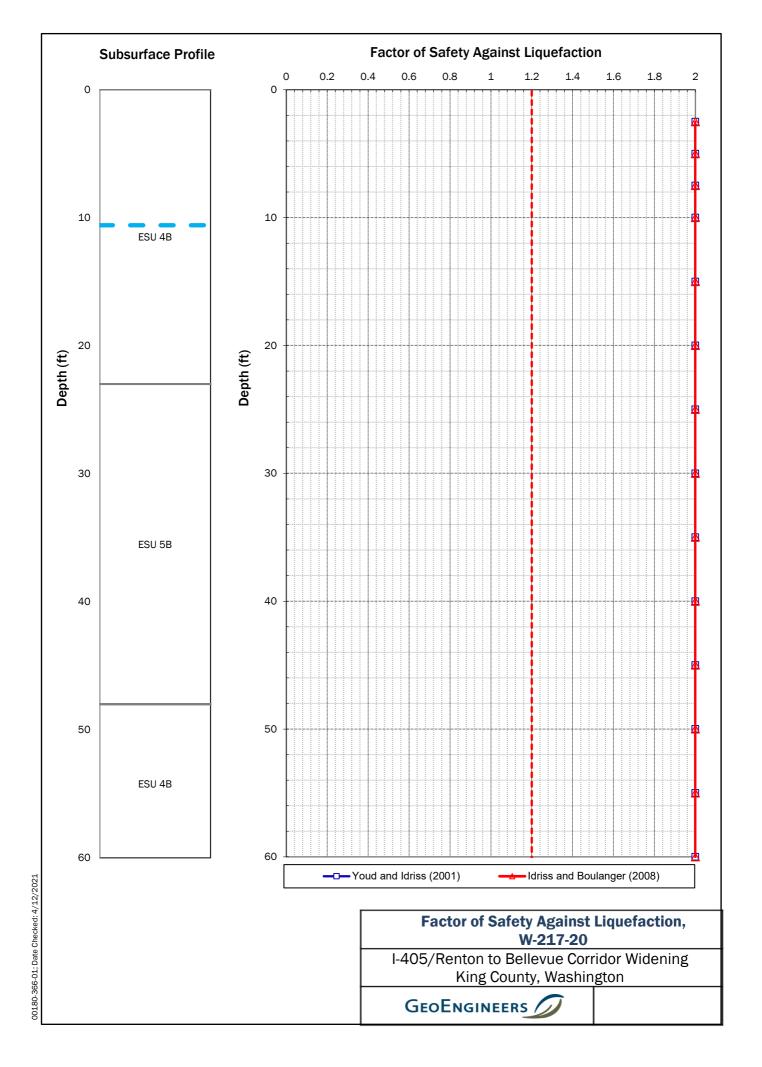
Idriss et al. (1998):

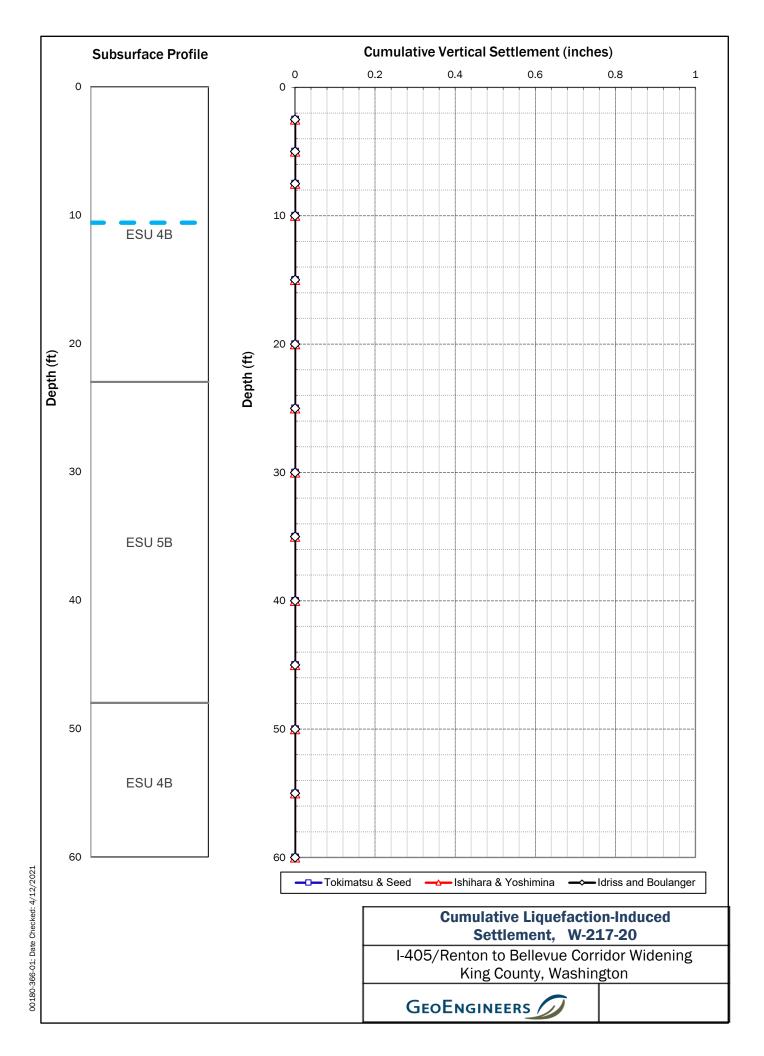
0.2

iquefaction and Residual Shear Strength Analysis. Results, W-217-20

I-405/Renton to Bellevue Corridor Widening King County, Washington







| General Information |  |  |  |  |  |  |  |
|---------------------|--|--|--|--|--|--|--|
| Project:            | I-405/Renton to Bellevue Corridor Widening |  |  |  |  |  |  |
| Project Location:   | King County, Washington                    |  |  |  |  |  |  |
| Job Number:         | 00180-366-01                               |  |  |  |  |  |  |
| Boring Designation: | H-1-85                                     |  |  |  |  |  |  |
| Analysis by:        | BZ   |  |  |  |  |  |  |
| Date Analyzed:      | 4/12/2021                                  |  |  |  |  |  |  |
| Checked by:         | ТВ   |  |  |  |  |  |  |
| Date Checked:       | 4/12/2021                                  |  |  |  |  |  |  |

| Sampling Information  |      |  |  |  |  |  |  |
|---|------|--|--|--|--|--|--|
| Depth to Groundwater (ft):                                  | 19.6 |  |  |  |  |  |  |
| SPT Liner (Yes/No):   | No   |  |  |  |  |  |  |
| Hammer Energy, %:   | 60   |  |  |  |  |  |  |
| Distance from sample hammer to ground/mudline surface (ft): | 5    |  |  |  |  |  |  |
| Borehole Diameter (in)                                      | 3    |  |  |  |  |  |  |

| Earthquake Information      |      |  |  |  |  |  |
|-----------------------------|------|--|--|--|--|--|
| Max Acceleration (g): 0.505 |      |  |  |  |  |  |
| Farthquake Magnitude:       | 7.00 |  |  |  |  |  |

| Title Block Information |  |  |  |  |  |  |  |
|-------------------------|--|--|--|--|--|--|--|
| Line 1:                 | I-405/Renton to Bellevue Corridor Widening |  |  |  |  |  |  |
| Line 2:                 | King County, Washington                    |  |  |  |  |  |  |

| gINT Collection Information         |  |  |  |  |  |  |  |
|-------------------------------------|--|--|--|--|--|--|--|
| P-Drive File Path to gINT database: |  |  |  |  |  |  |  |
| Boring Selected from<br>Database:   |  |  |  |  |  |  |  |

| Residual Strength Weighting                       |     |  |  |  |  |  |
|---|-----|--|--|--|--|--|
| Olsen & Stark (2002):                             | 0.2 |  |  |  |  |  |
| Idriss & Boulanger Void Redistribution (2007):    | 0.2 |  |  |  |  |  |
| Idriss & Boulanger No Void Redistribution (2007): | 0.0 |  |  |  |  |  |
| Kramer, Wang Hybrid (2008):                       | 0.4 |  |  |  |  |  |
| Idriss et al. (1998):                             | 0.2 |  |  |  |  |  |

| Collect Data From gINT | Automate %F from USCS |
|------------------------|-----------------------|
| Auto %F from WSDOT GDM | COMPUTE               |

\*You must hit "COMPUTE" again anytime you change any of the blue or purple inputs. If the output tab is blank or has errors hit "COMPUTE" again.

User Input

Fine -Grain Soil Susceptibility

PI Cutoff Value:

gINT or User

Input

12

| SPT Sample Number | Depth<br>(ft) | Measured N | USCS  | Fines Content<br>(%) | Geologic Unit/<br>ESU | Unit Weight (pcf) | PI<br>(%) | Non-liquefiable (i.e.<br>"unstaturated",<br>"cohesive",etc) | User Override*  |
|-------------------|---------------|------------|-------|----------------------|-----------------------|-------------------|-----------|---|-----------------|
|                   | 1.0           | 4          | SM    | 18                   | ESU 1A                | 90                |           | Unsaturated   |                 |
|                   | 3.0           | 8          | SM    | 18                   | ESU 1A                | 110               |           | Unsaturated   |                 |
|                   | 5.0           | 3          | SM    | 22                   | ESU 2A                | 90                |           | Unsaturated   |                 |
|                   | 7.5           | 4          | SM    | 28                   | ESU 2A                | 90                |           | Unsaturated   |                 |
|                   | 10.0          | 10         | SM    | 18                   | ESU 2A                | 110               |           | Unsaturated   |                 |
|                   | 12.5          | 9          | SM    | 31                   | ESU 2A                | 110               |           | Unsaturated   |                 |
|                   | 15.0          | 138        | SP-SM | 8                    | ESU 4B                | 135               |           | Non-Liquefiable   | Non-Liquefiable |
|                   | 17.5          | 297        | SP-SM | 9                    | ESU 4B                | 135               |           | Non-Liquefiable   | Non-Liquefiable |
|                   | 20.0          | 400        | SP-SM | 7                    | ESU 4B                | 135               |           | Non-Liquefiable   | Non-Liquefiable |
|                   | 25.0          | 300        | SP-SM | 6                    | ESU 4B                | 135               |           | Non-Liquefiable   | Non-Liquefiable |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
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|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
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|                   |               |            |       |                      |                       |                   |           |   |                 |

GW based on SEEP/W analysis

Site Class D

SEE

\*User Override column is *NOT* required to be filled out, unless needed. See "Read Me" tab.

|                      |               |            |                |                         | Liquefaction Analysis        |                                   |   |                                   |                     |                         |                         |                         |   | Residual S              | Shear Stren                       | gth Analysis | 5                       |              |                                  |  |                         |
|----------------------|---------------|------------|----------------|-------------------------|------------------------------|-----------------------------------|---|-----------------------------------|---------------------|-------------------------|-------------------------|-------------------------|---|-------------------------|-----------------------------------|--------------|-------------------------|--------------|----------------------------------|--|-------------------------|
|                      |               |            |                |                         | N <sub>2</sub>               | 1,60                              | Liquefaction Factor of Safety  Liquefaction-Induced Settlement (in)  Liquefaction-Induced Settlement (in)  (ft)  R  N <sub>1,60</sub> |                                   |                     |                         |                         | Residual Shea           |   |                         |                                   |              |                         |              |                                  |  |                         |
| SPT Sample<br>Number | Depth<br>(ft) | Measured N | USCS           | Fines<br>Content<br>(%) | Youd and<br>Idriss<br>(2001) | Idriss and<br>Boulanger<br>(2008) | Youd and<br>Idriss<br>(2001)  | Idriss and<br>Boulanger<br>(2014) | Tokimatsu &<br>Seed | Ishihara &<br>Yoshimine | Idriss and<br>Boulanger | Idriss and<br>Boulanger | Idriss & Boulanger Void Distribution (2007) | Olsen & Stark<br>(2002) | Kramer &<br>Wang Hybrid<br>(2008) | WSDOT        | Olsen & Stark<br>(2002) | Idriss &     | Idriss &<br>Boulanger<br>No Void | Kramer &<br>Wang Hybrid<br>(2008)                | Idriss et al.<br>(1998) |
|                      | 1.0           | 4          | SM             | 18                      | 5                            | 5                                 | 2.00  | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 5.1   | 5.1                     | 6.0                               | n.a.         | n.a.                    | n.a.         | n.a.                             | n.a.   | n.a.                    |
|                      | 3.0           | 8          | SM             | 18                      | 10                           | 10                                | 2.00  | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 10.2  | 10.2                    | 9.8                               | n.a.         | n.a.                    | n.a.         | n.a.                             | n.a.   | n.a.                    |
|                      | 5.0<br>7.5    | 3          | SM<br>SM       | 22                      | 4<br>5                       | 4<br>5                            | 2.00  | 2.00<br>2.00                      | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 4.1   | 4.1                     | 3.5                               | n.a.         | n.a.                    | n.a.         | n.a.                             | n.a.   | n.a.                    |
|                      | 10.0          | 10         | SM             | 18                      | 11                           | 12                                | 2.00  | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 5.4<br>12.2                                 | 5.4<br>12.4             | 4.3<br>10.5                       | n.a.<br>n.a. | n.a.                    | n.a.<br>n.a. | n.a.<br>n.a.                     | n.a.<br>n.a.                                     | n.a.<br>n.a.            |
|                      | 12.5          | 9          | SM             | 31                      | 9                            | 10                                | 2.00  | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 9.8   | 9.9                     | 8.8                               | n.a.         | n.a.                    | n.a.         | n.a.                             | n.a.   | n.a.                    |
|                      | 15.0<br>17.5  | 138<br>297 | SP-SM<br>SP-SM | 8                       | 107<br>99                    | 102<br>97                         | 2.00<br>2.00  | 2.00<br>2.00                      | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 141.0<br>288.7                              | 150.7<br>294.7          | 141.0<br>285.5                    | n.a.<br>n.a. | n.a.                    | n.a.<br>n.a. | n.a.<br>n.a.                     | n.a.<br>n.a.                                     | n.a.<br>n.a.            |
|                      | 20.0          | 400        | SP-SM          | 7                       | 92                           | 93                                | 2.00  | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 373.8                                       | 368.3                   | 365.6                             | n.a.         | n.a.                    | n.a.         | n.a.                             | n.a.   | n.a.                    |
|                      | 25.0          | 300        | SP-SM          | 6                       | 86                           | 90                                | 2.00  | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 269.5                                       | 256.4                   | 259.9                             | n.a.         | n.a.                    | n.a.         | n.a.                             | n.a.   | n.a.                    |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |              |                                  |  |                         |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |              |                                  |  |                         |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |              |                                  |  |                         |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |              |                                  |  |                         |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |              |                                  |  |                         |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |              |                                  |  |                         |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |              |                                  |  |                         |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |              |                                  |  |                         |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |              |                                  |  |                         |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |              |                                  |  |                         |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |              |                                  |  |                         |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |              |                                  |  |                         |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |              |                                  |  |                         |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |              |                                  |  |                         |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |              |                                  |  |                         |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |              |                                  |  |                         |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |              |                                  |  |                         |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |              |                                  |  |                         |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |              |                                  |  |                         |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |              |                                  |  |                         |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |              |                                  |  |                         |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         | -   |                         |                                   |              | +                       |              |                                  | <del>                                     </del> |                         |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |              |                                  |  |                         |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |              |                                  |  |                         |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         | <u> </u>                                    |                         |                                   |              |                         |              |                                  |  |                         |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |              |                                  |  |                         |
|                      | _             |            |                |                         |                              |                                   |   | _                                 | _                   | _                       |                         |                         |   |                         |                                   |              |                         | _            |                                  |  |                         |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         | 1   |                         |                                   |              | +                       |              |                                  |  |                         |
|                      |               |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |              |                                  |  |                         |
|                      |               |            |                |                         | 1                            |                                   |   | Residu                            | al Strength Wei     |                         |                         |                         |   |                         |                                   |              |                         |              |                                  |  |                         |
| Seismic Parameters   |               |            |                |                         | WSDOT:                       | 0                                 |   |                                   |                     |                         |                         | Liquefac                | ction and R                                 | esidual Sh              | ear Streng                        | gth Analysis |                         |              |                                  |  |                         |

Seismic Parameters

Max Acceleration (g): 0.505

Earthquake Magnitude: 7.00

WSDOT: 0
Olsen & Stark (2002): 0.2
Idriss & Boulanger Void Redistribution (2007): 0.2
Idriss & Boulanger No Void Redistribution (2007): 0
Kramer, Wang Hybrid (2008): 0.4

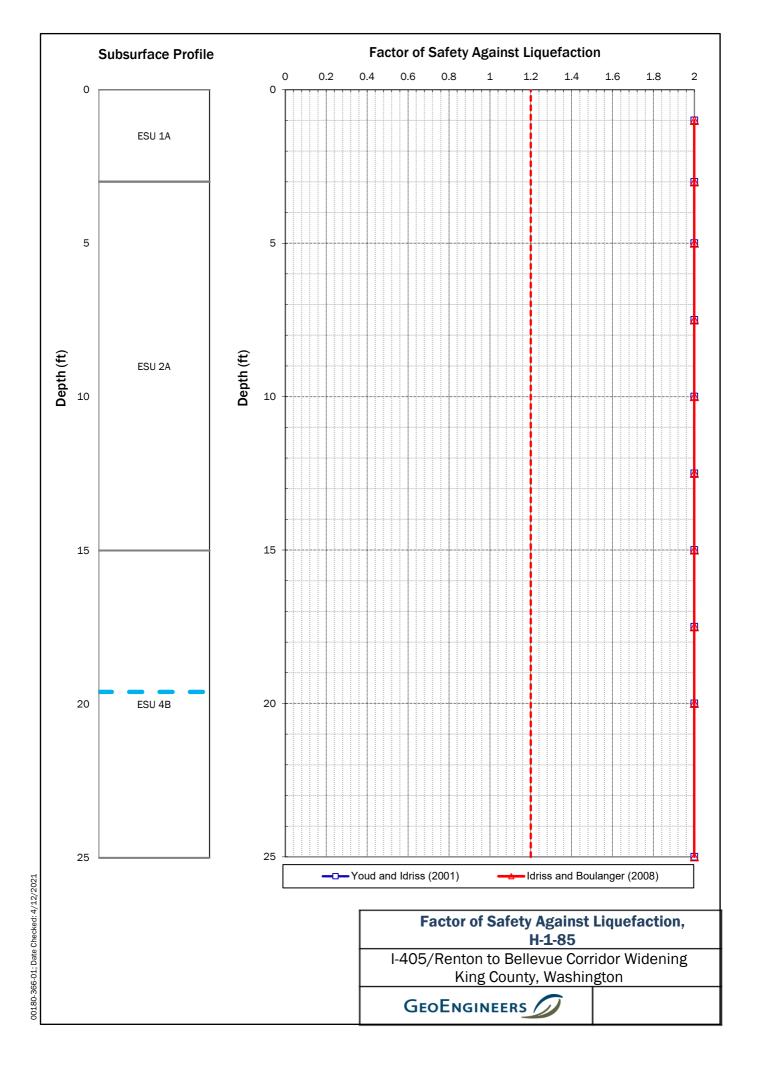
Idriss et al. (1998):

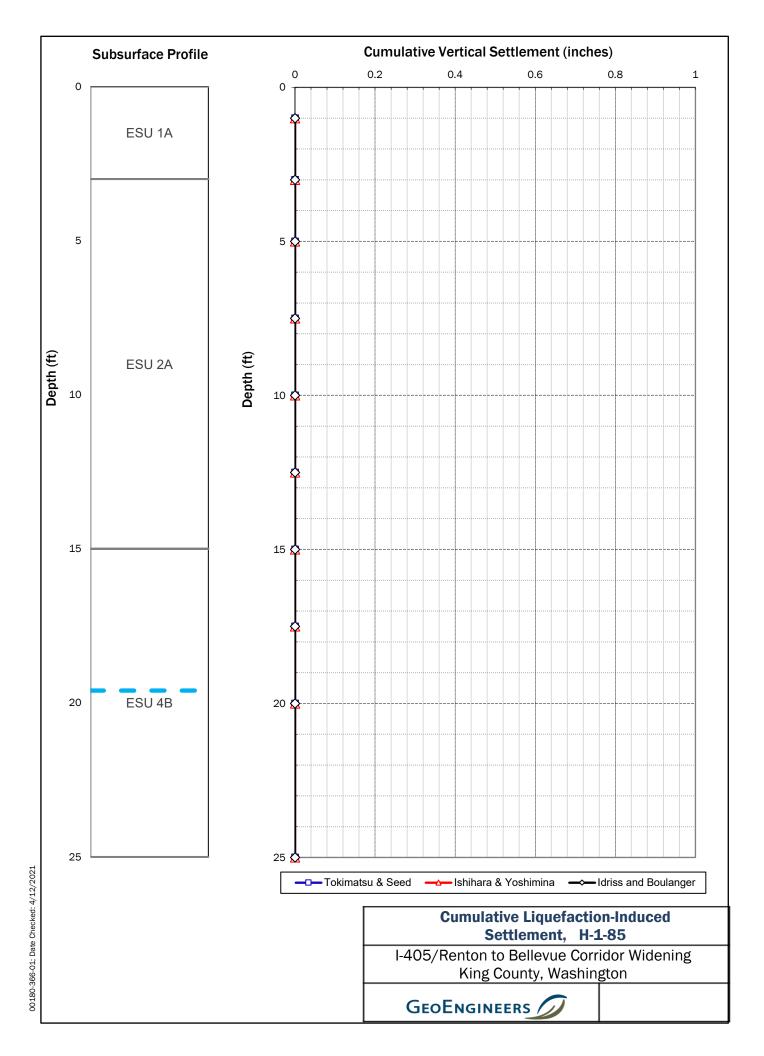
0.2

iquefaction and Residual Shear Strength Analysis. Results, H-1-85

I-405/Renton to Bellevue Corridor Widening King County, Washington







| General Information |  |  |  |  |  |  |  |
|---------------------|--|--|--|--|--|--|--|
| Project:            | I-405/Renton to Bellevue Corridor Widening |  |  |  |  |  |  |
| Project Location:   | King County, Washington                    |  |  |  |  |  |  |
| Job Number:         | 00180-366-01                               |  |  |  |  |  |  |
| Boring Designation: | H-2-85                                     |  |  |  |  |  |  |
| Analysis by:        | BZ   |  |  |  |  |  |  |
| Date Analyzed:      | 4/12/2021                                  |  |  |  |  |  |  |
| Checked by:         | ТВ   |  |  |  |  |  |  |
| Date Checked:       | 4/12/2021                                  |  |  |  |  |  |  |

| Sampling Information  | า    |
|---|------|
| Depth to Groundwater (ft):                                  | 24.1 |
| SPT Liner (Yes/No):   | No   |
| Hammer Energy, %:   | 60   |
| Distance from sample hammer to ground/mudline surface (ft): | 5    |
| Borehole Diameter (in)                                      | 3    |

| Earthquake Information      | on    |
|-----------------------------|-------|
| Max Acceleration (As) (g) : | 0.505 |
| Farthquake Magnitude:       | 7.00  |

| Title Block Information |  |  |  |  |  |
|-------------------------|--|--|--|--|--|
| Line 1:                 | I-405/Renton to Bellevue Corridor Widening |  |  |  |  |
| Line 2:                 | King County, Washington                    |  |  |  |  |

| gINT Collection Information         |  |  |  |  |
|-------------------------------------|--|--|--|--|
| givi collection illiorillation      |  |  |  |  |
| P-Drive File Path to gINT database: |  |  |  |  |
| Boring Selected from<br>Database:   |  |  |  |  |

| Residual Strength Weighting                       |     |  |  |  |  |
|---|-----|--|--|--|--|
| Olsen & Stark (2002):                             | 0.2 |  |  |  |  |
| Idriss & Boulanger Void Redistribution (2007):    | 0.2 |  |  |  |  |
| Idriss & Boulanger No Void Redistribution (2007): | 0.0 |  |  |  |  |
| Kramer, Wang Hybrid (2008):                       | 0.4 |  |  |  |  |
| Idriss et al. (1998):                             | 0.2 |  |  |  |  |

| Collect Data From gINT | Automate %F from USCS |  |  |  |
|------------------------|-----------------------|--|--|--|
| Auto %F from WSDOT GDM | COMPUTE               |  |  |  |

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gINT or User

Input

12

| s hit "COMPUTE" again. |  |
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|                        |  |

User Input

Fine -Grain Soil Susceptibility

PI Cutoff Value:

| SPT Sample Number | Depth<br>(ft) | Measured N | USCS  | Fines Content<br>(%) | Geologic Unit/<br>ESU | Unit Weight (pcf) | PI<br>(%) | Non-liquefiable (i.e.<br>"unstaturated",<br>"cohesive",etc) | User Override*  |
|-------------------|---------------|------------|-------|----------------------|-----------------------|-------------------|-----------|---|-----------------|
|                   | 1.0           | 7          | SM    | 15                   | ESU 1A                | 110               |           | Unsaturated   |                 |
|                   | 3.0           | 17         | SM    | 24                   | ESU 2A                | 115               |           | Unsaturated   |                 |
|                   | 5.0           | 13         | SM    | 15                   | ESU 2A                | 110               |           | Unsaturated   |                 |
|                   | 7.5           | 20         | SM    | 18                   | ESU 2A                | 115               |           | Unsaturated   |                 |
|                   | 10.0          | 8          | SM    | 16                   | ESU 2A                | 110               |           | Unsaturated   |                 |
|                   | 12.5          | 7          | SM    | 30                   | ESU 2A                | 110               |           | Unsaturated   |                 |
|                   | 15.0          | 7          | SM    | 22                   | ESU 2A                | 110               |           | Unsaturated   |                 |
|                   | 17.5          | 20         | SM    | 25                   | ESU 2A                | 115               |           | Unsaturated   |                 |
|                   | 20.0          | 10         | SM    | 27                   | ESU 2A                | 110               |           | Unsaturated   |                 |
|                   | 22.5          | 7          | SM    | 24                   | ESU 2A                | 110               |           | Unsaturated   |                 |
|                   | 25.0          | 18         | SM    | 26                   | ESU 2B                | 115               |           |   |                 |
|                   | 27.5          | 17         | ML    | 60                   | ESU 2B                | 115               |           |   |                 |
|                   | 30.0          | 11         | ML    | 51                   | ESU 2B                | 110               |           |   |                 |
|                   | 32.5          | 21         | SM    | 33                   | ESU 2B                | 115               |           |   |                 |
|                   | 35.0          | 16         | SM    | 22                   | ESU 2B                | 110               |           |   |                 |
|                   | 37.5          | 71         | SP-SM | 7                    | ESU 4B                | 135               |           | Non-Liquefiable   | Non-Liquefiable |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
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|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
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|                   |               |            |       |                      |                       |                   |           |   |                 |
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GW based on

SEEP/W analysis

Site Class D

SEE

\*User Override column is **NOT** required to be filled out, unless needed. See "Read Me" tab.

|                      |               |            |            |                         |                              |                                   | Liquefaction Analysis        |                                   |                     |                          |                         |                         | Residual Shear Strength Analysis            |                         |                                   |                                      |                         |                               |  |                                   |                         |
|----------------------|---------------|------------|------------|-------------------------|------------------------------|-----------------------------------|------------------------------|-----------------------------------|---------------------|--------------------------|-------------------------|-------------------------|---|-------------------------|-----------------------------------|--------------------------------------|-------------------------|-------------------------------|--|-----------------------------------|-------------------------|
|                      |               |            |            |                         | N                            | 1,60                              | Liquefactio<br>Saf           | n Factor of<br>ety                | Liquefact           | ion-Induced Settle       | ement (in)              | LDI<br>(ft)             | N <sub>1,60</sub>                           |                         |                                   | Residual Shear Strength, Sr<br>(psf) |                         |                               |  |                                   |                         |
| SPT Sample<br>Number | Depth<br>(ft) | Measured N | USCS       | Fines<br>Content<br>(%) | Youd and<br>Idriss<br>(2001) | Idriss and<br>Boulanger<br>(2008) | Youd and<br>Idriss<br>(2001) | Idriss and<br>Boulanger<br>(2014) | Tokimatsu &<br>Seed | Ishihara &<br>Yoshimine  | Idriss and<br>Boulanger | Idriss and<br>Boulanger | Idriss & Boulanger Void Distribution (2007) | Olsen & Stark<br>(2002) | Kramer &<br>Wang Hybrid<br>(2008) | WSDOT                                | Olsen & Stark<br>(2002) | Idriss &<br>Boulanger<br>Void | Idriss &<br>Boulanger<br>No Void<br>Redistribution<br>(2007) | Kramer &<br>Wang Hybrid<br>(2008) | Idriss et al.<br>(1998) |
|                      | 1.0           | 7          | SM         | 15                      | 9                            | 9                                 | 2.00                         | 2.00                              | 2.1                 | 4.3                      | 3.3                     | 1.9                     | 8.9   | 8.9                     | 10.4                              | n.a.                                 | n.a.                    | n.a.                          | n.a.   | n.a.                              | n.a.                    |
|                      | 3.0           | 17         | SM         | 24                      | 21                           | 22                                | 2.00                         | 2.00                              | 2.1                 | 4.3                      | 3.3                     | 1.9                     | 21.7  | 21.7                    | 20.3                              | n.a.                                 | n.a.                    | n.a.                          | n.a.   | n.a.                              | n.a.                    |
|                      | 7.5           | 13<br>20   | SM<br>SM   | 15<br>18                | 16<br>22                     | 18<br>23                          | 2.00                         | 2.00                              | 2.1                 | 4.3<br>4.3               | 3.3<br>3.3              | 1.9<br>1.9              | 17.7<br>22.8                                | 17.7<br>25.3            | 14.8<br>20.6                      | n.a.<br>n.a.                         | n.a.<br>n.a.            | n.a.<br>n.a.                  | n.a.<br>n.a.   | n.a.<br>n.a.                      | n.a.<br>n.a.            |
|                      | 10.0          | 8          | SM         | 16                      | 9                            | 9                                 | 2.00                         | 2.00                              | 2.1                 | 4.3                      | 3.3                     | 1.9                     | 9.4   | 9.3                     | 8.1                               | n.a.                                 | n.a.                    | n.a.                          | n.a.   | n.a.                              | n.a.                    |
|                      | 12.5          | 7          | SM         | 30                      | 7                            | 7                                 | 2.00                         | 2.00                              | 2.1                 | 4.3                      | 3.3                     | 1.9                     | 7.4   | 7.3                     | 6.7                               | n.a.                                 | n.a.                    | n.a.                          | n.a.   | n.a.                              | n.a.                    |
|                      | 15.0<br>17.5  | 7 20       | SM<br>SM   | 22<br>25                | 7<br>20                      | 8<br>20                           | 2.00                         | 2.00                              | 2.1                 | 4.3<br>4.3               | 3.3<br>3.3              | 1.9<br>1.9              | 7.5<br>19.6                                 | 7.5<br>19.7             | 7.1<br>19.2                       | n.a.                                 | n.a.                    | n.a.                          | n.a.   | n.a.                              | n.a.                    |
|                      | 20.0          | 10         | SM         | 27                      | 9                            | 9                                 | 2.00                         | 2.00                              | 2.1                 | 4.3                      | 3.3                     | 1.9                     | 9.2   | 9.2                     | 9.2                               | n.a.<br>n.a.                         | n.a.<br>n.a.            | n.a.<br>n.a.                  | n.a.<br>n.a.   | n.a.<br>n.a.                      | n.a.<br>n.a.            |
|                      | 22.5          | 7          | SM         | 24                      | 6                            | 6                                 | 2.00                         | 2.00                              | 2.1                 | 4.3                      | 3.3                     | 1.9                     | 6.1   | 6.1                     | 6.2                               | n.a.                                 | n.a.                    | n.a.                          | n.a.   | n.a.                              | n.a.                    |
|                      | 25.0<br>27.5  | 18<br>17   | SM<br>ML   | 26<br>60                | 15<br>14                     | 15<br>14                          | 0.82                         | 0.73<br>0.67                      | 2.1                 | 4.3                      | 3.3                     | 1.9                     | 15.3  | 15.0                    | 15.3                              | 526                                  | 391                     | 402                           | 1131   | 519                               | 802                     |
|                      | 30.0          | 11         | ML         | 51                      | 9                            | 9                                 | 0.56                         | 0.49                              | 1.7                 | 3.6<br>2.7               | 2.8<br>2.1              | 1.7<br>1.3              | 9.3   | 13.9<br>9.3             | 14.2<br>9.5                       | 537<br>331                           | 385<br>297              | 341                           | 1584<br>459  | 471<br>296                        | 916<br>424              |
|                      | 32.5          | 21         | SM         | 33                      | 17                           | 18                                | 0.91                         | 0.81                              | 0.8                 | 1.5                      | 1.2                     | 0.6                     | 17.9  | 17.3                    | 17.9                              | 734                                  | 499                     | 542                           | 2145   | 707                               | 1217                    |
|                      | 35.0          | 16         | SM         | 22                      | 13                           | 13                                | 0.59                         | 0.55                              | 0.5                 | 1.0                      | 0.8                     | 0.5                     | 13.2  | 12.9                    | 13.4                              | 441                                  | 412                     | 391                           | 585  | 457                               | 487                     |
|                      | 37.5          | 71         | SP-SM      | 7                       | 55                           | 63                                | 2.00                         | 2.00                              | 0.0                 | 0.0                      | 0.0                     | 0.0                     | 62.6  | 55.8                    | 58.4                              | n.a.                                 | n.a.                    | n.a.                          | n.a.   | n.a.                              | n.a.                    |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                          |                         |                         |   |                         |                                   |                                      |                         |                               |  |                                   |                         |
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|                      |               | Seisr      | nic Parame | eters                   |                              |                                   |                              | Kesidu                            | al Strength Wei     | ghting Factors<br>WSDOT: | 0                       |                         |   |                         |                                   |                                      | Liquefac                | tion and R                    | esidual Sh   | ear Streng                        | gth Analysis            |

Seismic Parameters

Max Acceleration (As) (g): 0.505

Earthquake Magnitude: 7.00

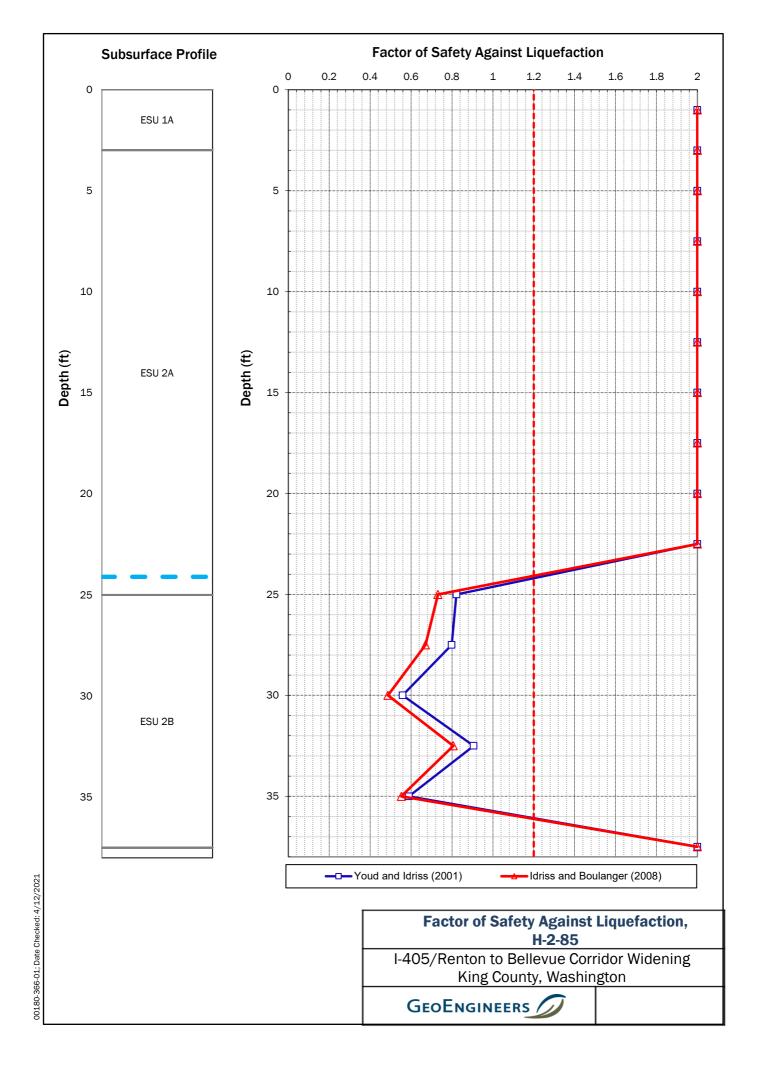
WSDOT: 0
Olsen & Stark (2002): 0.2
Idriss & Boulanger Void Redistribution (2007): 0.2
Idriss & Boulanger No Void Redistribution (2007): 0
Kramer, Wang Hybrid (2008): 0.4

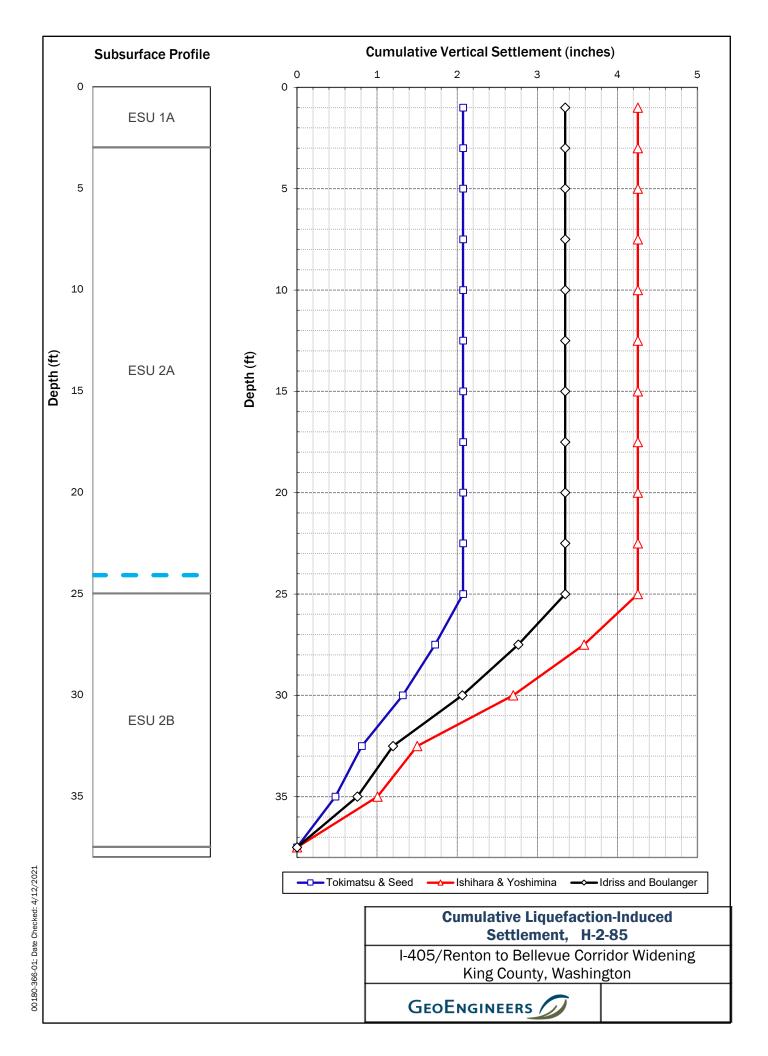
Idriss et al. (1998):

0.2

Liquefaction and Residual Shear Strength Analysis Results, H-2-85







| General Information |  |  |  |  |  |  |  |  |  |
|---------------------|--|--|--|--|--|--|--|--|--|
| Project:            | I-405/Renton to Bellevue Corridor Widening |  |  |  |  |  |  |  |  |
| Project Location:   | King County, Washington                    |  |  |  |  |  |  |  |  |
| Job Number:         | 00180-366-01                               |  |  |  |  |  |  |  |  |
| Boring Designation: | H-3-85                                     |  |  |  |  |  |  |  |  |
| Analysis by:        | BZ   |  |  |  |  |  |  |  |  |
| Date Analyzed:      | 4/12/2021                                  |  |  |  |  |  |  |  |  |
| Checked by:         | ТВ   |  |  |  |  |  |  |  |  |
| Date Checked:       | 4/12/2021                                  |  |  |  |  |  |  |  |  |

| Sampling Information  | n    |
|---|------|
| Depth to Groundwater (ft):                                  | 30.0 |
| SPT Liner (Yes/No):   | No   |
| Hammer Energy, %:   | 60   |
| Distance from sample hammer to ground/mudline surface (ft): | 5    |
| Borehole Diameter (in)                                      | 3    |

| Earthquake Information | on    |
|------------------------|-------|
| Max Acceleration (g):  | 0.505 |
| Earthquake Magnitude:  | 7.00  |

|         | Title Block Information                    |  |  |  |  |  |  |  |  |  |  |
|---------|--|--|--|--|--|--|--|--|--|--|--|
| Line 1: | I-405/Renton to Bellevue Corridor Widening |  |  |  |  |  |  |  |  |  |  |
| Line 2: | King County, Washington                    |  |  |  |  |  |  |  |  |  |  |

| gIN                                 | NT Collection Information |
|-------------------------------------|---------------------------|
| P-Drive File Path to gINT database: |                           |
| Boring Selected from<br>Database:   |                           |

| Residual Strength Weighting                       |     |  |  |  |  |  |  |  |
|---|-----|--|--|--|--|--|--|--|
| Olsen & Stark (2002):                             | 0.2 |  |  |  |  |  |  |  |
| Idriss & Boulanger Void Redistribution (2007):    | 0.2 |  |  |  |  |  |  |  |
| Idriss & Boulanger No Void Redistribution (2007): | 0.0 |  |  |  |  |  |  |  |
| Kramer, Wang Hybrid (2008):                       | 0.4 |  |  |  |  |  |  |  |
| Idriss et al. (1998):                             | 0.2 |  |  |  |  |  |  |  |

| Collect Data From gINT | Automate %F from USCS |
|------------------------|-----------------------|
| Auto %F from WSDOT GDM | COMPUTE               |

\*You must hit "COMPUTE" again anytime you change any of the blue or purple inputs. If the output tab is blank or has errors hit "COMPUTE" again.

User Input

Fine -Grain Soil Susceptibility

PI Cutoff Value:

gINT or User

Input

12

| column is <i>NOT</i> |
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| required to be       |
| filled out, unless   |
| needed. See          |
| "Read Me" tab.       |

| SPT Sample Number | Depth<br>(ft) | Measured N | USCS  | Fines Content<br>(%) | Geologic Unit/<br>ESU | Unit Weight (pcf) | PI<br>(%) | Non-liquefiable (i.e. "unstaturated", | User Override*  |
|-------------------|---------------|------------|-------|----------------------|-----------------------|-------------------|-----------|---------------------------------------|-----------------|
|                   | (11)          |            |       | (70)                 | LSU                   |                   | (70)      | "cohesive",etc)                       |                 |
|                   | 1.0           | 5          | SP    | 4                    | ESU 1A                | 105               |           | Unsaturated                           |                 |
|                   | 3.0           | 3          | SP    | 4                    | ESU 1A                | 105               |           | Unsaturated                           |                 |
|                   | 5.0           | 5          | SP    | 4                    | ESU 1A                | 105               |           | Unsaturated                           |                 |
|                   | 7.5           | 11         | SP-SM | 5                    | ESU 1A                | 115               |           | Unsaturated                           |                 |
|                   | 10.0          | 5          | SP-SM | 10                   | ESU 2A                | 100               |           | Unsaturated                           |                 |
|                   | 12.5          | 8          | SP-SM | 12                   | ESU 2A                | 115               |           | Unsaturated                           |                 |
|                   | 15.0          | 6          | SM    | 12                   | ESU 2A                | 100               |           | Unsaturated                           |                 |
|                   | 17.5          | 11         | SM    | 19                   | ESU 2A                | 110               |           | Unsaturated                           |                 |
|                   | 20.0          | 19         | ML    | 70                   | ESU 2B                | 115               |           | Unsaturated                           |                 |
|                   | 22.5          | 118        | SP-SM | 11                   | ESU 4B                | 135               |           | Non-Liquefiable                       | Non-Liquefiable |
|                   | 25.0          | 153        | SM    | 11                   | ESU 4B                | 130               |           | Non-Liquefiable                       | Non-Liquefiable |
|                   |               |            |       |                      |                       |                   |           |                                       |                 |
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GW based on SEEP/W

analysis

Site Class D

SEE

|                      |                   |            |                |                         |                              |                                   | Lique   | Residual Shear Strength Analysis  |                     |                         |                         |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|----------------------|-------------------|------------|----------------|-------------------------|------------------------------|-----------------------------------|---|-----------------------------------|---------------------|-------------------------|-------------------------|-------------------------|---|--------------------------------------|-----------------------------------|--------------|-------------------------|--------------|----------------------------------|-----------------------------------|-------------------------|
|                      | N <sub>1,60</sub> |            |                |                         |                              | 1,60                              | Liquefaction Factor of Safety  Liquefaction-Induced Settlement (in) |                                   |                     | LDI<br>(ft)             | N <sub>1,60</sub>       |                         |   | Residual Shear Strength, Sr<br>(psf) |                                   |              |                         |              |                                  |                                   |                         |
| SPT Sample<br>Number | Depth<br>(ft)     | Measured N | USCS           | Fines<br>Content<br>(%) | Youd and<br>Idriss<br>(2001) | Idriss and<br>Boulanger<br>(2008) | Youd and<br>Idriss<br>(2001)  | Idriss and<br>Boulanger<br>(2014) | Tokimatsu &<br>Seed | Ishihara &<br>Yoshimine | Idriss and<br>Boulanger | Idriss and<br>Boulanger | Idriss & Boulanger Void Distribution (2007) | Olsen & Stark<br>(2002)              | Kramer &<br>Wang Hybrid<br>(2008) | WSDOT        | Olsen & Stark<br>(2002) | Idriss &     | Idriss &<br>Boulanger<br>No Void | Kramer &<br>Wang Hybrid<br>(2008) | Idriss et al.<br>(1998) |
|                      | 1.0               | 5          | SP             | 4                       | 6                            | 6                                 | 2.00  | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 6.4   | 6.4                                  | 7.5                               | n.a.         | n.a.                    | n.a.         | n.a.                             | n.a.                              | n.a.                    |
|                      | 3.0               | 3          | SP             | 4                       | 4                            | 4                                 | 2.00  | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 3.8   | 3.8                                  | 3.6                               | n.a.         | n.a.                    | n.a.         | n.a.                             | n.a.                              | n.a.                    |
|                      | 5.0               | 5          | SP             | 4                       | 6                            | 7                                 | 2.00  | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 6.8   | 6.8                                  | 5.8                               | n.a.         | n.a.                    | n.a.         | n.a.                             | n.a.                              | n.a.                    |
|                      | 7.5<br>10.0       | 11<br>5    | SP-SM<br>SP-SM | 5<br>10                 | 12<br>5                      | 14<br>6                           | 2.00  | 2.00<br>2.00                      | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 14.1<br>6.3                                 | 14.2<br>6.0                          | 11.5<br>5.2                       | n.a.         | n.a.                    | n.a.         | n.a.                             | n.a.                              | n.a.                    |
|                      | 12.5              | 8          | SP-SM          | 12                      | 8                            | 9                                 | 2.00  | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 8.6   | 8.5                                  | 7.7                               | n.a.<br>n.a. | n.a.                    | n.a.<br>n.a. | n.a.<br>n.a.                     | n.a.<br>n.a.                      | n.a.<br>n.a.            |
|                      | 15.0              | 6          | SM             | 12                      | 6                            | 7                                 | 2.00  | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 6.7   | 6.6                                  | 6.1                               | n.a.         | n.a.                    | n.a.         | n.a.                             | n.a.                              | n.a.                    |
|                      | 17.5              | 11         | SM             | 19                      | 11                           | 11                                | 2.00  | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 11.1  | 11.1                                 | 10.7                              | n.a.         | n.a.                    | n.a.         | n.a.                             | n.a.                              | n.a.                    |
|                      | 20.0              | 19<br>118  | ML<br>SP-SM    | 70<br>11                | 18<br>88                     | 18<br>91                          | 2.00  | 2.00<br>2.00                      | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 20.0<br>107.3                               | 20.0<br>103.1                        | 20.0<br>103.9                     | n.a.         | n.a.                    | n.a.         | n.a.                             | n.a.                              | n.a.                    |
|                      | 25.0              | 153        | SM             | 11                      | 82                           | 88                                | 2.00  | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 134.7                                       | 125.8                                | 128.8                             | n.a.<br>n.a. | n.a.                    | n.a.<br>n.a. | n.a.<br>n.a.                     | n.a.<br>n.a.                      | n.a.                    |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     | 0.0                     | 3.0                     |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              | +                       |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              | <u> </u>                |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              | <u> </u>                |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         | <u> </u>                                    |                                      |                                   |              | <u> </u>                |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   |                                   |                     |                         |                         |                         |   |                                      |                                   |              |                         |              |                                  |                                   |                         |
|                      |                   |            |                |                         |                              |                                   |   | Residu                            | al Strength Wei     | ghting Factors          |                         |                         |   | <u>l</u>                             |                                   |              |                         |              |                                  |                                   |                         |
| Seismic Parameters   |                   |            |                |                         |                              |                                   |   | <u> </u>                          | WSDOT:              | 0                       |                         |                         |   |                                      |                                   | Liquefac     | ction and R             | esidual Sh   | ear Streng                       | gth Analysis                      |                         |

Seismic Parameters

Max Acceleration (g): 0.505

Earthquake Magnitude: 7.00

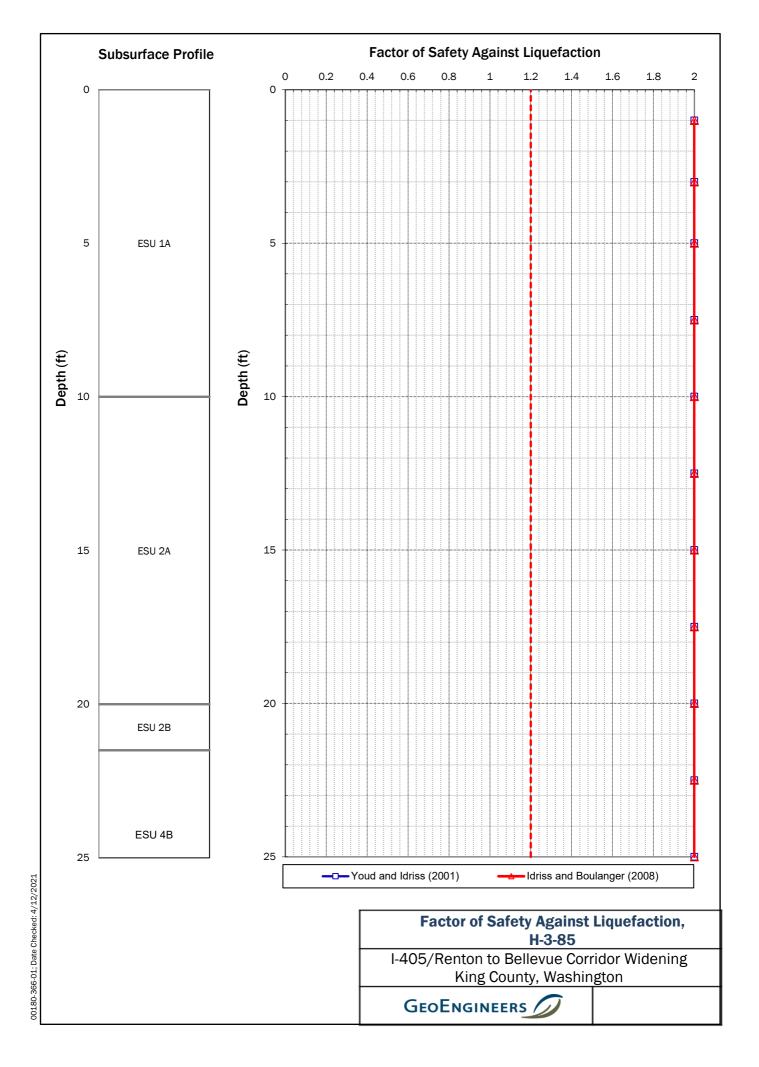
WSDOT: 0
Olsen & Stark (2002): 0.2
Idriss & Boulanger Void Redistribution (2007): 0.2
Idriss & Boulanger No Void Redistribution (2007): 0
Kramer, Wang Hybrid (2008): 0.4

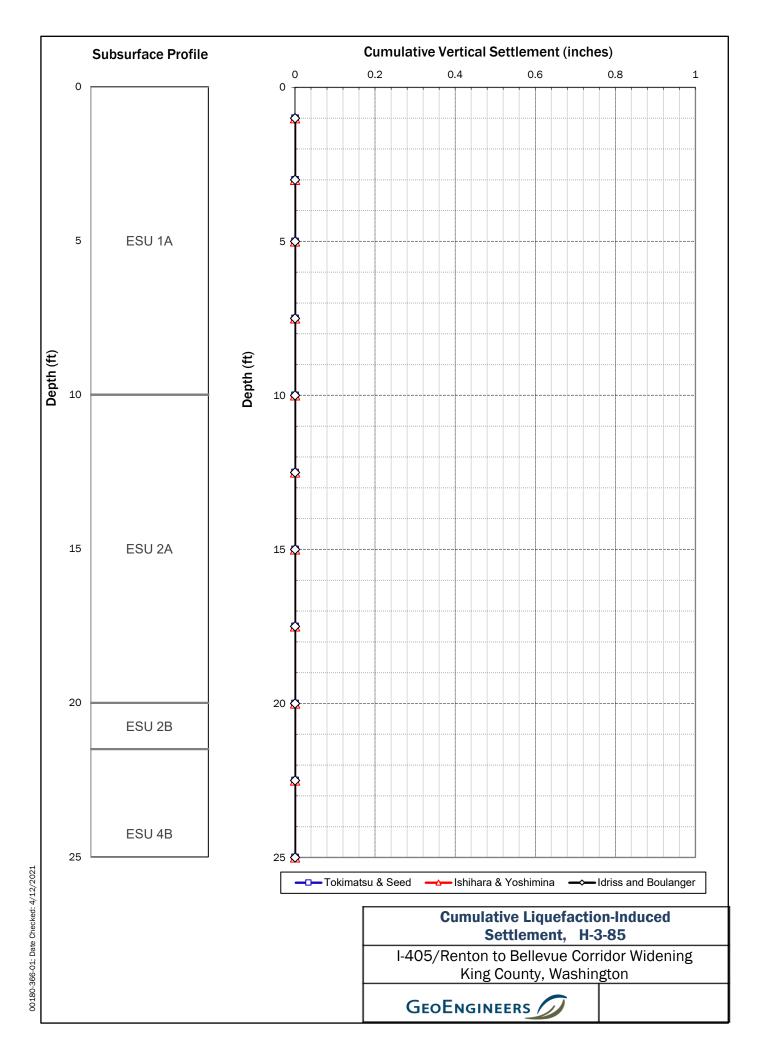
Idriss et al. (1998):

0.2

iquefaction and Residual Shear Strength Analysis. Results, H-3-85







# **Lateral Earth Pressures for Cohesionless Soils**

### **Project Information**

| Project:     | I-405/Renton to Bellevue Corridor Widening |
|--------------|--|
| Owner:       | WSDOT                                      |
| Job Number:  | 00180-366-01                               |
| Analysis by: | YTT  |
| Date/Time:   | 1/11/2022 3:32 PM                          |
| Checked by:  | ТВ   |

### **Input Parameters**

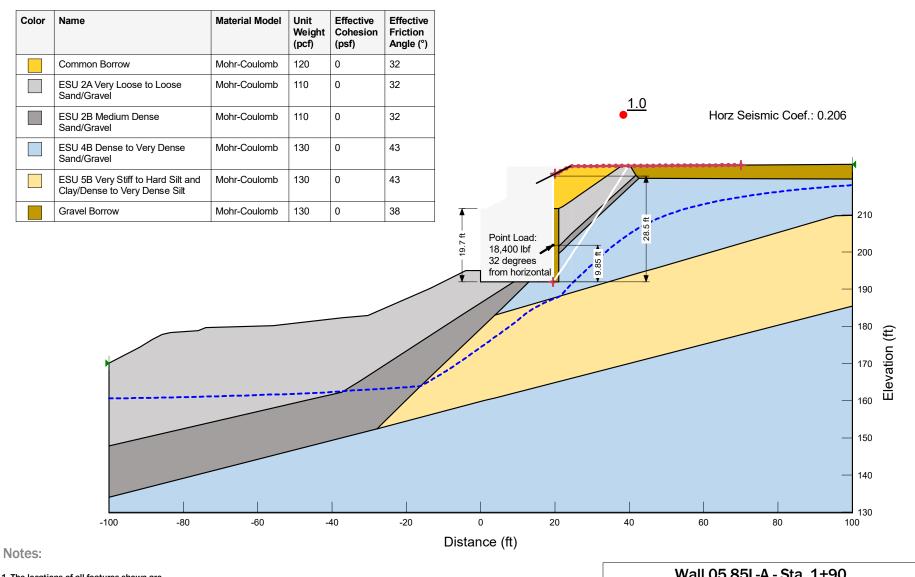
| Material | φ<br>Friction Angle<br>(deg) | β <sub>2</sub> (-)<br>Foreslope<br>(deg) | i (+)<br>Backslope<br>(deg) | δ<br>Wall Friction - Active<br>(deg) | δ<br>Wall Friction - Passive<br>(deg) | β<br>Wall Batter<br>(deg) | γ <sub>m</sub><br>(pcf) | γ <sub>b</sub> (pcf) | Passive<br>Factor of<br>Safety | k <sub>h</sub><br>(g) | k <sub>v</sub> (g)                               |
|----------|------------------------------|--|-----------------------------|--------------------------------------|---------------------------------------|---------------------------|-------------------------|----------------------|--------------------------------|-----------------------|--|
| ESU 2A   | 32                           | -27                                      | 27                          | 21                                   | 0                                     | 0                         | 110                     | 47.6                 | 1                              | 0                     | 0  |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       |  |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       |  |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       | <del>                                     </del> |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       |  |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       |  |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       |  |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       | <u> </u>   |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       | <del>                                     </del> |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       |  |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       |  |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       |  |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       | <del>                                     </del> |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       | <del>                                     </del> |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       |  |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       |  |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       |  |

### **Lateral Earth Pressures**

#### Output

| Material | K <sub>a</sub> | <u>Active</u><br>γ <sub>a</sub> | γ'a   | K <sub>p</sub> | $\gamma_{p(all)}$ | $\gamma'_{p(all)}$ | ssive<br>γ <sub>pe(all)</sub> | γ' <sub>pe(all)</sub> | K <sub>o</sub> | At Rest<br>γ <sub>o</sub> |       | Single Tieback | EP Trapezoid  Mult. Tiebacks <sup>1</sup> , <b>X</b> | K <sub>ae</sub> | γ <sub>ae</sub> | eismic<br>γ' <sub>ae</sub> | K <sub>pe</sub> | Seismic Pressure -<br>Rectangular |
|----------|----------------|---------------------------------|-------|----------------|-------------------|--------------------|-------------------------------|-----------------------|----------------|---------------------------|-------|----------------|--|-----------------|-----------------|----------------------------|-----------------|-----------------------------------|
|          |                | (pcf)                           | (pcf) |                | (pcf)             | (pcf)              | (pcf)                         | (pcf)                 |                | (pcf)                     | (pcf) | (psf * H)      |  |                 | (pcf)           | (pcf)                      |                 | (psf * H)                         |
| ESU 2A   | 0.46           | 51.02                           | 22.08 | 1.21           | 132.63            | 57.39              | 618.20                        | 267.51                | 0.47           | 51.71                     | 22.38 | 51.02          | 51.02  | 0.46            | 51.02           | 22.08                      | 5.62            | 0.00                              |
|          |                |                                 |       | <u> </u>       |                   |                    |                               |                       |                |                           |       |                |  |                 |                 |                            |                 |                                   |
|          |                |                                 |       |                |                   |                    |                               |                       |                |                           |       |                |  |                 |                 |                            |                 |                                   |
|          |                |                                 |       |                |                   |                    |                               |                       |                |                           |       |                |  |                 |                 |                            |                 |                                   |
|          |                |                                 |       |                |                   |                    |                               |                       |                |                           |       |                |  |                 |                 |                            |                 |                                   |
|          |                |                                 |       |                |                   |                    |                               |                       |                |                           |       |                |  |                 |                 |                            |                 |                                   |
|          |                |                                 |       |                |                   |                    |                               |                       |                |                           |       |                |  |                 |                 |                            |                 |                                   |
|          |                |                                 |       |                |                   |                    |                               |                       |                |                           |       |                |  |                 |                 |                            |                 |                                   |
|          |                |                                 |       |                |                   |                    |                               |                       |                |                           |       |                |  |                 |                 |                            |                 |                                   |
|          |                |                                 |       |                |                   |                    |                               |                       |                |                           |       |                |  |                 |                 |                            |                 |                                   |
|          |                |                                 |       |                |                   |                    |                               |                       |                |                           |       |                |  |                 |                 |                            |                 |                                   |
|          |                |                                 |       |                |                   |                    |                               |                       |                |                           |       |                |  |                 |                 |                            |                 |                                   |
|          |                |                                 |       |                |                   |                    |                               |                       |                |                           |       |                |  |                 |                 |                            |                 |                                   |
|          |                |                                 |       |                |                   |                    |                               |                       |                |                           |       |                |  |                 |                 |                            |                 |                                   |
|          | ļ              | 1                               | l     | l              | 1                 | l                  |                               |                       | l              | 1                         |       |                |  |                 | 1               | l                          |                 |                                   |
|          |                |                                 |       |                |                   |                    |                               |                       |                |                           |       |                |  |                 |                 |                            |                 |                                   |
|          |                |                                 |       |                |                   |                    |                               |                       |                |                           |       |                |  |                 |                 |                            |                 |                                   |
|          |                |                                 |       |                |                   |                    |                               |                       |                |                           |       |                |  |                 |                 |                            |                 |                                   |
|          |                |                                 |       |                |                   |                    |                               |                       |                |                           |       |                |  |                 |                 |                            |                 |                                   |
|          |                |                                 |       |                |                   |                    |                               |                       |                |                           |       |                |  |                 |                 |                            |                 |                                   |



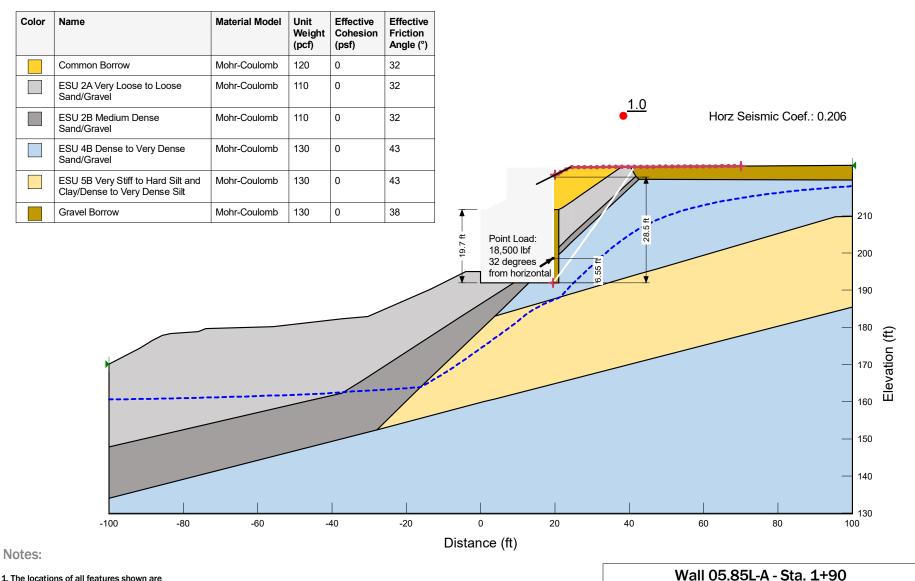


1. The locations of all features shown are approximate.

This drawing is for information purposes. It is intended to assist in showing features discussed in an attached document.

GeoEngineers, Inc. cannot guarantee the accuracy and context of electronic files. The master file is stored by GeoEngineers, Inc. and will serve as the official record of this communication. Wall 05.85L-A - Sta. 1+90 LEP - GLE Approach (Spencer, 1/2H)





1. The locations of all features shown are approximate.

This drawing is for information purposes. It is intended to assist in showing features discussed in an attached document.

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Project: 405 Renton to Bellveue By: YT Checked By: TB

#### Project Number: <u>00180-366-01</u> Date: 10/01/21 Page 1 of 1

### Seismic Earth Pressure Calculation Wall 05.85L-A

Active and seismic earth pressures using the limit equilibrium method outlined in NCHRP Report 611 Section 4.2.1 (Anderson et al., 2008) per AASHTO A11.3.3.

Earth pressures were developed from the bottom of footing to ground surface. Different application location of the force at one-third from the base (1/3H, where H is retained soil height) and at one half from the base were examined to determine the maximum seismic earth pressure. Spencer's methods was used to verify Pa and Pae.

Friction angle of the ESU 2A is used to define the inclination fo the applied point load in the model.

 $\phi = 32$ 

Friction angle of ESU 2A

$$P_{AE2} = 18400 \ \frac{lbf}{ft}$$

Location of force = 1/2H

$$P_{AE3} = 18500 \ \frac{\textit{lbf}}{\textit{ft}}$$

Location of force = 1/3H

(See slopeW output attached)

Given:  $\gamma = 110 \ pcf$ 

 $H \coloneqq 19.7 \ \mathbf{ft}$ 

Height of wall

$$k_n = 0$$

 $k_v = 0$   $k_h = 0.206$ 

Half of PGA applied for flexible system, PGA reduced to 0.412g for wave scatter effects.

$$K_{AE2} := \frac{P_{AE2} \cdot 2}{\gamma \cdot H^2 \cdot (1 - k_v)} = 0.862$$

Location of force = 1/2H

$$K_{AE3} := \frac{P_{AE3} \cdot 2}{\gamma \cdot H^2 \cdot (1 - k_v)} = 0.867$$

Location of force = 1/3H

Seismic+active earth pressures

$$\max \left( \gamma \cdot K_{AE2}, \gamma \cdot K_{AE3} \right) = 95 \frac{lbf}{ft^3}$$



# **Sliding Coefficients of Friction**

| Foundation Soil Type | φ' | Discontinuous Reinforcements |
|----------------------|----|------------------------------|
| ESU 2A               | 32 | 0.62                         |
| Common Borrow        | 32 | 0.62                         |
| Select Borrow        | 36 | 0.73                         |
| Gravel Borrow        | 38 | 0.78                         |

#### Notes:

Sliding coefficients calculated according to AASHTO Equation 10.6.3.4-2

Structural Earth Walls (SEW) are termed Mechanically Stabilized Earth (MSE) walls in AASHTO.

### Coefficient of Friction for Discontinuous Reinforcements, e.g., Strips:

Coefficient of friction = 1.0\*tan(Phi')

Phi' = lesser of friction angle of foundation soil and friction angle of reinforced fill per AASHTO 11.10.5.3

### **AASHTO 10.6.3.4:**

$$R_{\tau} = CV \tan \phi_f \qquad (10.6.3.4-2)$$

for which:

C = 1.0 for MSE Wall per AASHTO Table 11.5.7-1

where:

 $\phi_f$  = internal friction angle of drained soil

(degrees)

V = total vertical force (kips)

### LRFD Foundation Design

### Spreadsheet Reference Section 10.6.3.1.2 of The 2014 AASHTO LRFD Bridge Design Specifications

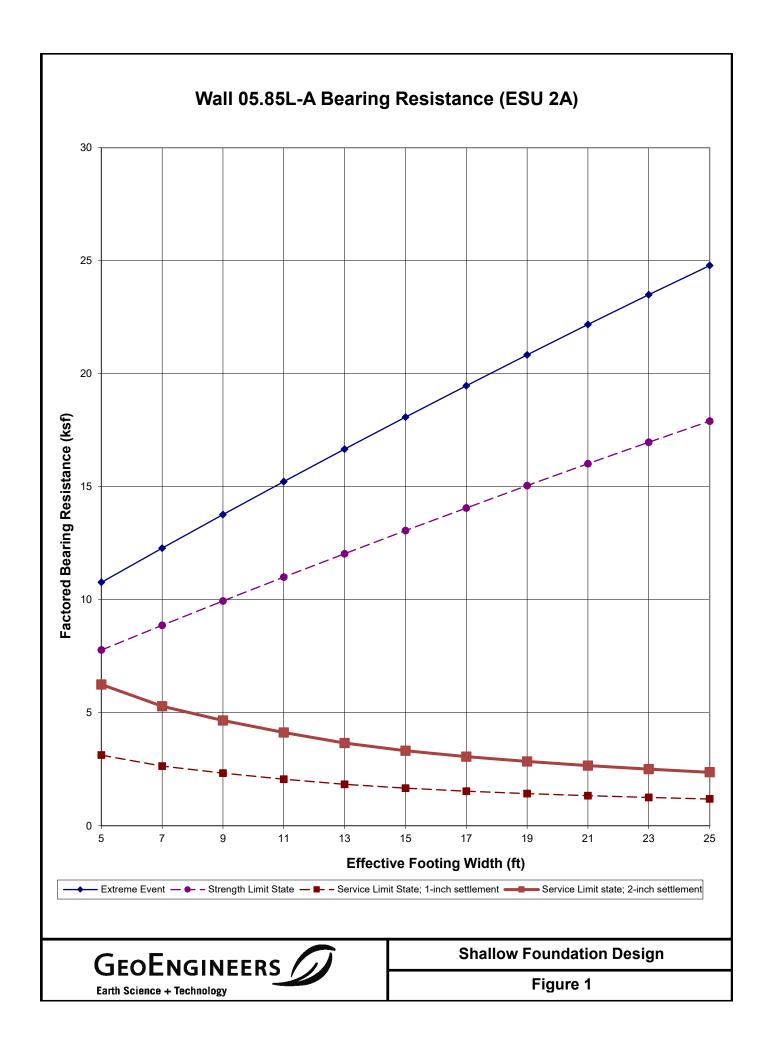
| Date/Time:    | 1/11/22 10:37 AM  |
|---------------|---|
| Project Name: | I-405/Renton to Bellevue Corridor Widening - Wall 05.85L-A (ESU 2A) |
| Project No.:  | 00180-366-01  |

| Foundation Soil Condi                     | tions |
|---|-------|
| Unit Weight, γ (pcf)                      | 110   |
| Friction angle, Φ (degrees)               | 32    |
| Friction angle, Φ (rad)                   | 0.558 |
| Cohesion, C (psf)                         | 0     |
| Embedment, D <sub>f</sub> (ft)            | 3     |
| Depth to Groundwater, D <sub>w</sub> (ft) | 7.2   |
| Footing Length, L (ft)                    | 100   |
| Footing Width, B (ft)                     | 1     |
| Poissons Ration, v                        | 0.33  |
| Young's Modulus, E <sub>s</sub> (ksf)     | 530   |

| Bearing Capacity Factor | ors |
|-------------------------|-----|
| N <sub>Y</sub>          | 30  |
| N <sub>c</sub>          | 36  |
| $N_q$                   | 23  |

|                            | Water Dep             | th Factors             |           | Shape Factors       |      | Unfactored | Extreme Event Resistance                       | Working Bearing Resistance             | Deflection from Elastic | Deflection from Elastic |
|----------------------------|-----------------------|------------------------|-----------|---------------------|------|------------|--|--|-------------------------|-------------------------|
| Effective Footing Width, B |                       |                        |           | onapo i actoro      |      | Bearing    | Resistance Factor (0.9) for MSE walls (Section | Resistance Factor (0.65) for MSE walls | Settlement Spreadsheet  | Settlement Spreadsheet  |
| <u> </u>                   | <u>C<sub>wq</sub></u> | <u>C<sub>w-y</sub></u> | <u>Sc</u> | $\underline{S}_{Y}$ | Sq   | Resistance | 11.5.8 AASHTO)                                 | (Table 11.5.7-1)                       | 1" Deflection           | 2" Deflection           |
| (ft)                       |                       |                        |           |                     |      | (ksf)      | (ksf)  | (ksf)                                  | (ksf)                   | (ksf)                   |
| 5.0                        | 1.0                   | 0.5                    | 1.03      | 0.98                | 1.03 | 12.0       | 10.8   | 7.8                                    | 3.1                     | 6.3                     |
| 7.0                        | 1.0                   | 0.5                    | 1.05      | 0.97                | 1.04 | 13.6       | 12.3   | 8.9                                    | 2.6                     | 5.3                     |
| 9.0                        | 1.0                   | 0.5                    | 1.06      | 0.96                | 1.06 | 15.3       | 13.8   | 9.9                                    | 2.3                     | 4.7                     |
| 11.0                       | 1.0                   | 0.5                    | 1.07      | 0.96                | 1.07 | 16.9       | 15.2   | 11.0                                   | 2.1                     | 4.1                     |
| 13.0                       | 1.0                   | 0.5                    | 1.08      | 0.95                | 1.08 | 18.5       | 16.7   | 12.0                                   | 1.8                     | 3.7                     |
| 15.0                       | 1.0                   | 0.5                    | 1.10      | 0.94                | 1.09 | 20.1       | 18.1   | 13.1                                   | 1.7                     | 3.3                     |
| 17.0                       | 1.0                   | 0.5                    | 1.11      | 0.93                | 1.11 | 21.6       | 19.5   | 14.1                                   | 1.5                     | 3.1                     |
| 19.0                       | 1.0                   | 0.5                    | 1.12      | 0.92                | 1.12 | 23.1       | 20.8   | 15.0                                   | 1.4                     | 2.8                     |
| 21.0                       | 1.0                   | 0.5                    | 1.14      | 0.92                | 1.13 | 24.6       | 22.2   | 16.0                                   | 1.3                     | 2.7                     |
| 23.0                       | 1.0                   | 0.5                    | 1.15      | 0.91                | 1.14 | 26.1       | 23.5   | 17.0                                   | 1.3                     | 2.5                     |
| 25.0                       | 1.0                   | 0.5                    | 1.16      | 0.90                | 1.16 | 27.5       | 24.8   | 17.9                                   | 1.2                     | 2.4                     |

Note: Depth and inclination modifier were taken as 1 because the load is applied axially and during construction the soils above the footing are to be excavated.





- 1. The locations of all features shown are approximate.
- This drawing is for information purposes. It is intended to assist in showing features discussed in an attached document.

-100

-80

-60

-40

-20

Distance (ft)

20

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# SEW Wall 05.85L-A - Sta. 1+90 Steady State Seepage

210

200

190

180 (t) Elevation (ft)

150

140

130

I-405/Renton to Bellevue Corridor Widening King County, Washington



60

40

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# Wall 05.85L-A - Sta. 1+90 Static Global Stability (Spencer)



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# Wall 05.85L-A - Sta. 1+90 Static Global Stability (M-P)



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# Wall 05.85L-A - Sta. 1+90 Pseudo-Static Global Stability (Spencer)



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# Wall 05.85L-A - Sta. 1+90 Pseudo-Static Global Stability (M-P)



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# Wall 05.85L-A - Sta. 1+90 Post-Seismic Global Stability (Spencer)



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# Wall 05.85L-A - Sta. 1+90 Post-Seismic Global Stability (M-P)



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# Wall 05.85L-A - Sta. 1+90 Static Global Stability + FC Wall (Spencer)



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# Wall 05.85L-A - Sta. 1+90 Static Global Stability + FC Wall (M-P)



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# Wall 05.85L-A - Sta. 1+90 Pseudo-Static Global Stability + FC Wall (S)



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### Wall 05.85L-A - Sta. 1+90 Pseudo-Static Global Stability + FC Wall (M-P)



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# Wall 05.85L-A - Sta. 1+90 Post-Seismic Global Stability + FC Wall (S)



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### Wall 05.85L-A - Sta. 1+90 Post-Seismic Global Stability + FC Wall (M-P)



Project: WSDOT I-405 Renton to Bellevue

Project Number: 01800-366-01

Date: 9/30/21

### Calculating MSE Strip Properties for Slope/W (Wall 05.85L-A Sta. 1+90)

Page 1 of 7

Analysis By: YTT

Checked By: TB

For global stability analyses, the MSE wall is modeled as a high strength material and the failure is forced outside of the reinforced zone. To check for compound stability, the high strength material is replaced with gravel borrow and reinforcing strips. The properties of the metal strips are calculated based on FHWA NHI-10-024 and NHI-10-025. The reinforcement properties are converted to per unit width basis, and implemented as a continous layer in Slope/W.

### **Input Soil Properties:**

Backfill meeting WSDOT standard specifications 9-03.14(4), Gravel Borrow for Structural Earth Wall.

$$\phi_{gravel} = 38 \ deg$$

### **Input Strip Properties:**

50mm wide and 4mm thick with Grade 65 steel.

width = 2 in

$$thickness := \frac{5}{32}$$
 in Gross thickness (no corrosion)

$$f_y = 65.0 \text{ } ksi$$
 Yield stress

### **Calculate Corrosion Reduction:**

Calculate new cross-sectional area of steel straps after 75 years of corrosion exposure.

| Category      | Stee1                      | Minimum Galvanization |  |  |
|---------------|----------------------------|-----------------------|--|--|
| Category      | Thickness                  | Thickness             |  |  |
| Strip         | < 1/4 in. (6.4 mm)         | 3.4 mils (85 µm)      |  |  |
|               | > 1/4 in. (6.4 mm)         | 3.9 mils (100 µm)     |  |  |
| Wire*         | All diameters              | 3.4 mils (85 µm)      |  |  |
| * For bar mat | s fabricated from uncoated | steel wire.           |  |  |

The corrosion rates presented in Table 3-8 are suitable for conservative design. These rates assume a moderately corrosive backfill material having the controlled electrochemical property limits that are discussed under electrochemical properties in this chapter.

Table 3-8 Steel Corrosion Rates for Moderately Corrosive Reinforced Fill.

|                                 | 0.58 mils/yr (15 µm/year) (first 2 years) 0.16 mils/yr (4 µm/year) (thereafter) |
|---------------------------------|---|
|                                 |   |
| For residual carbon steel/side: | 0.47 mils/yr (12 µm/year) (thereafter)  |

Calculate time (in years) to corrode through galvinization.

$$0.58 \cdot 2 + 0.16 \cdot (t_g - 2) = 3.4$$

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Analysis By: YTT Checked By: TB

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$$t_g := \frac{3.4 - 0.58 \cdot 2}{0.16} + 2 = 16$$

$$t_{75\_years}\!\coloneqq\!thickness-0.47\boldsymbol{\cdot}0.001\ \frac{\textit{in}}{\textit{yr}}\boldsymbol{\cdot}\left(75-t_g\right)\ \textit{yr}\boldsymbol{\cdot}2\!=\!0.101\ \textit{in}$$

$$A_c \coloneqq width \cdot t_{75\ years} = 0.202\ in^2$$

New cross-sectional area after 75 years of corrosion exposure

# LRFD Resistance Factors for Tensile and Pullout Resistance for MSE Walls with Metal Straps:

Table 4-7. Resistance Factors, φ, for Tensile and Pullout Resistance for MSE Walls (after Table 11.5.6-1, AASHTO {2007}).

| Reinforcen                                   | ent Type and Loading Condition             | Resistance<br>Factor |  |  |  |  |
|--|--|----------------------|--|--|--|--|
|  | Strip reinforcements (A)                   |                      |  |  |  |  |
|  | Static loading                             | 0.75                 |  |  |  |  |
|  | Combined static/earthquake loading         | 1.00                 |  |  |  |  |
| Metallic reinforcement and                   | Combined static/traffic barrier impact (B) | 1.00                 |  |  |  |  |
| connectors                                   | Grid reinforcements (A, C)                 |                      |  |  |  |  |
|  | Static loading                             | 0.65                 |  |  |  |  |
|  | Combined static/earthquake loading         | 0.85                 |  |  |  |  |
|  | Combined static/traffic barrier impact (B) | 0.85                 |  |  |  |  |
|  | Static loading                             | 0.90                 |  |  |  |  |
| Geosynthetic reinforcement<br>and connectors | Combined static/earthquake loading         | 1.20                 |  |  |  |  |
| and connectors                               | Combined static/traffic barrier impact (B) | 1.20                 |  |  |  |  |
| Pullout resistance of tensile                | Static loading                             | 0.90                 |  |  |  |  |
| reinforcement (metallic and                  | Combined static/earthquake loading         | 1.20                 |  |  |  |  |
| geosynthetic)                                | Combined static/traffic barrier impact (B) | 1.00                 |  |  |  |  |

### Notes:

- A. Apply to gross cross-section less sacrificial area. For sections with holes, reduce gross area in accordance with AASHTO (2007) Article 6.8.3 and apply to net section less sacrificial area.
- B. Combined static/traffic barrier impact resistance factors are not presented in AASHTO.
- C. Applies to grid reinforcements connected to rigid facing element, e.g., a concrete panel or block. For grid reinforcements connected to a flexible facing mat or which are continuous with the facing mat, use the resistance factor for strip reinforcements.

$$\Phi_{static} \coloneqq 0.75 \qquad \qquad \Phi_{pullout\_static} \coloneqq 0.9$$

$$\varPhi_{seismic} \coloneqq 1.0 \qquad \qquad \varPhi_{pullout\_seismic} \coloneqq 1.2$$

Page 3 of 7 Analysis By: YTT Date: 9/30/21 Checked By: TB

### **Calculate Slope/W Reinforcement Inputs:**

$$H_{wall} = 19.7 \; ft$$

Assuming strip layout based on typical RECO A panel, the vertical  $(s_v)$  and the horizontal  $(s_h)$  spacing of the steel straps within each SE wall panel was determined. For calculation efficiency, the calculations are performed using matrices.

$$s_{v} \coloneqq \begin{bmatrix} 1.7 \\ 2.4 \\ 2.4 \\ 2.4 \\ 2.4 \\ 2.4 \\ 2.4 \\ 2.4 \\ 2.4 \end{bmatrix} \boldsymbol{ft} \qquad s_{h} \coloneqq \begin{bmatrix} 1.25 \\ 1.25 \\ 2.5 \\ 2.5 \\ 2.5 \\ 2.5 \\ 2.5 \\ 2.5 \\ 2.5 \\ 2.5 \\ 2.5 \end{bmatrix} \boldsymbol{ft}$$

The matrix respresents the same order of the SE Wall reinforcement. Top row of the matrix represents the bottom row of the SE Wall reinforcement and the bottom row of the matrix represents the row of reinforcement closest to the ground surface.

$$i = 0 \dots \operatorname{length}(s_v) - 1$$

Calculate number of elements

$$elevation_{_{i}} \coloneqq \sum_{j=0}^{i} s_{v_{_{j}}} = \begin{bmatrix} 1.7 \\ 4.1 \\ 6.5 \\ 8.9 \\ 11.3 \\ 13.7 \\ 16.1 \\ 18.5 \end{bmatrix} \textbf{\textit{ft}}$$

Calculate each strap's vertical elevation, with the base of the wall as elevation 0 ft. Top row of the matrix represents the bottom reinforcement row.

$$depth_{i} \coloneqq H_{wall} - elevation_{i} = \begin{bmatrix} 18 \\ 15.6 \\ 13.2 \\ 10.8 \\ 8.4 \\ 6 \\ 3.6 \\ 1.2 \end{bmatrix} \textbf{ft} \qquad \text{Calculate each strap's depth from the ground surface}.$$

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### Calculate Pullout Resistance Slope/W Input:

For design and comparison purposes, a normalized definition of pullout resistance will be used throughout the manual. The pullout resistance, Pr, at each of the reinforcement levels per unit width of reinforcement is given by:

$$\mathbf{P}_{r} = \mathbf{F} + \alpha \sigma'_{r} \mathbf{L}_{r} \mathbf{C} \tag{3-2}$$

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where:

L<sub>e</sub> C = the total surface area per unit width of the reinforcement in the resistive zone behind the failure surface

Le = the embedment or adherence length in the resisting zone behind the failure

C = the reinforcement effective unit perimeter; e.g., C = 2 for and sheets, and because the edges are neglected C = 2 for strips and grids

 $F^*$  = the pullout resistance (or friction-bearing-interaction) factor

α = a scale effect correction factor to account for a non linear stress reduction over the embedded length of highly extensible reinforcements, based on laboratory data (generally 1.0 for metallic reinforcements and 0.6 to 1.0 for geosynthetic reinforcements, see Table 3-6).

 $\sigma'_v$  = the effective vertical stress at the soil-reinforcement interfaces.

The <u>factored</u> pullout resistance <u>per unit width of the wall</u> is then given by:

$$P_r = \Phi_{pullout} \left( F \boldsymbol{\cdot} \alpha \boldsymbol{\cdot} \sigma_v' \boldsymbol{\cdot} L_e \boldsymbol{\cdot} C \right) \boldsymbol{\cdot} \frac{width}{s_h}$$

In Slope/W, pullout resistance per unit width of wall is given by:

$$P_r = \left(c + \sigma_v' \cdot tan\left(\phi_{interface}\right)\right) \cdot \alpha \cdot L_e \cdot C$$

Where  $\alpha$  and C can be defined within the reinforcement properties, and are set to be the same as defined above. Overburden pressure,  $\sigma_{v}{}'$  and effective length, Le are determined from the limit equilibrium analysis performed in Slope/W. Interface adhesion, c, is assumed to be negligable for metal straps in granular backfill.

To select a representative  $\phi_{interface}$  that will produce the same factored resistance per unit width of wall, the two expressions are set to be equal:

$$\varPhi_{pullout}\left(F\boldsymbol{\cdot}\alpha\boldsymbol{\cdot}\sigma_{v}{'}\boldsymbol{\cdot}L_{e}\boldsymbol{\cdot}C\right)\boldsymbol{\cdot}\frac{width}{s_{h}}\boldsymbol{=}\sigma_{v}{'}\boldsymbol{\cdot}tan\left(\phi_{interface}\right)\boldsymbol{\cdot}\alpha\boldsymbol{\cdot}L_{e}\boldsymbol{\cdot}C$$

Removing common constants and rearranging produces:

$$\phi_{interface} = atan \left( \frac{\Phi_{pullout} \cdot F \cdot width}{s_h} \right)$$

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### Calculate Pullout Resistance Factor F\*:

In the absence of site-specific pullout testing data, it is reasonable to use the semi-empirical relationships described in the following paragraphs in conjunction with the standard specifications for reinforced fill to provide a conservative evaluation of pullout resistance.

For steel ribbed reinforcement, the Pullout Resistance Factor F\* is commonly taken as:

$$F^* = \tan \rho = 1.2 + \log C_u$$
 at the top of the structure = 2.0 maximum (3-4)

$$F^* = \tan \phi$$
 at a depth of 20 ft (6 m) and below (3-5)

where  $C_u$  is the uniformity coefficient of the backfill ( $D_{60}/D_{10}$ ). If the specific  $C_u$  for the wall backfill is unknown at design time, a  $C_u = 4$  should be assumed (i.e.,  $F^* = 1.8$  at the top of the wall) for reinforced fills meeting the requirements of Section 3.1 of this chapter.

$$C_u = 6.3$$

Backfill used will need to meet gradation assumed

$$F_{max} = 1.2 + \log(C_u) = 1.999$$

$$F = \begin{bmatrix} 0.9\\ 1.05\\ 1.2\\ 1.34\\ 1.49\\ 1.63\\ 1.78\\ 1.93 \end{bmatrix}$$

Calculated F\* for each row of reinforcement. Top row of matrix represents the bottom row of reinforcement.

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### Calculate Interface Shear Angle (degrees):

$$\phi_{interface\_static} \coloneqq \operatorname{atan} \left( \frac{\Phi_{pullout\_static} \cdot F \cdot width}{s_h} \right) = \begin{bmatrix} 6.2 \\ 7.2 \\ 4.1 \\ 4.6 \\ 5.1 \\ 5.6 \\ 6.1 \\ 6.6 \end{bmatrix} \mathbf{\textit{deg}}$$

Static interface shear angle for each row of reinforcement. Top row of matrix represents the bottom reinforcement row.

$$\phi_{interface\_seismic} \coloneqq \operatorname{atan}\left(\frac{\Phi_{pullout\_seismic} \cdot F \cdot width}{s_h}\right) = \begin{bmatrix} 8.2\\ 9.5\\ 5.5\\ 6.1\\ 6.8\\ 7.4\\ 8.1\\ 8.8 \end{bmatrix} deg$$

Seismic interface shear angle for each row of reinforcement. Top row of matrix represents the bottom reinforcement row.

### Calculate Allowable Tensile Capacity of Steel Straps:

$$T_{al\_static} \coloneqq \Phi_{static} \cdot f_y A_c = 9.83 \ \textit{kip}$$

$$T_{al\_seismic}\!\coloneqq\! \varPhi_{seismic}\!\cdot\! f_y\; A_c\!=\!13.1\; \pmb{kip}$$

Slope/W does not have strap reinforcement inputs. Therefore, the tensile strength of the straps were modeled as continuous reinforcement. The calculated allowable tensile strap capacity was converted to a continuous reinforcement tensile capcity by distributing the capacity over the tributary width.

$$T_{al\_static\_row} \coloneqq rac{T_{al\_static}}{s_h} = egin{bmatrix} 7.86 \ 7.86 \ 3.93 \ 3$$

Static tensile capacity Slope/W inputs for each wall reinforcement row. Top row of the matrix represents the bottowm row of the SE Wall reinforcement.

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Date: 9/30/21

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| $T_{al\_seismic\_row} \coloneqq \frac{T_{al\_seismic}}{s_h} = \begin{bmatrix} 10 \\ 10 \\ 5 \\ 5 \\ 5 \\ 5 \\ 5 \end{bmatrix}$ |
|--|
|--|

Seismic tensile capacity Slope/W inputs for each wall reinforcement row. Top row of the matrix represents the bottowm row of the SE Wall reinforcement.

Distance (ft)

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# Wall 05.85L-A - Sta. 1+90 Static Compound Stability (Spencer)



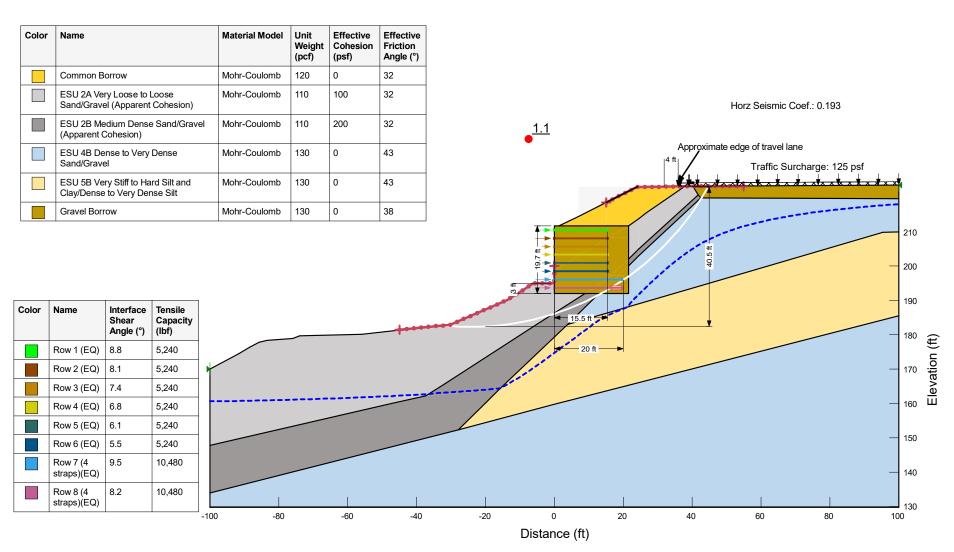
Distance (ft)

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# Wall 05.85L-A - Sta. 1+90 Static Compound Stability (M-P)

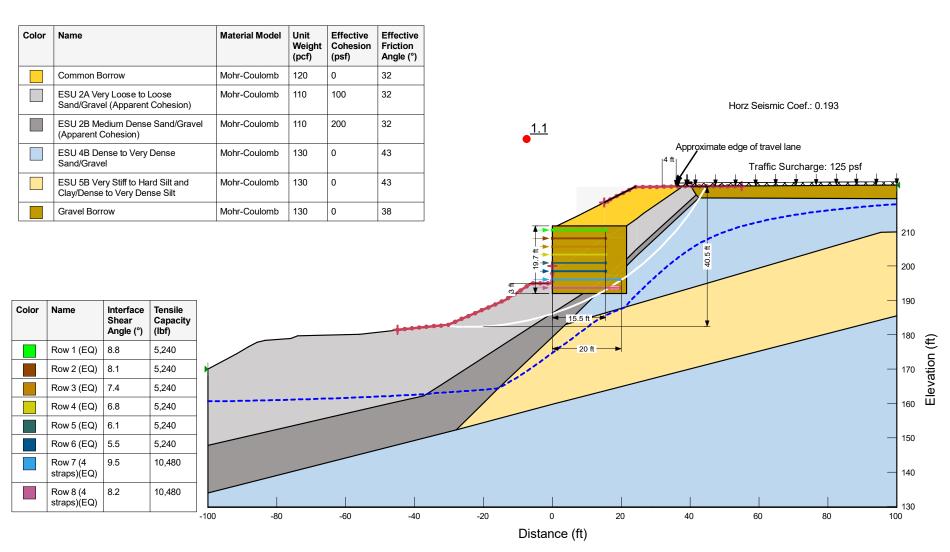




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# Wall 05.85L-A - Sta. 1+90 Pseudo-Static Compound Stability (Spencer)





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# Wall 05.85L-A - Sta. 1+90 Pseudo-Static Compound Stability (M-P)



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# Wall 05.85L-A - Sta. 1+90 Post-Seismic Compound Stability (Spencer)

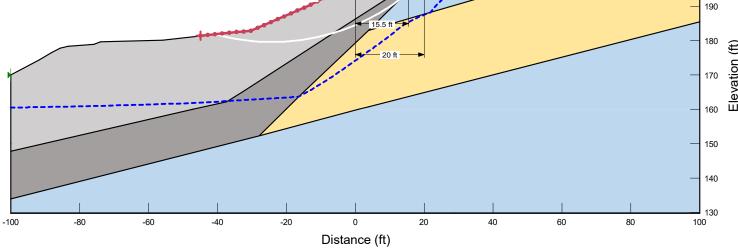


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# Wall 05.85L-A - Sta. 1+90 Post-Seismic Compound Stability (M-P)



| Color | Name                | Interface<br>Shear<br>Angle (°) | Tensile<br>Capacity<br>(lbf) |
|-------|---------------------|---------------------------------|------------------------------|
|       | Row 1               | 6.6                             | 3,930                        |
|       | Row 2               | 6.1                             | 3,930                        |
|       | Row 3               | 5.6                             | 3,930                        |
|       | Row 4               | 5.1                             | 3,930                        |
|       | Row 5               | 4.6                             | 3,930                        |
|       | Row 6               | 4.1                             | 3,930                        |
|       | Row 7 (4<br>straps) | 7.2                             | 7,860                        |
|       | Row 8 (4<br>straps) | 6.2                             | 7,860                        |



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# Wall 05.85L-A - Sta. 1+90 Static Compound Stability + FC Wall (Spencer)

Traffic Surcharge: 250 psf

210

200



| ensile<br>Capacity<br>lbf) |  |
|----------------------------|--|
| ,930                       |  |
| ,930                       |  |
| ,930                       |  |
| ,930                       |  |
| ,930                       |  |
| ,930                       |  |
| 7,860                      |  |
| ,860                       |  |

Angle (°)

6.6

6.1

5.6

5.1

4.6

4.1

7.2

6.2

Row 1

Row 2

Row 3

Row 4

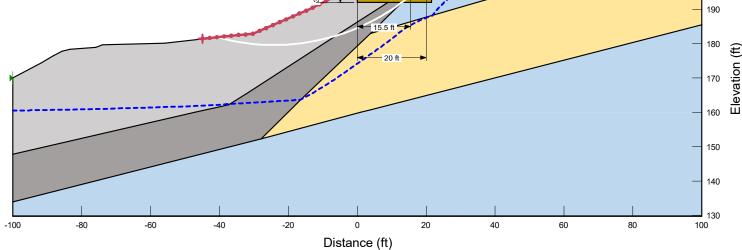
Row 5

Row 6

Row 7 (4

Row 8 (4 straps)

straps)



<u>1.3</u>

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# Wall 05.85L-A - Sta. 1+90 Static Compound Stability + FC Wall (M-P)

I-405/Renton to Bellevue Corridor Widening King County, Washington



Approximate edge of travel lane

Traffic Surcharge: 250 psf

210

200

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# Wall 05.85L-A - Sta. 1+90 Pseudo-Static Compound Stability + FC Wall (S)



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# Wall 05.85L-A - Sta. 1+90 Pseudo-Static Compound Stability+FC Wall (M-P)



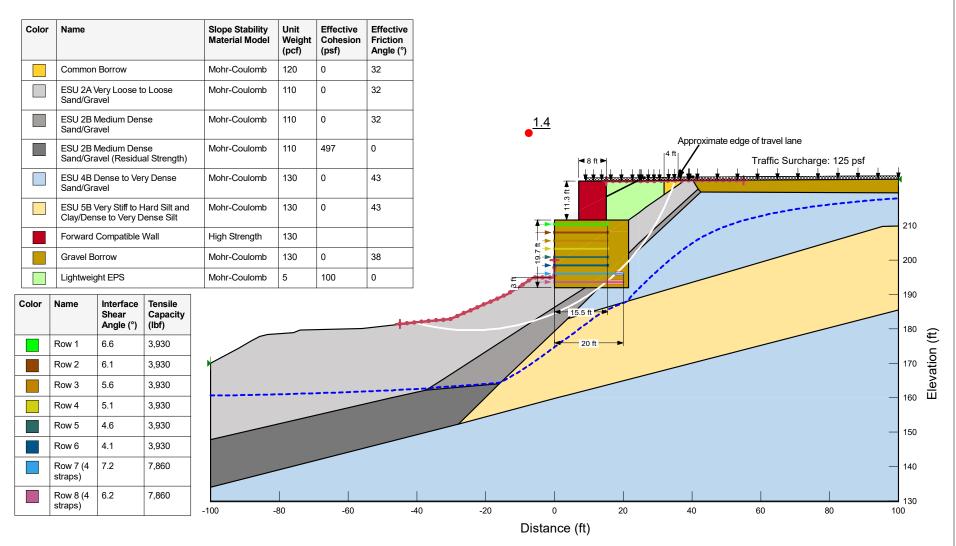
Distance (ft)

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# Wall 05.85L-A - Sta. 1+90 Post-Seismic Compound Stability + FC Wall (S)





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# Wall 05.85L-A - Sta. 1+90 Post-Seismic Compound Stability + FC Wall (M-P)









# Appendix F Wall 05.85L-B Calculations







# APPENDIX F - WALL 05.85L-B CALCULATIONS

# General

This appendix presents geotechnical calculations for Wall 05.85L-B including:

- **ESU Soil Properties**
- Seismic Hazard Analysis
- Lateral Earth Pressures
- Coefficients of Friction for Sliding
- Bearing Resistance and Elastic Settlement
- Global Stability
- Compound Stability

# **ESU Soil Properties**

Design soil properties were developed in accordance with the Project GDM, AASHTO LRFD, and FHWA. We calculated the average, geometric mean, and standard deviation within each ESU. We verified the reliability of the ESU data set by comparing the COV of each calculated geometric mean value to measured and interpreted values presented in Sabatini et al. (2002) Table 52.

A detailed description of the soil property development is presented in Section 7.1 of this geotechnical engineering report. Supporting calculations are provided in this appendix.

# **Seismic Hazard Analysis**

We selected a representative site class for each wall from the site class evaluation of nearby borings. We evaluated the site class of each boring using a spreadsheet developed by GeoEngineers in accordance with AASHTO LRFD Section 3.10.3.1.

We developed seismic design parameters using the WSDOT Bridge Engineering Software BEToolbox/BridgeLink in accordance with the WSDOT BDM based on the projected ground motion at the project site that has a 7 percent (SEE) probability of exceedance in a 75-year period (approximate 1,000-year return period).

We used a mean earthquake magnitude at the PGA period is 6.97 for the SEE based on the Hart Crowser design report "I-405 R2B Segment 1a Site-Specific Hazard Analysis RFU," dated March 25, 2021.

We evaluated the FS against liquefaction and liquefaction-induced settlement of saturated, loose to medium dense soils in accordance with the Project GDM Chapter 6 using a spreadsheet developed by GeoEngineers. The FSs against liquefaction at Wall 05.85L-B were greater than 1.2 for all soil analyzed; per Project GDM Section 6-4.2.3, soils with liquefaction potential are defined as those with FSs against liquefaction less than 1.2.

Detailed descriptions of our seismic hazard analysis methodology and the results are presented in Section 7.2 and Section 8.1, respectively, of this report. Site class calculations, WSDOT BDM software outputs, and liquefaction analyses are provided in this appendix.

# **Lateral Earth Pressures**

Active static lateral pressure coefficients and corresponding lateral earth pressures for ESU 2B were calculated on the back of Wall 05.85L-B in accordance with AASHTO LRFD Section 3.11.5 using the proposed 2H:1V backslope behind the wall and 3.7H:1V foreslope in front of the wall. Static lateral earth pressures shall be applied using a triangular distribution. An LRFD load factor of 1.5 shall be applied to the static earth pressures in accordance with AASHTO LRFD Table 3.4.1-2.

Due to relatively shallow embedment of the wall combined with a foreslope condition, passive lateral earth pressures shall be ignored.

Active static + seismic lateral pressure coefficients and static + seismic lateral earth pressures were calculated using the GLE Method in accordance with AASHTO LRFD Section A11.3.3 and NCHRP Report 611 Section 7.4. The GLE analysis was







evaluated for Spencer's method using the computer design software Slope/W (Geo Slope International, Ltd. 2020). For the static + seismic earth pressures, we used a modified horizontal seismic coefficient, kh, coupling a 50 percent reduction for flexible wall displacements with a reduction for wave scattering effects. Static + seismic lateral earth pressures shall be applied using a triangular distribution. An LRFD load factor of 1.0 shall be applied to the static + seismic earth pressures in accordance with AASHTO LRFD Table 3.4.1-1.

Surcharge loads (such as traffic loading, fill loads above the wall, and forward compatible loading for future I-405 widening) and appropriate load factors shall also be applied to evaluate wall stability. All surcharges shall apply load factors in accordance with AASHTO LRFD Tables 3.4.1-1 and 3.4.1-2.

A detailed description of our analysis methodology and the calculated results are presented in Section 7.3 and Section 8.2, respectively. Supporting calculations are provided in this appendix.

# Coefficients of Friction for Sliding

Coefficients of friction for sliding on surficial native soils, common borrow, select borrow, and gravel borrow were calculated using AASHTO LRFD equation 10.6.3.4-2.

A detailed description of our analysis methodology and the results are presented in Section 7.4 and Section 8.3, respectively, of this report. Supporting calculations are provided in this appendix.

# **Bearing Resistance and Elastic Settlement**

We estimated the bearing resistance and elastic settlement of the wall using a spreadsheet developed by GeoEngineers in accordance with AASHTO LRFD Section 10.6.3. We estimated elastic settlement from procedures outlined in AASHTO LRFD and Section 10.6.2.4. Sliding, overturning, and internal stability are being evaluated by the design-build team's wall designers and will be submitted under separate cover.

A detailed description of our analysis methodology and the results are presented in Section 7.5 and Section 8.4, respectively, of this report. Supporting calculations are provided in this appendix.

# **Global Stability**

We performed global stability analyses for the following critical design section:

Section Sta. 2+60 – Maximum overall slope height

Global stability was evaluated using limit equilibrium analysis methodology outlined in the Project GDM using the computer design software Slope/W (Geo Slope International, Ltd. 2020). We analyzed FSs using Spencer's method and Morgenstern-Price for a circular failure surface.

We used an apparent cohesion in the surficial native soils for pseudo-static analyses. Apparent cohesion was based on the fines content ranges presented in Table 11-2 of the FHWA Geotechnical Engineering Circular No. 3. We used 50 psf apparent cohesion in the common borrow backfill behind the wall for the pseudo-static analyses; see the Compound Stability section below for a discussion on apparent cohesion in common borrow for this wall.

We modeled a 4-foot horizontal bench in front of the wall per AASHTO LRFD Section 11.10.2.2. We modeled a front face embedment depth of 3.5 feet based on the slope from the front of the horizontal bench to the existing ground surface using criteria outlined in AASHTO LRFD Table C11.10.2.2-1.

We used a minimum reinforcement length of 0.7H to model the SEW. We modeled a 1.5-foot clearance between the reinforced zone and the temporary shoring, which was backfilled with imported gravel borrow. See Section 8.8.3 in this geotechnical report for discussion on temporary shoring.

A uniform traffic surcharge of 250 psf was included in static stability analysis. A uniform traffic surcharge of 125 psf was included for the pseudo-static stability analyses. In accordance with Section 15.4.12 of the Project GDM, we used a load factor of 1.0 for the static traffic surcharge because it is a non-structural load.

The groundwater level was modeled using results from the seepage analysis at Wall 05.85L-A. Steady-state seepage results are presented in Appendix E.







We also evaluated the global stability of the wall with a forward compatible wall for future I-405 widening. We modeled the forward compatible wall directly above the proposed SEW with the face of the forward compatible wall set back 7 feet from the face of the SEW. We modeled the backfill behind the forward compatible wall as lightweight EPS using the strength properties presented in Table 7 and truncated the EPS behind the forward compatible wall at 4 feet from the proposed edge of the traveled way. The required minimum static and pseudo-static FSs were met for all forward compatible wall cases.

Detailed descriptions of our global stability analysis methodology and the results of our analyses are presented in Section 7.8 and Section 8.6, respectively, of this report. Global stability models showing FS for critical failures at the design section are provided in this appendix. Slope/W reports are provided in Appendix J.

# **Compound Stability**

We used the results of the global stability analyses to model and evaluate compound stability at the critical design section using the minimum reinforcement lengths required to meet the minimum FSs from the global stability analyses. We modeled 10 rows of reinforcing strips at a length of 0.7H (2 strips per row per panel).

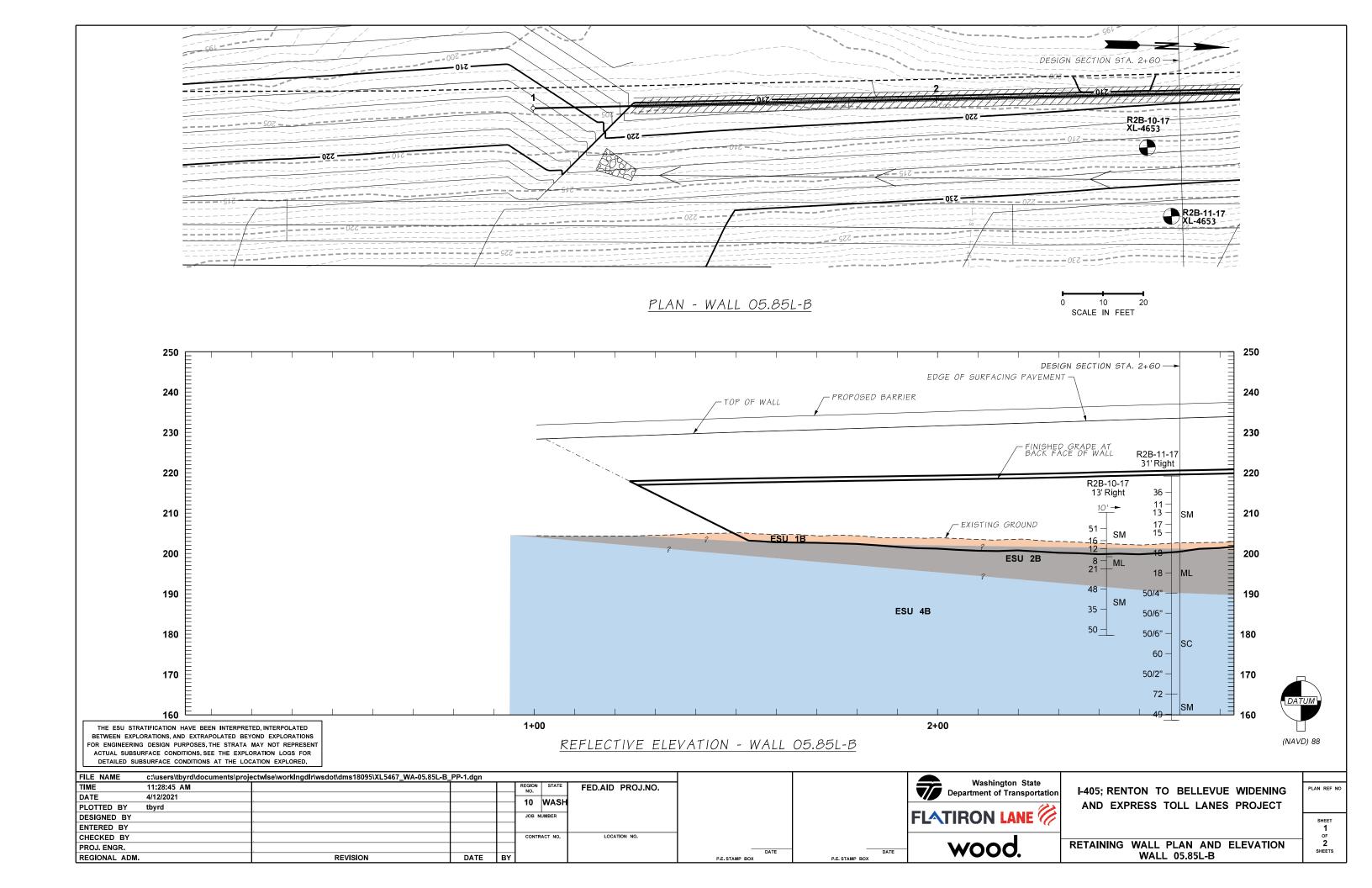
We used the horizontal seismic coefficient, kh, for compound stability presented in Table 8 and applied the apparent cohesion for native soils presented in Table 6 for the pseudo-static analysis. To meet minimum FSs for Wall 05.85L-B, we applied 50 psf apparent cohesion to the common borrow backfill. To meet the fines content required to use an apparent cohesion of 50 psf, as specified in FHWA Geotechnical Engineering Circular No. 3 Table 11-2, common borrow backfill shall be Option 2 per WSDOT Standard Specification 9-03.14(3).

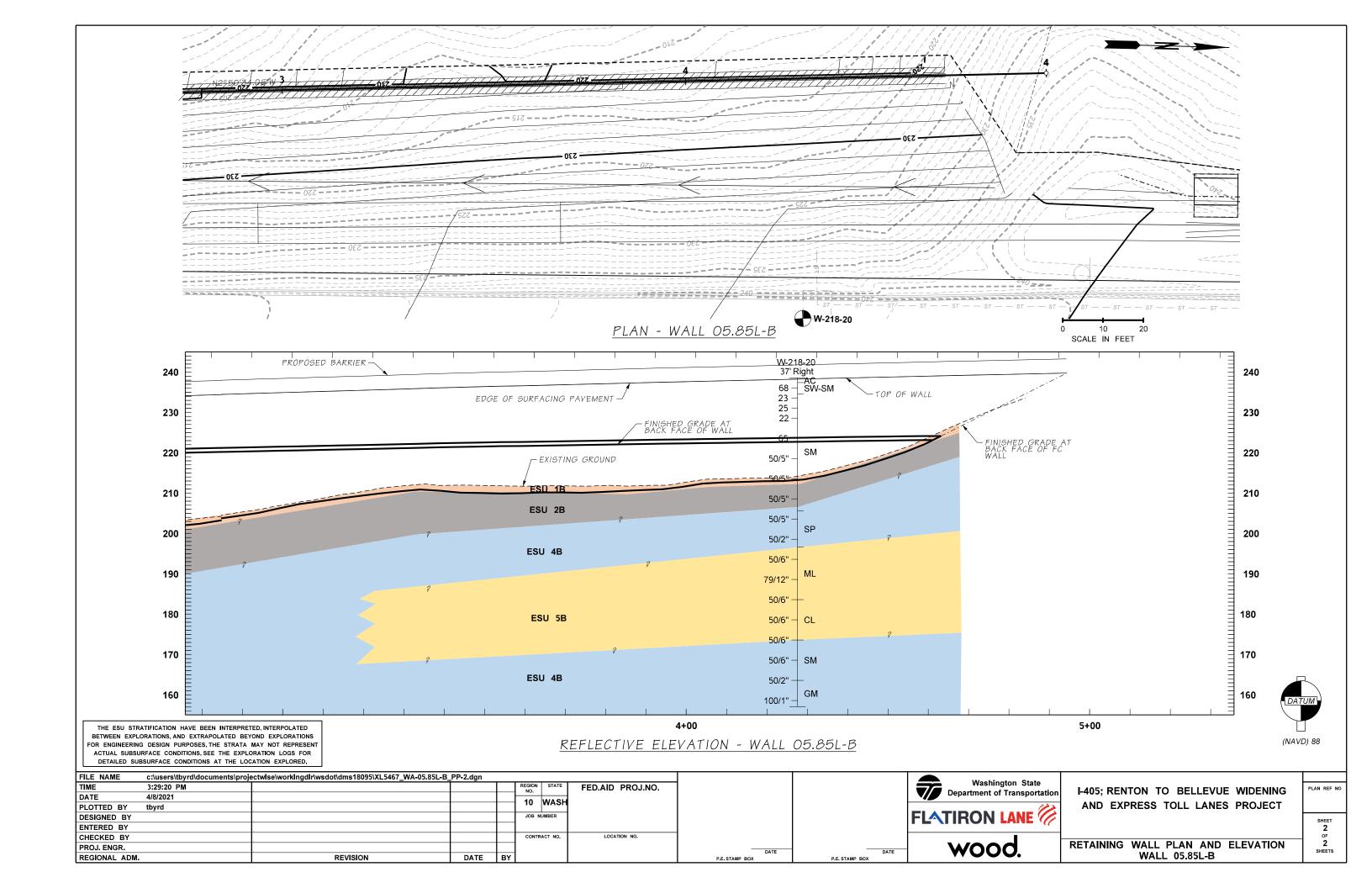
We applied a uniform traffic surcharge of 437.5 psf directly over the reinforced zone and a uniform traffic surcharge of 250 psf outside of the reinforced zone for the static compound stability analysis, and a traffic surcharge of 125psf for the pseudo-static compound stability analysis.

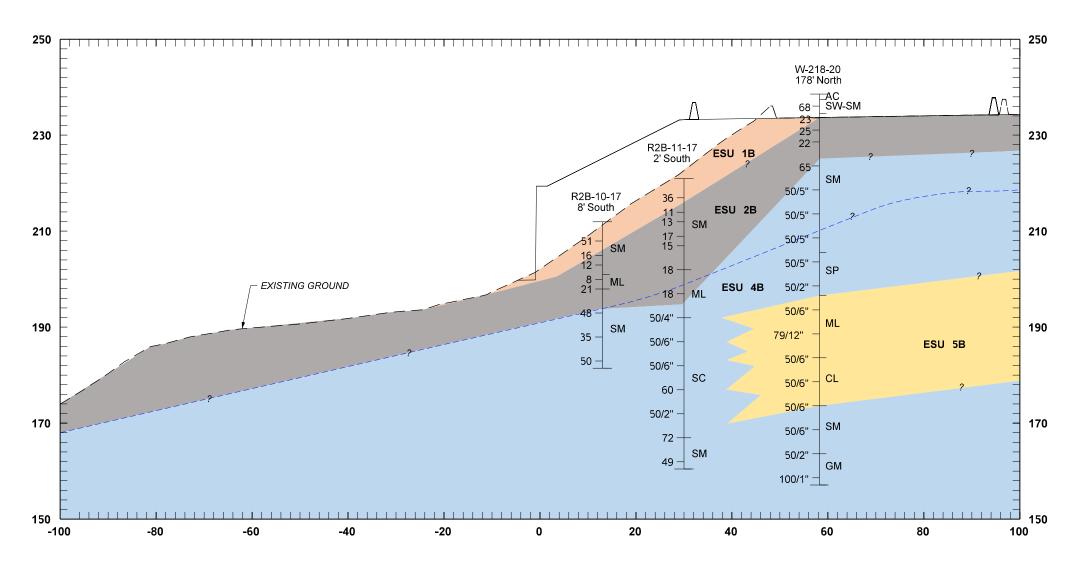
We used the piezometric surface from the seepage analysis at Wall 05.85L-A to model the groundwater level. Steady-state seepage results are presented in Appendix E.

We also evaluated the compound stability of proposed Wall 05.85L-B considering forward compatible walls for future I-405 widening, using the same geometry and strength properties from the global stability analyses for the forward compatible wall. As one option to meet required compound stability minimum FSs, we modeled the backfill as lightweight EPS. We did not explore all potential options as design of the forward compatible walls is outside the scope of this project, but minimally, the option we did analyze demonstrated that future I-405 widening projects can be designed and constructed without demolition or reconstruction of Wall 05.85L-B.Detailed descriptions of our compound stability analysis methodology and the results of our analyses are presented in Section 7.9 and Section 8.7, respectively, of this geotechnical report. Compound stability models showing FS for critical failures at the design section are provided in this appendix. Slope/W reports are provided in Appendix K.

# Appendix F.1 - Wall 05.85L-B Plan, Profile and Sections







WALL 05.85L-B STATION 2+60

THE ESU STRATIFICATION HAVE BEEN INTERPRETED, INTERPOLATED BETWEEN EXPLORATIONS, AND EXTRAPOLATED BEYOND EXPLORATIONS FOR ENGINEERING DESIGN PURPOSES, THE STRATA MAY NOT REPRESENT ACTUAL SUBSURFACE CONDITIONS, SEE THE EXPLORATION LOGS FOR DETAILED SUBSURFACE CONDITIONS AT THE LOCATION EXPLORED,

| FILE NAME    | c:\users\tbyra\aocuments\proj | jectwise\workingair\wsaot\ams18095\XL5467_wA-05.85L-B | _xs.agn |    |              |                  |                |                | 14/2 - 12/2 - 14 - 12 - 04 - 4 -        |                                    |             |
|--------------|-------------------------------|---|---------|----|--------------|------------------|----------------|----------------|---|------------------------------------|-------------|
| TIME         | 6:28:28 PM                    |   |         |    | REGION STATE | FED.AID PROJ.NO. |                |                | Washington State                        | I-405: RENTON TO BELLEVUE WIDENING | PLAN REF NO |
| DATE         | 4/9/2021                      |   |         |    | 10 WASH      | <u> </u>         |                |                | Department of Transportation            | ,                                  |             |
| PLOTTED BY   | tbyrd                         |   |         |    | I IU WASI    | ]                |                |                |   | AND EXPRESS TOLL LANES PROJECT     |             |
| DESIGNED BY  |                               |   |         |    | JOB NUMBER   |                  |                |                | FLATIRON LANE 🥢                         |                                    | SHEET       |
| ENTERED BY   |                               |   |         |    |              |                  |                |                | , _ ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, |                                    | 1           |
| CHECKED BY   |                               |   |         |    | CONTRACT NO. | LOCATION NO.     |                |                |   |                                    | OF OF       |
| PROJ. ENGR.  |                               |   |         |    |              |                  | DATE           | DATE           | WOOD.                                   | WALL 05.85L-B                      | 1<br>SHEETS |
| REGIONAL ADM | <u>.</u>                      | REVISION  | DATE    | BY |              |                  | P.E. STAMP BOX | P.E. STAMP BOX | <b>******</b>                           | DESIGN SECTION AT STA. 2+60        | 0.122.10    |

# Appendix F.2 - Wall 05.85L-B ESU Soil Property Calculations

| ESU  | Description  | Total No. of<br>Samples <sup>b</sup> | USCS <sup>c</sup> | Fines <sup>d</sup><br>(%) | Plasticity<br>Index,<br>PI <sup>e</sup> (%) | Raw N<br>(bpf) | N <sub>e</sub><br>(b | <sub>60</sub> f<br>pf) | (N <sub>1</sub> | .) <sub>60</sub> <sup>f</sup><br>pf) |       | l Unit<br>t <sup>g</sup> (pcf) | Effective<br>Angle, φ |                  | Softened | Effective<br>c' <sup>j</sup> (psf) |       | Residual Shear<br>Strength, Sr (psf) |       | ed Shear<br>, Su (psf) |
|------|--|--------------------------------------|-------------------|---------------------------|---|----------------|----------------------|------------------------|-----------------|--------------------------------------|-------|--------------------------------|-----------------------|------------------|----------|------------------------------------|-------|--------------------------------------|-------|------------------------|
|      |  |                                      |                   | Value                     | Value                                       | Value          | Value                | COV <sup>a</sup>       | Value           | COV <sup>a</sup>                     | Value | COV <sup>a</sup>               | Value                 | COV <sup>a</sup> | Value    | Value                              | Value | Value                                | Value | COV                    |
| 1 1B | Medium Dense to Very Dense<br>Coarse-Grained Fill            | 3                                    | SM                | 21                        | -   | 50             | 51                   | 20%                    | 77              | 24%                                  | 130   | 0%                             | 41                    | 3%               | -        | -                                  | -     | -                                    | -     | -                      |
| 2B   | Medium Dense Sand/Gravel                                     | 13                                   | SM                | 38                        | 3   | 16             | 19                   | 25%                    | 23              | 22%                                  | 115   | 3%                             | 34                    | 3%               | -        | -                                  | 1     | -                                    | -     | -                      |
| 4B   | Dense to Very Dense Sand/Gravel                              | 20                                   | SM                | 19                        | 5   | 113            | 103                  | 27%                    | 89              | 27%                                  | 130   | 1%                             | 43                    | 3%               | -        | -                                  | -     | -                                    | -     | -                      |
| I 5B | Very Stiff to Hard Silt and<br>Clay/Dense to Very Dense Silt | 4                                    | CL/ML             | 96                        | 10  | 94             | 108                  | 11%                    | 86              | 11%                                  | 130   | 0%                             | 42                    | 1%               | -        | -                                  | -     | -                                    | -     | -                      |

- a. Coefficient of Variation (COV) percentage calculated to verify the variability and reliability of sample data within ESU (WSDOT GDM Section 5.11.2 (2015)). Calculated COV percentage compared to ranges presented in Table 52 (Sabatini et al. 2002) (below).
- b. Number of samples excludes outliers.
- c. Predominant USCS classification of all samples in ESU. Sandstone, where encountered, denoted as (SS).
- d. Fines content percentage calculated as the geometric mean of all samples, whose values were determined through lab testing or estimated from field classification.
- e. For coarse-grained ESUs, the plasticity index was estimated on the fine-grained portion of the soil. For fine-grained ESUs, if lab data is limited, the plasticity index may not be representative of the overall soil unit.
- f. Corrected blow counts ( $N_{60}$  and  $(N_1)_{60}$ ) were calculated following WSDOT GDM Section 5.5 (2015).
- g. Individual sample unit weights were correlated using CALTRANS Geotechnical Manual (2014), verified with applicable ranges presented in Codotu (2001), as specified in WOOD SPM. The geometric mean of the unit weights was rounded to the nearest 5pcf, as specified in WOOD SPM. Unit weight data variability and quality were evaluated by comparing the calculated COV percentage to the applicable Sabatini range.
- h. Design friction angles were selected by considering fines content. Friction angle data variability and quality were evaluated by comparing the calculated COV percentage to the applicable Sabatini range.
- i. Where applicable, fully softened friction angle was estimated following WSDOT GDM, Figure 5-7 (After Stark and Hussain, 2013).
- j. Where applicable, effective cohesion was calculated using Equations 6 through 8 in the WOOD Geotechnical SPM.
- k. Where applicable, residual friction angle (to be used for slope stability evaluation) was estimated following WSDOT GDM, Figure 5-5 (After NAVFAC, 1971).

| Measured or interpreted parameter value               | Coefficient of Variation, V (%) |
|---|---------------------------------|
| Unit weight, γ  | 3 to 7 %                        |
| Buoyant unit weight, γ <sub>b</sub>                   | 0 to 10 %                       |
| Effective stress friction angle, φ'                   | 2 to 13 %                       |
| Undrained shear strength, s <sub>u</sub>              | 13 to 40 %                      |
| Undrained strength ratio $(s_u/\sigma_v')$            | 5 to 15 %                       |
| Compression index, C <sub>c</sub>                     | 10 to 37 %                      |
| Preconsolidation stress, σ <sub>p</sub> '             | 10 to 35 %                      |
| Hydraulic conductivity of saturated clay, k           | 68 to 90 %                      |
| Hydraulic conductivity of partly-saturated clay, k    | 130 to 240 %                    |
| Coefficient of consolidation, cv                      | 33 to 68 %                      |
| Standard penetration blowcount, N                     | 15 to 45 %                      |
| Electric cone penetration test, q <sub>c</sub>        | 5 to 15 %                       |
| Mechanical cone penetration test, q <sub>c</sub>      | 15 to 37 %                      |
| Vane shear test undrained strength, s <sub>uVST</sub> | 10 to 20 %                      |

Source: Table 52 (Sabatini et al. 2002)

|           | ESU Name: |                 | ESU 1B - Medium Dense to Very Dense Coarse-Grained Fill |                 |             |                       |                      |                  |             |                 |  |  |
|-----------|-----------|-----------------|---|-----------------|-------------|-----------------------|----------------------|------------------|-------------|-----------------|--|--|
| Ï         | N         | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub>                         | %F              | PI<br>(Lab) | φ'<br>(high)<br>(deg) | φ'<br>(low)<br>(deg) | Sat. Unit Weight | Su<br>(psf) | Sr<br>(psf)     |  |  |
| GeoMean:  | 50        | 51              | 77  | 21              | -           | 44                    | 39                   | 130              | -           | -               |  |  |
| Average:  | 52        | 52              | 79  | 24              | -           | 44                    | 39                   | 130              | -           | -               |  |  |
| St. Dev.: | 16.0      | 10.3            | 19.2  | -               | -           | 1.1                   | 1.1                  | 0.0              | -           | -               |  |  |
| cov:      | 0.31      | 0.20            | 0.24  | -               | -           | 0.02                  | 0.03                 | 0.00             | -           | -               |  |  |
| Flevation | N         | N               | (N.)  | %E <sup>3</sup> | PI          | φ'<br>(high)          | φ'                   | Sat Unit Weight  | Su          | Sr <sup>4</sup> |  |  |

| W-218-20 236  |      |    | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub> | %F <sup>3</sup> | PI<br>(Lab) | φ'<br>(high)<br>(deg) | φ'<br>(low)<br>(deg) | Sat. Unit Weight | Su<br>(psf) | Sr <sup>4</sup><br>(psf) | USCS  | Explanation for Sample Removal |
|---------------|------|----|-----------------|---------------------------------|-----------------|-------------|-----------------------|----------------------|------------------|-------------|--------------------------|-------|--------------------------------|
| W 210 20 250  | 36.1 | 68 | 59              | 97                              | 9               | -           | 45                    | 40                   | #N/A             | -           | -                        | SW-SM |                                |
| R2B-11-17 215 | 15.2 | 36 | 40              | 59                              | 29              | -           | 43                    | 38                   | 130              | -           | -                        | SM    |                                |
| R2B-10-17 206 | 06.2 | 51 | 56              | 82                              | 35              | -           | 45                    | 40                   | 130              | -           | -                        | SM    |                                |
|               |      |    |                 |                                 |                 |             |                       |                      |                  |             |                          |       |                                |
|               |      |    |                 |                                 |                 |             |                       |                      |                  |             |                          |       |                                |
|               |      |    |                 |                                 |                 |             |                       |                      |                  |             |                          |       |                                |
|               |      |    |                 |                                 |                 |             |                       |                      |                  |             |                          |       |                                |
|               |      |    |                 |                                 |                 |             |                       |                      |                  |             |                          |       |                                |
|               |      |    |                 |                                 |                 |             |                       |                      |                  |             |                          |       |                                |
|               |      |    |                 |                                 |                 |             |                       |                      |                  |             |                          |       |                                |
|               |      |    |                 |                                 |                 |             |                       |                      |                  |             |                          |       |                                |
|               |      |    |                 |                                 |                 |             |                       |                      |                  |             |                          |       |                                |
|               |      |    |                 |                                 |                 |             |                       |                      |                  |             |                          |       |                                |
|               |      |    |                 |                                 |                 |             |                       |                      |                  |             |                          |       |                                |
|               |      |    | 1               |                                 |                 |             |                       |                      |                  |             |                          |       |                                |
|               |      |    | 1               |                                 |                 |             |                       |                      |                  |             |                          |       |                                |
|               |      |    |                 |                                 |                 |             |                       |                      |                  |             |                          |       |                                |
|               |      |    |                 |                                 |                 |             |                       |                      |                  |             |                          |       |                                |
|               |      |    |                 |                                 |                 |             |                       |                      |                  |             |                          |       |                                |
|               |      |    |                 |                                 |                 |             |                       |                      |                  |             |                          |       |                                |
|               |      |    |                 |                                 |                 |             |                       |                      |                  |             |                          |       |                                |
|               |      |    |                 |                                 |                 |             |                       |                      |                  |             |                          |       |                                |

- 1. Highlighted cells in yellow if shown represent samples that were removed as outliers.
- 2. Friction angle, unit weight, and corrected blow count values were correlated using specified methodology in the WOOD Geotechnical SPM. Where applicable, undrained Shear Strength of fine grained ESUs were determined using Equation 9 in the WOOD Geotechnical SPM.
- 3. Fines content percentages determined through laboratory testing are highlighted in orange if shown. Non-highlighted values have been estimated from sample field classifications, applying the fines content of a lab tested sample with similar properties, or using the average of two lab tested samples.
- 4. Where applicable, residual strength is calculated using the existing relationships and weighting scheme per the GDM (section 6-2.2) to determine residual strengths for samples with (N1)60cs less than or equal to 20. Per Kramer 2008, samples that triggered liquefaction (FoS<1.2) but also has an (N1)60cs>20, uses the residual strength value for a soil with (N1)60cs=20, effectively capping the residual strength calculation at (N1)60cs=20.

## 1. Check N160 COV is between 15 and 45%

| Selected Design N160:           | 77   |
|---------------------------------|------|
| Coefficient of Variation (COV): | 0.24 |

<sup>\* 15</sup> and 45% come from GEC 5 Sabatini (2002)

## 2. Check Phi' is between 2 to 13%

| (N <sub>1</sub> ) <sub>60</sub> (blows per foot) | Friction angle φ |
|--|------------------|
| (N <sub>1</sub> / <sub>60</sub> (blows per 100t) | (degrees)        |
| 2.5  | 25               |
| 2.5  | 30               |
| 4  | 27               |
| 4  | 32               |
| 10   | 30               |
| 10   | 35               |
| 30   | 35               |
| 30   | 40               |
| 50   | 38               |
| 50   | 43               |
| * Phi' Developed from WSDOT Correlation          |                  |

<sup>\* 2</sup> to 13% comes from GEC 5 Sabatini (2002)

| y = 4.236lr        | n(x) + 25.903 |    |                                    |    |  |
|--------------------|---------------|----|------------------------------------|----|--|
| R <sup>2</sup> = 0 | 0.9924        |    |                                    |    |  |
| <br>               |               |    | y = 4.236ln(<br>R <sup>2</sup> = 0 |    |  |
| <br>               |               |    |                                    |    |  |
|                    |               |    |                                    |    |  |
| 10                 | 20            | 30 | 40                                 | 50 |  |

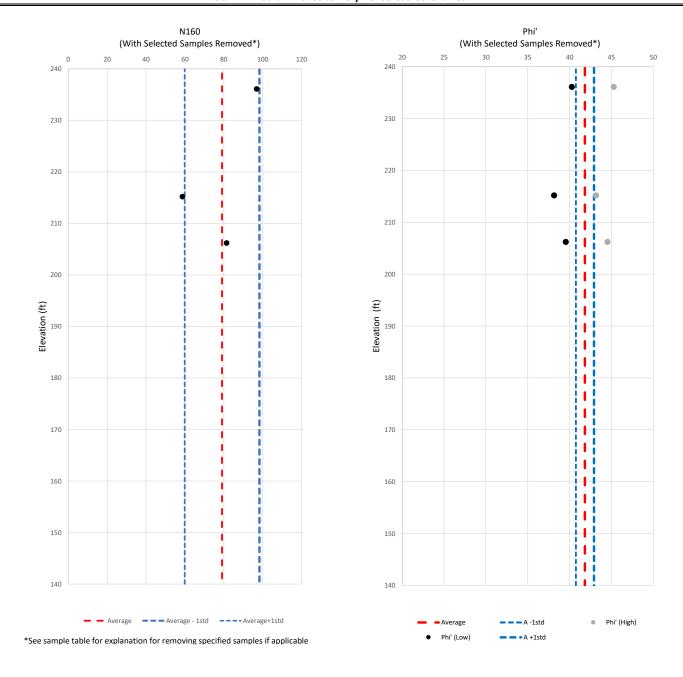
WSDOT GDM Table 5-1

|          | φ (high) | ф (low) | ф (avg) |
|----------|----------|---------|---------|
| GeoMean: | 44       | 39      | 42      |

| φ' COV |
|--------|
| 0.03   |

| Selected Design Phi' (deg): | 41                             |  |
|-----------------------------|--------------------------------|--|
| Notes on Selection:         | The estimated fine 30% fines). | es content is 21% (geomean). The friction angle is interpolated based on fines content (phi' (high) at 5% fines, and phi' (low) at |

| Pick Representative USCS:        | SM  | *Using Predominant USCS Classification  |
|----------------------------------|-----|---|
| Pick Representative Unit Weight: | 130 |   |
| Notes on Selection:              | •   | unit weights were correlated using CALTRANS Geotechnical Manual (2014), verified with applicable ranges presented in Codotu d in WOOD SPM. The geometric mean of the unit weights was rounded to the nearest 5pcf, as specified in WOOD SPM. Data set |



|           | ESU Name: |                 | ESU 2B - Medium Dense Sand/Gravel |                 |             |                       |                      |                  |             |                 |  |  |  |
|-----------|-----------|-----------------|-----------------------------------|-----------------|-------------|-----------------------|----------------------|------------------|-------------|-----------------|--|--|--|
| 1         | N         | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub>   | %F              | PI<br>(Lab) | φ'<br>(high)<br>(deg) | ф'<br>(low)<br>(deg) | Sat. Unit Weight | Su<br>(psf) | Sr<br>(psf)     |  |  |  |
| GeoMean:  | 16        | 19              | 23                                | 38              | 3           | 39                    | 34                   | 115              | -           | -               |  |  |  |
| Average:  | 17        | 20              | 24                                | 43              | 3           | 39                    | 34                   | 115              | -           | -               |  |  |  |
| St. Dev.: | 5.0       | 5.0             | 5.2                               | -               | -           | 1.1                   | 1.1                  | 3.8              | -           | -               |  |  |  |
| cov:      | 0.30      | 0.25            | 0.22                              | -               | -           | 0.03                  | 0.03                 | 0.03             | -           | -               |  |  |  |
| Elevation | N         | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub>   | %F <sup>3</sup> | PI<br>(Lab) | φ'<br>(high)          | ф'<br>(low)          | Sat. Unit Weight | Su<br>(nef) | Sr <sup>4</sup> |  |  |  |

| Boring   Elevation   N   N <sub>60</sub>   (N <sub>1</sub> ) <sub>60</sub>   %F <sup>3</sup>   P <sub>1</sub> (Lab)   (high) (deg) (deg) (deg) (deg)   Sat. Unit Weight (psf)   Sat. Unit Weight (psf)   USCS   Explanation (psf)   Sat. Unit Weight (psf)   Sat. Unit Weight (psf)   USCS   Explanation (psf)   Sat. Unit Weight (psf)   Sat. Unit Weight (psf)   USCS   Explanation (psf)   Sat. Unit Weight (psf)   Sat. Unit Weight (psf)   USCS   USCS | n for Sample Removal |
|---|----------------------|
| W-218-20 233.6 23 21 32 33 - 41 36 120 5M   |                      |
|   |                      |
| W-218-20 231.1 25 23 30 <mark>33</mark> - 40 35 120 5M  |                      |
| W-218-20 228.6 22 22 26 33 - 40 35 120 SM   |                      |
| R2B-11-17 212.2 11 13 19 29 - 38 33 115 SM  |                      |
| R2B-11-17 210.2 13 16 22 29 - 39 34 115 SM  |                      |
| R2B-11-17 207.2 17 21 25 29 - 40 35 120 SM  |                      |
| R2B-11-17 205.2 15 19 21 29 - 39 34 115 SM  |                      |
| R2B-11-17 200.2 18 25 25 97 - 40 35 110 ML  |                      |
| R2B-11-17 195.2 18 25 24 97 3 39 34 115 ML  |                      |
| R2B-10-17 203.2 16 19 26 35 - 40 35 120 SM  |                      |
| R2B-10-17 201.2 12 15 20 35 - 39 34 115 SM  |                      |
| R2B-10-17 198.2 8 10 12 70 - 36 31 110 ML   |                      |
| R2B-10-17 196.2 21 26 29 15 - 40 35 120 SM  |                      |
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- 1. Highlighted cells in yellow if shown represent samples that were removed as outliers.
- 2. Friction angle, unit weight, and corrected blow count values were correlated using specified methodology in the WOOD Geotechnical SPM. Where applicable, undrained Shear Strength of fine grained ESUs were determined using Equation 9 in the WOOD Geotechnical SPM.
- 3. Fines content percentages determined through laboratory testing are highlighted in orange if shown. Non-highlighted values have been estimated from sample field classifications, applying the fines content of a lab tested sample with similar properties, or using the average of two lab tested samples.
- 4. Where applicable, residual strength is calculated using the existing relationships and weighting scheme per the GDM (section 6-2.2) to determine residual strengths for samples with (N1)60cs less than or equal to 20. Per Kramer 2008, samples that triggered liquefaction (FoS<1.2) but also has an (N1)60cs>20, uses the residual strength value for a soil with (N1)60cs=20, effectively capping the residual strength calculation at (N1)60cs=20.

## 1. Check N160 COV is between 15 and 45%

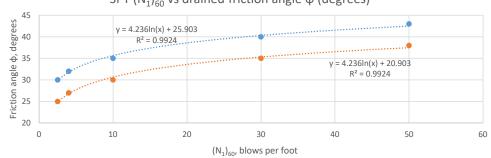
| Selected Design N160:           | 23   |
|---------------------------------|------|
| Coefficient of Variation (COV): | 0.22 |

<sup>\* 15</sup> and 45% come from GEC 5 Sabatini (2002)

#### 2. Check Phi' is between 2 to 13%

| (N <sub>1</sub> ) <sub>60</sub> (blows per foot) | Friction angle φ (degrees) |
|--|----------------------------|
| 2.5  | 25                         |
| 2.5  | 30                         |
| 4  | 27                         |
| 4  | 32                         |
| 10   | 30                         |
| 10   | 35                         |
| 30   | 35                         |
| 30   | 40                         |
| 50   | 38                         |
| 50   | 43                         |

SPT  $(N_1)_{60}$  vs drained friction angle  $\varphi$  (degrees)



|          | φ (high) | ф (low) | ф (avg) |
|----------|----------|---------|---------|
| GeoMean: | 39       | 34      | 37      |

| φ' cov |
|--------|
| 0.03   |

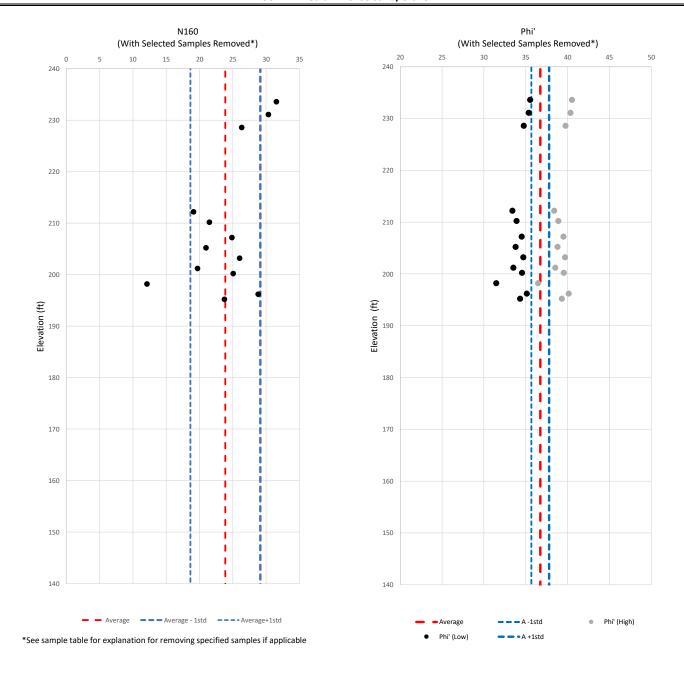
| Selected Design Phi' (deg): | 34                 |  |
|-----------------------------|--------------------|--|
| Notes on Selection:         | The estimated fine | es content is 38% (geomean). The high fines content supports the use of the lower bound of the friction angle range. |

| Pick Representative USCS:        | SM  | *Using Predominant USCS Classification  |
|----------------------------------|-----|---|
| Pick Representative Unit Weight: | 115 |   |
| Notes on Selection:              | •   | unit weights were correlated using CALTRANS Geotechnical Manual (2014), verified with applicable ranges presented in Codotu d in WOOD SPM. The geometric mean of the unit weights was rounded to the nearest 5pcf, as specified in WOOD SPM. Data set |

WSDOT GDM Table 5-1

<sup>\*</sup> Phi' Developed from WSDOT Correlation

<sup>\* 2</sup> to 13% comes from GEC 5 Sabatini (2002)



|           |           | ESU Name: |                 | ESU 4B - Dense to Very Dense Sand/Gravel |                 |             |                       |                      |                  |             |                          |      |                                |
|-----------|-----------|-----------|-----------------|--|-----------------|-------------|-----------------------|----------------------|------------------|-------------|--------------------------|------|--------------------------------|
|           | ,         | N         | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub>          | %F              | PI<br>(Lab) | ф'<br>(high)<br>(deg) | ф'<br>(low)<br>(deg) | Sat. Unit Weight | Su<br>(psf) | Sr<br>(psf)              |      |                                |
|           | GeoMean:  | 113       | 103             | 89                                       | 19              | 5           | 45                    | 40                   | 130              | -           | -                        |      |                                |
|           | Average:  | 175       | 107             | 92                                       | 22              | 6           | 45                    | 40                   | 130              | -           | -                        |      |                                |
|           | St. Dev.: | 255.0     | 28.9            | 24.5                                     | _               | _           | 1.2                   | 1.2                  | 1.5              | -           | -                        | 1    |                                |
|           | COV:      | 1.45      | 0.27            | 0.27                                     | -               | -           | 0.03                  | 0.03                 | 0.01             | -           | -                        | 1    |                                |
| Boring    | Elevation | N         | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub>          | %F <sup>3</sup> | PI<br>(Lab) | φ'<br>(high)<br>(deg) | φ'<br>(low)<br>(deg) | Sat. Unit Weight | Su<br>(psf) | Sr <sup>4</sup><br>(psf) | uscs | Explanation for Sample Removal |
| W-218-20  | 223.6     | 65        | 71              | 74                                       | 41              | -           | 44                    | 39                   | 130              | -           | -                        | SM   |                                |
| W-218-20  | 218.6     | 120       | 109             | 105                                      | 45              | 3           | 46                    | 41                   | 130              | -           | -                        | SM   |                                |
| W-218-20  | 213.6     | 120       | 109             | 99                                       | 36              | -           | 45                    | 40                   | 130              | -           | -                        | SM   |                                |
| W-218-20  | 208.6     | 120       | 115             | 99                                       | 36              | -           | 45                    | 40                   | 130              | -           | -                        | SM   |                                |
| W-218-20  | 203.6     | 120       | 115             | 97                                       | 5               |             | 45                    | 40                   | 135              | -           | -                        | SP   |                                |
| W-218-20  | 198.6     | 300       | 115             | 95                                       | 5               | -           | 45                    | 40                   | 135              | -           | -                        | SP   |                                |
| W-218-20  | 173.6     | 100       | 115             | 87                                       | 15              | -           | 45                    | 40                   | 130              | -           | -                        | SM   |                                |
| W-218-20  | 168.6     | 100       | 115             | 86                                       | 15              | -           | 45                    | 40                   | 130              | -           | -                        | SM   |                                |
| W-218-20  | 163.6     | 300       | 115             | 85                                       | 25              | -           | 45                    | 40                   | 130              | -           | -                        | GM   |                                |
| W-218-20  | 158.6     | 1200      | 115             | 84                                       | 25              | -           | 45                    | 40                   | 130              | -           | -                        | GM   |                                |
| R2B-11-17 | 190.2     | 150       | 147             | 137                                      | 22              | -           | 47                    | 42                   | 130              | -           | -                        | SC   |                                |
| R2B-11-17 | 185.2     | 100       | 147             | 133                                      | 22              | 9           | 47                    | 42                   | 130              | -           | -                        | SC   |                                |
| R2B-11-17 | 180.2     | 100       | 147             | 129                                      | 22              | -           | 46                    | 41                   | 130              | -           | -                        | SC   |                                |
| R2B-11-17 | 175.2     | 60        | 88              | 76                                       | 22              | -           | 44                    | 39                   | 130              | -           | -                        | SC   |                                |
| R2B-11-17 | 170.2     | 300       | 147             | 123                                      | 22              | -           | 46                    | 41                   | 130              | -           | -                        | SC   |                                |
| R2B-11-17 | 165.2     | 72        | 106             | 87                                       | 18              | -           | 45                    | 40                   | 130              | -           | -                        | SM   |                                |
| R2B-11-17 | 160.2     | 49        | 72              | 58                                       | 18              | -           | 43                    | 38                   | 130              | -           | -                        | SM   |                                |
| R2B-10-17 | 191.2     | 48        | 67              | 67                                       | 15              | -           | 44                    | 39                   | 130              | -           | -                        | SM   |                                |
| R2B-10-17 | 186.2     | 35        | 49              | 47                                       | 15              | -           | 42                    | 37                   | 130              | -           | -                        | SM   |                                |
| R2B-10-17 | 181.2     | 50        | 74              | 69                                       | 15              | -           | 44                    | 39                   | 130              | -           | -                        | SM   |                                |
|           |           |           |                 |  |                 |             |                       |                      |                  |             |                          |      |                                |
|           |           |           |                 |  |                 |             |                       |                      |                  |             |                          |      |                                |

- 1. Highlighted cells in yellow if shown represent samples that were removed as outliers.
- 2. Friction angle, unit weight, and corrected blow count values were correlated using specified methodology in the WOOD Geotechnical SPM. Where applicable, undrained Shear Strength of fine grained ESUs were determined using Equation 9 in the WOOD Geotechnical SPM.
- 3. Fines content percentages determined through laboratory testing are highlighted in orange if shown. Non-highlighted values have been estimated from sample field classifications, applying the fines content of a lab tested sample with similar properties, or using the average of two lab tested samples.
- 4. Where applicable, residual strength is calculated using the existing relationships and weighting scheme per the GDM (section 6-2.2) to determine residual strengths for samples with (N1)60cs less than or equal to 20. Per Kramer 2008, samples that triggered liquefaction (FoS<1.2) but also has an (N1)60cs>20, uses the residual strength value for a soil with (N1)60cs=20, effectively capping the residual strength calculation at (N1)60cs=20.

## 1. Check N160 COV is between 15 and 45%

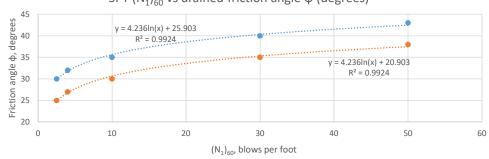
| Selected Design N160:           | 89   |
|---------------------------------|------|
| Coefficient of Variation (COV): | 0.27 |

<sup>\* 15</sup> and 45% come from GEC 5 Sabatini (2002)

## 2. Check Phi' is between 2 to 13%

| (N <sub>1</sub> ) <sub>60</sub> (blows per foot) | Friction angle φ<br>(degrees) |
|--|-------------------------------|
| 2.5  | 25                            |
| 2.5  | 30                            |
| 4  | 27                            |
| 4  | 32                            |
| 10   | 30                            |
| 10   | 35                            |
| 30   | 35                            |
| 30   | 40                            |
| 50   | 38                            |
| 50   | 43                            |

SPT  $(N_1)_{60}$  vs drained friction angle  $\varphi$  (degrees)



|          | φ (high) | ф (low) | ф (avg) |
|----------|----------|---------|---------|
| GeoMean: | 45       | 40      | 42      |

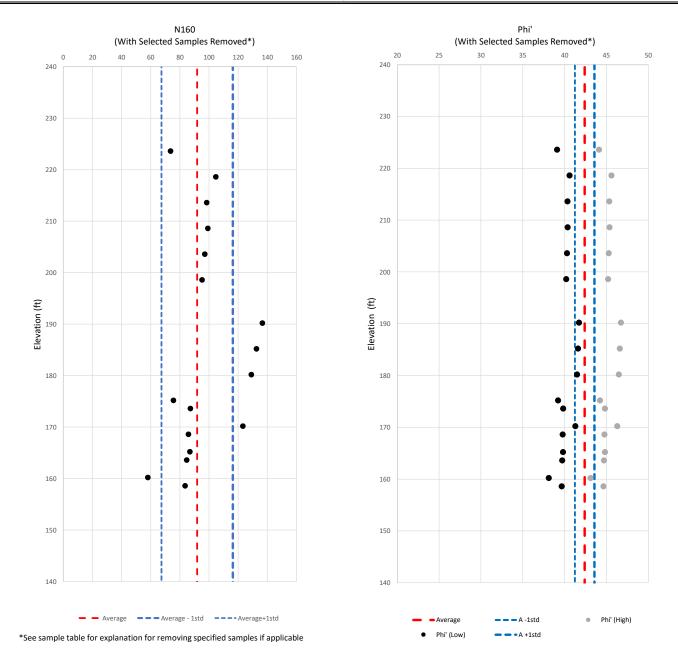
| Selected Design Phi' (deg): | 43                |  |
|-----------------------------|-------------------|--|
| Notes on Selection:         | The estimated geo | mean fines content is 19% (geomean). The friction angle is taken as the upper bound and capped at 43 degrees for glacially |
| Notes on Selection.         | consolidated mate | erial with fines content less than 70%   |

| Pick Representative USCS:        | SM  | *Using Predominant USCS Classification   |
|----------------------------------|-----|--|
| Pick Representative Unit Weight: | 130 |  |
| Notes on Selection:              | •   | unit weights were correlated using CALTRANS Geotechnical Manual (2014), verified with applicable ranges presented in Codotud in WOOD SPM. The geometric mean of the unit weights was rounded to the nearest 5pcf, as specified in WOOD SPM. Data set |

WSDOT GDM Table 5-1

<sup>\*</sup> Phi' Developed from WSDOT Correlation

<sup>\* 2</sup> to 13% comes from GEC 5 Sabatini (2002)



|          |           | ESU Name: |                 | ESU 5B - Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt |                 |             |                       |                      |  |             |                          |      |                                |
|----------|-----------|-----------|-----------------|--|-----------------|-------------|-----------------------|----------------------|--|-------------|--------------------------|------|--------------------------------|
|          | '         | N         | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub>                                    | %F              | PI<br>(Lab) | φ'<br>(high)<br>(deg) | ф'<br>(low)<br>(deg) | Sat. Unit Weight                                 | Su<br>(psf) | Sr<br>(psf)              |      |                                |
|          | GeoMean:  | 94        | 108             | 86   | 96              | 10          | 45                    | 40                   | 130  | -           | -                        |      |                                |
|          | Average:  | 95        | 109             | 86   | 97              | 11          | 45                    | 40                   | 130  | -           | -                        |      |                                |
|          | St. Dev.: | 10.5      | 12.1            | 9.4  | -               | -           | 0.5                   | 0.5                  | 0.0  | -           | -                        |      |                                |
|          | cov:      | 0.11      | 0.11            | 0.11   | -               | -           | 0.01                  | 0.01                 | 0.00   | -           | -                        |      |                                |
| Boring   | Elevation | N         | N <sub>60</sub> | (N <sub>1</sub> ) <sub>60</sub>                                    | %F <sup>3</sup> | PI<br>(Lab) | φ'<br>(high)<br>(deg) | ф'<br>(low)<br>(deg) | Sat. Unit Weight                                 | Su<br>(psf) | Sr <sup>4</sup><br>(psf) | USCS | Explanation for Sample Removal |
| W-218-20 | 193.6     | 100       | 115             | 93   | 98              | 8           | 45                    | 40                   | 130  | =           | -                        | ML   |                                |
| W-218-20 | 188.6     | 79        | 91              | 72   | 98              | -           | 44                    | 39                   | 130  | -           | -                        | ML   |                                |
| W-218-20 | 183.6     | 100       | 115             | 90   | 95              | 13          | 45                    | 40                   | 130  | -           | -                        | CL   |                                |
| W-218-20 | 178.6     | 100       | 115             | 89   | 95              | -           | 45                    | 40                   | 130  | -           | -                        | CL   |                                |
|          |           |           |                 |  |                 |             |                       |                      |  |             |                          |      |                                |
|          |           |           |                 |  |                 |             |                       |                      |  |             |                          |      |                                |
|          |           |           |                 |  |                 |             |                       |                      |  |             |                          |      |                                |
|          |           |           |                 |  |                 |             |                       |                      |  |             |                          |      |                                |
|          |           |           |                 |  |                 |             |                       |                      |  |             |                          |      |                                |
|          |           |           |                 |  |                 |             |                       |                      |  |             |                          |      |                                |
|          |           |           |                 |  |                 |             |                       |                      | +  |             |                          |      |                                |
|          |           |           |                 |  |                 |             |                       |                      |  |             |                          |      |                                |
|          |           |           |                 |  |                 |             |                       |                      |  |             |                          |      |                                |
|          |           |           |                 |  |                 |             |                       |                      |  |             |                          |      |                                |
|          |           |           |                 |  |                 |             |                       |                      |  |             |                          |      |                                |
|          |           |           |                 |  |                 |             |                       |                      | <del>                                     </del> |             |                          |      |                                |
|          | 1         |           | l               |  | l               | l           | l                     | l                    | 1  |             |                          |      |                                |

- 1. Highlighted cells in yellow if shown represent samples that were removed as outliers.
- 2. Friction angle, unit weight, and corrected blow count values were correlated using specified methodology in the WOOD Geotechnical SPM. Where applicable, undrained Shear Strength of fine grained ESUs were determined using Equation 9 in the WOOD Geotechnical SPM.
- 3. Fines content percentages determined through laboratory testing are highlighted in orange if shown. Non-highlighted values have been estimated from sample field classifications, applying the fines content of a lab tested sample with similar properties, or using the average of two lab tested samples.
- 4. Where applicable, residual strength is calculated using the existing relationships and weighting scheme per the GDM (section 6-2.2) to determine residual strengths for samples with (N1)60cs less than or equal to 20. Per Kramer 2008, samples that triggered liquefaction (FoS<1.2) but also has an (N1)60cs>20, uses the residual strength value for a soil with (N1)60cs=20, effectively capping the residual strength calculation at (N1)60cs=20.

## 1. Check N160 COV is between 15 and 45%

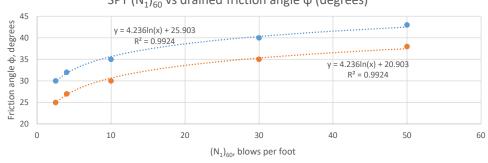
| Selected Design N160:           | 86   |
|---------------------------------|------|
| Coefficient of Variation (COV): | 0.11 |

<sup>\* 15</sup> and 45% come from GEC 5 Sabatini (2002)

#### 2. Check Phi' is between 2 to 13%

| (N <sub>1</sub> ) <sub>60</sub> (blows per foot) | Friction angle φ |
|--|------------------|
| (11760 (516115 per 1665)                         | (degrees)        |
| 2.5  | 25               |
| 2.5  | 30               |
| 4  | 27               |
| 4  | 32               |
| 10   | 30               |
| 10   | 35               |
| 30   | 35               |
| 30   | 40               |
| 50   | 38               |
| 50   | 43               |

WSDOT GDM Table 5-1 SPT  $(N_1)_{60}$  vs drained friction angle  $\phi$  (degrees)



|          | φ (high) | ф (low) | ф (avg) |
|----------|----------|---------|---------|
| GeoMean: | 45       | 40      | 42      |

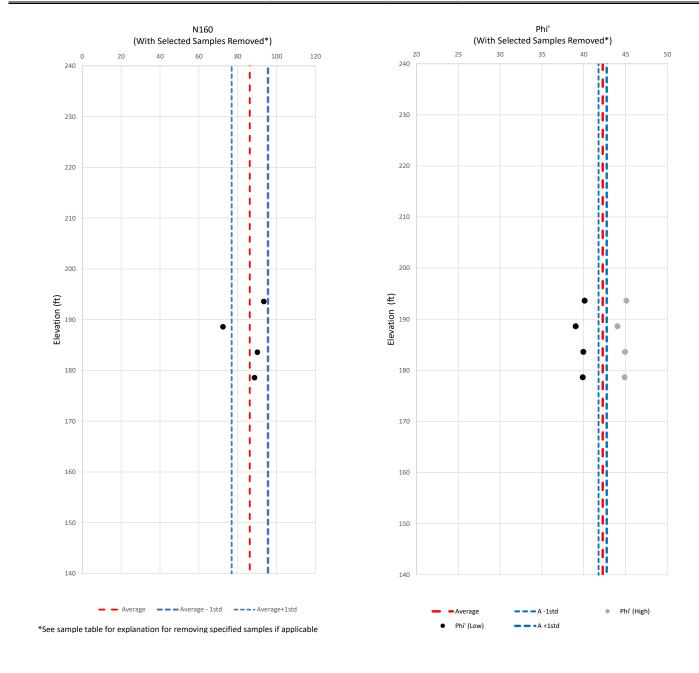
| φ' cov |  |
|--------|--|
| 0.01   |  |

| Selected Design Phi' (deg): | 42                 |   |
|-----------------------------|--------------------|---|
| Notes on Selection:         | The estimated ged  | omean fines content is 96% (geomean). The friction angle is taken as the average of upper bound and lower bound and capped at |
|                             | 43 degrees for gla | cially consolidated material with fines content more than 70%.  |

| Pick Representative USCS:        | CL/ML  | CL/ML *Using Predominant USCS Classification |  |
|----------------------------------|--|--|--|
| Pick Representative Unit Weight: | 130  |  |  |
| Notes on Selection:              | Individual sample unit weights were correlated using CALTRANS Geotechnical Manual (2014), verified with applicable ranges presented in Codotu (2001), as specified in WOOD SPM. The geometric mean of the unit weights was rounded to the nearest 5pcf, as specified in WOOD SPM. Data set COV was 0%. |  |  |

<sup>\*</sup> Phi' Developed from WSDOT Correlation

<sup>\* 2</sup> to 13% comes from GEC 5 Sabatini (2002)



One of the primary shortcomings of the Mononobe-Okabe method is that it cannot consider the effect of cohesion in the backfill on the seismic active earth pressure. Even relatively small amounts of cohesion in the backfill can significantly reduce the seismic active earth pressure. Sources of cohesion in backfill soils include both true cohesion due to inter-particle bonding and apparent cohesion due to capillary forces in the backfill. The influence of cohesion on the seismic active earth pressure is a function of the normalizing parameter  $c\gamma/H$ , where  $\gamma$  is the unit weight of the backfill soil. Figure 11-14 presents a plot of the seismic active earth pressure coefficient,  $k_{AE}$ , as a function of the normalizing parameter  $c/\gamma H$  and the seismic coefficient,  $k_h$ , for a friction angle of 35° and for a uniform level backfill. An Appendix in NCHRP Report 611 presents additional plots for friction angles of 30° and 40°.

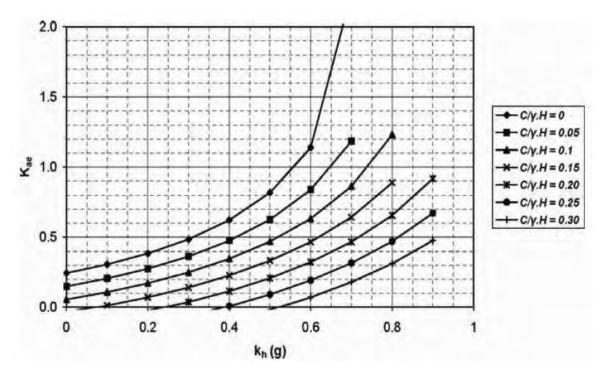


Figure 11-14 Effect of cohesion on the seismic active earth pressure coefficient for  $\phi = 35^{\circ}$  (NCHRP, 2008)

NCHRP Report 611 provides recommendations for the maximum amount of apparent cohesion that should be assumed for backfill soil as a function of the fines content of the soil. These recommendations are presented in Table 11-2.

| <b>TABLE 11-2</b> | MAXIMUM AMOUNT OF APPARENT COHESION THAT SHOULD BE |
|-------------------|--|
|                   | ASSUMED FOR BACKFILL SOILS (NCHRP, 2008)           |

% (by weight) passing #200 sieve maximum apparent cohesion

| 5 - 15  | 50 psf  |                   |
|---------|---------|-------------------|
| 15 - 25 | 100 psf | ← ESU 1B (FC=20%) |
| 25-50   | 200 psf | ←—ESU 2B (FC=39%) |

# 11.3.3 Log Spiral Earth Pressure Theory

The Mononobe-Okabe and Trial Wedge methods for calculating earth pressure assume that the failure surface in the backfill is planar. It has been long recognized that when there is a significant soil-wall friction angle, the assumption of the planar failure surface is incorrect. Instead, in a homogeneous soil a logarithmic surface gives the critical values for the active and passive earth pressure in a limit equilibrium analysis. Note, however, that when there is no wall friction the logarithmic surface degenerates to a planar surface. As illustrated in Figure 11-15, or the active case the difference between the critical log spiral surface and the critical planar surface is small enough that it can be ignored, even when there is wall friction. However, as illustrated in Figure 11-15, the critical log spiral surface for the passive case differs significantly from the critical planar surface when the wall friction angle is more than one-third the value of the backfill friction angle. In these cases it is essential to consider the logarithmic surface: failure to do so can result in an unconservative assessment of the seismic passive earth pressure.

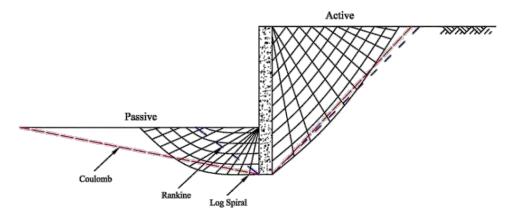


Figure 11-15 Critical Log Spiral Surfaces Compared to Planar Critical Surfaces

The log spiral method can be used to evaluate seismic passive earth pressures accounting for backfill friction and cohesion, soil-wall interface friction angle, and backslope angle. Shamsabadi et al. (2007) describe the general method that can be used to do this. The soil-wall interface friction angle is a key parameter in this approach. The soil-wall interface friction angle for static loading is often assumed to

The coefficient of consolidation,  $c_{\nu_{t}}$ , should be determined from the results of onedimensional consolidation tests. The variability in laboratory determination of  $\emph{c}_{\emph{V}}$  results should be considered in the final selection of the value of  $c_V$  to be used for design.

Where evaluation of elastic settlement is critical to the design of the foundation or selection of the foundation type, in-situ methods such as PMT or *DMT* for evaluating the modulus of the stratum should be used.

ESU 2B Medium Dense Sand/ Gravel Es = 4.6 ksi = 660 ksfPoisson Ratio = 0.33

A profile of  $\sigma_{\sigma'}$ , or OCR =  $\sigma_{\sigma'}/\sigma_{\sigma'}$ , with depth should be developed for the site for design applications where the stress history could have a significant impact on the design properties selected and the performance of the foundation. As with consolidation properties, an upper and lower bound profile should be developed based on laboratory tests and plotted with a profile based on particular in-situ test(s), if used. It is particularly important to accurately compute preconsolidation stress values for relatively shallow depths where in-situ effective stresses are low. An underestimation of the preconsolidation stress at shallow depths will result in overly conservative estimates of settlement for shallow soil layers.

Due to the numerous simplifying assumptions associated with conventional consolidation theory, on which the coefficient of consolidation is based, it is unlikely that even the best estimates of  $c_{\nu}$  from high-quality laboratory tests will result in predictions of time rate of settlement in the field that are significantly better than a prediction within one order of magnitude. In general, the in-situ value of  $c_{
u}$  is larger than the value measured in the laboratory test. Therefore, a rational approach is to select average, upper, and lower bound values for the appropriate stress range of concern for the design application. These values should be compared to values obtained from previous work performed in the same soil deposit. Under the best-case conditions, these values should be compared to values computed from measurements of excess pore pressures or settlement rates during construction of other structures.

 $\ensuremath{\textit{CPTu}}$  tests in which the pore pressure dissipation rate is measured may be used to estimate the field coefficient of consolidation.

For preliminary analyses or where accurate prediction of settlement is not critical. values obtained from correlations to index properties presented in Sabatini et al. (2002)

For preliminary design or for final design where the prediction of deformation is not critical to structure performance, i.e., the structure design can tolerate the potential inaccuracies inherent in the correlations. The elastic properties  $(E_{sr}, \nu)$  of a soil may be estimated from empirical relationships presented in Table C10.4.6.3-1.

The specific definition of  $E_s$  is not always consistent for the various correlations and methods of in-situ measurement. See Sabatini et al. (2002) for additional details regarding the definition and determination of  $E_s$ .

An alternative method of evaluating the equivalent elastic modulus using measured shear wave velocities is presented in Sabatini et al. (2002).

Table C10.4.6.3-1—Elastic Constants of Various Soils (modified after U.S. Denartment of the Navv. 1982; Bowles, 1988)

| Department of the                | Navy, 1982; Bowles, 1988)                            |                              |
|----------------------------------|--|------------------------------|
| Soil Type                        | Typical Range of Young's Modulus Values, $E_s$ (ksi) | Poisson's Ratio, $\nu$ (dim) |
| Clay:                            |  |                              |
| Soft sensitive                   |  |                              |
| Medium stiff to stiff            | 0.347–2.08   | 0.4–0.5 (undrained)          |
|                                  | 2.08-6.94  |                              |
| Very stiff                       | 6.94–13.89   |                              |
| Loess                            | 2.08-8.33  | 0.1-0.3                      |
| Silt                             | 0.278–2.78   | 0.3-0.35                     |
| Fine Sand:                       |  |                              |
| Loose                            | 1.11–1.67  | 0.25                         |
| Medium dense                     | 1.67–2.78  |                              |
| Dense                            | 2.78–4.17  |                              |
| Sand:                            |  |                              |
| Loose                            | 1.39–4.17  | 0.20-0.36                    |
| Medium dense                     | 4.17-6.94  | $\cdots$                     |
| Dense                            | 6.94–11.11   | 0.30-0.40                    |
| Gravel:                          |  |                              |
| Loose                            | 4.17–11.11   | 0.20-0.35                    |
| Medium dense                     | 11.11–13.89  |                              |
| Dense                            | 13.89–27.78  | 0.30-0.40                    |
| Estimating E <sub>s</sub> from S | GPT N Value  |                              |
|                                  | $E_s$ (ksi)  |                              |
| Silts, sandy silts, slig         | 0.056 N <sub>160</sub>                               |                              |
| Clean fine to medium             | 0.097 M <sub>160</sub>                               |                              |
| Coarse sands and sa              | 0.139 <i>N</i> 1 <sub>60</sub>                       |                              |
| Sandy gravel and gra             | 0.167 <i>N</i> 1 <sub>60</sub>                       |                              |
| Estimating E <sub>s</sub> from q | c (static cone resistance)                           |                              |
| Sandy soils                      | 0.028 <i>qc</i>                                      |                              |
|                                  |  |                              |

The modulus of elasticity for normally consolidated granular soils tends to increase with depth. An alternative method of defining the soil modulus for granular soils is to assume that it increases linearly with depth starting at zero at the ground surface in accordance with the following equation:

$$E_s = nh \times z \tag{C10.4.6.3-1}$$

where:

# Appendix F.3 - Wall 05.85L-B Design Calculations

## **AASHTO Average Blowcount in Upper 100 feet**

|          | Α         | В              | С               | D                              | E                | F      | G           | Н | I           | J                 | K                  | L               | М              | N                 | 0                             | Р          |
|----------|-----------|----------------|-----------------|--------------------------------|------------------|--------|-------------|---|-------------|-------------------|--------------------|-----------------|----------------|-------------------|-------------------------------|------------|
| 30       |           | Soil Profile T | ype             | v <sub>s</sub> (f <sub>l</sub> | os)              |        | N           |   | •           | •                 | •                  |                 | •              | •                 | •                             |            |
| 31       |           | S <sub>A</sub> |                 | >50                            | 5000             |        |             |   | Note:       |                   |                    |                 |                |                   |                               |            |
| 32       |           | S <sub>B</sub> |                 | 2,500 to                       | 5,000            |        | N/A         |   |             | ercent (Energy is | input BC/60). T    | This spreadshee | et approximate | s the layer thick | kness based on a fi           | unction w  |
| 33       |           | Sc             |                 | 1,200 to                       | 2,500            |        | >50         |   |             |                   |                    |                 |                |                   | input their own laye          | er thickne |
| 34       |           | S <sub>D</sub> |                 | 600 to                         | 1,200            | 15     | 5≤N≤50      |   |             | er extends at 7.5 |                    |                 |                |                   | ckness).<br>nd Transportation | Official   |
| 35       |           | S <sub>E</sub> |                 | <60                            | 00               |        | <15         |   | (AASHTO).   | t based on Sect   | 1011 3. 10.3. 1 01 | American Ass    | ociation of 5  | ate nigilway a    | nu rransportation             | Officials  |
| 36       |           |                | Table 3.10.3.1- | 1—Site Class Det               | finitions from A | ASHTO  |             |   | ( = := := ) |                   |                    |                 |                |                   |                               |            |
| 37       |           |                |                 |                                |                  |        |             |   |             |                   |                    |                 |                |                   |                               |            |
| 38       | Name      |                |                 |                                | Nave             | Soil P | rofile Type |   |             |                   |                    |                 |                |                   |                               |            |
|          | W-218-20  |                |                 |                                | 74.1             |        | С           |   |             |                   |                    |                 |                |                   |                               |            |
|          | R2B-11-17 |                |                 |                                | 51.7             |        | С           |   |             |                   |                    |                 |                |                   |                               |            |
|          | R2B-10-17 | •              |                 |                                | 55.2             |        | С           |   |             |                   |                    |                 |                |                   |                               |            |
| 42       |           |                |                 |                                |                  |        |             |   |             |                   |                    |                 |                |                   |                               |            |
| 43       |           |                |                 |                                |                  |        |             | _ |             |                   |                    |                 |                |                   |                               |            |
| 44<br>45 |           |                |                 |                                |                  |        |             |   |             |                   |                    |                 |                |                   |                               |            |
| 46       |           |                |                 |                                | +                |        |             | _ |             |                   |                    |                 |                |                   |                               |            |
| 47       |           |                |                 |                                | 1                |        |             | - |             |                   |                    |                 |                |                   |                               |            |
| 48       |           |                |                 |                                |                  |        |             |   |             |                   |                    |                 |                |                   |                               |            |
| 49       |           |                |                 |                                |                  |        |             |   |             |                   |                    |                 |                |                   |                               |            |
| 50       |           |                |                 |                                |                  |        |             |   |             |                   |                    |                 |                |                   |                               |            |
| 51       |           |                |                 |                                |                  |        |             |   |             |                   |                    |                 |                |                   |                               |            |
| 52       |           |                |                 |                                |                  |        |             |   |             |                   |                    |                 |                |                   |                               |            |

## **AASHTO Average Blowcount in Upper 100 feet**

|    | Α     | В                  | С   | D   | Е                    | F                              | G                                    | Н                | I     | J                  | K   | L                               | М       | N           | 0              | Р    |
|----|-------|--------------------|---|---|----------------------|--------------------------------|--------------------------------------|------------------|-------|--------------------|---|---------------------------------|---------|-------------|----------------|------|
| 1  |       |                    |   | W-2   | 218-20               |                                |                                      |                  |       | •                  | •   | R2B                             | -11-17  |             |                |      |
| 2  | Depth | Field<br>Blowcount | Energy<br>Corrected<br>Blowcount,<br>N <sub>i</sub> | Layer<br>thickness d <sub>i</sub><br>(feet) | Sum(d <sub>i</sub> ) | d <sub>i</sub> /N <sub>i</sub> | Sum(d <sub>i</sub> /N <sub>i</sub> ) | N <sub>ave</sub> | Depth | Field<br>Blowcount | Energy<br>Corrected<br>Blowcount,<br>N <sub>i</sub> | Layer<br>thickness<br>di (feet) | Sum(di) | di/Ni       | Sum(di/Ni)     | Nave |
| 3  | 2.5   | 68                 | 68  | 3.75  | 100                  | 0.06                           | 1.3495                               | 74.1             | 4     | 36                 | 53  | 5.5                             | 100     | 0.10        | 1.9            | 51.7 |
| 4  | 5     | 23                 | 23  | 2.5   |                      | 0.11                           |                                      |                  | 7     | 11                 | 16  | 2.5                             |         | 0.15        |                |      |
| 5  | 7.5   | 25                 | 25  | 2.5   |                      | 0.10                           |                                      |                  | 9     | 13                 | 19  | 2.5                             |         | 0.13        |                |      |
| 6  | 10    | 22                 | 22  | 3.75  |                      | 0.17                           |                                      |                  | 12    | 17                 | 25  | 2.5                             |         | 0.10        |                |      |
| 7  | 15    | 65                 | 65  | 5   |                      | 0.08                           | Driving Energy                       | 60%              | 14    | 15                 | 22  | 3.5                             |         | 0.16        | Driving Energy | 88%  |
| 8  | 20    | 120                | 100   | 5   |                      | 0.05                           |                                      |                  | 19    | 18                 | 27  | 5                               |         | 0.19        |                |      |
| 9  | 25    | 120                | 100   | 5   |                      | 0.05                           |                                      |                  | 24    | 18                 | 27  | 5                               |         | 0.19        |                |      |
| 10 | 30    | 120                | 100   | 5   |                      | 0.05                           |                                      |                  | 29    | 150                | 100   | 5                               |         | 0.05        |                |      |
| 11 | 35    | 120                | 100   | 5   |                      | 0.05                           |                                      |                  | 34    | 100                | 100   | 5                               |         | 0.05        |                |      |
| 12 | 40    | 300                | 100   | 5   |                      | 0.05                           |                                      |                  | 39    | 100                | 100   | 5                               |         | 0.05        |                |      |
| 13 | 45    | 100                | 100   | 5   |                      | 0.05                           |                                      |                  | 44    | 60                 | 88  | 5                               |         | 0.06        |                |      |
| 14 | 50    | 79                 | 79  | 5   |                      | 0.06                           |                                      |                  | 49    | 300                | 100   | 5                               |         | 0.05        |                |      |
| 15 | 55    | 100                | 100   | 5   |                      | 0.05                           |                                      |                  | 54    | 72                 | 100   | 5                               |         | 0.05        |                |      |
| 16 | 60    | 100                | 100   | 5   |                      | 0.05                           |                                      |                  | 59    | 49                 | 72  | 43.5                            |         | 0.60        |                |      |
| 17 | 65    | 100                | 100   | 5   |                      | 0.05                           |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |
| 18 | 70    | 100                | 100   | 5   |                      | 0.05                           |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |
| 19 | 75    | 300                | 100   | 5   |                      | 0.05                           |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |
| 20 | 80    | 1200               | 100   | 22.5  |                      | 0.23                           |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |
| 21 |       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |
| 22 |       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |
| 23 |       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |
| 24 |       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |
| 25 |       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |
| 26 |       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |
| 27 |       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |
| 28 |       |                    |   |   |                      | End of Data                    |                                      |                  |       |                    |   |                                 |         | End of Data |                |      |

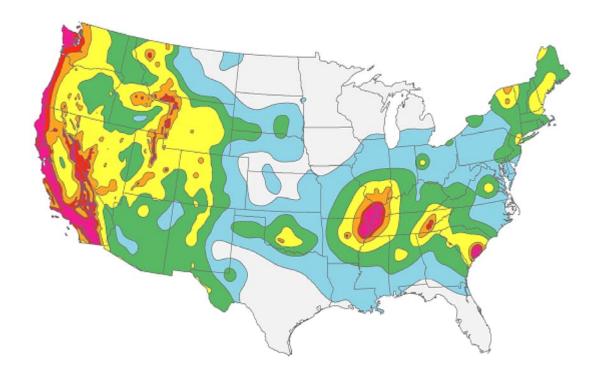
## **AASHTO Average Blowcount in Upper 100 feet**

| The content of the |    | Q     | R  | S                    | Т         | U       | V           | W              | Х    | Υ |   | Z | AA | AB | AC | AD | AE | AF |
|---|----|-------|----|----------------------|-----------|---------|-------------|----------------|------|---|---|---|----|----|----|----|----|----|
| Corrected Blowcount,   Thickness   Sum(di)   Sum(diNi)   Nave   | 1  |       | •  | •                    | R2B-      | -10-17  |             |                |      |   | • |   | •  |    |    | •  |    |    |
| 3 4 51 75 5.5 100 0.07 1.8113 55.2 4 7 16 24 2.5 5 9 12 18 2.5 6 12 8 12 2.6 7 14 21 31 3.5 8 19 48 71 5 9 24 35 52 5 10 0.07 10 29 50 74 73.5 11   | 2  | Depth |    | Corrected Blowcount, | thickness | Sum(di) | di/Ni       | Sum(di/Ni)     | Nave |   |   |   |    |    |    |    |    |    |
| 4         7         16         24         2.5         0.11         0.14         5         9         12         18         2.5         0.21         0.14 <td< td=""><td></td><td></td><td>51</td><td></td><td></td><td></td><td></td><td>` '</td><td></td><td>1</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>  |    |       | 51 |                      |           |         |             | ` '            |      | 1 |   |   |    |    |    |    |    |    |
| 5         9         12         18         2.5         0.14         0.21   |    | 7     |    |                      |           |         |             |                |      | 1 |   |   |    |    |    |    |    |    |
| 7   | 5  | 9     | 12 |                      |           |         | 0.14        |                |      |   |   |   |    |    |    |    |    |    |
| 8 19 48 71 5 0.07 9 24 35 52 5 0.10 10 29 50 74 73.5 1.00 End of Data   | 6  | 12    | 8  | 12                   | 2.5       |         | 0.21        |                |      |   |   |   |    |    |    |    |    |    |
| 9   | 7  | 14    | 21 | 31                   | 3.5       |         | 0.11        | Driving Energy | 88%  | 1 |   |   |    |    |    |    |    |    |
| 10  | 8  | 19    | 48 | 71                   | 5         |         | 0.07        |                |      |   |   |   |    |    |    |    |    |    |
| End of Data   |    | 24    | 35 | 52                   | 5         |         | 0.10        |                |      |   |   |   |    |    |    |    |    |    |
| End of Data   |    | 29    | 50 | 74                   | 73.5      |         | 1.00        |                |      |   |   |   |    |    |    |    |    |    |
| End of Data   |    |       |    |                      |           |         | End of Data |                |      |   |   |   |    |    |    |    |    |    |
| 14  |    |       |    |                      |           |         |             |                |      |   |   |   |    |    |    |    |    |    |
| End of Data   |    |       |    |                      |           |         |             |                |      |   |   |   |    |    |    |    |    |    |
| End of Data   |    |       |    |                      |           |         |             |                |      |   |   |   |    |    |    |    |    |    |
| 17       End of Data         18       End of Data         19       End of Data         20       End of Data         21       End of Data         22       End of Data         23       End of Data         24       End of Data         25       End of Data         26       End of Data         27       End of Data  |    |       |    |                      |           |         |             |                |      |   |   |   |    |    |    |    |    |    |
| 18  |    |       |    |                      |           |         |             |                |      |   |   |   |    |    |    |    |    |    |
| 19  |    |       |    |                      |           |         |             |                |      |   |   |   |    |    |    |    |    |    |
| End of Data   |    |       |    |                      |           |         |             |                |      |   |   |   |    |    |    |    |    |    |
| End of Data   |    |       |    |                      |           |         |             |                |      |   |   |   |    |    |    |    |    |    |
| 22       End of Data         23       End of Data         24       End of Data         25       End of Data         26       End of Data         27       End of Data         End of Data       End of Data         End of Data       End of Data   | 20 |       |    |                      |           |         |             |                |      |   |   |   |    |    |    |    |    |    |
| 23         End of Data           24         End of Data           25         End of Data           26         End of Data           27         End of Data           End of Data         End of Data  | 21 |       |    |                      |           |         |             |                |      |   |   |   |    |    |    |    |    |    |
| 25         End of Data           26         End of Data           27         End of Data           End of Data         End of Data  | 22 |       |    |                      |           |         |             |                |      |   |   |   |    |    |    |    |    |    |
| 25         End of Data           26         End of Data           27         End of Data           End of Data         End of Data  | 24 |       |    |                      |           |         |             |                |      |   |   |   |    |    |    |    |    |    |
| 26 End of Data 27 End of Data   | 25 |       |    | 1                    |           |         |             |                |      |   |   |   |    |    |    |    |    |    |
| 27 End of Data  | 26 |       |    | 1                    |           |         |             |                |      |   |   |   |    |    |    |    |    |    |
| End of Balla  | 27 |       |    |                      |           |         |             |                |      |   |   |   |    |    |    |    |    |    |
| 28 End of Data  | 28 |       |    |                      |           |         |             |                |      |   |   |   |    |    |    |    |    |    |
| 29  |    |       | I  | L                    | l         | l       |             |                |      | J |   |   |    |    |    |    |    |    |

# $\textbf{BEToolbox}^{^{\text{TM}}}$

Spectra
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Version 6.0.0.6 BETA - Built on Jan 7 2021



## 05.85L-B

WSDOT Bridge Design Manual 2014 Seismic Hazard Map, 7% probability of exceedance in 75 years

Site Coordinates (Latitude,Longitude): 47.5109° N, 122.198° W Site Soil Classification: Site Class C - Very Dense Soil and Soft Rock

Seismic hazard maps are for sites at the boundary of Site Classes B and C, which is  $\overline{v}_s = 2500$  ft/s (760 m/s). Adjustments for

other Site Classes are made as needed.

| Period<br>(sec) | Sa<br>(g) |  |
|-----------------|-----------|--|
| 0.0             | 0.433     | PGA - Site Class B/C Boundary            |
| 0.2             | 0.987     | S <sub>s</sub> - Site Class B/C Boundary |
| 1.0             | 0.283     | S <sub>1</sub> - Site Class B/C Boundary |

Values of Site Coefficient,  $F_{pqa}$ , for Peak Ground Acceleration

| Site Class | Мар       | ped Peak G | round Acc | eleration Co | efficient (F | PGA)      |
|------------|-----------|------------|-----------|--------------|--------------|-----------|
|            | PGA≤ 0.10 | PGA= 0.20  | PGA= 0.30 | PGA= 0.40    | PGA= 0.50    | PGA≥ 0.60 |
| Α          | 0.8       | 0.8        | 0.8       | 0.8          | 0.8          | 0.8       |
| В          | 0.9       | 0.9        | 0.9       | 0.9          | 0.9          | 0.9       |
| С          | 1.3       | 1.2        | 1.2       | 1.2          | 1.2          | 1.2       |
| D          | 1.6       | 1.4        | 1.3       | 1.2          | 1.1          | 1.1       |
| E          | 2.4       | 1.9        | 1.6       | 1.4          | 1.2          | 1.1       |

For Site Class C, F<sub>pga</sub> = 1.200

Values for Site Coefficient,  $\rm F_a$ , for 0.2 sec Period Spectral Acceleration

| Site Class | Mapped S              | Mapped Spectral Acceleration Coefficient at Period 0.2 sec (S <sub>s</sub> ) |                       |                       |                       |                       |  |  |  |  |  |  |
|------------|-----------------------|--|-----------------------|-----------------------|-----------------------|-----------------------|--|--|--|--|--|--|
|            | S <sub>s</sub> ≤ 0.25 | S <sub>s</sub> = 0.50  | S <sub>s</sub> = 0.75 | S <sub>s</sub> = 1.00 | S <sub>s</sub> = 1.25 | S <sub>s</sub> ≥ 1.50 |  |  |  |  |  |  |
| Α          | 0.8                   | 0.8  | 0.8                   | 0.8                   | 8.0                   | 0.8                   |  |  |  |  |  |  |
| В          | 0.9                   | 0.9  | 0.9                   | 0.9                   | 0.9                   | 0.9                   |  |  |  |  |  |  |
| С          | 1.3                   | 1.3  | 1.2                   | 1.2                   | 1.2                   | 1.2                   |  |  |  |  |  |  |
| D          | 1.6                   | 1.4  | 1.2                   | 1.1                   | 1.0                   | 1.0                   |  |  |  |  |  |  |
| Е          | 2.4                   | 1.7  | 1.3                   | 1.0                   | 0.9                   | 0.9                   |  |  |  |  |  |  |

For Site Class C,  $F_a = 1.200$ 

Values of Site Coefficient, F<sub>v</sub>, for 1.0 sec Period Spectral Acceleration

| Site Class | Mapped S             | Mapped Spectral Acceleration Coefficient at Period 1.0 sec (S <sub>1</sub> ) |                      |                      |                      |                      |  |  |  |  |  |  |
|------------|----------------------|--|----------------------|----------------------|----------------------|----------------------|--|--|--|--|--|--|
|            | S <sub>1</sub> ≤ 0.1 | S <sub>1</sub> = 0.2   | S <sub>1</sub> = 0.3 | S <sub>1</sub> = 0.4 | S <sub>1</sub> = 0.5 | S <sub>1</sub> ≥ 0.6 |  |  |  |  |  |  |
| Α          | 0.8                  | 0.8  | 0.8                  | 0.8                  | 0.8                  | 0.8                  |  |  |  |  |  |  |
| В          | 0.8                  | 0.8  | 0.8                  | 0.8                  | 8.0                  | 0.8                  |  |  |  |  |  |  |
| С          | 1.5                  | 1.5  | 1.5                  | 1.5                  | 1.5                  | 1.4                  |  |  |  |  |  |  |
| D          | 2.4                  | 2.2  | 2.0                  | 1.9                  | 1.8                  | 1.7                  |  |  |  |  |  |  |
| Е          | 4.2                  | 3.3  | 2.8                  | 2.4                  | 2.2                  | 2.0                  |  |  |  |  |  |  |

For Site Class C,  $F_v = 1.500$ 

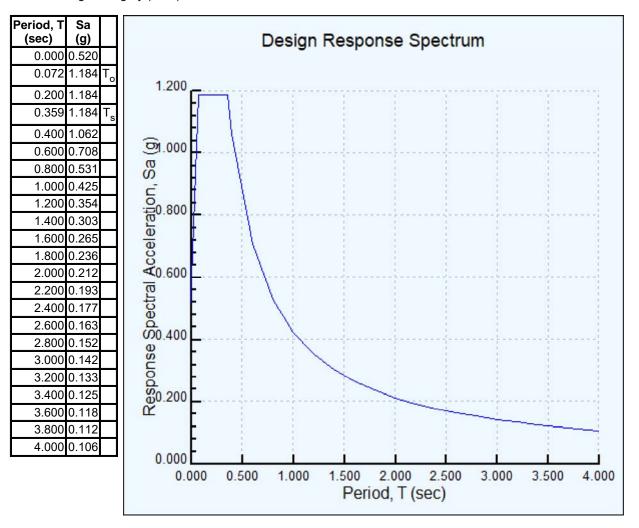
$$\begin{split} & A_{\rm S} = F_{\rm pga} \; {\rm PGA} = (\; 1.200)(\; 0.433g) = 0.520g \\ & S_{\rm DS} = F_{\rm a} \; S_{\rm s} = (\; 1.200)(\; 0.987g) = 1.184g \\ & S_{\rm D1} = F_{\rm v} \; S_{\rm 1} = (\; 1.500)(\; 0.283g) = 0.425g \\ & T_{\rm o} = 0.2T_{\rm s} = (0.2)(\; 0.359) = 0.072 \; {\rm sec} \\ & T_{\rm s} = S_{\rm D1}/S_{\rm DS} = (\; 0.425)/(\; 1.184) = 0.359 \; {\rm sec} \end{split}$$

# 05.85L-B

Partitions for Seismic Design Categories A, B, C, and D

| S <sub>D1</sub>               | SDC |
|-------------------------------|-----|
| S <sub>D1</sub> < 0.15        | Α   |
| 0.15 ≤ S <sub>D1</sub> < 0.30 | В   |
| $0.30 \le S_{D1} < 0.50$      | С   |
| 0.50 ≤ S <sub>D1</sub>        | D   |

Seismic Design Category (SDC) = C



Project: <u>405 Renton to Bellveue</u> By: <u>YT</u> Checked By: <u>TB</u>

#### 

# Calculating Wall Seismic Acceleration Considering Wave Scattering for Wall 05.85L-B

Per National Cooperative Highway Research Program (NCHRP) Report 611 the site class adjusted peak ground acceleration (PGA), As, can be corrected to account for vertical variations in the average ground acceleration observed behind tall retaining walls and/ or slopes greater than 20-feet in height by applying a wall height acceleration reduction factor (or  $\alpha$  coefficient) to the As.

| Site | C | ลรร | D                          |
|------|---|-----|----------------------------|
| JILL |   | uss | $\boldsymbol{\mathcal{L}}$ |

M = 6.97

Mean earthquake magnitude at the PGA period based on the Hart Crowser seismic design report "I-405 R2B Segment 1a Site-Specific Hazard Analysis RFU," dated March 25, 2021.

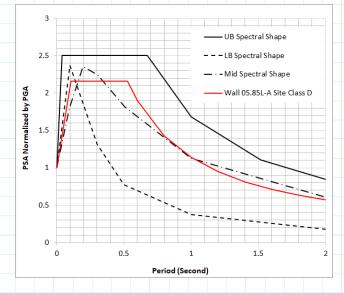
Determine response spectrum using WSDOT Bridge Engineering Software BEToolbox/BridgeLink Version 6.0.0.6 BETA in accordance with the WSDOT BDM based on the projected ground motion at the project site that has a 7 percent (SEE) probability of exceedance in a 75-year period (approximate 1,000-year return period).

$$A_s = 0.520$$
 (g)  
 $S_{D1} = 0.425$ 

Site Class Adjusted PGA

Determine the most appropriate spectral curve shape based on NCHRP Report 611 Figure 5-4.

- 1. Normalize response spectrum by the peak ground acceleration (PGA).
- 2. The peak spectral acceleration (PSA) normalized by PGA is then overlaid on the spectral shapes shown on Figure 5-4 to determine the most appropriate spectral curve shape for the design condition. Three spectral shapes shown on Figure 5-4 include an upper bound (UB), lower bound (LB), and intermediate (Mid) spectral shape.



The Mid spectral shape was selected.



Project: 405 Renton to Bellveue
By: YT Checked By: TB

Determine wall height acceleration reduction factor (or  $\alpha$  coefficient) using wall height and the spectral shapes based on NCHRP Report 611 Figure 6-13.

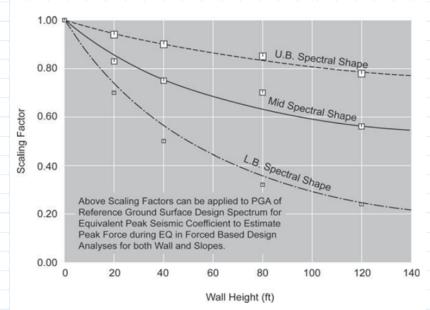


Figure 6-13. Resultant wave scattering  $\alpha$  coefficients for retaining wall design.

#### Station 2+60 (Current design)

For <u>Lateral Earth Pressure</u> calculations, slope height is taken as 30 ft. (vertical distance between proposed ground surface prior to Forward Compatible Wall construction and SEW wall base at the back of wall heel) The wall height acceleration reduction factor selected from Figure 6-13 is:

$$\alpha = 0.808$$

Wall seismic acceleration considering wave scattering

$$PGA_a := A_s \cdot \alpha = 0.42$$

Horizontal seismic coefficient for use in pseudo-static slope stability analyses

$$k_h \coloneqq \frac{PGA_a}{2} = 0.210$$

For <u>Compound Stability</u> calculations, the slope height is taken as 32 ft based on the height of the critical failure surface (refer to Slope/W figures). The wall height acceleration reduction factor selected from Figure 6-13 is:



$$\alpha = 0.799$$

Wall seismic acceleration considering wave scattering

$$PGA_a := A_s \cdot \alpha = 0.415$$

Horizontal seismic coefficient for use in pseudo-static slope stability analyses

$$k_h = \frac{PGA_a}{2} = 0.208$$

For <u>Global Stability</u> calculations, the slope height is taken as 43.5 ft based on the height of the critical failure surface (refer to Slope/W figures). The wall height acceleration reduction factor selected from Figure 6-13 is:

$$\alpha = 0.755$$

Wall seismic acceleration considering wave scattering

$$PGA_{\alpha} := A_{s} \cdot \alpha = 0.393$$

Horizontal seismic coefficient for use in pseudo-static slope stability analyses

$$k_h = \frac{PGA_a}{2} = 0.196$$

### Station 2+60 (with Forward Compatible Wall)

For <u>Compound Stability</u> calculations, the slope height is taken as 44 ft based on the height of the critical failure surface (refer to Slope/W figures). The wall height acceleration reduction factor selected from Figure 6-13 is:

$$\alpha = 0.753$$

Wall seismic acceleration considering wave scattering

$$PGA_a := A_s \cdot \alpha = 0.392$$

Horizontal seismic coefficient for use in pseudo-static slope stability analyses

$$k_h \coloneqq \frac{PGA_a}{2} = 0.196$$

Project: <u>405 Renton to Bellveue</u> By: <u>YT</u> Checked By: <u>TB</u> For <u>Global Stability</u> calculations, the slope height is taken as 43 ft based on the height of the critical failure surface (refer to Slope/W figures). The wall height acceleration reduction factor selected from Figure 6-13 is:

$$\alpha = 0.756$$

Wall seismic acceleration considering wave scattering

$$PGA_a := A_s \cdot \alpha = 0.393$$

Horizontal seismic coefficient for use in pseudo-static slope stability analyses

$$k_h = \frac{PGA_a}{2} = 0.197$$

| General Information |  |  |  |  |  |  |  |  |  |
|---------------------|--|--|--|--|--|--|--|--|--|
| Project:            | I-405/Renton to Bellevue Corridor Widening |  |  |  |  |  |  |  |  |
| Project Location:   | King County, Washington                    |  |  |  |  |  |  |  |  |
| Job Number:         | 00180-366-01                               |  |  |  |  |  |  |  |  |
| Boring Designation: | W-218-20                                   |  |  |  |  |  |  |  |  |
| Analysis by:        | BZ   |  |  |  |  |  |  |  |  |
| Date Analyzed:      | 4/8/2021                                   |  |  |  |  |  |  |  |  |
| Checked by:         | ТВ   |  |  |  |  |  |  |  |  |
| Date Checked:       | 4/8/2021                                   |  |  |  |  |  |  |  |  |

| Sampling Information  | n    | 1                |
|---|------|------------------|
| Depth to Groundwater (ft):                                  | 28.6 | GW based on      |
| SPT Liner (Yes/No):   | No   | SEEP/W           |
| Hammer Energy, %:   | 60   | analysis at Wall |
| Distance from sample hammer to ground/mudline surface (ft): | 5    | 05.85L-A         |
| Borehole Diameter (in)                                      | 6    | _                |

| Earthquake Information     |       |              |  |  |  |  |  |
|----------------------------|-------|--------------|--|--|--|--|--|
| Max Acceleration (As) (g): | 0.520 | Site Class C |  |  |  |  |  |
| Earthquake Magnitude:      | 6.97  | SEE          |  |  |  |  |  |

| Title Block Information |  |  |  |  |  |  |  |
|-------------------------|--|--|--|--|--|--|--|
| Line 1:                 | I-405/Renton to Bellevue Corridor Widening |  |  |  |  |  |  |
| Line 2:                 | King County, Washington                    |  |  |  |  |  |  |

| gINT Collection Information            |  |  |  |  |  |  |  |
|--|--|--|--|--|--|--|--|
| P-Drive File Path to gINT<br>database: |  |  |  |  |  |  |  |
| Boring Selected from<br>Database:      |  |  |  |  |  |  |  |

| Residual Strength Weighting                       |     |  |  |  |  |  |
|---|-----|--|--|--|--|--|
| Olsen & Stark (2002):                             | 0.2 |  |  |  |  |  |
| Idriss & Boulanger Void Redistribution (2007):    | 0.2 |  |  |  |  |  |
| Idriss & Boulanger No Void Redistribution (2007): | 0.0 |  |  |  |  |  |
| Kramer, Wang Hybrid (2008):                       | 0.4 |  |  |  |  |  |
| Idriss et al. (1998):                             | 0.2 |  |  |  |  |  |

| Collect Data From gINT | Automate %F from USCS |
|------------------------|-----------------------|
| Auto %F from WSDOT GDM | СОМРИТЕ               |

\*You must hit "COMPUTE" again anytime you change any of

User Input

Fine -Grain Soil Susceptibility

PI Cutoff Value:

gINT or User

Input

12

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| he blue or purple inputs. If the output tab is blank or ha | as   |
| rrors hit "COMPUTE" again.                                 |      |
|  |      |

| SPT Sample Number | Depth<br>(ft) | Measured N | USCS  | Fines Content<br>(%) | Geologic Unit/<br>ESU | Unit Weight (pcf) | PI<br>(%) | Non-liquefiable (i.e.<br>"unstaturated",<br>"cohesive",etc) | User Override*  |
|-------------------|---------------|------------|-------|----------------------|-----------------------|-------------------|-----------|---|-----------------|
|                   | 2.5           | 68         | SW-SM | 9                    | ESU 1B                | 125               |           | Unsaturated   |                 |
|                   | 5.0           | 23         | SM    | 33                   | ESU 2B                | 115               |           | Unsaturated   |                 |
|                   | 7.5           | 25         | SM    | 33                   | ESU 2B                | 120               |           | Unsaturated   |                 |
|                   | 10.0          | 22         | SM    | 33                   | ESU 2B                | 115               |           | Unsaturated   |                 |
|                   | 15.0          | 65         | SM    | 41                   | ESU 4B                | 130               |           | Non-Liquefiable   | Non-Liquefiable |
|                   | 20.0          | 120        | SM    | 45                   | ESU 4B                | 130               | 3.0       | Non-Liquefiable   | Non-Liquefiable |
|                   | 25.0          | 120        | SM    | 36                   | ESU 4B                | 130               |           | Non-Liquefiable   | Non-Liquefiable |
|                   | 30.0          | 120        | SM    | 36                   | ESU 4B                | 130               |           | Non-Liquefiable   | Non-Liquefiable |
|                   | 35.0          | 120        | SP    | 5                    | ESU 4B                | 125               |           | Non-Liquefiable   | Non-Liquefiable |
|                   | 40.0          | 300        | SP    | 5                    | ESU 4B                | 125               |           | Non-Liquefiable   | Non-Liquefiable |
|                   | 45.0          | 100        | ML    | 98                   | ESU 5B                | 130               | 8.0       | Non-Liquefiable   | Non-Liquefiable |
|                   | 50.0          | 79         | ML    | 98                   | ESU 5B                | 130               | 5.0       | Non-Liquefiable   | Non-Liquefiable |
|                   | 55.0          | 100        | CL    | 95                   | ESU 5B                | 130               | 13.0      | Non-Liquefiable   | Non-Liquefiable |
|                   | 60.0          | 100        | CL    | 95                   | ESU 5B                | 130               | 1010      | Non-Liquefiable   | Non-Liquefiable |
|                   | 65.0          | 100        | SM    | 15                   | ESU 4B                | 135               |           | Non-Liquefiable   | Non-Liquefiable |
|                   | 70.0          | 100        | SM    | 15                   | ESU 4B                | 135               |           | Non-Liquefiable   | Non-Liquefiable |
|                   | 75.0          | 300        | GM    | 25                   | ESU 4B                | 130               |           | Non-Liquefiable   | Non-Liquefiable |
|                   | 80.0          | 1200       | GM    | 25                   |                       | 130               |           |   | Non-Liquefiable |
|                   | 80.0          | 1200       | GIVI  | 25                   | ESU 4B                | 130               |           | Non-Liquefiable   | Non-Liquenable  |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           | <del> </del>  |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           | -   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |
|                   |               |            |       |                      |                       |                   |           |   |                 |

\*User Override column is *NOT* required to be filled out, unless needed. See "Read Me" tab.

|                      | Liquefaction Analysis Residual Shear Strength Analysis |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |   |                                  |                                   |                         |
|----------------------|--|------------|----------|-------------------------|------------------------------|-----------------------------------|------------------------------|-----------------------------------|---------------------|-------------------------|-------------------------|-------------------------|---|-------------------------|-----------------------------------|--------------|-------------------------|---|----------------------------------|-----------------------------------|-------------------------|
|                      |  |            |          |                         | N.                           | 1,60                              | Liquefaction Saf             | on Factor of<br>ety               | Liquefact           | ion-Induced Settle      | ement (in)              | LDI<br>(ft)             | N <sub>1,60</sub>                                       |                         |                                   |              |                         | Residual Shea                                 |                                  |                                   |                         |
| SPT Sample<br>Number | Depth<br>(ft)  | Measured N | USCS     | Fines<br>Content<br>(%) | Youd and<br>Idriss<br>(2001) | Idriss and<br>Boulanger<br>(2008) | Youd and<br>Idriss<br>(2001) | Idriss and<br>Boulanger<br>(2014) | Tokimatsu &<br>Seed | Ishihara &<br>Yoshimine | Idriss and<br>Boulanger | Idriss and<br>Boulanger | Idriss &<br>Boulanger<br>Void<br>Distribution<br>(2007) | Olsen & Stark<br>(2002) | Kramer &<br>Wang Hybrid<br>(2008) | WSDOT        | Olsen & Stark<br>(2002) | Idriss & Boulanger Void Redistribution (2007) | Idriss &<br>Boulanger<br>No Void | Kramer &<br>Wang Hybrid<br>(2008) | Idriss et al.<br>(1998) |
|                      | 2.5  | 68         | SW-SM    | 9                       | 96                           | 97                                | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 97.0  | 99.7                    | 95.2                              | n.a.         | n.a.                    | n.a.  | n.a.                             | n.a.                              | n.a.                    |
|                      | 5.0  | 23         | SM       | 33                      | 31                           | 32                                | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 31.5  | 36.0                    | 29.7                              | n.a.         | n.a.                    | n.a.  | n.a.                             | n.a.                              | n.a.                    |
|                      | 7.5<br>10.0  | 25<br>22   | SM<br>SM | 33<br>33                | 31<br>27                     | 30<br>26                          | 2.00                         | 2.00<br>2.00                      | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 30.4<br>26.3  | 35.3<br>28.7            | 29.2<br>25.3                      | n.a.<br>n.a. | n.a.<br>n.a.            | n.a.<br>n.a.                                  | n.a.<br>n.a.                     | n.a.<br>n.a.                      | n.a.                    |
|                      | 15.0   | 65         | SM       | 41                      | 76                           | 74                                | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 73.7  | 76.2                    | 73.2                              | n.a.         | n.a.                    | n.a.  | n.a.                             | n.a.                              | n.a.                    |
|                      | 20.0   | 120        | SM       | 45                      | 101                          | 105                               | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 125.6   | 120.9                   | 121.8                             | n.a.         | n.a.                    | n.a.  | n.a.                             | n.a.                              | n.a.                    |
|                      | 25.0<br>30.0   | 120<br>120 | SM<br>SM | 36<br>36                | 90<br>86                     | 99<br>99                          | 2.00<br>2.00                 | 2.00<br>2.00                      | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 118.2<br>119.1  | 107.7<br>104.4          | 111.6<br>109.9                    | n.a.         | n.a.                    | n.a.  | n.a.                             | n.a.                              | n.a.                    |
|                      | 35.0   | 120        | SP       | 5                       | 82                           | 97                                | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 116.6   | 100.2                   | 106.1                             | n.a.<br>n.a. | n.a.<br>n.a.            | n.a.<br>n.a.                                  | n.a.<br>n.a.                     | n.a.<br>n.a.                      | n.a.                    |
|                      | 40.0   | 300        | SP       | 5                       | 78                           | 95                                | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 285.8   | 241.3                   | 256.6                             | n.a.         | n.a.                    | n.a.  | n.a.                             | n.a.                              | n.a.                    |
|                      | 45.0<br>50.0   | 100<br>79  | ML       | 98<br>98                | 74                           | 93<br>72                          | 2.00                         | 2.00<br>2.00                      | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 93.4  | 77.5                    | 82.6                              | n.a.         | n.a.                    | n.a.  | n.a.                             | n.a.                              | n.a.                    |
|                      | 55.0   | 100        | ML<br>CL | 95                      | 56<br>68                     | 90                                | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 72.4<br>90.1  | 59.1<br>72.4            | 63.2<br>77.4                      | n.a.<br>n.a. | n.a.<br>n.a.            | n.a.<br>n.a.                                  | n.a.<br>n.a.                     | n.a.<br>n.a.                      | n.a.                    |
|                      | 60.0   | 100        | CL       | 95                      | 65                           | 89                                | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 88.7  | 70.2                    | 75.1                              | n.a.         | n.a.                    | n.a.  | n.a.                             | n.a.                              | n.a.                    |
|                      | 65.0   | 100        | SM       | 15                      | 62                           | 87                                | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 87.3  | 68.1                    | 72.7                              | n.a.         | n.a.                    | n.a.  | n.a.                             | n.a.                              | n.a.                    |
|                      | 70.0<br>75.0   | 100<br>300 | SM<br>GM | 15<br>25                | 60<br>58                     | 86<br>85                          | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 85.9<br>254.3   | 66.1<br>193.3           | 70.5<br>205.4                     | n.a.         | n.a.                    | n.a.  | n.a.                             | n.a.                              | n.a.                    |
|                      | 80.0   | 1200       | GM       | 25                      | 56                           | 84                                | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 1004.3  | 754.5                   | 799.1                             | n.a.<br>n.a. | n.a.<br>n.a.            | n.a.<br>n.a.                                  | n.a.<br>n.a.                     | n.a.<br>n.a.                      | n.a.                    |
|                      |  |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |   |                                  |                                   |                         |
|                      |  |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |   |                                  |                                   |                         |
|                      |  |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |   |                                  |                                   |                         |
|                      |  |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |   |                                  |                                   |                         |
|                      |  |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |   |                                  |                                   |                         |
|                      |  |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |   |                                  |                                   |                         |
|                      |  |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |   |                                  |                                   |                         |
|                      |  |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |   |                                  |                                   |                         |
|                      |  |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |   |                                  |                                   |                         |
|                      |  |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |   |                                  |                                   |                         |
|                      |  |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |   |                                  |                                   |                         |
|                      |  |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |   |                                  |                                   |                         |
|                      |  |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |   |                                  |                                   |                         |
|                      |  |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |   |                                  |                                   |                         |
|                      |  |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |   |                                  |                                   |                         |
|                      |  |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |   |                                  |                                   |                         |
|                      |  |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |   |                                  |                                   |                         |
|                      |  |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |   |                                  |                                   |                         |
|                      |  |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |   |                                  |                                   |                         |
|                      |  |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |   |                                  |                                   |                         |
|                      |  |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |   |                                  |                                   |                         |
|                      |  |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |   |                                  |                                   |                         |
|                      |  |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |   |                                  |                                   |                         |
|                      |  |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |   |                                  |                                   |                         |
|                      |  |            |          |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |              |                         |   |                                  |                                   |                         |
| <del>-</del>         |  |            |          |                         | 1                            |                                   |                              | Residu                            | al Strength Wei     | ghting Factors          |                         |                         |   |                         |                                   |              |                         |   |                                  |                                   |                         |
|                      | Seismic Parameters WSDOT: 0                            |            |          |                         |                              |                                   |                              |                                   |                     | Liquefac                | tion and R              | esidual Sh              | ear Streng  | th Analysis             |                                   |              |                         |   |                                  |                                   |                         |

Seismic Parameters

Max Acceleration (As) (g): 0.520

Earthquake Magnitude: 6.97

WSDOT: 0
Olsen & Stark (2002): 0.2
Idriss & Boulanger Void Redistribution (2007): 0.2
Idriss & Boulanger No Void Redistribution (2007): 0
Kramer, Wang Hybrid (2008): 0.4

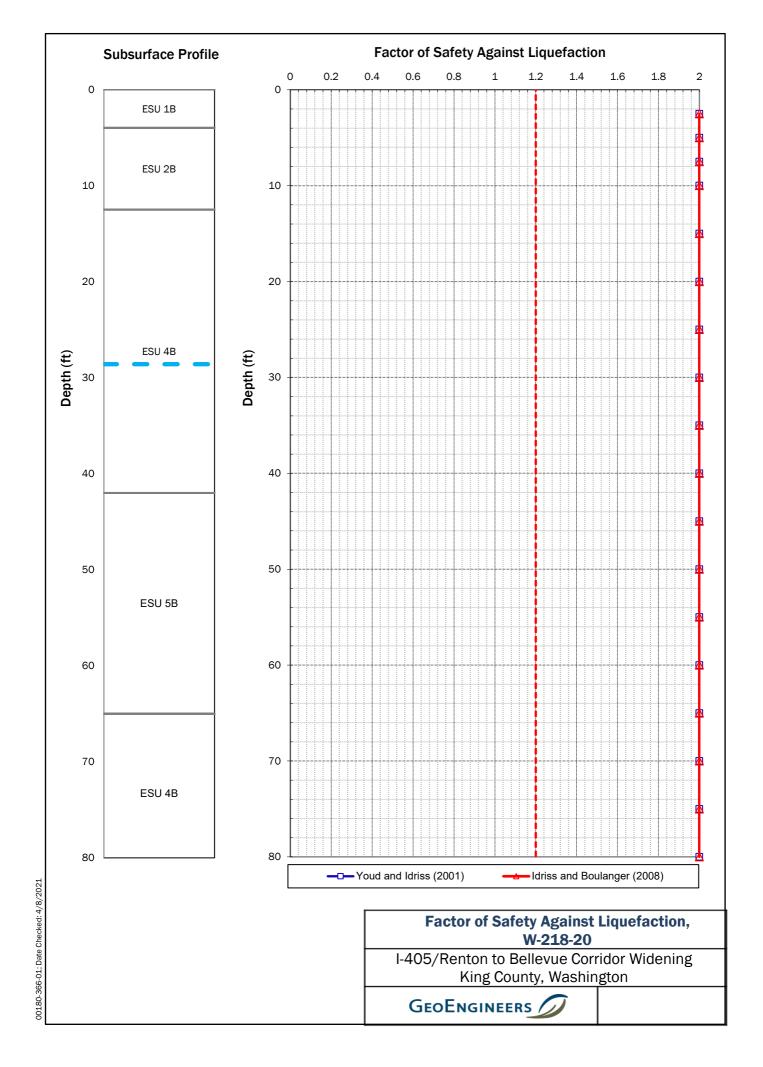
Idriss et al. (1998):

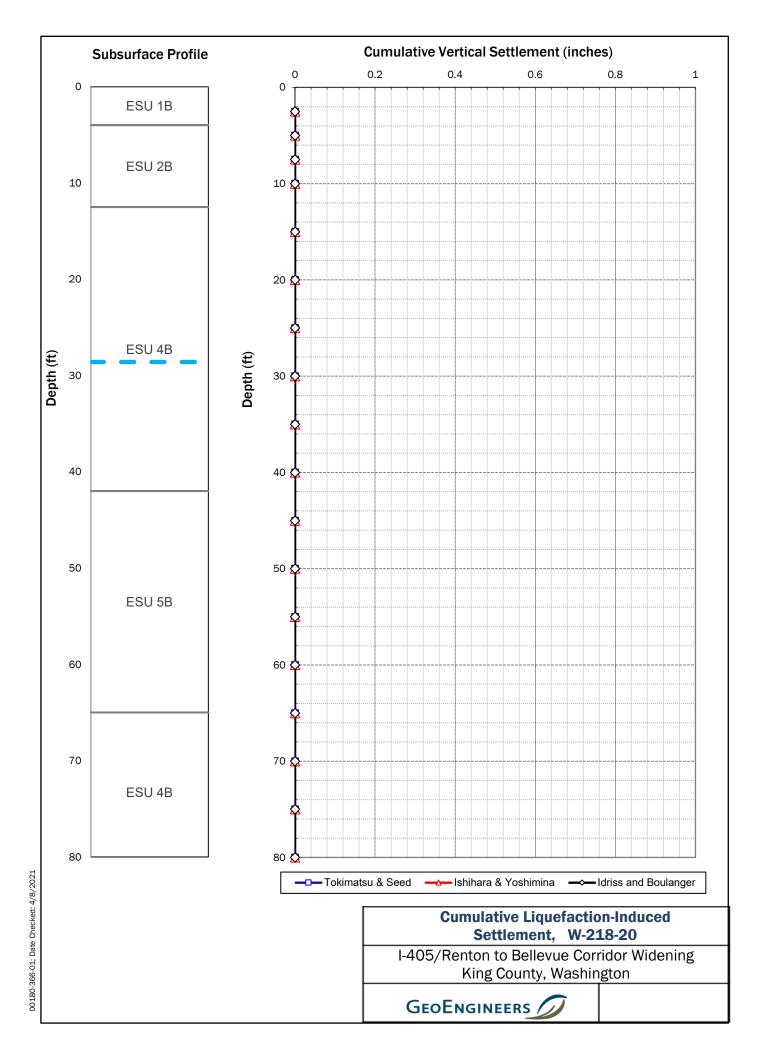
0.2

Liquefaction and Residual Shear Strength Analysis Results, W-218-20

I-405/Renton to Bellevue Corridor Widening King County, Washington







| General Information |  |  |  |  |  |  |  |
|---------------------|--|--|--|--|--|--|--|
| Project:            | I-405/Renton to Bellevue Corridor Widening |  |  |  |  |  |  |
| Project Location:   | King County, Washington                    |  |  |  |  |  |  |
| Job Number:         | 00180-366-01                               |  |  |  |  |  |  |
| Boring Designation: | R2B-10-17                                  |  |  |  |  |  |  |
| Analysis by:        | BZ   |  |  |  |  |  |  |
| Date Analyzed:      | 4/8/2021                                   |  |  |  |  |  |  |
| Checked by:         | ТВ   |  |  |  |  |  |  |
| Date Checked:       | 4/9/2021                                   |  |  |  |  |  |  |

|   |      | _ L              |
|---|------|------------------|
| Sampling Information  | n    |                  |
| Depth to Groundwater (ft):                                  | 16.2 | GW based on      |
| SPT Liner (Yes/No):   | No   | SEEP/W           |
| Hammer Energy, %:   | 88.4 | analysis at Wall |
| Distance from sample hammer to ground/mudline surface (ft): | 5    | 05.85L-A         |
| Borehole Diameter (in)                                      | 4    |                  |

| Earthquake Information     | on    |              |
|----------------------------|-------|--------------|
| Max Acceleration (As) (g): | 0.520 | Site Class C |
| Earthquake Magnitude:      | 6.97  | SEE          |

| Title Block Information |  |  |  |  |  |  |  |
|-------------------------|--|--|--|--|--|--|--|
| Line 1:                 | I-405/Renton to Bellevue Corridor Widening |  |  |  |  |  |  |
| Line 2:                 | King County, Washington                    |  |  |  |  |  |  |

| gIN                                 | NT Collection Information |
|-------------------------------------|---------------------------|
| P-Drive File Path to gINT database: |                           |
| Boring Selected from<br>Database:   |                           |

| Residual Strength Weighting                       |     |  |  |  |  |
|---|-----|--|--|--|--|
| Olsen & Stark (2002):                             | 0.2 |  |  |  |  |
| Idriss & Boulanger Void Redistribution (2007):    | 0.2 |  |  |  |  |
| Idriss & Boulanger No Void Redistribution (2007): | 0.0 |  |  |  |  |
| Kramer, Wang Hybrid (2008):                       | 0.4 |  |  |  |  |
| Idriss et al. (1998):                             | 0.2 |  |  |  |  |

| Collect Data From gINT | Automate %F from USCS |
|------------------------|-----------------------|
| 1                      |                       |
| Auto %F from WSDOT GDM | COMPUTE               |

\*You must hit "COMPUTE" again anytime you change any of the blue or purple inputs. If the output tab is blank or has errors hit "COMPUTE" again.

User Input

Fine -Grain Soil Susceptibility

PI Cutoff Value:

gINT or User

Input

12

| SPT Sample Number | Depth<br>(ft) | Measured N | USCS | Fines Content<br>(%) | Geologic Unit/<br>ESU | Unit Weight (pcf) | PI<br>(%) | Non-liquefiable (i.e.<br>"unstaturated",<br>"cohesive",etc) | User Override*  |
|-------------------|---------------|------------|------|----------------------|-----------------------|-------------------|-----------|---|-----------------|
|                   | 4.0           | 51         | SM   | 35                   | ESU 1B                | 130               |           | Unsaturated   |                 |
|                   | 7.0           | 16         | SM   | 35                   | ESU 2B                | 110               |           | Unsaturated   |                 |
|                   | 9.0           | 12         | SM   | 35                   | ESU 2B                | 110               |           | Unsaturated   |                 |
|                   | 12.0          | 8          | ML   | 70                   | ESU 2B                | 110               |           | Unsaturated   |                 |
|                   | 14.0          | 21         | SM   | 15                   | ESU 2B                | 115               |           |   |                 |
|                   | 19.0          | 48         | SM   | 15                   | ESU 4B                | 130               |           | Non-Liquefiable   | Non-Liquefiable |
|                   | 24.0          | 35         | SM   | 15                   | ESU 4B                | 120               |           |   | Non-Liquefiable |
|                   | 29.0          | 50         | SM   | 15                   | ESU 4B                | 130               |           |   | Non-Liquefiable |
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"Read Me" tab.

|                      | Liquefaction Analysis |            |            |                         |                              |                                   |                              |   |                     |                         |                         |                         | Residual S                                  | Shear Streng            | gth Analysis                      | <u> </u>     |                         |                 |  |                                   |                         |
|----------------------|-----------------------|------------|------------|-------------------------|------------------------------|-----------------------------------|------------------------------|---|---------------------|-------------------------|-------------------------|-------------------------|---|-------------------------|-----------------------------------|--------------|-------------------------|-----------------|--|-----------------------------------|-------------------------|
|                      |                       |            |            |                         | N <sub>2</sub>               | 1,60                              |                              | Liquefaction Factor of Safety  Liquefaction-Induced Settlement (in) |                     |                         | LDI<br>(ft)             |                         | N <sub>1,60</sub>                           |                         |                                   |              | Residual Shea           | or Strength, Sr |  |                                   |                         |
| SPT Sample<br>Number | Depth<br>(ft)         | Measured N | USCS       | Fines<br>Content<br>(%) | Youd and<br>Idriss<br>(2001) | Idriss and<br>Boulanger<br>(2008) | Youd and<br>Idriss<br>(2001) | Idriss and<br>Boulanger<br>(2014)                                   | Tokimatsu &<br>Seed | Ishihara &<br>Yoshimine | ldriss and<br>Boulanger | Idriss and<br>Boulanger | Idriss & Boulanger Void Distribution (2007) | Olsen & Stark<br>(2002) | Kramer &<br>Wang Hybrid<br>(2008) | WSDOT        | Olsen & Stark<br>(2002) | Void            | Idriss & Boulanger No Void Redistribution (2007) | Kramer &<br>Wang Hybrid<br>(2008) | Idriss et al.<br>(1998) |
|                      | 4.0                   | 51         | SM         | 35                      | 86                           | 82                                | 2.00                         | 2.00  | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 81.5  | 95.8                    | 81.8                              | n.a.         | n.a.                    | n.a.            | n.a.   | n.a.                              | n.a.                    |
|                      | 7.0<br>9.0            | 16<br>12   | SM<br>SM   | 35<br>35                | 26<br>19                     | 26<br>20                          | 2.00<br>2.00                 | 2.00  | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 26.0<br>19.7                                | 29.8<br>21.1            | 24.3<br>18.2                      | n.a.<br>n.a. | n.a.<br>n.a.            | n.a.<br>n.a.    | n.a.<br>n.a.                                     | n.a.<br>n.a.                      | n.a.<br>n.a.            |
|                      | 12.0                  | 8          | ML         | 70                      | 12                           | 12                                | 2.00                         | 2.00  | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 12.1  | 12.3                    | 11.2                              | n.a.         | n.a.                    | n.a.            | n.a.   | n.a.                              | n.a.                    |
|                      | 14.0<br>19.0          | 21<br>48   | SM<br>SM   | 15<br>15                | 29<br>67                     | 29<br>67                          | 2.00                         | 2.00  | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 28.8<br>67.3                                | 30.0<br>67.4            | 28.1<br>66.2                      | n.a.<br>n.a. | n.a.                    | n.a.<br>n.a.    | n.a.<br>n.a.                                     | n.a.<br>n.a.                      | n.a.<br>n.a.            |
|                      | 24.0<br>29.0          | 35<br>50   | SM<br>SM   | 15<br>15                | 46<br>65                     | 47<br>69                          | 2.00<br>2.00                 | 2.00  | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 47.4<br>68.9                                | 46.1<br>64.8            | 46.1<br>66.1                      | n.a.         | n.a.                    | n.a.            | n.a.   | n.a.                              | n.a.                    |
|                      | 29.0                  | 30         | Sivi       | 13                      | 03                           | 03                                | 2.00                         | 2.00  | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 68.9  | 64.8                    | 99.1                              | n.a.         | n.a.                    | n.a.            | n.a.   | n.a.                              | n.a.                    |
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|                      |                       |            |            |                         |                              |                                   |                              | Residu  | al Strength Wei     | ghting Factors          |                         |                         |   |                         |                                   |              |                         |                 |  |                                   |                         |
|                      |                       | Seisn      | nic Parame | eters                   | ]                            |                                   |                              | , , , , ,   | <u> </u>            | WSDOT:                  | 0                       |                         |   |                         |                                   |              | Liquefac                | tion and R      | esidual Sh                                       | ear Streng                        | gth Analysis            |

Seismic Parameters

Max Acceleration (As) (g): 0.520

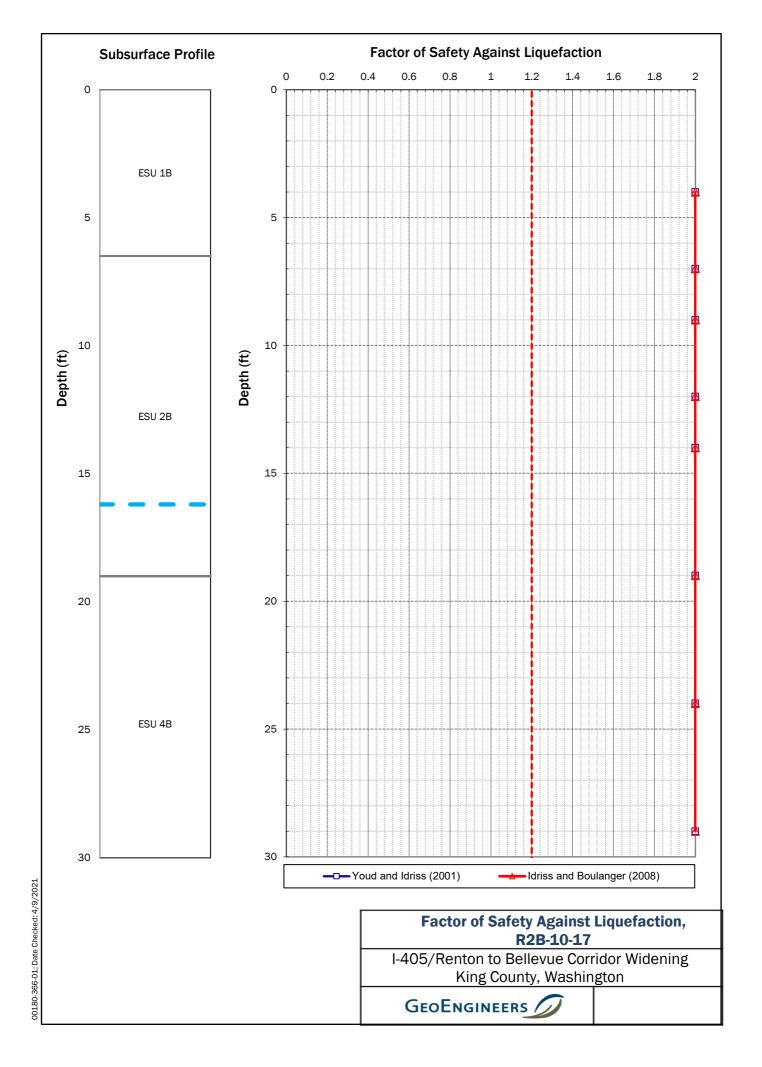
Earthquake Magnitude: 6.97

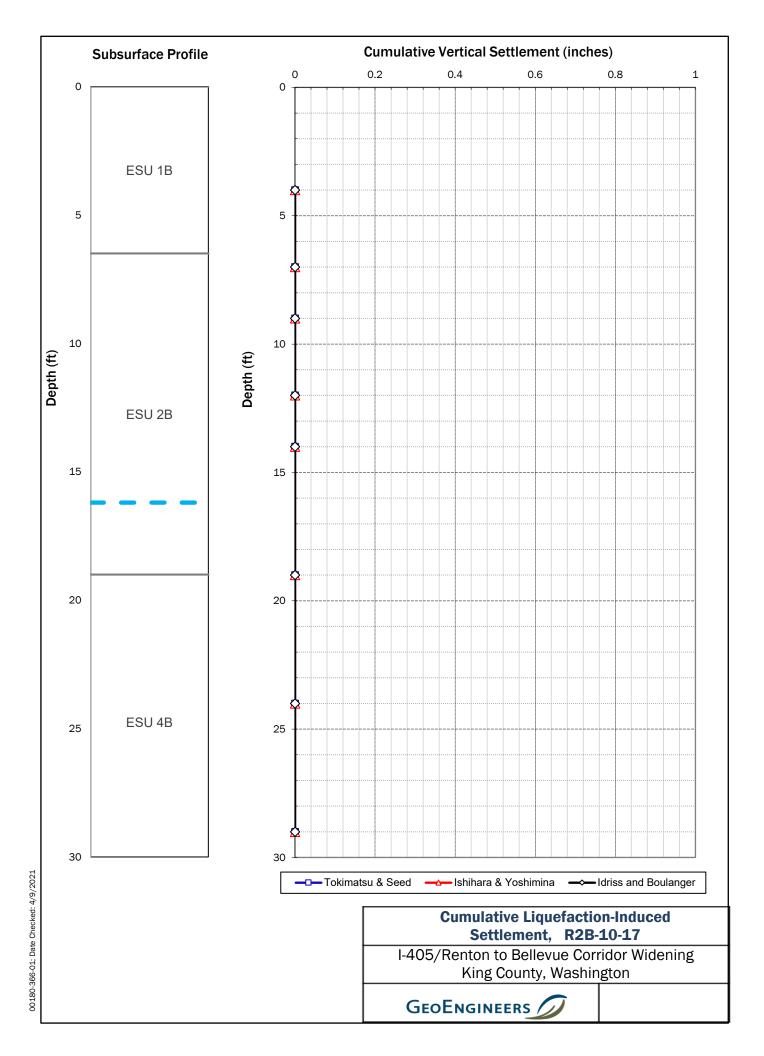
WSDOT: 0
Olsen & Stark (2002): 0.2
Idriss & Boulanger Void Redistribution (2007): 0.2
Idriss & Boulanger No Void Redistribution (2007): 0
Kramer, Wang Hybrid (2008): 0.4
Idriss et al. (1998): 0.2

iquefaction and Residual Shear Strength Analysis Results, R2B-10-17

I-405/Renton to Bellevue Corridor Widening King County, Washington







| General Information |  |  |  |  |
|---------------------|--|--|--|--|
| Project:            | I-405/Renton to Bellevue Corridor Widening |  |  |  |
| Project Location:   | King County, Washington                    |  |  |  |
| Job Number:         | 00180-366-01                               |  |  |  |
| Boring Designation: | R2B-11-17                                  |  |  |  |
| Analysis by:        | BZ   |  |  |  |
| Date Analyzed:      | 4/8/2021                                   |  |  |  |
| Checked by:         | ТВ   |  |  |  |
| Date Checked:       | 4/9/2021                                   |  |  |  |

|   |      | _ L              |
|---|------|------------------|
| Sampling Information  |      |                  |
| Depth to Groundwater (ft):                                  | 20.2 | GW based on      |
| SPT Liner (Yes/No):   | No   | SEEP/W           |
| Hammer Energy, %:   | 88.4 | analysis at Wall |
| Distance from sample hammer to ground/mudline surface (ft): | 5    | 05.85L-A         |
| Borehole Diameter (in)                                      | 4    | _                |

| Earthquake Information      | 1     |              |    |
|-----------------------------|-------|--------------|----|
| Max Acceleration (As) (g) : | 0.520 | Site Class C |    |
| Earthquake Magnitude:       | 6.97  | SEE          | Au |

|         | Fitle Block Information                    |
|---------|--|
| Line 1: | I-405/Renton to Bellevue Corridor Widening |
| Line 2: | King County, Washington                    |

| gIN                                 | IT Collection Information |
|-------------------------------------|---------------------------|
| P-Drive File Path to gINT database: |                           |
| Boring Selected from<br>Database:   |                           |

| Residual Strength Weighting                       |     |  |  |  |  |
|---|-----|--|--|--|--|
| Olsen & Stark (2002):                             | 0.2 |  |  |  |  |
| Idriss & Boulanger Void Redistribution (2007):    | 0.2 |  |  |  |  |
| Idriss & Boulanger No Void Redistribution (2007): | 0.0 |  |  |  |  |
| Kramer, Wang Hybrid (2008):                       | 0.4 |  |  |  |  |
| Idriss et al. (1998):                             | 0.2 |  |  |  |  |

| Collect Data From gINT | Automate %F from USCS |
|------------------------|-----------------------|
| Auto %F from WSDOT GDM | COMPUTE               |

User Input

gINT or User Input

| Fine -Grain Soil Susceptib | ility |
|----------------------------|-------|
| PI Cutoff Value:           | 12    |

\*You must hit "COMPUTE" again anytime you change any of the blue or purple inputs. If the output tab is blank or has errors hit "COMPUTE" again.

| SPT Sample Number | Depth<br>(ft) | Measured N | USCS | Fines Content<br>(%) | Geologic Unit/<br>ESU | Unit Weight (pcf) | PI<br>(%) | Non-liquefiable (i.e.<br>"unstaturated",<br>"cohesive",etc) | User Override*  |
|-------------------|---------------|------------|------|----------------------|-----------------------|-------------------|-----------|---|-----------------|
|                   | 4.0           | 36         | SM   | 29                   | ESU 1B                | 120               |           | Unsaturated   |                 |
|                   | 7.0           | 11         | SM   | 29                   | ESU 2B                | 110               | 0.0       | Unsaturated   |                 |
|                   | 9.0           | 13         | SM   | 29                   | ESU 2B                | 110               |           | Unsaturated   |                 |
|                   | 12.0          | 17         | SM   | 29                   | ESU 2B                | 115               |           | Unsaturated   |                 |
|                   | 14.0          | 15         | SM   | 29                   | ESU 2B                | 110               |           | Unsaturated   |                 |
|                   | 19.0          | 18         | ML   | 97                   | ESU 2B                | 110               |           |   |                 |
|                   | 24.0          | 18         | ML   | 97                   | ESU 2B                | 115               | 3.0       |   |                 |
|                   | 29.0          | 150        | SC   | 22                   | ESU 4B                | 130               |           | Non-Liquefiable   | Non-Liquefiable |
|                   | 34.0          | 100        | SC   | 22                   | ESU 4B                | 130               | 9.0       | Non-Liquefiable   | Non-Liquefiable |
|                   | 39.0          | 100        | SC   | 22                   | ESU 4B                | 130               |           | Non-Liquefiable   | Non-Liquefiable |
|                   | 44.0          | 60         | SC   | 22                   | ESU 4B                | 130               |           | Non-Liquefiable   | Non-Liquefiable |
|                   | 49.0          | 300        | SC   | 22                   | ESU 4B                | 130               |           | Non-Liquefiable   | Non-Liquefiable |
|                   | 54.0          | 72         | SM   | 18                   | ESU 4B                | 130               |           | Non-Liquefiable   | Non-Liquefiable |
|                   | 59.0          | 49         | SM   | 18                   | ESU 4B                | 130               |           | Non-Liquefiable   | Non-Liquefiable |
|                   | 0010          | 10         | Olvi | 10                   | 200 10                | 100               |           | 11011 Elquoliubio   |                 |
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\*User Override column is *NOT* required to be filled out, unless needed. See "Read Me" tab.

|                      |               |            |            |                         |                              |                                   |                              | Lique                             | efaction Anal       | ysis                    |                         |                         |   |                         |                                   | Residual Shear Strength Analysis |                         |                               |  |                                   |                         |
|----------------------|---------------|------------|------------|-------------------------|------------------------------|-----------------------------------|------------------------------|-----------------------------------|---------------------|-------------------------|-------------------------|-------------------------|---|-------------------------|-----------------------------------|----------------------------------|-------------------------|-------------------------------|--|-----------------------------------|-------------------------|
|                      |               |            |            |                         | N <sub>2</sub>               | 1,60                              |                              | on Factor of<br>ety               | Liquefact           | ion-Induced Settle      | ement (in)              | LDI<br>(ft)             |   | N <sub>1,60</sub>       |                                   |                                  |                         | Residual Shea                 |  |                                   |                         |
| SPT Sample<br>Number | Depth<br>(ft) | Measured N | USCS       | Fines<br>Content<br>(%) | Youd and<br>Idriss<br>(2001) | Idriss and<br>Boulanger<br>(2008) | Youd and<br>Idriss<br>(2001) | Idriss and<br>Boulanger<br>(2014) | Tokimatsu &<br>Seed | Ishihara &<br>Yoshimine | Idriss and<br>Boulanger | Idriss and<br>Boulanger | Idriss &<br>Boulanger<br>Void<br>Distribution<br>(2007) | Olsen & Stark<br>(2002) | Kramer &<br>Wang Hybrid<br>(2008) | WSDOT                            | Olsen & Stark<br>(2002) | Idriss &<br>Boulanger<br>Void | Idriss &<br>Boulanger<br>No Void<br>Redistribution<br>(2007) | Kramer &<br>Wang Hybrid<br>(2008) | Idriss et al.<br>(1998) |
|                      | 4.0           | 36         | SM         | 29                      | 61                           | 59                                | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.1                     | 0.1                     | 58.8  | 67.6                    | 58.8                              | n.a.                             | n.a.                    | n.a.                          | n.a.   | n.a.                              | n.a.                    |
|                      | 7.0           | 11         | SM         | 29                      | 18                           | 19                                | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.1                     | 0.1                     | 19.1  | 21.0                    | 16.9                              | n.a.                             | n.a.                    | n.a.                          | n.a.   | n.a.                              | n.a.                    |
|                      | 9.0           | 13<br>17   | SM<br>SM   | 29<br>29                | 21<br>25                     | 22<br>25                          | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.1                     | 0.1                     | 21.5<br>24.9  | 23.3<br>26.4            | 19.9<br>24.0                      | n.a.<br>n.a.                     | n.a.                    | n.a.<br>n.a.                  | n.a.<br>n.a.   | n.a.<br>n.a.                      | n.a.<br>n.a.            |
|                      | 14.0          | 15         | SM         | 29                      | 21                           | 21                                | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.1                     | 0.1                     | 21.0  | 21.6                    | 20.2                              | n.a.                             | n.a.                    | n.a.                          | n.a.   | n.a.                              | n.a.                    |
|                      | 19.0          | 18         | ML         | 97                      | 25                           | 25                                | 2.00                         | 1.97                              | 0.0                 | 0.0                     | 0.1                     | 0.1                     | 25.1  | 25.0                    | 24.6                              | n.a.                             | n.a.                    | n.a.                          | n.a.   | n.a.                              | n.a.                    |
|                      | 24.0          | 18<br>150  | ML<br>SC   | 97<br>22                | 23<br>128                    | 24<br>137                         | 2.00                         | 1.50<br>2.00                      | 0.0                 | 0.0                     | 0.1                     | 0.1                     | 23.8  | 23.3                    | 23.4                              | n.a.                             | n.a.                    | n.a.                          | n.a.   | n.a.                              | n.a.                    |
|                      | 34.0          | 100        | SC         | 22                      | 120                          | 133                               | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 204.9<br>132.6  | 191.4<br>120.6          | 196.0<br>125.1                    | n.a.<br>n.a.                     | n.a.<br>n.a.            | n.a.<br>n.a.                  | n.a.<br>n.a.   | n.a.<br>n.a.                      | n.a.<br>n.a.            |
|                      | 39.0          | 100        | SC         | 22                      | 114                          | 129                               | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 129.1   | 114.6                   | 120.1                             | n.a.                             | n.a.                    | n.a.                          | n.a.   | n.a.                              | n.a.                    |
|                      | 44.0          | 60         | SC         | 22                      | 65                           | 76                                | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 75.6  | 65.7                    | 69.3                              | n.a.                             | n.a.                    | n.a.                          | n.a.   | n.a.                              | n.a.                    |
|                      | 49.0<br>54.0  | 300<br>72  | SC<br>SM   | 22<br>18                | 102<br>70                    | 123<br>87                         | 2.00                         | 2.00<br>2.00                      | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 369.7<br>86.9   | 314.8<br>72.7           | 334.1<br>77.4                     | n.a.<br>n.a.                     | n.a.                    | n.a.<br>n.a.                  | n.a.<br>n.a.   | n.a.<br>n.a.                      | n.a.<br>n.a.            |
|                      | 59.0          | 49         | SM         | 18                      | 45                           | 58                                | 2.00                         | 2.00                              | 0.0                 | 0.0                     | 0.0                     | 0.0                     | 58.0  | 47.7                    | 50.9                              | n.a.                             | n.a.                    | n.a.                          | n.a.   | n.a.                              | n.a.                    |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               |            |            |                         |                              |                                   |                              |                                   |                     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
| <b>_</b>             |               |            |            |                         |                              |                                   |                              | Residu                            | al Strength Wei     |                         |                         |                         |   |                         |                                   |                                  |                         |                               |  |                                   |                         |
|                      |               | Seisn      | nic Parame | eters                   |                              |                                   |                              |                                   |                     | WSDOT:                  | 0                       |                         |   |                         |                                   |                                  | Liquefac                | tion and R                    | esidual Sh   | ear Streng                        | th Analysis             |

Seismic Parameters

Max Acceleration (As) (g): 0.520

Earthquake Magnitude: 6.97

WSDOT: 0
Olsen & Stark (2002): 0.2
Idriss & Boulanger Void Redistribution (2007): 0.2
Idriss & Boulanger No Void Redistribution (2007): 0
Kramer, Wang Hybrid (2008): 0.4

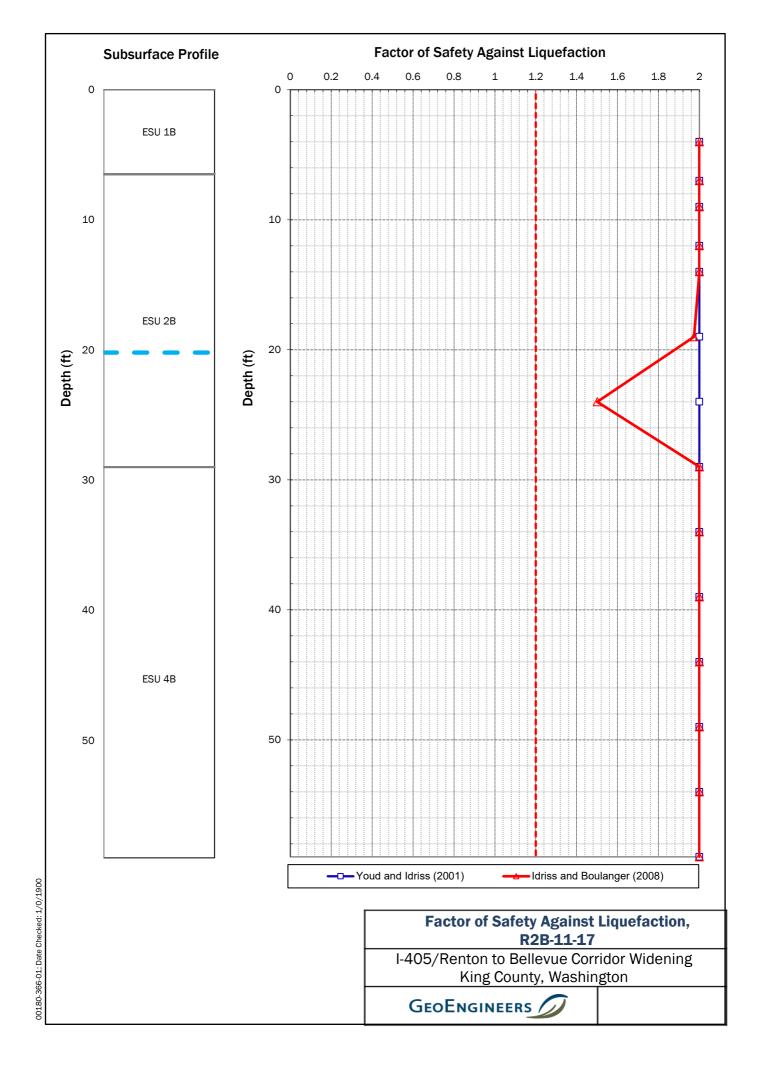
Idriss et al. (1998):

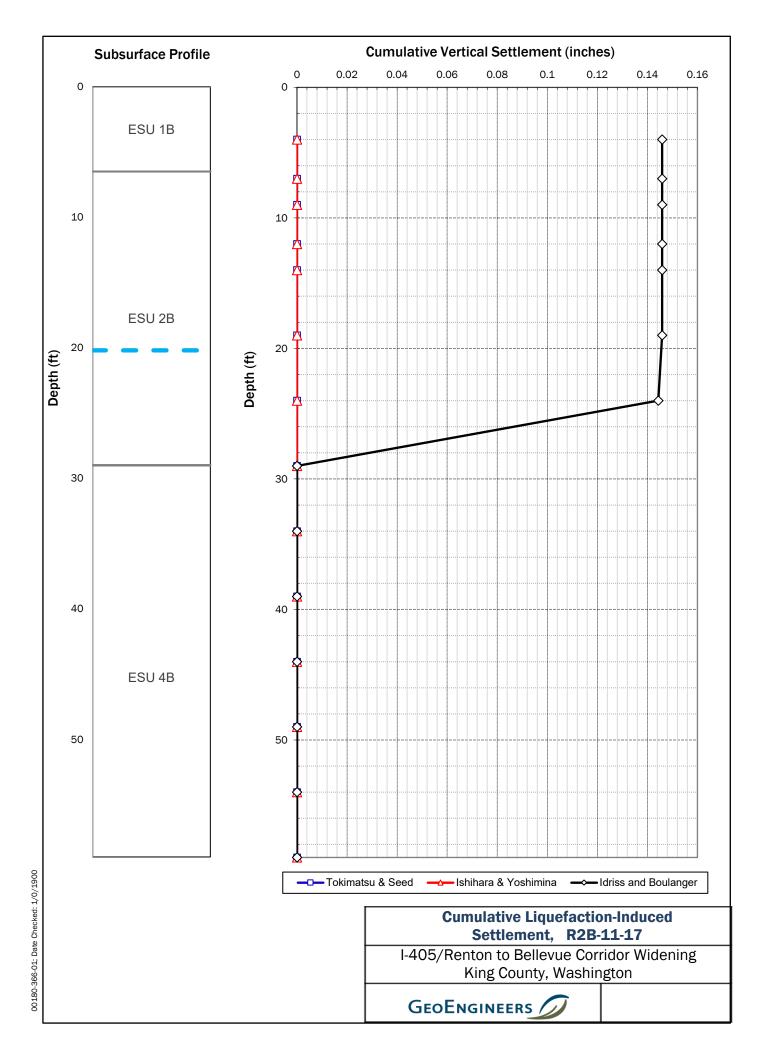
0.2

Liquefaction and Residual Shear Strength Analysis Results, R2B-11-17

I-405/Renton to Bellevue Corridor Widening King County, Washington







# **Lateral Earth Pressures for Cohesionless Soils**

#### **Project Information**

| Project:     | I-405/Renton to Bellevue Corridor Widening |
|--------------|--|
| Owner:       | WSDOT                                      |
| Job Number:  | 00180-366-01                               |
| Analysis by: | YTT  |
| Date/Time:   | 1/11/2022 3:35 PM                          |
| Checked by:  | ТВ   |

#### **Input Parameters**

| Material | φ<br>Friction Angle<br>(deg) | β <sub>2</sub> (-)<br>Foreslope<br>(deg) | i (+)<br>Backslope<br>(deg) | δ<br>Wall Friction - Active<br>(deg) | δ<br>Wall Friction - Passive<br>(deg) | β<br>Wall Batter<br>(deg) | γ <sub>m</sub><br>(pcf) | γ <sub>b</sub> (pcf) | Passive<br>Factor of<br>Safety | k <sub>h</sub><br>(g) | k <sub>v</sub> (g) |
|----------|------------------------------|--|-----------------------------|--------------------------------------|---------------------------------------|---------------------------|-------------------------|----------------------|--------------------------------|-----------------------|--------------------|
| ESU 2B   | 34                           | -15                                      | 27                          | 23                                   | 0                                     | 0                         | 115                     | 52.6                 | 1                              | 0                     | 0                  |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       |                    |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       |                    |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       |                    |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       |                    |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       |                    |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       |                    |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       |                    |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       |                    |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       |                    |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       |                    |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       |                    |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       |                    |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       |                    |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       |                    |
|          |                              |  |                             |                                      |                                       |                           | -                       |                      |                                |                       |                    |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       |                    |
|          |                              |  |                             |                                      |                                       |                           |                         |                      |                                |                       |                    |

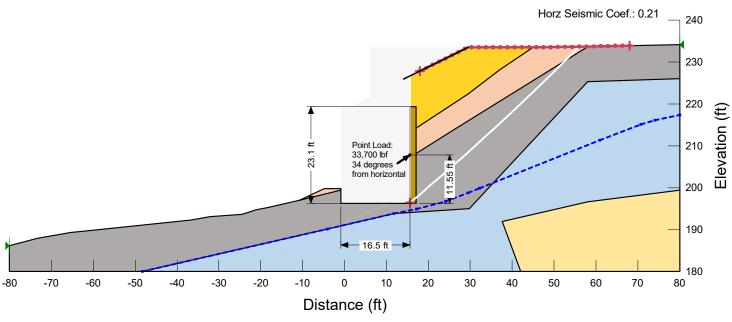
#### **Lateral Earth Pressures**

#### Output

|          |      | <u>Active</u>           |                          |       |                              | <u>Pa</u>                     | ssive                         |                                |                | At Rest                 |              |                             | EP Trapezoid                    |                 | <u>s</u>                 | eismic_                   | 1        | Seismic Pressure -       |
|----------|------|-------------------------|--------------------------|-------|------------------------------|-------------------------------|-------------------------------|--------------------------------|----------------|-------------------------|--------------|-----------------------------|---------------------------------|-----------------|--------------------------|---------------------------|----------|--------------------------|
| Material | Ka   | γ <sub>a</sub><br>(pcf) | γ' <sub>a</sub><br>(pcf) | $K_p$ | γ <sub>p(all)</sub><br>(pcf) | γ' <sub>p(all)</sub><br>(pcf) | γ <sub>pe(all)</sub><br>(pcf) | γ' <sub>pe(all)</sub><br>(pcf) | K <sub>o</sub> | γ <sub>o</sub><br>(pcf) | γ'。<br>(pcf) | Single Tieback<br>(psf * H) | Mult. Tiebacks <sup>1</sup> , X | K <sub>ae</sub> | γ <sub>ae</sub><br>(pcf) | γ' <sub>ae</sub><br>(pcf) | $K_{pe}$ | Rectangular<br>(psf * H) |
| ESU 2B   | 0.41 | 46.87                   | 21.44                    | 2.15  | 246.85                       | 112.91                        | 742.90                        | 339.80                         | 0.44           | 50.69                   | 23.19        | 46.87                       | 46.87                           | 0.41            | 46.87                    | 21.44                     | 6.46     | 0.00                     |
|          |      |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|          |      |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|          |      |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|          |      |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|          |      |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|          |      |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|          |      |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|          |      |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|          |      |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|          |      |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|          |      |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|          |      |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|          |      |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|          |      |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|          |      |                         |                          |       |                              |                               |                               |                                |                |                         |              |                             |                                 |                 |                          |                           |          |                          |
|          |      |                         | l                        | l     | ·                            | l                             |                               |                                |                |                         |              | <u> </u>                    |                                 |                 | l                        |                           |          | 1                        |



| Color | Name   | Material Model | Unit<br>Weight<br>(pcf) | Effective<br>Cohesion<br>(psf) | Effective<br>Friction<br>Angle (°) |
|-------|--|----------------|-------------------------|--------------------------------|------------------------------------|
|       | Common Borrow (Apparent Cohesion)                                | Mohr-Coulomb   | 120                     | 50                             | 32                                 |
|       | ESU 1B Medium Dense to Very Dense<br>Coarse-Grained Fill         | Mohr-Coulomb   | 130                     | 0                              | 41                                 |
|       | ESU 2B Medium Dense Sand/Gravel                                  | Mohr-Coulomb   | 115                     | 0                              | 34                                 |
|       | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | Mohr-Coulomb   | 130                     | 0                              | 43                                 |
|       | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | Mohr-Coulomb   | 130                     | 0                              | 42                                 |
|       | Gravel Borrow  | Mohr-Coulomb   | 130                     | 0                              | 38                                 |



1. The locations of all features shown are approximate.

- This drawing is for information purposes. It is intended to assist in showing features discussed in an attached document.
- GeoEngineers, Inc. cannot guarantee the accuracy and context of electronic files. The master file is stored by GeoEngineers, Inc. and will serve as the official record of this communication.

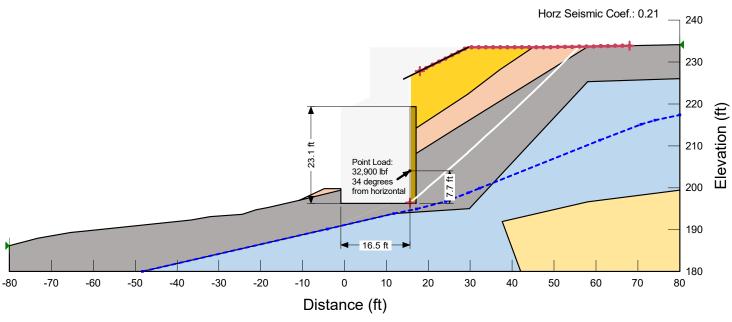
Wall 05.85L-B - Sta. 2+60 LEP - GLE Approach (Spencer, 1/2H)

I-405/Renton to Bellevue Corridor Widening King County, Washington



1.0

| Color | Name   | Material Model | Unit<br>Weight<br>(pcf) | Effective<br>Cohesion<br>(psf) | Effective<br>Friction<br>Angle (°) |
|-------|--|----------------|-------------------------|--------------------------------|------------------------------------|
|       | Common Borrow (Apparent Cohesion)                                | Mohr-Coulomb   | 120                     | 50                             | 32                                 |
|       | ESU 1B Medium Dense to Very Dense<br>Coarse-Grained Fill         | Mohr-Coulomb   | 130                     | 0                              | 41                                 |
|       | ESU 2B Medium Dense Sand/Gravel                                  | Mohr-Coulomb   | 115                     | 0                              | 34                                 |
|       | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | Mohr-Coulomb   | 130                     | 0                              | 43                                 |
|       | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | Mohr-Coulomb   | 130                     | 0                              | 42                                 |
|       | Gravel Borrow  | Mohr-Coulomb   | 130                     | 0                              | 38                                 |



1. The locations of all features shown are approximate.

- This drawing is for information purposes. It is intended to assist in showing features discussed in an attached document.
- GeoEngineers, Inc. cannot guarantee the accuracy and context of electronic files. The master file is stored by GeoEngineers, Inc. and will serve as the official record of this communication.

Wall 05.85L-B - Sta. 2+60 LEP - GLE Approach (Spencer, 1/3H)

I-405/Renton to Bellevue Corridor Widening King County, Washington



1.0

Project: 405 Renton to Bellveue By: YT Checked By: TB

#### Project Number: <u>00180-366-01</u> Date: 10/01/21 Page 1 of 1

#### Seismic Earth Pressure Calculation Wall 05.85L-B

Active and seismic earth pressures using the limit equilibrium method outlined in NCHRP Report 611 Section 4.2.1 (Anderson et al., 2008) per AASHTO A11.3.3.

Earth pressures were developed from the bottom of footing to ground surface. Different application location of the force at one-third from the base (1/3H, where H is retained soil height) and at one half from the base were examined to determine the maximum seismic earth pressure. Spencer's methods was used to verify Pa and Pae.

Friction angle of the ESU 2B is used to define the inclination fo the applied point load in the model.

 $\phi = 34$ 

Friction angle of ESU 2B

$$P_{AE2} = 33700 \ \frac{\textbf{lbf}}{\textbf{ft}}$$

Location of force = 1/2H

$$P_{AE3} = 32900 \ \frac{\textit{lbf}}{\textit{ft}}$$

Location of force = 1/3H

(See slopeW output attached)

Given:  $\gamma := 115 \ pcf$ 

 $H \coloneqq 23.1 \ \mathbf{ft}$ 

Height of wall

$$k_n = 0$$

$$k_v = 0$$
  $k_h = 0.21$ 

Half of PGA applied for flexible system, PGA reduced to 0.42g for wave scatter effects.

$$K_{AE2} \coloneqq \frac{P_{AE2} \cdot 2}{\gamma \cdot H^2 \cdot (1 - k_v)} = 1.1$$

Location of force = 1/2H

$$K_{AE3} = \frac{P_{AE3} \cdot 2}{\gamma \cdot H^2 \cdot (1 - k_v)} = 1.07$$

Location of force = 1/3H

Seismic+active earth pressures

$$\max \left( \gamma \cdot K_{AE2}, \gamma \cdot K_{AE3} \right) = 126 \frac{lbf}{ft^3}$$



# **Sliding Coefficients of Friction**

| Foundation Soil Type | φ' | Discontinuous Reinforcements |
|----------------------|----|------------------------------|
| ESU 2B               | 34 | 0.67                         |
| Common Borrow        | 32 | 0.62                         |
| Select Borrow        | 36 | 0.73                         |
| Gravel Borrow        | 38 | 0.78                         |

#### Notes:

Sliding coefficients calculated according to AASHTO Equation 10.6.3.4-2

Structural Earth Walls (SEW) are termed Mechanically Stabilized Earth (MSE) walls in AASHTO.

#### Coefficient of Friction for Discontinuous Reinforcements, e.g., Strips:

Coefficient of friction = 1.0\*tan(Phi')

Phi' = lesser of friction angle of foundation soil and friction angle of reinforced fill per AASHTO 11.10.5.3

#### **AASHTO 10.6.3.4:**

$$R_{\tau} = CV \tan \phi_f \qquad (10.6.3.4-2)$$

for which:

C = 1.0 for MSE Wall per AASHTO Table 11.5.7-1

where:

 $\phi_f$  = internal friction angle of drained soil

(degrees)

V = total vertical force (kips)

#### LRFD Foundation Design

#### Spreadsheet Reference Section 10.6.3.1.2 of The 2014 AASHTO LRFD Bridge Design Specifications

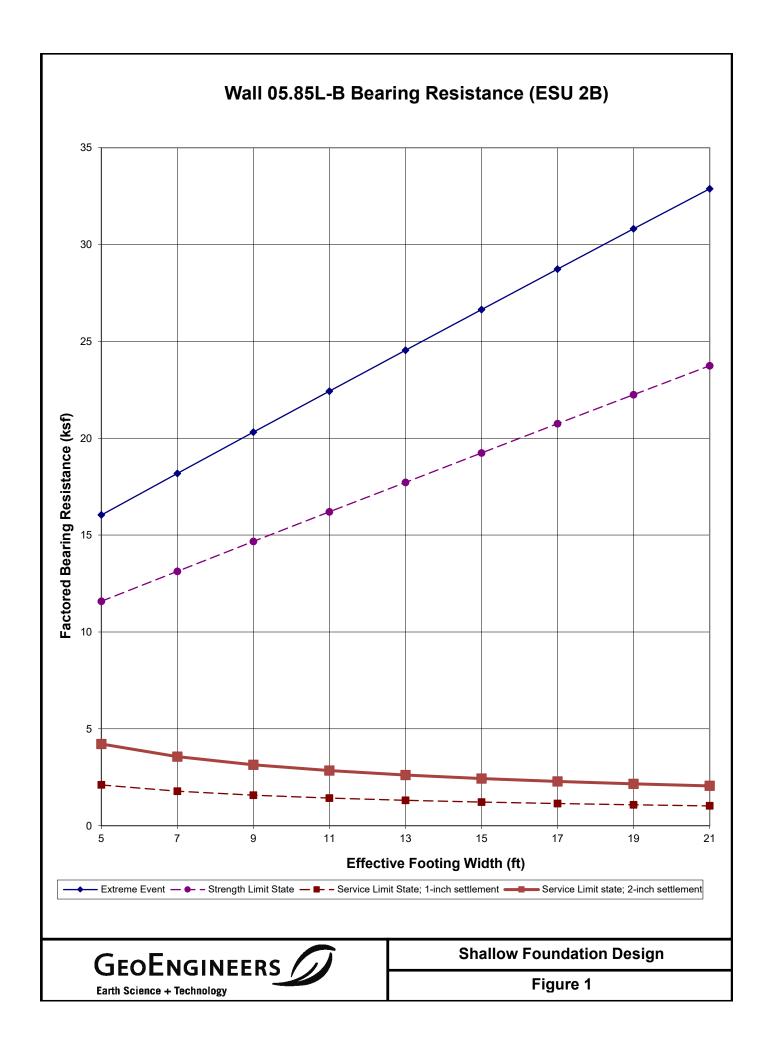
| Date/Time:    | 1/11/22 11:07 AM  |
|---------------|---|
| Project Name: | I-405/Renton to Bellevue Corridor Widening - Wall 05.85L-B (ESU 2B) |
| Project No.:  | 00180-366-01  |

| Foundation Soil Conditions           Unit Weight, γ (pcf)         115           Friction angle, Φ (degrees)         34           Friction angle, Φ (rad)         0.593           Cohesion, C (psf)         0           Embedment, D <sub>r</sub> (ft)         3.5           Depth to Groundwater, D <sub>w</sub> (ft)         1.8           Footing Length, L (ft)         340           Footing Width, B (ft)         1 |       |  |  |
|--|-------|--|--|
| Unit Weight, γ (pcf)   | 115   |  |  |
| Friction angle, Φ (degrees)  | 34    |  |  |
| Friction angle, Φ (rad)  | 0.593 |  |  |
| Cohesion, C (psf)  | 0     |  |  |
| Embedment, D <sub>f</sub> (ft)   | 3.5   |  |  |
| Depth to Groundwater, D <sub>w</sub> (ft)  | 1.8   |  |  |
| Footing Length, L (ft)   | 340   |  |  |
| Footing Width, B (ft)  | 1     |  |  |
| Poissons Ration, v   | 0.33  |  |  |
| Young's Modulus, E <sub>s</sub> (ksf)  | 660   |  |  |

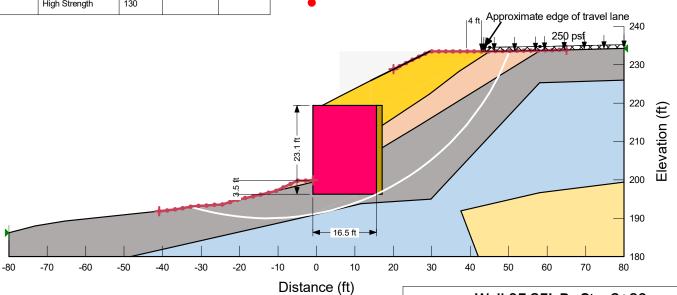
| Bearing Capacity Factor | ors . |
|-------------------------|-------|
| N <sub>Y</sub>          | 41    |
| N <sub>c</sub>          | 42    |
| $N_q$                   | 29    |

|                            | Water Dep             | th Factors             | Shape Factors |                       |      | Unfactored            | Extreme Event Resistance   | Working Bearing Resistance                                    | Deflection from Elastic<br>Settlement Spreadsheet | Deflection from Elastic<br>Settlement Spreadsheet |
|----------------------------|-----------------------|------------------------|---------------|-----------------------|------|-----------------------|--|---|---|---|
| Effective Footing Width, B | <u>C<sub>wq</sub></u> | <u>C<sub>w-y</sub></u> | <u>Sc</u>     | <u>S</u> <sub>y</sub> | Sq   | Bearing<br>Resistance | Resistance Factor (0.9) for MSE walls (Section<br>11.5.8 AASHTO) | Resistance Factor (0.65) for MSE walls (Table Table 11.5.7-1) | 1" Deflection                                     | 2" Deflection                                     |
| (ft)                       |                       |                        |               |                       |      | (ksf)                 | (ksf)  | (ksf)   | (ksf)   | (ksf)   |
| 5.0                        | 1.0                   | 0.5                    | 1.01          | 0.99                  | 1.01 | 17.8                  | 16.0   | 11.6  | 2.1   | 4.2   |
| 7.0                        | 1.0                   | 0.5                    | 1.01          | 0.99                  | 1.01 | 20.2                  | 18.2   | 13.1  | 1.8   | 3.6   |
| 9.0                        | 1.0                   | 0.5                    | 1.02          | 0.99                  | 1.02 | 22.6                  | 20.3   | 14.7  | 1.6   | 3.1   |
| 11.0                       | 1.0                   | 0.5                    | 1.02          | 0.99                  | 1.02 | 24.9                  | 22.4   | 16.2  | 1.4   | 2.8   |
| 13.0                       | 1.0                   | 0.5                    | 1.03          | 0.98                  | 1.03 | 27.3                  | 24.5   | 17.7  | 1.3   | 2.6   |
| 15.0                       | 1.0                   | 0.5                    | 1.03          | 0.98                  | 1.03 | 29.6                  | 26.6   | 19.2  | 1.2   | 2.4   |
| 17.0                       | 1.0                   | 0.5                    | 1.03          | 0.98                  | 1.03 | 31.9                  | 28.7   | 20.7  | 1.1   | 2.3   |
| 19.0                       | 1.0                   | 0.5                    | 1.04          | 0.98                  | 1.04 | 34.2                  | 30.8   | 22.2  | 1.1   | 2.2   |
| 21.0                       | 1.0                   | 0.5                    | 1.04          | 0.98                  | 1.04 | 36.5                  | 32.9   | 23.7  | 1.0   | 2.1   |
|                            |                       |                        |               |                       |      |                       |  |   |   |   |
|                            |                       |                        |               |                       |      |                       |  |   |   |   |

Note: Depth and inclination modifier were taken as 1 because the load is applied axially and during construction the soils above the footing are to be excavated.



| Color | Name   | Material Model | Unit<br>Weight<br>(pcf) | Effective<br>Cohesion<br>(psf) | Effective<br>Friction<br>Angle (°) |
|-------|--|----------------|-------------------------|--------------------------------|------------------------------------|
|       | Common Borrow  | Mohr-Coulomb   | 120                     | 0                              | 32                                 |
|       | ESU 1B Medium Dense to Very Dense<br>Coarse-Grained Fill         | Mohr-Coulomb   | 130                     | 0                              | 41                                 |
|       | ESU 2B Medium Dense Sand/Gravel                                  | Mohr-Coulomb   | 115                     | 0                              | 34                                 |
|       | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | Mohr-Coulomb   | 130                     | 0                              | 43                                 |
|       | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | Mohr-Coulomb   | 130                     | 0                              | 42                                 |
|       | Gravel Borrow  | Mohr-Coulomb   | 130                     | 0                              | 38                                 |
|       | SEW Wall   | High Strength  | 130                     |                                |                                    |



1. The locations of all features shown are approximate.

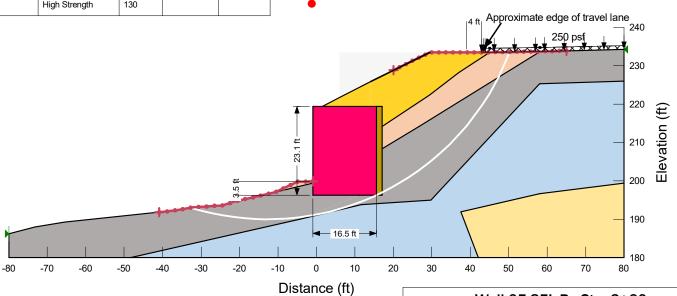
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Wall 05.85L-B - Sta. 2+60 Static Global Stability (Spencer)

I-405/Renton to Bellevue Corridor Widening King County, Washington



| Color | Name   | Material Model | Unit<br>Weight<br>(pcf) | Effective<br>Cohesion<br>(psf) | Effective<br>Friction<br>Angle (°) |
|-------|--|----------------|-------------------------|--------------------------------|------------------------------------|
|       | Common Borrow  | Mohr-Coulomb   | 120                     | 0                              | 32                                 |
|       | ESU 1B Medium Dense to Very Dense<br>Coarse-Grained Fill         | Mohr-Coulomb   | 130                     | 0                              | 41                                 |
|       | ESU 2B Medium Dense Sand/Gravel                                  | Mohr-Coulomb   | 115                     | 0                              | 34                                 |
|       | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | Mohr-Coulomb   | 130                     | 0                              | 43                                 |
|       | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | Mohr-Coulomb   | 130                     | 0                              | 42                                 |
|       | Gravel Borrow  | Mohr-Coulomb   | 130                     | 0                              | 38                                 |
|       | SEW Wall   | High Strength  | 130                     |                                |                                    |



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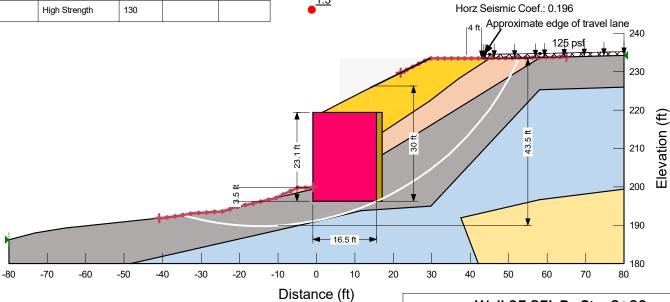
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Wall 05.85L-B - Sta. 2+60 Static Global Stability (M-P)

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| Color | Name   | Material Model | Unit<br>Weight<br>(pcf) | Effective<br>Cohesion<br>(psf) | Effective<br>Friction<br>Angle (°) |
|-------|--|----------------|-------------------------|--------------------------------|------------------------------------|
|       | Common Borrow (Apparent Cohesion)  | Mohr-Coulomb   | 120                     | 50                             | 32                                 |
|       | ESU 1B Medium Dense to Very Dense<br>Coarse-Grained Fill (Apparent Cohesion) | Mohr-Coulomb   | 130                     | 100                            | 41                                 |
|       | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                          | Mohr-Coulomb   | 115                     | 200                            | 34                                 |
|       | ESU 4B Dense to Very Dense Sand/Gravel                                       | Mohr-Coulomb   | 130                     | 0                              | 43                                 |
|       | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt             | Mohr-Coulomb   | 130                     | 0                              | 42                                 |
|       | Gravel Borrow  | Mohr-Coulomb   | 130                     | 0                              | 38                                 |
|       | SEW Wall   | High Strength  | 130                     |                                |                                    |



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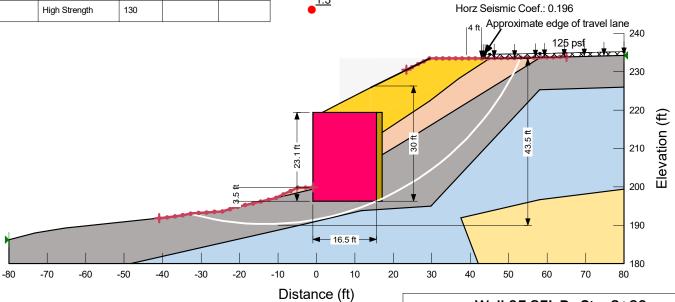
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| Color | Name   | Material Model | Unit<br>Weight<br>(pcf) | Effective<br>Cohesion<br>(psf) | Effective<br>Friction<br>Angle (°) |
|-------|--|----------------|-------------------------|--------------------------------|------------------------------------|
|       | Common Borrow (Apparent Cohesion)  | Mohr-Coulomb   | 120                     | 50                             | 32                                 |
|       | ESU 1B Medium Dense to Very Dense<br>Coarse-Grained Fill (Apparent Cohesion) | Mohr-Coulomb   | 130                     | 100                            | 41                                 |
|       | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                          | Mohr-Coulomb   | 115                     | 200                            | 34                                 |
|       | ESU 4B Dense to Very Dense Sand/Gravel                                       | Mohr-Coulomb   | 130                     | 0                              | 43                                 |
|       | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt             | Mohr-Coulomb   | 130                     | 0                              | 42                                 |
|       | Gravel Borrow  | Mohr-Coulomb   | 130                     | 0                              | 38                                 |
|       | SEW Wall   | High Strength  | 130                     |                                |                                    |



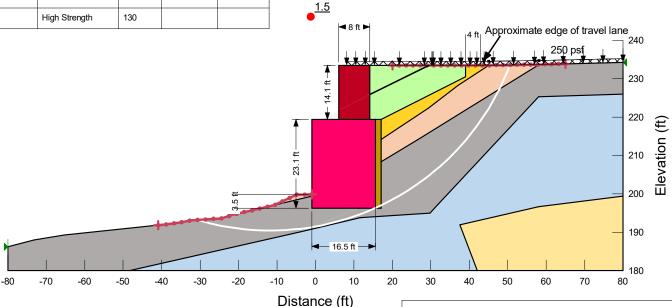
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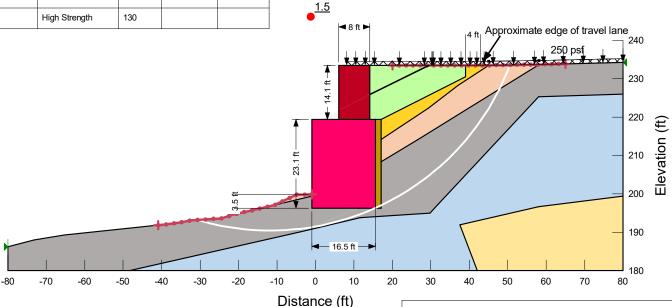
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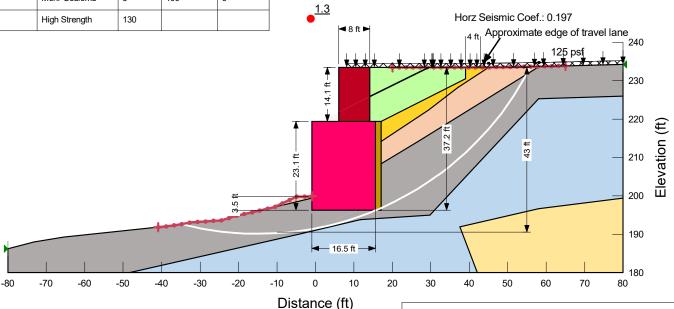
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Wall 05.85L-B - Sta. 2+60 Static Global Stability + FC Wall (M-P)

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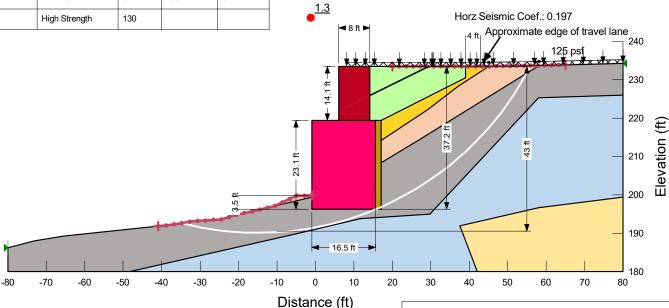
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Wall 05.85L-B - Sta. 2+60 Pseudo-Static Global Stability + FC Wall (S)

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Wall 05.85L-B - Sta. 2+60 Pseudo-Static Global Stability + FC Wall (M-P)

I-405/Renton to Bellevue Corridor Widening King County, Washington



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#### Calculating MSE Strip Properties for Slope/W (Wall 05.85L-B Sta. 2+60)

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For global stability analyses, the MSE wall is modeled as a high strength material and the failure is forced outside of the reinforced zone. To check for compound stability, the high strength material is replaced with gravel borrow and reinforcing strips. The properties of the metal strips are calculated based on FHWA NHI-10-024 and NHI-10-025. The reinforcement properties are converted to per unit width basis, and implemented as a continous layer in Slope/W.

#### **Input Soil Properties:**

Backfill meeting WSDOT standard specifications 9-03.14(4), Gravel Borrow for Structural Earth Wall.

$$\phi_{gravel} = 38 \ deg$$

#### **Input Strip Properties:**

50mm wide and 4mm thick with Grade 65 steel.

width = 2 in

$$thickness := \frac{5}{32}$$
 in Gross thickness (no corrosion)

$$f_y = 65.0 \text{ } ksi$$
 Yield stress

#### **Calculate Corrosion Reduction:**

Calculate new cross-sectional area of steel straps after 75 years of corrosion exposure.

| Catagoria   | Stee1                          | Minimum Galvanization |  |  |
|---|--------------------------------|-----------------------|--|--|
| Category  | Thickness                      | Thickness             |  |  |
| Strip   | < 1/4 in. (6.4 mm)             | 3.4 mils (85 µm)      |  |  |
|   | > 1/4 in. (6.4 mm)             | 3.9 mils (100 µm)     |  |  |
| Wire*   | All diameters 3.4 mils (85 μm) |                       |  |  |
| * For bar mats fabricated from uncoated steel wire. |                                |                       |  |  |

The corrosion rates presented in Table 3-8 are suitable for conservative design. These rates assume a moderately corrosive backfill material having the controlled electrochemical property limits that are discussed under electrochemical properties in this chapter.

Table 3-8 Steel Corrosion Rates for Moderately Corrosive Reinforced Fill.

|                                 | 0.58 mils/yr (15 µm/year) (first 2 years)<br>0.16 mils/yr (4 µm/year) (thereafter) |  |
|---------------------------------|--|--|
|                                 |  |  |
| For residual carbon steel/side: | 0.47 mils/yr (12 µm/year) (thereafter)   |  |

Calculate time (in years) to corrode through galvinization.

$$0.58 \cdot 2 + 0.16 \cdot (t_g - 2) = 3.4$$

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$$t_g := \frac{3.4 - 0.58 \cdot 2}{0.16} + 2 = 16$$

$$t_{75\_years}\!\coloneqq\!thickness-0.47\boldsymbol{\cdot}0.001\ \frac{\textit{in}}{\textit{yr}}\boldsymbol{\cdot}\left(75-t_g\right)\ \textit{yr}\boldsymbol{\cdot}2\!=\!0.101\ \textit{in}$$

$$A_c \coloneqq width \cdot t_{75\ years} = 0.202\ in^2$$

New cross-sectional area after 75 years of corrosion exposure

# LRFD Resistance Factors for Tensile and Pullout Resistance for MSE Walls with Metal Straps:

Table 4-7. Resistance Factors, φ, for Tensile and Pullout Resistance for MSE Walls (after Table 11.5.6-1, AASHTO {2007}).

| Reinforcement Type and Loading Condition     |  |      |
|--|--|------|
|  | Strip reinforcements (A)                   |      |
|  | Static loading                             | 0.75 |
|  | Combined static/earthquake loading         | 1.00 |
| Metallic reinforcement and                   | Combined static/traffic barrier impact (B) | 1.00 |
| connectors                                   | Grid reinforcements (A, C)                 |      |
|  | Static loading                             | 0.65 |
|  | Combined static/earthquake loading         | 0.85 |
|  | Combined static/traffic barrier impact (B) | 0.85 |
|  | Static loading                             | 0.90 |
| Geosynthetic reinforcement<br>and connectors | Combined static/earthquake loading         | 1.20 |
| and connectors                               | Combined static/traffic barrier impact (B) | 1.20 |
| Pullout resistance of tensile                | Static loading                             | 0.90 |
| reinforcement (metallic and                  | Combined static/earthquake loading         | 1.20 |
| geosynthetic)                                | Combined static/traffic barrier impact (B) | 1.00 |

#### Notes:

- A. Apply to gross cross-section less sacrificial area. For sections with holes, reduce gross area in accordance with AASHTO (2007) Article 6.8.3 and apply to net section less sacrificial area.
- B. Combined static/traffic barrier impact resistance factors are not presented in AASHTO.
- C. Applies to grid reinforcements connected to rigid facing element, e.g., a concrete panel or block. For grid reinforcements connected to a flexible facing mat or which are continuous with the facing mat, use the resistance factor for strip reinforcements.

$$\Phi_{static} \coloneqq 0.75 \qquad \qquad \Phi_{pullout\_static} \coloneqq 0.9$$

$$\varPhi_{seismic} \coloneqq 1.0 \qquad \qquad \varPhi_{pullout\_seismic} \coloneqq 1.2$$

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#### **Calculate Slope/W Reinforcement Inputs:**

$$H_{wall} = 23.1 \, ft$$

Assuming strip layout based on typical RECO A panel, the vertical  $(s_v)$  and the horizontal  $(s_h)$  spacing of the steel straps within each SE wall panel was determined. For calculation efficiency, the calculations are performed using matrices.

$$s_v \coloneqq egin{bmatrix} 0.5 \ 2.4 \ 2.4 \ 2.4 \ 2.4 \ 2.4 \ 2.4 \ 2.4 \ 2.4 \ 2.4 \ 2.4 \ 2.4 \ 2.5 \ 2$$

The matrix respresents the same order of the SE Wall reinforcement. Top row of the matrix represents the bottom row of the SE Wall reinforcement and the bottom row of the matrix represents the row of reinforcement closest to the ground surface.

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$$i = 0 \dots \operatorname{length}(s_v) - 1$$

Calculate number of elements

$$elevation_{i}\coloneqq\sum_{j=0}^{i}s_{v_{j}}=\begin{bmatrix}0.5\\2.9\\5.3\\7.7\\10.1\\12.5\\14.9\\17.3\\19.7\\22.1\end{bmatrix}\boldsymbol{ft}$$

Calculate each strap's vertical elevation, with the base of the wall as elevation 0 ft. Top row of the matrix represents the bottom reinforcement row.

Calculate each strap's depth from the ground surface.

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#### Calculate Pullout Resistance Slope/W Input:

For design and comparison purposes, a normalized definition of pullout resistance will be used throughout the manual. The pullout resistance, Pr, at each of the reinforcement levels per unit width of reinforcement is given by:

$$\mathbf{P}_{r} = \mathbf{F} + \alpha \sigma'_{r} \mathbf{L}_{r} \mathbf{C} \tag{3-2}$$

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where:

L<sub>e</sub> C = the total surface area per unit width of the reinforcement in the resistive zone behind the failure surface

L<sub>e</sub> = the embedment or adherence length in the resisting zone behind the failure

C = the reinforcement effective unit perimeter; e.g., C = 2 for and sheets, and because the edges are neglected C = 2 for strips and grids

 $F^*$  = the pullout resistance (or friction-bearing-interaction) factor

α = a scale effect correction factor to account for a non linear stress reduction over the embedded length of highly extensible reinforcements, based on laboratory data (generally 1.0 for metallic reinforcements and 0.6 to 1.0 for geosynthetic reinforcements, see Table 3-6).

 $\sigma'_v$  = the effective vertical stress at the soil-reinforcement interfaces.

The <u>factored</u> pullout resistance <u>per unit width of the wall</u> is then given by:

$$P_r = \Phi_{pullout} \left( F \boldsymbol{\cdot} \alpha \boldsymbol{\cdot} \sigma_v' \boldsymbol{\cdot} L_e \boldsymbol{\cdot} C \right) \boldsymbol{\cdot} \frac{width}{s_h}$$

In Slope/W, pullout resistance per unit width of wall is given by:

$$P_r = \left(c + \sigma_v' \cdot tan\left(\phi_{interface}\right)\right) \cdot \alpha \cdot L_e \cdot C$$

Where  $\alpha$  and C can be defined within the reinforcement properties, and are set to be the same as defined above. Overburden pressure,  $\sigma_{v}{}'$  and effective length, Le are determined from the limit equilibrium analysis performed in Slope/W. Interface adhesion, c, is assumed to be negligable for metal straps in granular backfill.

To select a representative  $\phi_{interface}$  that will produce the same factored resistance per unit width of wall, the two expressions are set to be equal:

$$\varPhi_{pullout}\left(F\boldsymbol{\cdot}\alpha\boldsymbol{\cdot}\sigma_{v}{'}\boldsymbol{\cdot}L_{e}\boldsymbol{\cdot}C\right)\boldsymbol{\cdot}\frac{width}{s_{h}}\boldsymbol{=}\sigma_{v}{'}\boldsymbol{\cdot}tan\left(\phi_{interface}\right)\boldsymbol{\cdot}\alpha\boldsymbol{\cdot}L_{e}\boldsymbol{\cdot}C$$

Removing common constants and rearranging produces:

$$\phi_{interface} = atan \left( \frac{\Phi_{pullout} \cdot F \cdot width}{s_h} \right)$$

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#### Calculate Pullout Resistance Factor F\*:

In the absence of site-specific pullout testing data, it is reasonable to use the semi-empirical relationships described in the following paragraphs in conjunction with the standard specifications for reinforced fill to provide a conservative evaluation of pullout resistance.

For steel ribbed reinforcement, the Pullout Resistance Factor F\* is commonly taken as:

$$F^* = \tan \rho = 1.2 + \log C_u$$
 at the top of the structure = 2.0 maximum (3-4)

$$F^* = \tan \phi$$
 at a depth of 20 ft (6 m) and below (3-5)

where  $C_u$  is the uniformity coefficient of the backfill ( $D_{60}/D_{10}$ ). If the specific  $C_u$  for the wall backfill is unknown at design time, a  $C_u = 4$  should be assumed (i.e.,  $F^* = 1.8$  at the top of the wall) for reinforced fills meeting the requirements of Section 3.1 of this chapter.

$$C_u = 6.3$$

Backfill used will need to meet gradation assumed

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$$F_{max} = 1.2 + \log(C_u) = 1.999$$

$$F = \begin{bmatrix} 0.78 \\ 0.78 \\ 0.92 \\ 1.06 \\ 1.21 \\ 1.35 \\ 1.5 \\ 1.65 \\ 1.79 \\ 1.94 \end{bmatrix}$$

Calculated F\* for each row of reinforcement. Top row of matrix represents the bottom row of reinforcement.

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#### Calculate Interface Shear Angle (degrees):

$$\phi_{interface\_static} \coloneqq \operatorname{atan} \left( \frac{\phi_{pullout\_static} \cdot F \cdot width}{s_h} \right) = \begin{bmatrix} 2.7 \\ 2.7 \\ 3.1 \\ 3.6 \\ 4.1 \\ 4.6 \\ 5.1 \\ 5.6 \\ 6.1 \\ 6.6 \end{bmatrix} \mathbf{\textit{deg}}$$

Static interface shear angle for each row of reinforcement. Top row of matrix represents the bottom reinforcement row.

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$$\phi_{interface\_seismic} \coloneqq \operatorname{atan} \left( \frac{\phi_{pullout\_seismic} \cdot F \cdot width}{s_h} \right) = \begin{bmatrix} 3.6 \\ 3.6 \\ 4.2 \\ 4.9 \\ 5.5 \\ 6.2 \\ 6.8 \\ 7.5 \\ 8.2 \\ 8.8 \end{bmatrix}$$

Seismic interface shear angle for each row of reinforcement. Top row of matrix represents the bottom reinforcement row.

#### **Calculate Allowable Tensile Capacity of Steel Straps:**

$$T_{al\_static}\!\coloneqq\! \varPhi_{static}\!\cdot\! f_y\; A_c\!=\!9.83\; \pmb{kip}$$

$$T_{al\ seismic} := \Phi_{seismic} \cdot f_y A_c = 13.1 \ kip$$

Slope/W does not have strap reinforcement inputs. Therefore, the tensile strength of the straps were modeled as continuous reinforcement. The calculated allowable tensile strap capacity was converted to a continuous reinforcement tensile capcity by distributing the capacity over the tributary width.

$$T_{al\_static\_row} \coloneqq rac{T_{al\_static}}{s_h} = egin{bmatrix} 3.93 \\ 3$$

Static tensile capacity Slope/W inputs for each wall reinforcement row. Top row of the matrix represents the bottowm row of the SE Wall reinforcement.

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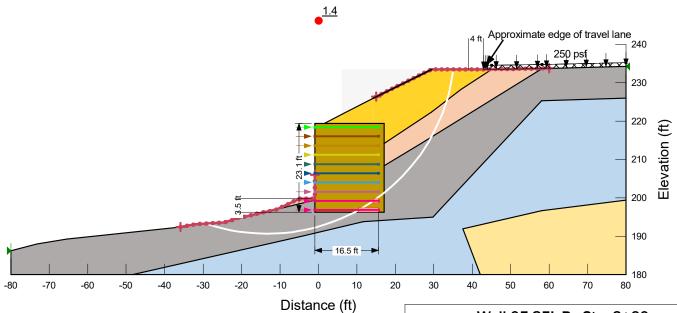
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| $egin{bmatrix} 5.24 \ 5.24 \ 5.24 \end{bmatrix}$ |
|--|
|--|

Seismic tensile capacity Slope/W inputs for each wall reinforcement row. Top row of the matrix represents the bottowm row of the SE Wall reinforcement.

| Color | Name   | Material Model | Unit<br>Weight<br>(pcf) | Effective<br>Cohesion<br>(psf) | Effective<br>Friction<br>Angle (°) |
|-------|--|----------------|-------------------------|--------------------------------|------------------------------------|
|       | Common Borrow  | Mohr-Coulomb   | 120                     | 0                              | 32                                 |
|       | ESU 1B Medium Dense to Very<br>Dense Coarse-Grained Fill         | Mohr-Coulomb   | 130                     | 0                              | 41                                 |
|       | ESU 2B Medium Dense<br>Sand/Gravel                               | Mohr-Coulomb   | 115                     | 0                              | 34                                 |
|       | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | Mohr-Coulomb   | 130                     | 0                              | 43                                 |
|       | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | Mohr-Coulomb   | 130                     | 0                              | 42                                 |
|       | Gravel Borrow  | Mohr-Coulomb   | 130                     | 0                              | 38                                 |

| Color | Name              | Interface<br>Shear<br>Angle (°) | Tensile<br>Capacity<br>(lbf) |
|-------|-------------------|---------------------------------|------------------------------|
|       | Row 1 (2 strips)  | 6.6                             | 3,930                        |
|       | Row 2 (2 strips)  | 6.1                             | 3,930                        |
|       | Row 3 (2 strips)  | 5.6                             | 3,930                        |
|       | Row 4 (2 strips)  | 5.1                             | 3,930                        |
|       | Row 5 (2 strips)  | 4.6                             | 3,930                        |
|       | Row 6 (2 strips)  | 4.1                             | 3,930                        |
|       | Row 7 (2 strips)  | 3.6                             | 3,930                        |
|       | Row 8 (2 strips)  | 3.1                             | 3,930                        |
|       | Row 9+ (2 strips) | 2.7                             | 3,930                        |



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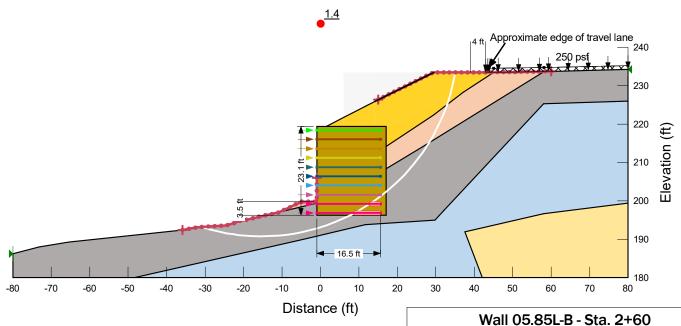
Wall 05.85L-B - Sta. 2+60 Static Compound Stability (Spencer)

I-405/Renton to Bellevue Corridor Widening King County, Washington



| Color | Name   | Material Model | Unit<br>Weight<br>(pcf) | Effective<br>Cohesion<br>(psf) | Effective<br>Friction<br>Angle (°) |
|-------|--|----------------|-------------------------|--------------------------------|------------------------------------|
|       | Common Borrow  | Mohr-Coulomb   | 120                     | 0                              | 32                                 |
|       | ESU 1B Medium Dense to Very<br>Dense Coarse-Grained Fill         | Mohr-Coulomb   | 130                     | 0                              | 41                                 |
|       | ESU 2B Medium Dense<br>Sand/Gravel                               | Mohr-Coulomb   | 115                     | 0                              | 34                                 |
|       | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | Mohr-Coulomb   | 130                     | 0                              | 43                                 |
|       | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | Mohr-Coulomb   | 130                     | 0                              | 42                                 |
|       | Gravel Borrow  | Mohr-Coulomb   | 130                     | 0                              | 38                                 |

| Color | Name              | Interface<br>Shear<br>Angle (°) | Tensile<br>Capacity<br>(lbf) |
|-------|-------------------|---------------------------------|------------------------------|
|       | Row 1 (2 strips)  | 6.6                             | 3,930                        |
|       | Row 2 (2 strips)  | 6.1                             | 3,930                        |
|       | Row 3 (2 strips)  | 5.6                             | 3,930                        |
|       | Row 4 (2 strips)  | 5.1                             | 3,930                        |
|       | Row 5 (2 strips)  | 4.6                             | 3,930                        |
|       | Row 6 (2 strips)  | 4.1                             | 3,930                        |
|       | Row 7 (2 strips)  | 3.6                             | 3,930                        |
|       | Row 8 (2 strips)  | 3.1                             | 3,930                        |
|       | Row 9+ (2 strips) | 2.7                             | 3,930                        |



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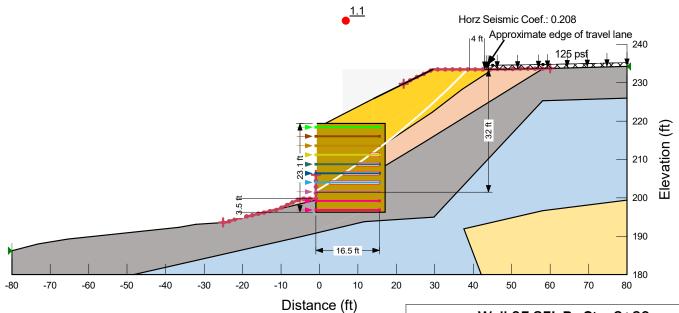
Static Compound Stability (M-P)

I-405/Renton to Bellevue Corridor Widening King County, Washington



| Color | Name   | Material Model | Unit<br>Weight<br>(pcf) | Effective<br>Cohesion<br>(psf) | Effective<br>Friction<br>Angle (°) |
|-------|--|----------------|-------------------------|--------------------------------|------------------------------------|
|       | Common Borrow (Apparent Cohesion)  | Mohr-Coulomb   | 120                     | 50                             | 32                                 |
|       | ESU 1B Medium Dense to Very Dense<br>Coarse-Grained Fill (Apparent Cohesion) | Mohr-Coulomb   | 130                     | 100                            | 41                                 |
|       | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                          | Mohr-Coulomb   | 115                     | 200                            | 34                                 |
|       | ESU 4B Dense to Very Dense Sand/Gravel                                       | Mohr-Coulomb   | 130                     | 0                              | 43                                 |
|       | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt             | Mohr-Coulomb   | 130                     | 0                              | 42                                 |
|       | Gravel Borrow  | Mohr-Coulomb   | 130                     | 0                              | 38                                 |

| Color | Name                  | Interface<br>Shear<br>Angle (°) | Tensile<br>Capacity<br>(lbf) |
|-------|-----------------------|---------------------------------|------------------------------|
|       | Row 1 (2 strips)(EQ)  | 8.8                             | 5,240                        |
|       | Row 2 (2 strips)(EQ)  | 8.2                             | 5,240                        |
|       | Row 3 (2 strips)(EQ)  | 7.5                             | 5,240                        |
|       | Row 4 (2 strips)(EQ)  | 6.8                             | 5,240                        |
|       | Row 5 (2 strips)(EQ)  | 6.2                             | 5,240                        |
|       | Row 6 (2 strips)(EQ)  | 5.5                             | 5,240                        |
|       | Row 7 (2 strips)(EQ)  | 4.9                             | 5,240                        |
|       | Row 8 (2 strips)(EQ)  | 4.2                             | 5,240                        |
|       | Row 9+ (2 strips)(EQ) | 3.6                             | 5,240                        |



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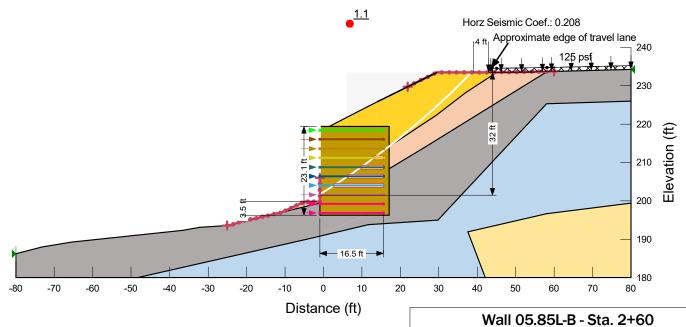
Wall 05.85L-B - Sta. 2+60
Pseudo-Static Compound Stability (Spencer)

I-405/Renton to Bellevue Corridor Widening King County, Washington



| Color | Name   | Material Model | Unit<br>Weight<br>(pcf) | Effective<br>Cohesion<br>(psf) | Effective<br>Friction<br>Angle (°) |
|-------|--|----------------|-------------------------|--------------------------------|------------------------------------|
|       | Common Borrow (Apparent Cohesion)  | Mohr-Coulomb   | 120                     | 50                             | 32                                 |
|       | ESU 1B Medium Dense to Very Dense<br>Coarse-Grained Fill (Apparent Cohesion) | Mohr-Coulomb   | 130                     | 100                            | 41                                 |
|       | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                          | Mohr-Coulomb   | 115                     | 200                            | 34                                 |
|       | ESU 4B Dense to Very Dense Sand/Gravel                                       | Mohr-Coulomb   | 130                     | 0                              | 43                                 |
|       | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt             | Mohr-Coulomb   | 130                     | 0                              | 42                                 |
|       | Gravel Borrow  | Mohr-Coulomb   | 130                     | 0                              | 38                                 |

| Color | Name                  | Interface<br>Shear<br>Angle (°) | Tensile<br>Capacity<br>(lbf) |
|-------|-----------------------|---------------------------------|------------------------------|
|       | Row 1 (2 strips)(EQ)  | 8.8                             | 5,240                        |
|       | Row 2 (2 strips)(EQ)  | 8.2                             | 5,240                        |
|       | Row 3 (2 strips)(EQ)  | 7.5                             | 5,240                        |
|       | Row 4 (2 strips)(EQ)  | 6.8                             | 5,240                        |
|       | Row 5 (2 strips)(EQ)  | 6.2                             | 5,240                        |
|       | Row 6 (2 strips)(EQ)  | 5.5                             | 5,240                        |
|       | Row 7 (2 strips)(EQ)  | 4.9                             | 5,240                        |
|       | Row 8 (2 strips)(EQ)  | 4.2                             | 5,240                        |
|       | Row 9+ (2 strips)(EQ) | 3.6                             | 5,240                        |



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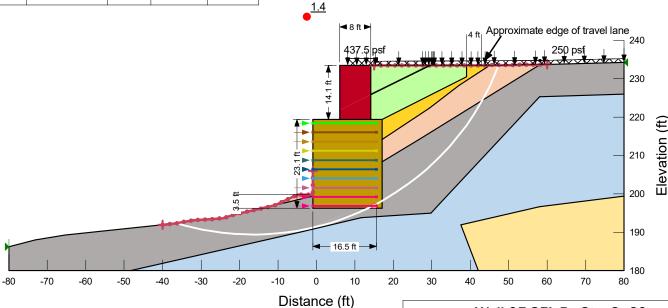
Pseudo-Static Compound Stability (M-P)

I-405/Renton to Bellevue Corridor Widening King County, Washington



| Color | Name   | Material Model | Unit<br>Weight<br>(pcf) | Effective<br>Cohesion<br>(psf) | Effective<br>Friction<br>Angle (°) |
|-------|--|----------------|-------------------------|--------------------------------|------------------------------------|
|       | Common Borrow  | Mohr-Coulomb   | 120                     | 0                              | 32                                 |
|       | ESU 1B Medium Dense to Very Dense<br>Coarse-Grained Fill         | Mohr-Coulomb   | 130                     | 0                              | 41                                 |
|       | ESU 2B Medium Dense Sand/Gravel                                  | Mohr-Coulomb   | 115                     | 0                              | 34                                 |
|       | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | Mohr-Coulomb   | 130                     | 0                              | 43                                 |
|       | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | Mohr-Coulomb   | 130                     | 0                              | 42                                 |
|       | Forward Compatible Wall  | High Strength  | 130                     |                                |                                    |
|       | Gravel Borrow  | Mohr-Coulomb   | 130                     | 0                              | 38                                 |
|       | Lightweight EPS  | Mohr-Coulomb   | 5                       | 100                            | 0                                  |

| Color | Name              | Interface<br>Shear<br>Angle (°) | Tensile<br>Capacity<br>(lbf) |
|-------|-------------------|---------------------------------|------------------------------|
|       | Row 1 (2 strips)  | 6.6                             | 3,930                        |
|       | Row 2 (2 strips)  | 6.1                             | 3,930                        |
|       | Row 3 (2 strips)  | 5.6                             | 3,930                        |
|       | Row 4 (2 strips)  | 5.1                             | 3,930                        |
|       | Row 5 (2 strips)  | 4.6                             | 3,930                        |
|       | Row 6 (2 strips)  | 4.1                             | 3,930                        |
|       | Row 7 (2 strips)  | 3.6                             | 3,930                        |
|       | Row 8 (2 strips)  | 3.1                             | 3,930                        |
|       | Row 9+ (2 strips) | 2.7                             | 3,930                        |



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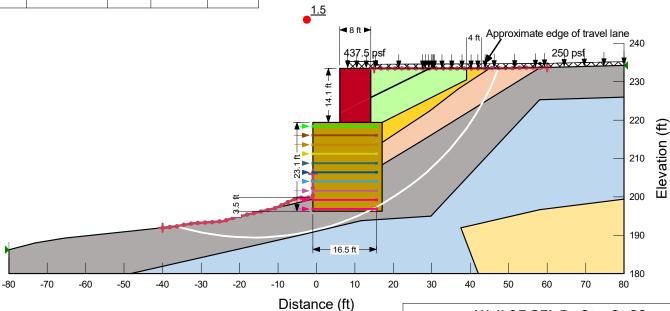
Wall 05.85L-B - Sta. 2+60 Static Compound Stability + FC Wall (Spencer)

I-405/Renton to Bellevue Corridor Widening King County, Washington



| Color | Name   | Material Model | Unit<br>Weight<br>(pcf) | Effective<br>Cohesion<br>(psf) | Effective<br>Friction<br>Angle (°) |
|-------|--|----------------|-------------------------|--------------------------------|------------------------------------|
|       | Common Borrow  | Mohr-Coulomb   | 120                     | 0                              | 32                                 |
|       | ESU 1B Medium Dense to Very Dense<br>Coarse-Grained Fill         | Mohr-Coulomb   | 130                     | 0                              | 41                                 |
|       | ESU 2B Medium Dense Sand/Gravel                                  | Mohr-Coulomb   | 115                     | 0                              | 34                                 |
|       | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | Mohr-Coulomb   | 130                     | 0                              | 43                                 |
|       | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | Mohr-Coulomb   | 130                     | 0                              | 42                                 |
|       | Forward Compatible Wall  | High Strength  | 130                     |                                |                                    |
|       | Gravel Borrow  | Mohr-Coulomb   | 130                     | 0                              | 38                                 |
|       | Lightweight EPS  | Mohr-Coulomb   | 5                       | 100                            | 0                                  |

| Color | Name              | Interface<br>Shear<br>Angle (°) | Tensile<br>Capacity<br>(lbf) |
|-------|-------------------|---------------------------------|------------------------------|
|       | Row 1 (2 strips)  | 6.6                             | 3,930                        |
|       | Row 2 (2 strips)  | 6.1                             | 3,930                        |
|       | Row 3 (2 strips)  | 5.6                             | 3,930                        |
|       | Row 4 (2 strips)  | 5.1                             | 3,930                        |
|       | Row 5 (2 strips)  | 4.6                             | 3,930                        |
|       | Row 6 (2 strips)  | 4.1                             | 3,930                        |
|       | Row 7 (2 strips)  | 3.6                             | 3,930                        |
|       | Row 8 (2 strips)  | 3.1                             | 3,930                        |
|       | Row 9+ (2 strips) | 2.7                             | 3,930                        |



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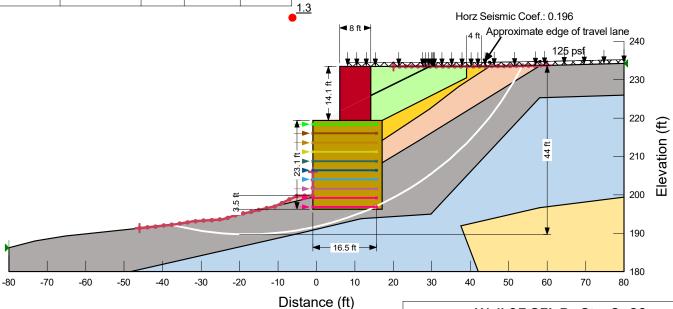
Wall 05.85L-B - Sta. 2+60 Static Compound Stability + FC Wall (M-P)

I-405/Renton to Bellevue Corridor Widening King County, Washington



| Color | Name   | Material Model | Unit<br>Weight<br>(pcf) | Effective<br>Cohesion<br>(psf) | Effective<br>Friction<br>Angle (°) |
|-------|--|----------------|-------------------------|--------------------------------|------------------------------------|
|       | Common Borrow (Apparent Cohesion)  | Mohr-Coulomb   | 120                     | 50                             | 32                                 |
|       | ESU 1B Medium Dense to Very Dense<br>Coarse-Grained Fill (Apparent Cohesion) | Mohr-Coulomb   | 130                     | 100                            | 41                                 |
|       | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                          | Mohr-Coulomb   | 115                     | 200                            | 34                                 |
|       | ESU 4B Dense to Very Dense Sand/Gravel                                       | Mohr-Coulomb   | 130                     | 0                              | 43                                 |
|       | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt             | Mohr-Coulomb   | 130                     | 0                              | 42                                 |
|       | Forward Compatible Wall  | High Strength  | 130                     |                                |                                    |
|       | Gravel Borrow  | Mohr-Coulomb   | 130                     | 0                              | 38                                 |
|       | Lightweight EPS  | Mohr-Coulomb   | 5                       | 100                            | 0                                  |

| Color | Name                  | Interface<br>Shear<br>Angle (°) | Tensile<br>Capacity<br>(lbf) |
|-------|-----------------------|---------------------------------|------------------------------|
|       | Row 1 (2 strips)(EQ)  | 8.8                             | 5,240                        |
|       | Row 2 (2 strips)(EQ)  | 8.2                             | 5,240                        |
|       | Row 3 (2 strips)(EQ)  | 7.5                             | 5,240                        |
|       | Row 4 (2 strips)(EQ)  | 6.8                             | 5,240                        |
|       | Row 5 (2 strips)(EQ)  | 6.2                             | 5,240                        |
|       | Row 6 (2 strips)(EQ)  | 5.5                             | 5,240                        |
|       | Row 7 (2 strips)(EQ)  | 4.9                             | 5,240                        |
|       | Row 8 (2 strips)(EQ)  | 4.2                             | 5,240                        |
|       | Row 9+ (2 strips)(EQ) | 3.6                             | 5,240                        |



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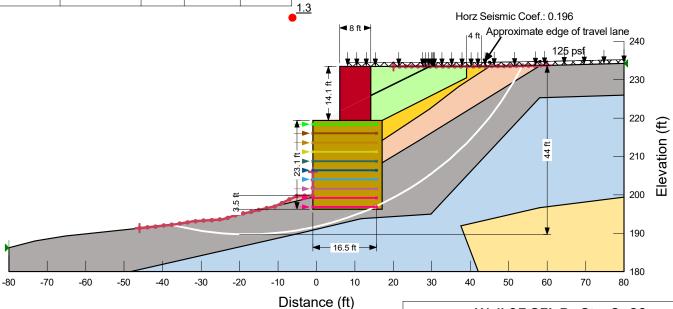
Wall 05.85L-B - Sta. 2+60 Pseudo-Static Compound Stability + FC Wall (S)

I-405/Renton to Bellevue Corridor Widening King County, Washington



| Color | Name   | Material Model | Unit<br>Weight<br>(pcf) | Effective<br>Cohesion<br>(psf) | Effective<br>Friction<br>Angle (°) |
|-------|--|----------------|-------------------------|--------------------------------|------------------------------------|
|       | Common Borrow (Apparent Cohesion)  | Mohr-Coulomb   | 120                     | 50                             | 32                                 |
|       | ESU 1B Medium Dense to Very Dense<br>Coarse-Grained Fill (Apparent Cohesion) | Mohr-Coulomb   | 130                     | 100                            | 41                                 |
|       | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                          | Mohr-Coulomb   | 115                     | 200                            | 34                                 |
|       | ESU 4B Dense to Very Dense Sand/Gravel                                       | Mohr-Coulomb   | 130                     | 0                              | 43                                 |
|       | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt             | Mohr-Coulomb   | 130                     | 0                              | 42                                 |
|       | Forward Compatible Wall  | High Strength  | 130                     |                                |                                    |
|       | Gravel Borrow  | Mohr-Coulomb   | 130                     | 0                              | 38                                 |
|       | Lightweight EPS  | Mohr-Coulomb   | 5                       | 100                            | 0                                  |

| Color | Name                  | Interface<br>Shear<br>Angle (°) | Tensile<br>Capacity<br>(lbf) |
|-------|-----------------------|---------------------------------|------------------------------|
|       | Row 1 (2 strips)(EQ)  | 8.8                             | 5,240                        |
|       | Row 2 (2 strips)(EQ)  | 8.2                             | 5,240                        |
|       | Row 3 (2 strips)(EQ)  | 7.5                             | 5,240                        |
|       | Row 4 (2 strips)(EQ)  | 6.8                             | 5,240                        |
|       | Row 5 (2 strips)(EQ)  | 6.2                             | 5,240                        |
|       | Row 6 (2 strips)(EQ)  | 5.5                             | 5,240                        |
|       | Row 7 (2 strips)(EQ)  | 4.9                             | 5,240                        |
|       | Row 8 (2 strips)(EQ)  | 4.2                             | 5,240                        |
|       | Row 9+ (2 strips)(EQ) | 3.6                             | 5,240                        |



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Wall 05.85L-B - Sta. 2+60 Pseudo-Static Global Stability + FC Wall (M-P)

I-405/Renton to Bellevue Corridor Widening King County, Washington









In Association with

# **Appendix G**

Embankment EMB: I-405 SB MP 5.97 TO 5.83 Calculations







In Association with

#### APPENDIX G – EMBANKMENT EMB: I-405 SB MP 5.97 TO 5.83 CALCULATIONS

#### General

This appendix presents geotechnical calculations for embankment EMB: I-405 SB MP 5.97 to 5.83 including:

- **ESU Soil Properties**
- Seismic Hazard Analysis
- Elastic Settlement
- Global Stability

#### **ESU Soil Properties**

Design soil properties developed for Wall 05.85L-A were used for embankment EMB: I-405 SB MP 5.97 to 5.83. A detailed description of the soil property development is presented in Section 7.1 of this geotechnical engineering report. Supporting calculations are provided in Appendix E. Supporting calculations for the development of elastic moduli used for the embankment elastic settlement analysis are presented in this appendix

#### **Seismic Hazard Analysis**

The representative site class, design seismic parameters, the mean earthquake magnitude, and liquefaction potential developed for Wall 05.85L-A were used for embankment EMB: I-405 SB MP 5.97 TO 5.83. Detailed descriptions of our seismic hazard analysis methodology and the results are presented in Section 7.2 and Section 8.1, respectively, of this report. Supporting calculations are provided in Appendix E.

#### **Elastic Settlement**

We estimated the static elastic settlement for the placement of new fill (common borrow) on the embankment using the computer design software Settle3 (Rocscience 2021). We modeled the applied fill load along the approximate length of the embankment and the fill slope at the design section. We used the elastic moduli of the ESUs beneath the new fill in the embankment to evaluate immediate settlement of the embankment.

Detailed descriptions of our elastic settlement methodology and the results of our analyses are presented in Section 7.5 and Section 8.4, respectively, of this report. Supporting calculations are provided in this appendix. Settle3 output reports are provided in Appendix H.

#### **Global Stability**

We performed global stability analyses for the following critical design section:

EMB I-405 SB MP 5.88 – Center of embankment

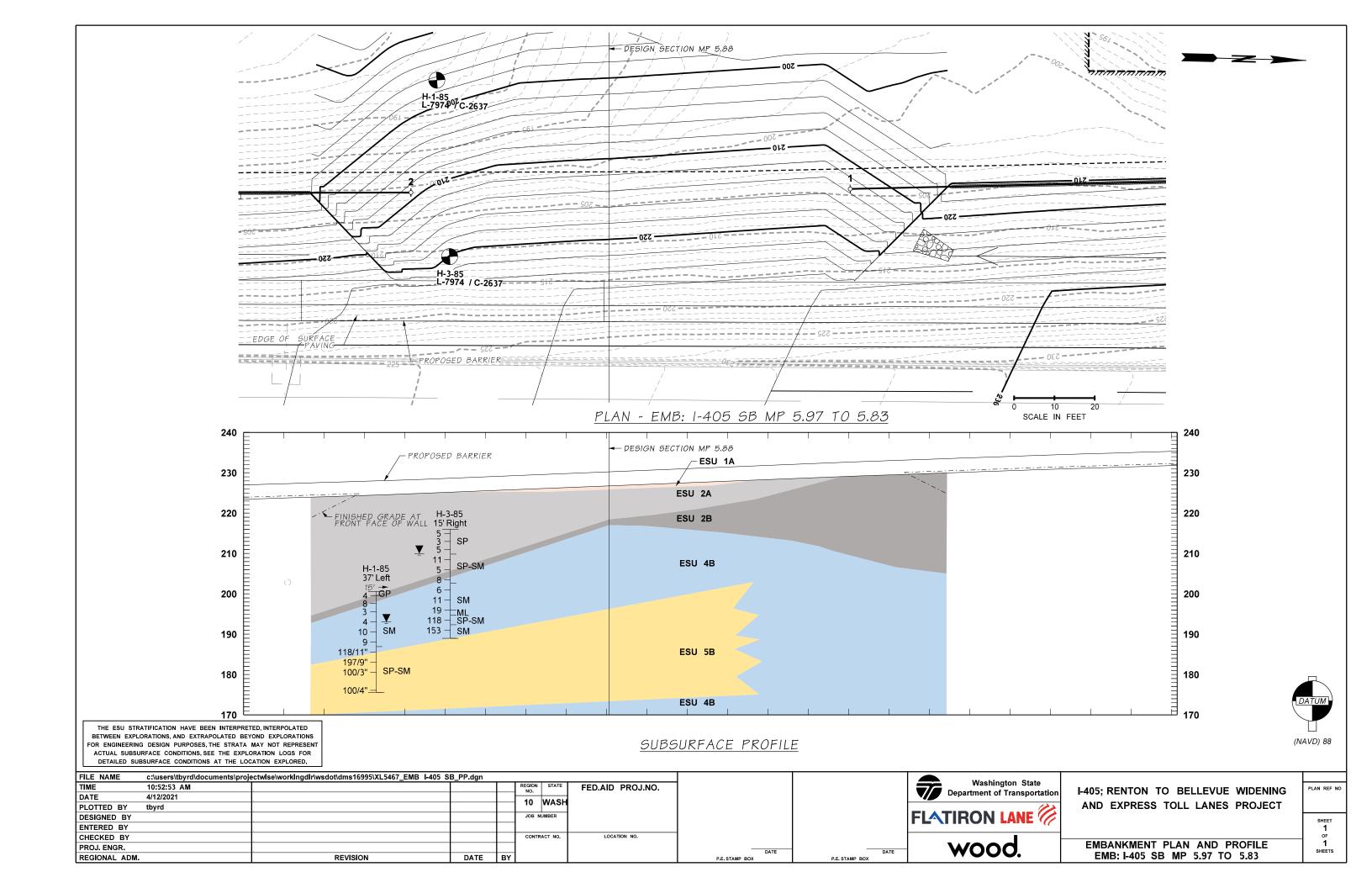
Global stability was evaluated using limit equilibrium analysis methodology outlined in the Project GDM using the computer design software Slope/W (Geo Slope International, Ltd. 2020). We analyzed FSs using Spencer's method and Morgenstern-Price for a circular failure surface.

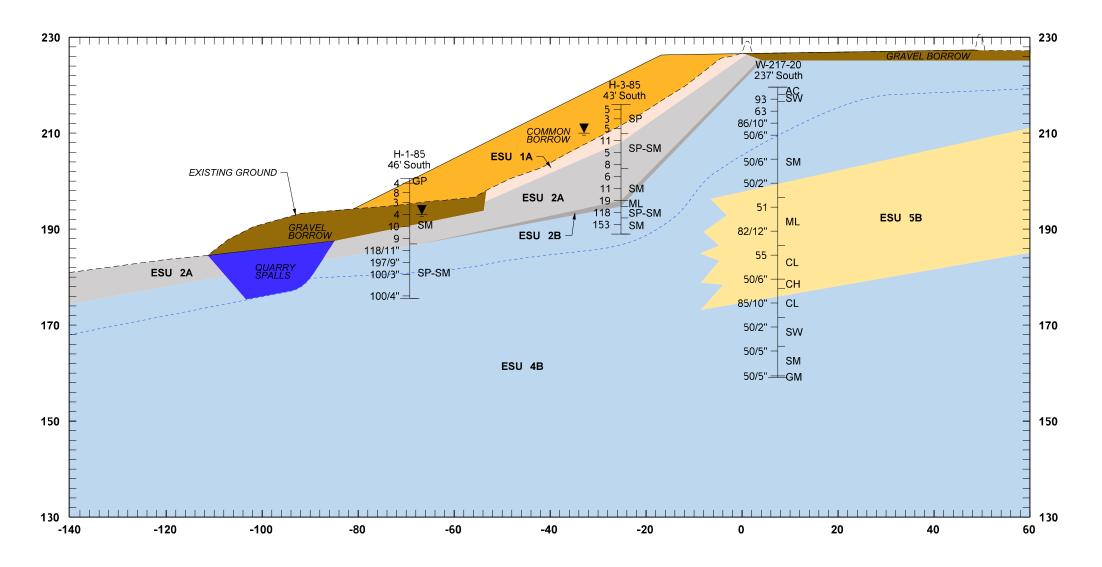
A traffic surcharge of 250 psf was applied at the top of the embankment for the static global stability analysis.

The groundwater level was modeled using results from the seepage analysis at Wall 05.85L-A. Steady-state seepage results are presented in Appendix E.

Detailed descriptions of our global stability analysis methodology and the results of our analyses are presented in Section 7.8 and Section 8.6, respectively, of this report. Global stability models showing FS for critical failures at the design section are provided in this appendix. Slope/W reports are provided in Appendix J.

Appendix G.1 - Embankment EMB: I-405 SB MP 5.97 to 5.83 Plan, Profile and Sections





EMB: 1-405 SB MP 5.88

THE ESU STRATIFICATION HAVE BEEN INTERPRETED, INTERPOLATED BETWEEN EXPLORATIONS, AND EXTRAPOLATED BEYOND EXPLORATIONS FOR ENGINEERING DESIGN PURPOSES, THE STRATA MAY NOT REPRESENT ACTUAL SUBSURFACE CONDITIONS, SEE THE EXPLORATION LOGS FOR DETAILED SUBSURFACE CONDITIONS AT THE LOCATION EXPLORED,

| FILE NAME    | c:\users\tbyra\aocuments\proj | ectwise\workingair\wsaot\ams16995\XL5467_EMB  i-405  S | SB_XS.agn |    |              |                  |                |                | 14/2 - 12/2 - 14 - 12 - 04 - 4 -        |                                    |             |   |
|--------------|-------------------------------|--|-----------|----|--------------|------------------|----------------|----------------|---|------------------------------------|-------------|---|
| TIME         | 9:53:42 AM                    |  |           |    | REGION STATE | FED.AID PROJ.NO. |                |                | Washington State                        | I-405: RENTON TO BELLEVUE WIDENING | PLAN REF NO | 1 |
| DATE         | 4/20/2021                     |  |           |    | 10 WASH      | <u> </u>         |                |                | Department of Transportation            | ,                                  |             |   |
| PLOTTED BY   | tbyrd                         |  |           |    | IU WASI      | ]                |                |                |   | AND EXPRESS TOLL LANES PROJECT     |             |   |
| DESIGNED BY  |                               |  |           |    | JOB NUMBER   |                  |                |                | FLATIRON LANE 🥢                         |                                    | SHEET       | 1 |
| ENTERED BY   |                               |  |           |    |              |                  |                |                | , _ ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, |                                    | 1           |   |
| CHECKED BY   |                               |  |           |    | CONTRACT NO. | LOCATION NO.     |                |                |   |                                    | OF          |   |
| PROJ. ENGR.  |                               |  |           |    |              |                  | DATE           | DATE           | Wood.                                   | EMB: I-405 SB MP 5.88              | 1<br>SHEETS |   |
| REGIONAL ADM | •                             | REVISION   | DATE      | BY |              |                  | P.E. STAMP BOX | P.E. STAMP BOX | <b>******</b>                           | DESIGN SECTION                     |             |   |

# Appendix G.2 - Embankment EMB: I-405 SB MP 5.97 to 5.83 ESU Soil Property Calculations

(See Wall 05.85L-A Appendix E.2 for Complete ESU Soil Property Calculations)

The coefficient of consolidation,  $c_V$ , should be determined from the results of one-dimensional consolidation tests. The variability in laboratory determination of  $c_V$  results should be considered in the final selection of the value of  $c_V$  to be used for design.

Where evaluation of elastic settlement is critical to the design of the foundation or selection of the foundation type, in-situ methods such as PMT or *DMT* for evaluating the modulus of the stratum should be used.

ESU 1A Loose to Medium Dense Coarse-Grained Fill

Es = 2.3 ksi = 330 ksf

ESU 2A Very Loose to Loose Sand/ Gravel

Es = 3.7 ksi = 530 ksf

ESU 2B Medium Dense Sand/Gravel

Es = 5.6 ksi = 800 ksf

ESU 4B Dense to Very Dense Sand/Gravel Es = 0.167\*111 = 18.5 ksi = 2670 ksf A profile of  $\sigma_{p'}$ , or OCR =  $\sigma_{p'}/\sigma_{o'}$ , with depth should be developed for the site for design applications where the stress history could have a significant impact on the design properties selected and the performance of the foundation. As with consolidation properties, an upper and lower bound profile should be developed based on laboratory tests and plotted with a profile based on particular in-situ test(s), if used. It is particularly important to accurately compute preconsolidation stress values for relatively shallow depths where in-situ effective stresses are low. An underestimation of the preconsolidation stress at shallow depths will result in overly conservative estimates of settlement for shallow soil layers.

Due to the numerous simplifying assumptions associated with conventional consolidation theory, on which the coefficient of consolidation is based, it is unlikely that even the best estimates of  $c_V$  from high-quality laboratory tests will result in predictions of time rate of settlement in the field that are significantly better than a prediction within one order of magnitude. In general, the in-situ value of  $c_V$  is larger than the value measured in the laboratory test. Therefore, a rational approach is to select average, upper, and lower bound values for the appropriate stress range of concern for the design application. These values should be compared to values obtained from previous work performed in the same soil deposit. Under the best-case conditions, these values should be compared to values computed from measurements of excess pore pressures or settlement rates during construction of other structures.

 $\it CPTu$  tests in which the pore pressure dissipation rate is measured may be used to estimate the field coefficient of consolidation.

For preliminary analyses or where accurate prediction of settlement is not critical, values obtained from correlations to index properties presented in Sabatini et al. (2002) may be used.

For preliminary design or for final design where the prediction of deformation is not critical to structure performance, i.e., the structure design can tolerate the potential inaccuracies inherent in the correlations. The elastic properties ( $E_s$ ,  $\nu$ ) of a soil may be estimated from empirical relationships presented in Table C10.4.6.3-1.

The specific definition of  $E_s$  is not always consistent for the various correlations and methods of in-situ measurement. See Sabatini et al. (2002) for additional details regarding the definition and determination of  $E_s$ .

An alternative method of evaluating the equivalent elastic modulus using measured shear wave velocities is presented in Sabatini et al. (2002).

Table C10.4.6.3-1—Elastic Constants of Various Soils (modified after U.S. Department of the Navy, 1982; Bowles, 1988)

| Department of the         | Navy, 1982; Bowles, 1988)                            |                                |
|---------------------------|--|--------------------------------|
| Soil Type                 | Typical Range of Young's Modulus Values, $E_s$ (ksi) | Poisson's Ratio, $\nu$ (dim)   |
| Clay:                     |  |                                |
| Soft sensitive            |  |                                |
| Medium stiff to stiff     | 0.347-2.08   | 0.4–0.5 (undrained)            |
|                           | 2.08-6.94  |                                |
| Very stiff                | 6.94–13.89   |                                |
| Loess                     | 2.08-8.33  | 0.1-0.3                        |
| Silt                      | 0.278–2.78   | 0.3-0.35                       |
| Fine Sand:                |  |                                |
| Loose                     | 1.11–1.67  | 0.25                           |
| Medium dense              | 1.67–2.78  |                                |
| Dense                     | 2.78-4.17  |                                |
| Sand:                     |  |                                |
| Loose                     | 1.39-4.17  | 0.20-0.36                      |
| Medium dense              | 4.17–6.94  | $\sim$                         |
| Dense                     | 6.94–11.11   | 0.30-0.40                      |
| Gravel:                   |  |                                |
| Loose                     | 4.17–11.11   | 0.20-0.35                      |
| Medium dense              | 11.11–13.89  |                                |
| Dense                     | 13.89–27.78  | 0.30-0.40                      |
| Estimating $E_s$ from $S$ | SPT N Value  |                                |
|                           | Soil Type  | $E_s$ (ksi)                    |
| Silts, sandy silts, slig  | 0.056 M <sub>160</sub>                               |                                |
| Clean fine to mediur      | 0.097 N <sub>160</sub>                               |                                |
| Coarse sands and sa       | ands with little gravel                              | 0.139 <i>N</i> 1 <sub>60</sub> |
| Sandy gravel and gr       | avels  | 0.167 M <sub>60</sub>          |
| Estimating $E_s$ from $a$ | $q_c$ (static cone resistance)                       |                                |
| Sandy soils               |  | 0.028 <i>qc</i>                |
|                           |  |                                |

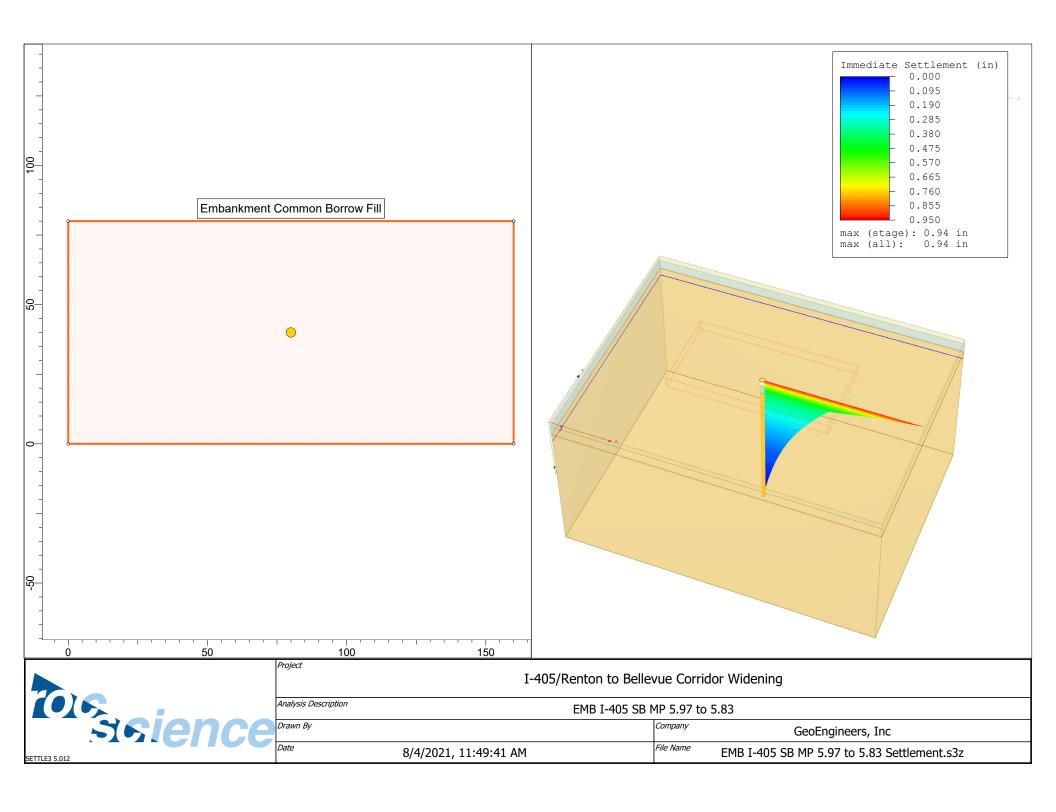
The modulus of elasticity for normally consolidated granular soils tends to increase with depth. An alternative method of defining the soil modulus for granular soils is to assume that it increases linearly with depth starting at zero at the ground surface in accordance with the following equation:

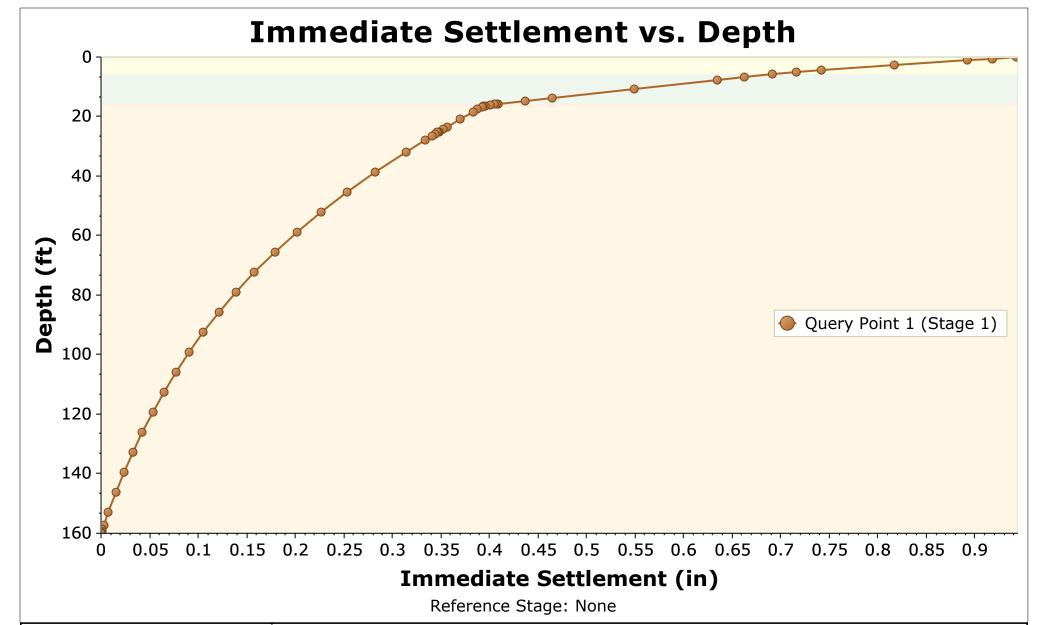
$$E_s = nh \times z \tag{C10.4.6.3-1}$$

where:

# Appendix G.3 - Embankment EMB: I-405 SB MP 5.97 to 5.83

(See Wall 05.85L-A Appendix E.3 for Complete Design Calculations)





|                | Project              | I-405/Renton to Bellev       | vue Corrid | lor Widening                                |  |
|----------------|----------------------|------------------------------|------------|---|--|
|                | Analysis Description | EMB I-405 SB MP 5.97 to 5.83 |            |   |  |
| <i>Selence</i> | Drawn By             |                              | Company    | GeoEngineers, Inc                           |  |
| SETTLE3 5 012  | Date                 | 8/4/2021, 11:49:41 AM        | File Name  | EMB I-405 SB MP 5.97 to 5.83 Settlement.s3z |  |

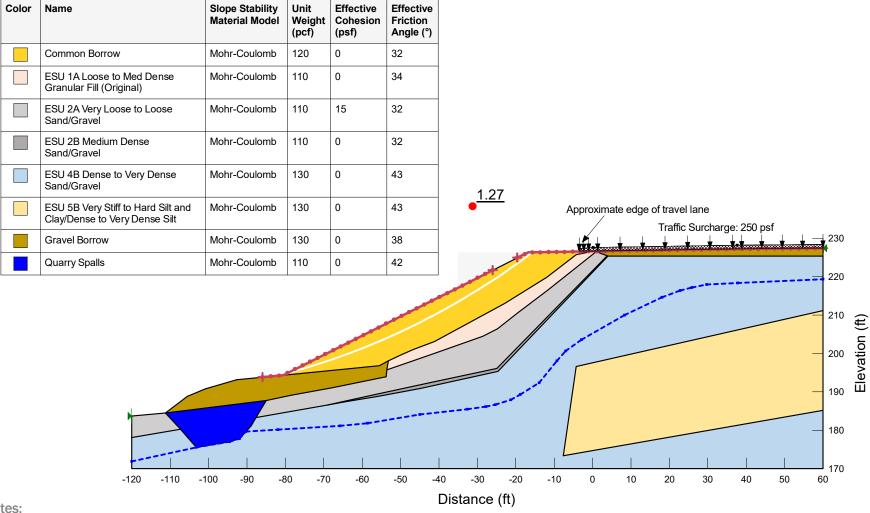
1. The locations of all features shown are approximate.

- 2. This drawing is for information purposes. It is intended to assist in showing features discussed in an attached document.
- 3. GeoEngineers, Inc. cannot guarantee the accuracy and context of electronic files. The master file is stored by GeoEngineers, Inc. and will serve as the official record of this communication.

EMB I-405 SB MP 5.97 to 5.83 - MP 5.88 **Static Global Stability (Spencer)** 

I-405/Renton to Bellevue Corridor Widening King County, Washington





1. The locations of all features shown are approximate.

2. This drawing is for information purposes. It is intended to assist in showing features discussed in an attached document.

3. GeoEngineers, Inc. cannot guarantee the accuracy and context of electronic files. The master file is stored by GeoEngineers, Inc. and will serve as the official record of this communication.

EMB I-405 SB MP 5.97 to 5.83 - MP 5.88 Static Global Stability (M-P)

I-405/Renton to Bellevue Corridor Widening King County, Washington









In Association with

## Appendix H **Settle3 Reports**

# rocscience



I-405/Renton to Bellevue Corridor Widening GeoEngineers, Inc Report Creation Date: 2021/09/23, 13:17:29

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| Piezometric Line Entities                     | C            |

# **Settle3 Analysis Information**

# I-405/Renton to Bellevue Corridor Widening

## **Project Settings**

Document Name Project Title Analysis Company Date Created EMB I-405 SB MP 5.97 to 5.83 Settlement.s3z I-405/Renton to Bellevue Corridor Widening EMB I-405 SB MP 5.97 to 5.83 GeoEngineers, Inc 8/4/2021, 11:49:41 AM

#### Comments

Stress Computation Method
Minimum settlement ratio for subgrade modulus
Use average properties to calculate layered stresses
Improve consolidation accuracy
Ignore negative effective stresses in settlement
calculations

Boussinesq 0.9

# **Stage Settings**

| Stage # | Name    |
|---------|---------|
| 1       | Stage 1 |

# **Results**

Time taken to compute: 0.101 seconds

Stage: Stage 1

| Data Type   | Minimum     | Maximum    |
|---|-------------|------------|
| Total Settlement [in]                                 | 0           | 0.942966   |
| Total Consolidation Settlement [in]                   | 0           | 0          |
| Virgin Consolidation Settlement [in]                  | 0           | 0          |
| Recompression Consolidation Settlement [in]           | 0           | 0          |
| Immediate Settlement [in]                             | 0           | 0.942966   |
| Loading Stress ZZ [ksf]                               | 0.235002    | 1.236      |
| Loading Stress XX [ksf]                               | -0.0299009  | 0.713296   |
| Loading Stress YY [ksf]                               | -0.00232925 | 1.0171     |
| Effective Stress ZZ [ksf]                             | 1.236       | 12.2832    |
| Effective Stress XX [ksf]                             | 0.713296    | 12.0208    |
| Effective Stress YY [ksf]                             | 1.0171      | 12.0459    |
| Total Stress ZZ [ksf]                                 | 1.236       | 20.701     |
| Total Stress XX [ksf]                                 | 0.713296    | 20.4386    |
| Total Stress YY [ksf]                                 | 1.0171      | 20.4637    |
| Modulus of Subgrade Reaction (Total) [ksf/ft]         | 0           | 16.6161    |
| Modulus of Subgrade Reaction (Immediate) [ksf/ft]     | 0           | 16.6161    |
| Modulus of Subgrade Reaction (Consolidation) [ksf/ft] | 0           | 0          |
| Total Strain  | 8.80751e-05 | 0.00374545 |
| Pore Water Pressure [ksf]                             | 0           | 8.41776    |
| Degree of Consolidation [%]                           | 0           | 0          |
| Pre-consolidation Stress [ksf]                        | 1.2668      | 12.2788    |
| Over-consolidation Ratio                              | 1           | 1          |
| Void Ratio  | 0           | 0          |
| Hydroconsolidation Settlement [in]                    | 0           | 0          |
| Undrained Shear Strength                              | 0           | 0.0399303  |

# Loads

## 1. Fill Load: "Embankment Common Borrow Fill"

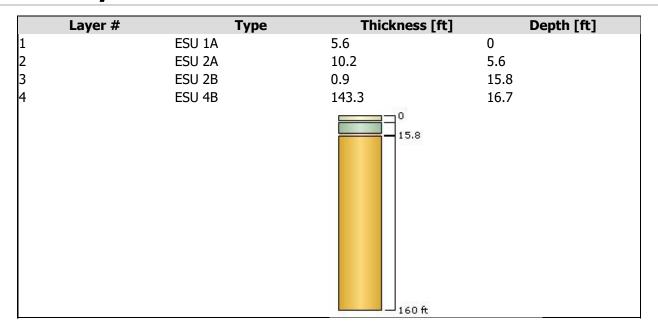
Label Embankment Common Borrow Fill

Load TypeFlexibleArea of Load12800 ft2Load1.236 ksfDepth0 ftInstallation StageStage 1

## **Coordinates**

| X [1 | t] Y [ft] |
|------|-----------|
| 160  | 0         |
| 160  | 80        |
| 0    | 80        |
| 0    | 0         |

# **Soil Layers**



# **Soil Properties**

| Property                            | ESU 1A  | ESU 2A  | ESU 2B  | ESU 4B  |
|-------------------------------------|---------|---------|---------|---------|
| Color                               |         |         |         |         |
| Unit Weight<br>[kips/ft3]           | 0.11    | 0.11    | 0.11    | 0.13    |
| Saturated Unit<br>Weight [kips/ft3] | 0.11    | 0.11    | 0.11    | 0.13    |
| K0                                  | 1       | 1       | 1       | 1       |
| Immediate<br>Settlement             | Enabled | Enabled | Enabled | Enabled |
| Es [ksf]                            | 330     | 530     | 800     | 2670    |
| Esur [ksf]                          | 330     | 530     | 800     | 2670    |
| Undrained Su A<br>[kips/ft2]        | 0       | 0       | 0       | 0       |
| Undrained Su S                      | 0.2     | 0.2     | 0.2     | 0.2     |
| Undrained Su m                      | 0.8     | 0.8     | 0.8     | 0.8     |
| Piezo Line ID                       | 0       | 0       | 0       | 1       |

# **Groundwater**

Groundwater method Water Unit Weight Piezometric Lines 0.0624 kips/ft3

# **Piezometric Line Entities**

| ID | Depth (ft) |
|----|------------|
| 1  | 25.1 ft    |







In Association with

# Appendix I Seep/W Reports

Steady State Page 1 of 19

# **Steady State**

Report generated using GeoStudio 2020. Copyright © 1991-2020 GEOSLOPE International Ltd.

## **File Information**

File Version: 10.02 Created By: Jon Cracolici Last Edited By: Carl Longton Revision Number: 428 Date: 04/09/2021 Time: 08:48:55 AM

Tool Version: 10.2.1.19666

File Name: Wall 05.85L-A - Sta 1+90 - 0.8H (No Coh).gsz

Directory: \geoengineers.com\WAN\Projects\0\0180366\01\Analysis\Wall 05.85L-A\04-02-21\

Last Solved Date: 04/09/2021 Last Solved Time: 08:49:04 AM

# **Project Settings**

Unit System: U.S. Customary Units

# **Analysis Settings**

#### **Steady State**

Kind: SEEP/W

Method: Steady-State

**Physics** 

Water Transfer

Free convection: thermal effects: No Free convection: solute effects: No Vapor transfer: isothermal: No Vapor transfer: thermal: No

Water Settings

Maximum Number of Iterations: 1,200

Maximum Difference: 0.1
Significant Digits: 2
Max # of Reviews: 20
Under-Relaxation Criteria
Initial Rate: 1

Minimum Rate: 0.1

Rate Reduction Factor: 0.65

Reduction Frequency (iterations): 10 Unit Weight of Water: 62.430189 pcf Bulk Modulus of Pore-Fluid: 43,511,321 psf

Time

Starting Time: 0 sec

Page 2 of 19 **Steady State** 

> Duration: 0 sec Ending Time: 0 sec

## **Materials**

#### **ESU 2A Very Loose to Loose Sand/Gravel**

#### Hydraulic

Model: Saturated / Unsaturated

Vol. WC. Function: 2A K-Function: 2A Ky'/Kx' Ratio: 0.8 Rotation: 0°

### **ESU 2B Medium Dense Sand/Gravel**

#### Hydraulic

Model: Saturated / Unsaturated

Vol. WC. Function: 2B K-Function: 2B Ky'/Kx' Ratio: 0.5 Rotation: 0°

### **ESU 4B Dense to Very Dense Sand/Gravel**

#### Hydraulic

Model: Saturated / Unsaturated

Vol. WC. Function: 4B K-Function: 4B Ky'/Kx' Ratio: 0.025

Rotation: 0 °

# ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

#### Hydraulic

Model: Saturated / Unsaturated

Vol. WC. Function: 5B K-Function: 5B Ky'/Kx' Ratio: 0.005 Rotation: 0°

# **Boundary Conditions**

#### **Right Total head constant**

Category: Hydraulic

Kind: Water Total Head 218 ft

Review: No

#### Total head at left side

Category: Hydraulic

Kind: Water Total Head 160 ft

Steady State Page 3 of 19

Review: No

#### Flux

Category: Hydraulic

Kind: Water Flux 2.6e-07 ft/sec

Review: No

## **Water K Functions**

#### **2A**

Model: Hyd K Data Point Function

Function: Water X-Conductivity vs. Water Pressure

Curve Fit to Data: 100 %
Segment Curvature: 100 %
Saturated Kx: 0.00011 ft/sec

Data Points: Matric Suction (psf), Water X-Conductivity (ft/sec)

Data Point: (0, 0.00011)

Data Point: (0.20885434, 8.9333881e-05) Data Point: (0.5979899, 7.1249845e-05) Data Point: (1.7121594, 5.3296999e-05) Data Point: (4.9022396, 3.5715785e-05)

Data Point: (14.036049, 1.9205855e-05) Data Point: (40.187891, 5.7423859e-06) Data Point: (115.06561, 8.39696e-07) Data Point: (329.45485, 7.8039872e-08)

Data Point: (943.2922, 1.8746458e-09) Data Point: (2,700.8259, 4.0795911e-11) Data Point: (7,732.9807, 1.3054938e-12) Data Point: (22,141.002, 6.1944672e-14)

Data Point: (63,393.92, 3.8288737e-15)
Data Point: (181,508.91, 2.574522e-16)
Data Point: (519,694.7, 1.5844563e-17)
Data Point: (1,487,985.3, 9.0105123e-19)
Data Point: (4,260,386.3, 9.746738e-20)

Data Point: (12,198,300, 5.2298422e-21) Data Point: (34,926,065, 6.7315785e-22)

Data Point: (1e+08, 6.7315785e-22)

#### **Estimation Properties**

Hyd. K-Function Estimation Method: Fredlund-Xing Function

Volume Water Content Function: 2A

Saturated Kx: 0.00011 ft/sec Maximum Suction: 1e+08 psf Minimum Suction: 0.20885434 psf

Num. Points: 20

#### **2B**

Model: Hyd K Data Point Function

Function: Water X-Conductivity vs. Water Pressure

Curve Fit to Data: 100 %

Steady State Page 4 of 19

Segment Curvature: 100 % Saturated Kx: 3.3e-05 ft/sec Data Points: Matric Suction (psf), Water X-Conductivity (ft/sec) Data Point: (0, 3.3e-05) Data Point: (0.20885434, 3.299866e-05) Data Point: (0.5979899, 3.2997094e-05) Data Point: (1.7121594, 3.2994155e-05) Data Point: (4.9022396, 3.2987267e-05) Data Point: (14.036049, 3.2969498e-05) Data Point: (40.187891, 3.2919439e-05) Data Point: (115.06561, 2.2304274e-05) Data Point: (329.45485, 4.2752274e-06) Data Point: (943.2922, 3.0302083e-07) Data Point: (2,700.8259, 8.9849806e-09) Data Point: (7,732.9807, 1.5483062e-10) Data Point: (22,141.002, 1.0024034e-11) Data Point: (63,393.92, 6.5084402e-13) Data Point: (181,508.91, 3.9333429e-14) Data Point: (519,694.7, 2.9574971e-15) Data Point: (1,487,985.3, 2.1008717e-16) Data Point: (4,260,386.3, 1.369693e-17) Data Point: (12,198,300, 5.1084724e-19) Data Point: (34,926,065, 5.6398058e-20) Data Point: (1e+08, 5.6398058e-20) **Estimation Properties** Hyd. K-Function Estimation Method: Fredlund-Xing Function Volume Water Content Function: 2B Saturated Kx: 3.3e-05 ft/sec Maximum Suction: 1e+08 psf Minimum Suction: 0.20885434 psf Num. Points: 20 Model: Hyd K Data Point Function Function: Water X-Conductivity vs. Water Pressure Curve Fit to Data: 100 % Segment Curvature: 100 % Saturated Kx: 3.8e-08 ft/sec Data Points: Matric Suction (psf), Water X-Conductivity (ft/sec) Data Point: (0, 3.8e-08) Data Point: (0.20885434, 3.7996746e-08) Data Point: (0.76200357, 3.7992863e-08) Data Point: (2.7801646, 3.7987317e-08) Data Point: (10.143411, 3.7975703e-08) Data Point: (37.008161, 3.7941901e-08) Data Point: (135.02401, 3.7814973e-08) Data Point: (492.63414, 1.9125018e-08) Data Point: (1,797.3721, 2.0225662e-09) Data Point: (6,557.6994, 8.5177476e-11) Data Point: (23,925.719, 1.8463817e-12)

**5B** 

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```
Data Point: (87,292.816, 5.3530075e-14)
     Data Point: (318,487.22, 2.8407525e-15)
     Data Point: (1,161,998.3, 1.1712864e-16)
     Data Point: (4,239,542.6, 4.7285973e-18)
     Data Point: (15,467,941, 7.3289464e-20)
     Data Point: (56,434,672, 2.2361549e-20)
     Data Point: (2.059015e+08, 2.2361549e-20)
     Data Point: (7.5123013e+08, 2.2361549e-20)
     Data Point: (2.7408578e+09, 2.2361549e-20)
     Data Point: (1e+10, 2.2361549e-20)
Estimation Properties
     Hyd. K-Function Estimation Method: Fredlund-Xing Function
     Volume Water Content Function: 5B
     Saturated Kx: 3.8e-08 ft/sec
     Maximum Suction: 1e+10 psf
     Minimum Suction: 0.20885434 psf
     Num. Points: 20
Model: Hyd K Data Point Function
Function: Water X-Conductivity vs. Water Pressure
     Curve Fit to Data: 100 %
     Segment Curvature: 100 %
Saturated Kx: 3.8e-07 ft/sec
Data Points: Matric Suction (psf), Water X-Conductivity (ft/sec)
     Data Point: (0, 3.8e-07)
     Data Point: (0.20885434, 3.7950884e-07)
     Data Point: (0.67503366, 3.7788512e-07)
     Data Point: (2.1817619, 3.7204474e-07)
     Data Point: (7.051626, 3.5178458e-07)
     Data Point: (22.79141, 2.9145936e-07)
     Data Point: (73.663629, 1.5126527e-07)
     Data Point: (238.08664, 1.9915981e-08)
     Data Point: (769.51476, 4.4819192e-10)
     Data Point: (2,487.1322, 5.4439896e-12)
     Data Point: (8,038.6069, 1.2190828e-13)
     Data Point: (25,981.41, 4.1653601e-15)
     Data Point: (83,973.96, 1.9402147e-16)
     Data Point: (271,410.44, 9.7218954e-18)
     Data Point: (877,219.9, 4.8068369e-19)
     Data Point: (2,835,243.7, 2.3331535e-20)
     Data Point: (9,163,730.7, 8.5897964e-22)
     Data Point: (29,617,898, 3.0771945e-23)
     Data Point: (95,727,377, 3.0771945e-23)
     Data Point: (3.0939841e+08, 3.0771945e-23)
     Data Point: (1e+09, 3.0771945e-23)
Estimation Properties
     Hyd. K-Function Estimation Method: Fredlund-Xing Function
     Volume Water Content Function: Vol. Water Content Function 5
     Saturated Kx: 3.8e-07 ft/sec
```

**4B** 

Steady State Page 6 of 19

Maximum Suction: 1e+09 psf Minimum Suction: 0.20885434 psf

Num. Points: 20

## **Vol. Water Content Functions**

#### **2B**

Model: Vol WC Data Point Function

Function: Volumetric Water Content vs. Water Pressure

Compressibility: 1.6e-06 /psf

Saturated Water Content: 0.25847892 Residual Water Content: 0.025847892

Curve Fit to Data: 100 % Segment Curvature: 100 %

Porosity: 0.25847892

Data Points: Matric Suction (psf), Volumetric Water Content

Data Point: (0, 0.26)

Data Point: (0.20885434, 0.25999914) Data Point: (1.0263211, 0.25998986) Data Point: (5.0433953, 0.25987244) Data Point: (24.783507, 0.25836008) Data Point: (121.78744, 0.24045669) Data Point: (598.46982, 0.14136566)

Data Point: (398.40982, 0.14130300)
Data Point: (2,940.9118, 0.05386754)
Data Point: (14,451.794, 0.026960934)
Data Point: (71,016.866, 0.015657812)
Data Point: (348,980.57, 0.0087977367)
Data Point: (1,714,908.7, 0.0042703917)
Data Point: (8,427,150.5, 0.0012637314)

Data Point: (41,411,456, -0.00079695154)
Data Point: (2.0349805e+08, -0.0022645468)

Data Point: (1e+09, -0.0033454343)

**Estimation Properties** 

Vol. WC Estimation Method: Sample functions

Saturated Water Content: 0.26

Sample Material: Silt Liquid Limit: 38 %

Diameter at 10% passing: 0.03
Diameter at 60% passing: 0.29
Maximum Suction: 1e+09 psf
Minimum Suction: 0.20885434 psf

Num. Points: 15

#### 2A

Model: Vol WC Data Point Function

Function: Volumetric Water Content vs. Water Pressure

Compressibility: 0.0016 /psf

Saturated Water Content: 0.32852554 Residual Water Content: 0.032852554 Steady State Page 7 of 19

Curve Fit to Data: 100 % Segment Curvature: 100 % Porosity: 0.32852554 Data Points: Matric Suction (psf), Volumetric Water Content Data Point: (0, 0.25) Data Point: (0.20885434, 0.24999684) Data Point: (0.46927854, 0.24998884) Data Point: (1.0544303, 0.24996032) Data Point: (2.3692182, 0.24985846) Data Point: (5.3234385, 0.24949445) Data Point: (11.961329, 0.24819935) Data Point: (26.876122, 0.2436797) Data Point: (60.388438, 0.22894402) Data Point: (135.68786, 0.18991252) Data Point: (304.87946, 0.12553108) Data Point: (685.03908, 0.070438829) Data Point: (1,539.2265, 0.040711103) Data Point: (3,458.5154, 0.026089671) Data Point: (7,770.9998, 0.01820571) Data Point: (17,460.798, 0.013394317) Data Point: (39,232.977, 0.010098407) Data Point: (88,153.274, 0.0076211802) Data Point: (198,073.16, 0.0056608452) Data Point: (445,054.11, 0.0040908298) Data Point: (1,000,000, 0.002838267) **Estimation Properties** Vol. WC Estimation Method: Sample functions Saturated Water Content: 0.25 Sample Material: Silty Sand Liquid Limit: 25 % Diameter at 10% passing: 0.04 Diameter at 60% passing: 0.57 Maximum Suction: 1,000,000 psf Minimum Suction: 0.20885434 psf Num. Points: 20 Model: Vol WC Data Point Function Function: Volumetric Water Content vs. Water Pressure Compressibility: 6.6e-07 /psf Saturated Water Content: 0.29968497 Residual Water Content: 0.029968497 Curve Fit to Data: 100 % Segment Curvature: 100 % Porosity: 0.29968497 Data Points: Matric Suction (psf), Volumetric Water Content Data Point: (0, 0.3) Data Point: (0.20885434, 0.29999961) Data Point: (1.3967379, 0.29999522) Data Point: (9.3408478, 0.29993071)

**5B** 

Steady State Page 8 of 19

```
Data Point: (62.468013, 0.29890928)
     Data Point: (417.76215, 0.28356122)
     Data Point: (2,793.8332, 0.18393497)
     Data Point: (18,684.087, 0.09044456)
     Data Point: (124,952.02, 0.050132829)
     Data Point: (835,631.23, 0.025233608)
     Data Point: (5,588,381.6, 0.0085088796)
     Data Point: (37,372,956, -0.0031902541)
     Data Point: (2.4993602e+08, -0.011859391)
     Data Point: (1.6714764e+09, -0.018604408)
     Data Point: (1.1178194e+10, -0.024051087)
     Data Point: (7.4755479e+10, -0.028576013)
     Data Point: (4.9993601e+11, -0.032419581)
     Data Point: (3.3433806e+12, -0.035742976)
     Data Point: (2.2359249e+13, -0.038658693)
     Data Point: (1.4953009e+14, -0.041247871)
     Data Point: (1e+15, -0.04357067)
Estimation Properties
     Vol. WC Estimation Method: Sample functions
     Saturated Water Content: 0.3
     Sample Material: Clay
     Liquid Limit: 0 %
     Diameter at 10% passing: 0
     Diameter at 60% passing: 0
     Maximum Suction: 1e+15 psf
     Minimum Suction: 0.20885434 psf
     Num. Points: 20
Model: Vol WC Data Point Function
Function: Volumetric Water Content vs. Water Pressure
     Compressibility: 6.6e-07 /psf
     Saturated Water Content: 0.21000004
     Residual Water Content: 0.021000004
     Curve Fit to Data: 100 %
     Segment Curvature: 100 %
Porosity: 0.21000004
Data Points: Matric Suction (psf), Volumetric Water Content
     Data Point: (0, 0.21)
     Data Point: (0.20885434, 0.20999735)
     Data Point: (0.5979899, 0.2099863)
     Data Point: (1.7121594, 0.20992864)
     Data Point: (4.9022396, 0.20962695)
     Data Point: (14.036049, 0.20805808)
     Data Point: (40.187891, 0.20023981)
     Data Point: (115.06561, 0.16838213)
     Data Point: (329.45485, 0.10016865)
     Data Point: (943.2922, 0.047118847)
     Data Point: (2,700.8259, 0.024843159)
     Data Point: (7,732.9807, 0.01532325)
```

**4B** 

Steady State Page 9 of 19

Data Point: (22,141.002, 0.01034229)
Data Point: (63,393.92, 0.007187387)
Data Point: (181,508.91, 0.004915693)
Data Point: (519,694.7, 0.0032158143)
Data Point: (1,487,985.3, 0.0019491585)
Data Point: (4,260,386.3, 0.0010055093)
Data Point: (12,198,300, 0.00029514708)
Data Point: (34,926,065, -0.00024768896)
Data Point: (1e+08, -0.00066891256)

**Estimation Properties** 

Vol. WC Estimation Method: Sample functions

Saturated Water Content: 0.21 Sample Material: Silty Sand

Liquid Limit: 0 %

Diameter at 10% passing: 0
Diameter at 60% passing: 0
Maximum Suction: 1e+08 psf
Minimum Suction: 0.20885434 psf

Num. Points: 20

## Geometry

Name: Default Geometry

## **Settings**

View: 2D

Element Thickness: 1 ft

#### **Points**

|          | Х           | Υ           |
|----------|-------------|-------------|
| Point 1  | 100 ft      | 160 ft      |
| Point 2  | 100 ft      | 185.5 ft    |
| Point 3  | 0.9 ft      | 160 ft      |
| Point 4  | 100 ft      | 211.1475 ft |
| Point 5  | 3.8 ft      | 183 ft      |
| Point 6  | -20.1275 ft | 160 ft      |
| Point 7  | 100 ft      | 219.64 ft   |
| Point 8  | 42.5825 ft  | 219.8525 ft |
| Point 9  | 40.2 ft     | 223.2 ft    |
| Point 10 | 100 ft      | 223.6 ft    |
| Point 11 | -14.745 ft  | 165.2079 ft |
| Point 12 | 0 ft        | 211.7 ft    |
| Point 13 | 0 ft        | 192 ft      |
| Point 14 | 15.8 ft     | 192 ft      |
| Point 15 | 15.8 ft     | 211.7 ft    |
| Point 16 | 13 ft       | 192 ft      |
| Point 17 | 17.3 ft     | 209.4 ft    |
|          |             |             |

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| Point<br>18 | 17.3 ft    | 192 ft   |
|-------------|------------|----------|
| Point<br>19 | 17.3 ft    | 196 ft   |
| Point<br>20 | 17.3 ft    | 198 ft   |
| Point<br>21 | 41.8 ft    | 220.7 ft |
| Point<br>22 | 39.4 ft    | 223.2 ft |
| Point<br>23 | 26.6 ft    | 215.4 ft |
| Point<br>24 | 37.9 ft    | 223.2 ft |
| Point<br>25 | 6.13959 ft | 185.3 ft |
| Point<br>26 | -58.7 ft   | 160 ft   |
| Point<br>27 | 8.9 ft     | 192 ft   |
| Point<br>28 | -100 ft    | 160 ft   |
| Point<br>29 | -100 ft    | 170.1 ft |
| Point<br>30 | -91.8 ft   | 174.4 ft |
| Point<br>31 | -88.3 ft   | 176.5 ft |
| Point<br>32 | -85.7 ft   | 177.8 ft |
| Point<br>33 | -83.4 ft   | 178.4 ft |
| Point<br>34 | -76 ft     | 178.9 ft |
| Point<br>35 | -74 ft     | 179.7 ft |
| Point<br>36 | -55.9 ft   | 180.2 ft |
| Point<br>37 | -37.3 ft   | 182.3 ft |
| Point<br>38 | -30.3 ft   | 182.9 ft |
| Point<br>39 | -13.6 ft   | 190.2 ft |
| Point<br>40 | 0 ft       | 195 ft   |
| Point<br>41 | 7 ft       | 223 ft   |

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| Point<br>42 | 15 ft          | 223 ft          |
|-------------|----------------|-----------------|
| Point<br>43 | 15 ft          | 211.7 ft        |
| Point<br>44 | 7 ft           | 211.7 ft        |
| Point<br>45 | -4 ft          | 196.2 ft        |
| Point<br>46 | 28.4 ft        | 208.3 ft        |
| Point<br>47 | 30.5 ft        | 208.5 ft        |
| Point<br>48 | 17.3 ft        | 206.4 ft        |
| Point<br>49 | 23.3 ft        | 207.4 ft        |
| Point<br>50 | -37.3275<br>ft | 162.2725<br>ft  |
| Point<br>51 | -47.26 ft      | 160 ft          |
| Point<br>52 | -35.7 ft       | 164.7 ft        |
| Point<br>53 | -5.125 ft      | 182.98095<br>ft |
| Point<br>54 | 80.7025<br>ft  | 160 ft          |
| Point<br>55 | -100 ft        | 129.8675<br>ft  |
| Point<br>56 | 100 ft         | 129.8675<br>ft  |
| Point<br>57 | -100 ft        | 147.8625<br>ft  |
| Point<br>58 | -27.95 ft      | 152.3875<br>ft  |
| Point<br>59 | -100 ft        | 133.97 ft       |
| Point<br>60 | 15.8 ft        | 196.6 ft        |
| Point<br>61 | 15.8 ft        | 194.7 ft        |
| Point<br>62 | 47.6775<br>ft  | 208.84 ft       |
| Point<br>63 | 100 ft         | 209.9025<br>ft  |
| Point<br>64 | 95.42762<br>ft | 209.80965<br>ft |
| Point<br>65 | 3.915 ft       | 160.77581<br>ft |

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| Point<br>66 | 17.7925<br>ft   | 187.09412<br>ft |
|-------------|-----------------|-----------------|
| Point<br>67 | 2.11662<br>ft   | 161.95136<br>ft |
| Point<br>68 | -26.69893<br>ft | 160 ft          |
| Point<br>69 | 28.7 ft         | 129.8675<br>ft  |
| Point<br>70 | 15.8 ft         | 208.5 ft        |
| Point<br>71 | 0 ft            | 198.7 ft        |
| Point<br>72 | 47.15 ft        | 195.68393<br>ft |
| Point<br>73 | -6.48 ft        | 194.6 ft        |
| Point<br>74 | 17.3 ft         | 194.753 ft      |
| Point<br>75 | 15.8 ft         | 194.69918<br>ft |
| Point<br>76 | 12.0389<br>ft   | 194.2 ft        |
| Point<br>77 | 0 ft            | 193.99246<br>ft |
| Point<br>78 | 42.67 ft        | 194.37311<br>ft |
| Point<br>79 | -8.4 ft         | 192.9 ft        |
| Point<br>80 | 17.3 ft         | 193.63688<br>ft |
| Point<br>81 | 15.8 ft         | 193.58544<br>ft |
| Point<br>82 | 14.51892<br>ft  | 193.40778<br>ft |
| Point<br>83 | 10.54633<br>ft  | 193.27156<br>ft |
| Point<br>84 | 0 ft            | 192.9 ft        |
| Point<br>85 | -32.3 ft        | 165.4 ft        |
| Point<br>86 | -6.9 ft         | 172.7 ft        |
| Point<br>87 | -100 ft         | 150.0525<br>ft  |
| Point<br>88 | -12 ft          | 170.6 ft        |
| Point<br>89 | -18.785 ft      | 168.6 ft        |

Steady State Page 13 of 19

| Point<br>90 | -71.0125<br>ft | 157.56 ft      |
|-------------|----------------|----------------|
| Point<br>91 | -77.8075<br>ft | 155.915 ft     |
| Point<br>92 | -79.7925<br>ft | 155.915 ft     |
| Point<br>93 | -80.36 ft      | 155.4225<br>ft |
| Point<br>94 | -97.6 ft       | 151.41 ft      |

# Lines

|         | Start Point | End Point | Hydraulic Boundary        | Length    | Angle    |
|---------|-------------|-----------|---------------------------|-----------|----------|
| Line 1  | 1           | 2         | Right Total head constant | 25.5 ft   | 90°      |
| Line 2  | 4           | 7         | Right Total head constant | 8.4925 ft | 90°      |
| Line 3  | 7           | 8         |                           | 57.418 ft | -0.212 ° |
| Line 4  | 7           | 10        |                           | 3.96 ft   | 90°      |
| Line 5  | 10          | 9         |                           | 59.801 ft | 0.383 °  |
| Line 6  | 11          | 6         |                           | 7.4896 ft | 44.1 °   |
| Line 7  | 14          | 16        |                           | 2.8 ft    | 0 °      |
| Line 8  | 18          | 14        |                           | 1.5 ft    | 0 °      |
| Line 9  | 17          | 15        |                           | 2.7459 ft | -56.9°   |
| Line 10 | 19          | 20        |                           | 2 ft      | 90°      |
| Line 11 | 9           | 21        |                           | 2.9682 ft | -57.4 °  |
| Line 12 | 21          | 8         |                           | 1.1535 ft | -47.3 °  |
| Line 13 | 22          | 9         |                           | 0.8 ft    | 0 °      |
| Line 14 | 17          | 23        | Flux                      | 11.068 ft | 32.8°    |
| Line 15 | 23          | 24        | Flux                      | 13.731 ft | 34.6°    |
| Line 16 | 24          | 22        |                           | 1.5 ft    | 0 °      |
| Line 17 | 16          | 25        |                           | 9.5893 ft | 44.3 °   |
| Line 18 | 25          | 5         |                           | 3.2808 ft | 44.5 °   |
| Line 19 | 27          | 16        |                           | 4.1 ft    | 0 °      |
| Line 20 | 26          | 28        |                           | 41.3 ft   | 0 °      |
| Line 21 | 28          | 29        |                           | 10.1 ft   | 90 °     |
| Line 22 | 29          | 30        | Flux                      | 9.259 ft  | 27.7°    |
| Line 23 | 30          | 31        | Flux                      | 4.0817 ft | 31 °     |
| Line 24 | 31          | 32        | Flux                      | 2.9069 ft | 26.6°    |
| Line 25 | 32          | 33        | Flux                      | 2.377 ft  | 14.6°    |
| Line 26 | 33          | 34        | Flux                      | 7.4169 ft | 3.87 °   |
| Line 27 | 34          | 35        | Flux                      | 2.1541 ft | 21.8°    |
| Line 28 | 35          | 36        | Flux                      | 18.107 ft | 1.58 °   |
| Line 29 | 36          | 37        | Flux                      | 18.718 ft | 6.44°    |
| Line 30 | 37          | 38        | Flux                      | 7.0257 ft | 4.9 °    |
| Line 31 | 38          | 39        | Flux                      | 18.226 ft | 23.6°    |
| Line 32 | 15          | 43        |                           | 0.8 ft    | 0 °      |

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| Line 33 | 43 | 44 | I                         | 8 ft      | 0 °     |
|---------|----|----|---------------------------|-----------|---------|
| Line 34 | 44 | 12 |                           | 7 ft      | 0°      |
| Line 35 | 41 | 42 |                           | 8 ft      | 0 °     |
| Line 36 | 42 | 43 |                           | 11.3 ft   | 90 °    |
| Line 37 | 44 | 41 |                           | 11.3 ft   | 90 °    |
| Line 38 | 24 | 42 |                           | 22.901 ft | 0.5 °   |
| Line 39 | 20 | 46 |                           | 15.143 ft | 42.9°   |
| Line 40 | 46 | 21 |                           | 18.257 ft | 42.8 °  |
| Line 41 | 8  | 47 |                           | 16.579 ft | 43.2 °  |
| Line 42 | 47 | 19 |                           | 18.179 ft | 43.4°   |
| Line 43 | 46 | 47 |                           | 2.1095 ft | 5.44°   |
| Line 44 | 20 | 48 |                           | 8.4 ft    | 90 °    |
| Line 45 | 48 | 17 |                           | 3 ft      | 90°     |
| Line 46 | 46 | 49 |                           | 5.1788 ft | 10 °    |
| Line 47 | 49 | 48 |                           | 6.0828 ft | 9.46 °  |
| Line 48 | 50 | 51 |                           | 10.189 ft | 12.9°   |
| Line 49 | 26 | 51 |                           | 11.44 ft  | 0 °     |
| Line 50 | 13 | 27 |                           | 8.9 ft    | 0 °     |
| Line 51 | 53 | 27 |                           | 16.675 ft | 32.7°   |
| Line 52 | 3  | 54 |                           | 79.802 ft | 0 °     |
| Line 53 | 54 | 1  |                           | 19.297 ft | 0 °     |
| Line 54 | 56 | 1  | Right Total head constant | 30.132 ft | 90°     |
| Line 55 | 51 | 57 |                           | 54.119 ft | 13 °    |
| Line 56 | 6  | 58 |                           | 10.915 ft | 44.2 °  |
| Line 57 | 57 | 59 | Total head at left side   | 13.893 ft | 90°     |
| Line 58 | 59 | 55 | Total head at left side   | 4.1025 ft | 90°     |
| Line 59 | 58 | 59 |                           | 74.367 ft | 14.3 °  |
| Line 60 | 3  | 58 |                           | 29.837 ft | 14.8 °  |
| Line 61 | 60 | 20 |                           | 2.0518 ft | 43 °    |
| Line 62 | 61 | 60 |                           | 1.9 ft    | 90 °    |
| Line 63 | 61 | 19 |                           | 1.9849 ft | 40.9 °  |
| Line 64 | 2  | 63 | Right Total head constant | 24.403 ft | 90 °    |
| Line 65 | 63 | 4  | Right Total head constant | 1.245 ft  | 90 °    |
| Line 66 | 4  | 64 |                           | 4.7641 ft | 16.3 °  |
| Line 67 | 63 | 64 |                           | 4.5733 ft | 1.16°   |
| Line 68 | 64 | 62 |                           | 47.76 ft  | 1.16°   |
| Line 69 | 62 | 47 |                           | 17.181 ft | 1.13 °  |
| Line 70 | 2  | 65 |                           | 99.215 ft | 14.4°   |
| Line 71 | 65 | 3  |                           | 3.1132 ft | 14.4°   |
| Line 72 | 66 | 5  |                           | 14.579 ft | 16.3°   |
| Line 73 | 67 | 65 |                           | 2.1485 ft | -33.2 ° |
|         |    |    |                           |           |         |

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| Line<br>74 | 67 | 3  |      | 2.2996 ft     | 58.1°  |
|------------|----|----|------|---------------|--------|
| Line<br>75 | 51 | 68 |      | 20.561 ft     | 0 °    |
| Line<br>76 | 68 | 6  |      | 6.5714 ft     | 0°     |
| Line<br>77 | 55 | 69 |      | 128.7 ft      | 0 °    |
| Line<br>78 | 69 | 56 |      | 71.3 ft       | 0°     |
| Line<br>79 | 60 | 70 |      | 11.9 ft       | 90°    |
| Line<br>80 | 70 | 15 |      | 3.2 ft        | 90°    |
| Line<br>81 | 17 | 70 |      | 1.7493 ft     | 31°    |
| Line<br>82 | 12 | 71 |      | 13 ft         | 90°    |
| Line<br>83 | 71 | 40 |      | 3.7 ft        | 90°    |
| Line<br>84 | 70 | 71 | Flux | 18.592 ft     | 31.8°  |
| Line<br>85 | 71 | 45 | Flux | 4.717 ft      | 32 °   |
| Line<br>86 | 64 | 72 |      | 50.302 ft     | 16.3 ° |
| Line<br>87 | 73 | 45 | Flux | 2.9513 ft     | 32.8°  |
| Line<br>88 | 19 | 74 |      | 1.247 ft      | 90°    |
| Line<br>89 | 75 | 61 |      | 0.00082<br>ft | 90°    |
| Line<br>90 | 76 | 60 |      | 4.4616 ft     | 32.5°  |
| Line<br>91 | 40 | 77 |      | 1.0075 ft     | 90°    |
| Line<br>92 | 72 | 78 |      | 4.6678 ft     | 16.3 ° |
| Line<br>93 | 78 | 66 |      | 25.921 ft     | 16.3 ° |
| Line<br>94 | 39 | 79 | Flux | 5.8592 ft     | 27.4°  |
| Line<br>95 | 79 | 73 | Flux | 2.5644 ft     | 41.5 ° |
| Line<br>96 | 74 | 80 |      | 1.1161 ft     | 90°    |
| Line<br>97 | 80 | 18 |      | 1.6369 ft     | 90°    |

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| Line<br>98  | 14 | 81 |                         | 1.5854 ft     | 90°    |
|-------------|----|----|-------------------------|---------------|--------|
| Line<br>99  | 81 | 75 |                         | 1.1137 ft     | 90°    |
| Line<br>100 | 16 | 82 |                         | 2.071 ft      | 42.8°  |
| Line<br>101 | 27 | 83 |                         | 2.0802 ft     | 37.7°  |
| Line<br>102 | 83 | 76 |                         | 1.7578 ft     | 31.9°  |
| Line<br>103 | 77 | 84 |                         | 1.0925 ft     | 90 °   |
| Line<br>104 | 84 | 13 |                         | 0.9 ft        | 90 °   |
| Line<br>105 | 84 | 79 |                         | 8.4 ft        | 0 °    |
| Line<br>106 | 11 | 86 |                         | 10.848 ft     | 43.7°  |
| Line<br>107 | 85 | 50 |                         | 5.9209 ft     | 31.9°  |
| Line<br>108 | 53 | 85 |                         | 32.366 ft     | 32.9°  |
| Line<br>109 | 86 | 5  |                         | 14.852 ft     | 43.9°  |
| Line<br>110 | 52 | 85 |                         | 3.4713 ft     | 11.6°  |
| Line<br>111 | 28 | 87 | Total head at left side | 9.9475 ft     | 90 °   |
| Line<br>112 | 87 | 57 | Total head at left side | 2.19 ft       | 90°    |
| Line<br>113 | 26 | 52 |                         | 23.475 ft     | 11.5°  |
| Line<br>114 | 88 | 86 |                         | 5.5154 ft     | 22.4°  |
| Line<br>115 | 85 | 89 |                         | 13.889 ft     | 13.3 ° |
| Line<br>116 | 89 | 88 |                         | 7.0736 ft     | 16.4°  |
| Line<br>117 | 26 | 90 |                         | 12.552 ft     | 11.2°  |
| Line<br>118 | 90 | 91 |                         | 6.9913 ft     | 13.6°  |
| Line<br>119 | 91 | 92 |                         | 1.985 ft      | 0°     |
| Line<br>120 | 92 | 93 |                         | 0.75141<br>ft | 41°    |
| Line<br>121 | 93 | 94 |                         | 17.701 ft     | 13.1°  |

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| Line<br>122 | 94 | 87 | 2.7573<br>ft | 29.5°  |
|-------------|----|----|--------------|--------|
| Line<br>123 | 61 | 82 | 1.8196<br>ft | 45.2 ° |

# Regions

|              | Material   | Points                                | Area                       |
|--------------|--|---------------------------------------|----------------------------|
| Region<br>1  | to Very Dense<br>Sand/Gravel   | 1,2,65,3,54                           | 1,263.5<br>ft <sup>2</sup> |
| Region 2     | ESU 5B Very<br>Stiff to Hard Silt<br>and Clay/Dense<br>to Very Dense<br>Silt | 65,2,63,64,72,78,66,5,86,11,6,58,3,67 | 2,652.9<br>ft <sup>2</sup> |
| Region 3     |  | 9,21,8,7,10                           | 214.55<br>ft <sup>2</sup>  |
| Region<br>4  |  | 12,71,70,15,43,44                     | 127.98<br>ft²              |
| Region<br>5  | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel                                 | 15,70,17                              | 2.4 ft <sup>2</sup>        |
| Region<br>6  | ESU 2B Medium<br>Dense<br>Sand/Gravel  | 47,19,20,46                           | 22.905<br>ft²              |
| Region<br>7  | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel                                 | 21,46,49,48,17,23,24,22,9             | 146.15<br>ft <sup>2</sup>  |
| Region<br>8  |  | 41,42,43,44                           | 90.4 ft <sup>2</sup>       |
| Region<br>9  |  | 24,42,43,15,17,23                     | 170.39<br>ft <sup>2</sup>  |
| Region<br>10 | ESU 2B Medium<br>Dense<br>Sand/Gravel  | 21,46,47,8                            | 21.242<br>ft <sup>2</sup>  |
| Region<br>11 | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel                                 | 46,49,48,20                           | 46.47<br>ft <sup>2</sup>   |
| Region<br>12 | ESU 2B Medium<br>Dense<br>Sand/Gravel  | 27,53,85,89,88,86,5,25,16             | 239.18<br>ft²              |
| Region<br>13 | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel                                 | 28,87,94,93,92,91,90,26               | 183.51<br>ft²              |
| Region<br>14 | ESU 4B Dense<br>to Very Dense<br>Sand/Gravel                                 | 55,69,56,1,54,3,58,59                 | 4,704.7<br>ft <sup>2</sup> |
| Region<br>15 |  | 51,57,59,58,6,68                      | 921.68<br>ft <sup>2</sup>  |

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|              | ESU 2B<br>Medium<br>Dense<br>Sand/Gravel  |  |                           |
|--------------|---|--|---------------------------|
| Region<br>16 | ESU 2B<br>Medium<br>Dense<br>Sand/Gravel  | 20,60,61,19                              | 2.925<br>ft <sup>2</sup>  |
| Region<br>17 | ESU 5B Very<br>Stiff to Hard<br>Silt and<br>Clay/Dense<br>to Very<br>Dense Silt | 4,64,63                                  | 2.8463<br>ft <sup>2</sup> |
| Region<br>18 | ESU 4B<br>Dense to<br>Very Dense<br>Sand/Gravel                                 | 4,7,8,47,62,64                           | 662.96<br>ft <sup>2</sup> |
| Region<br>19 | ESU 5B Very<br>Stiff to Hard<br>Silt and<br>Clay/Dense<br>to Very<br>Dense Silt | 65,67,3                                  | 2.4697<br>ft <sup>2</sup> |
| Region<br>20 | ESU 2B<br>Medium<br>Dense<br>Sand/Gravel  | 50,51,68,6,11,86,88,89,85                | 165.47<br>ft <sup>2</sup> |
| Region<br>21 | ESU 2A Very<br>Loose to<br>Loose<br>Sand/Gravel                                 | 60,20,48,17,70                           | 17.475<br>ft <sup>2</sup> |
| Region<br>22 | ESU 2A Very<br>Loose to<br>Loose<br>Sand/Gravel                                 | 76,60,70,71,40,77,84,13,27,83            | 166.85<br>ft <sup>2</sup> |
| Region<br>23 | ESU 2A Very<br>Loose to<br>Loose<br>Sand/Gravel                                 | 40,71,45,73,79,84,77                     | 26.032<br>ft <sup>2</sup> |
| Region<br>24 | ESU 4B<br>Dense to<br>Very Dense<br>Sand/Gravel                                 | 72,64,62,47,19,74,80,18,14,16,25,5,66,78 | 803.96<br>ft <sup>2</sup> |
| Region<br>25 | ESU 4B<br>Dense to<br>Very Dense<br>Sand/Gravel                                 | 74,19,61,75,81,14,18,80                  | 5.025<br>ft <sup>2</sup>  |
| Region<br>26 | ESU 4B<br>Dense to  | 75,61,82,16,14,81                        | 3.7004<br>ft <sup>2</sup> |

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|              | Very Dense<br>Sand/Gravel                       |   |                            |
|--------------|---|---|----------------------------|
| Region<br>27 | ESU 2A Very<br>Loose to<br>Loose<br>Sand/Gravel | 39,38,37,36,35,34,33,32,31,30,29,28,26,52,85,53,27,13,84,79 | 1,658.1<br>ft <sup>2</sup> |
| Region<br>28 | ESU 2B<br>Medium<br>Dense<br>Sand/Gravel        | 61,60,76,83,27,16,82  | 12.725<br>ft <sup>2</sup>  |
| Region<br>29 | ESU 2A Very<br>Loose to<br>Loose<br>Sand/Gravel | 85,52,26,51,50  | 40.647<br>ft <sup>2</sup>  |
| Region<br>30 | ESU 2A Very<br>Loose to<br>Loose<br>Sand/Gravel | 26,90,91,92,93,94,87,57,51                                  | 136.56<br>ft <sup>2</sup>  |

# **Mesh Properties**

Global Element Size: 5 ft







In Association with

# **Appendix J** Slope/W Reports – Global Stability

# Static - Spencer

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## **File Information**

File Version: 10.02 Title: 05.33R

Created By: Yi Tyan Tsai Last Edited By: Bo Zhang Revision Number: 54 Date: 08/03/2021 Time: 12:34:15 PM

Tool Version: 10.2.1.19666 File Name: 05.33R (2020.04).gsz

Directory: \\geoengineers.com\WAN\Projects\0\0180366\01\Analysis\05.33R\

Last Solved Date: 08/03/2021 Last Solved Time: 12:34:28 PM

# **Project Settings**

Unit System: U.S. Customary Units

# **Analysis Settings**

## Static - Spencer

Kind: SLOPE/W Method: Spencer

Settings

PWP Conditions from: Piezometric Line Apply Phreatic Correction: No Use Staged Rapid Drawdown: No Unit Weight of Water: 62.430189 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 1

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

Factor of Safety Convergence Settings
Maximum Number of Iterations: 100
Tolerable difference in F of S: 0.001

Solution Settings

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3 Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

#### **Materials**

### 4B Dense to V. Dense Sand/Gravel

Model: Mohr-Coulomb Unit Weight: 130 pcf Cohesion': 0 psf

Phi': 43 ° Phi-B: 0 °

Pore Water Pressure
Piezometric Line: 1

#### **Barrier**

Model: High Strength Unit Weight: 150 pcf Pore Water Pressure Piezometric Line: 1

#### 1B Med. Dense to V. Dense Coarse-Grained Fill

Model: Mohr-Coulomb Unit Weight: 120 pcf Cohesion': 0 psf Phi': 36 °

Phi-B: 0 °

Pore Water Pressure Piezometric Line: 1

## 1C V. Soft to Med. Stiff/V. Loose to Loose Fine-Grained Fill

Model: Mohr-Coulomb Unit Weight: 115 pcf Cohesion': 0 psf

Phi': 27 ° Phi-B: 0 °

Pore Water Pressure
Piezometric Line: 1

#### **Common Borrow**

Model: Mohr-Coulomb Unit Weight: 120 pcf Cohesion': 0 psf

Phi': 32 ° Phi-B: 0 °

Pore Water Pressure Piezometric Line: 1

# **Slip Surface Entry and Exit**

Left Type: Range

Left-Zone Left Coordinate: (-12.8, 123.63441) ft

Left-Zone Right Coordinate: (-2.8, 123.5) ft

Left-Zone Increment: 10 Right Type: Range

Right-Zone Left Coordinate: (-1, 127.47616) ft Right-Zone Right Coordinate: (11, 130.16923) ft

Right-Zone Increment: 12 Radius Increments: 10

# **Slip Surface Limits**

Left Coordinate: (-40, 124) ft Right Coordinate: (80, 125.5) ft

## **Piezometric Lines**

#### Piezometric Line 1

#### Coordinates

|              | Х      | Υ        |
|--------------|--------|----------|
| Coordinate 1 | -40 ft | 117.5 ft |
| Coordinate 2 | 80 ft  | 117.5 ft |

## Geometry

Name: 2D Geometry

## **Settings**

View: 2D

Element Thickness: 1 ft

#### **Points**

| ILS      |              |              |
|----------|--------------|--------------|
|          | Х            | Υ            |
| Point 1  | -40 ft       | 124 ft       |
| Point 2  | -1.1 ft      | 123.5 ft     |
| Point 3  | -1.2 ft      | 126 ft       |
| Point 4  | 10 ft        | 130.1 ft     |
| Point 5  | 23 ft        | 131 ft       |
| Point 6  | 80 ft        | 125.5 ft     |
| Point 7  | 80 ft        | 95 ft        |
| Point 8  | -40 ft       | 95 ft        |
| Point 9  | -2.8 ft      | 123.5 ft     |
| Point 10 | -2.2 ft      | 128.5 ft     |
| Point 11 | -1.3 ft      | 128.5 ft     |
| Point 12 | -40 ft       | 115 ft       |
| Point 13 | 80 ft        | 115 ft       |
| Point 14 | -40 ft       | 100 ft       |
| Point 15 | 80 ft        | 100 ft       |
| Point 16 | -1.258888 ft | 127.47219 ft |
| Point 17 | 3 ft         | 127.5375 ft  |
|          |              |              |

### **Regions**

|          | Material   | Points                 | Area                    |
|----------|--|------------------------|-------------------------|
| Region 1 | 1B Med. Dense to V. Dense Coarse-Grained Fill                | 1,9,2,3,17,4,5,6,13,12 | 1,442.5 ft <sup>2</sup> |
| Region 2 | Barrier  | 9,10,11,16,3,2         | 6.5 ft <sup>2</sup>     |
| Region 3 | 4B Dense to V. Dense Sand/Gravel                             | 7,8,14,15              | 600 ft <sup>2</sup>     |
| Region 4 | 1C V. Soft to Med. Stiff/V. Loose to Loose Fine-Grained Fill | 12,13,15,14            | 1,800 ft <sup>2</sup>   |
| Region 5 | Common Borrow  | 16,17,3                | 3.1369 ft <sup>2</sup>  |

# **Slip Results**

Slip Surfaces Analysed: 611 of 1573 converged

# **Current Slip Surface**

Slip Surface: 900 Factor of Safety: 1.69 Volume: 18.210888 ft<sup>3</sup> Weight: 2,380.3065 lbf

Resisting Moment: 10,249.147 lbf·ft Activating Moment: 6,064.1791 lbf·ft Resisting Force: 1,459.9305 lbf Activating Force: 863.55344 lbf Slip Rank: 1 of 1,573 slip surfaces

Exit: (-6.8, 123.55376) ft

Entry: (2.1139218, 127.52391) ft

Radius: 6.0990083 ft

Center: (-3.831987, 128.88188) ft

# Slip Slices

|            | X                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base<br>Material                               |
|------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|--|
| Slice<br>1 | -6.6461539<br>ft | 123.47371<br>ft | -372.93977<br>psf | 23.616385<br>psf         | 17.158308<br>psf       | 0 psf                | 0 psf               | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>2 | -6.3384615<br>ft | 123.32427<br>ft | -363.61026<br>psf | 59.144735<br>psf         | 42.971165<br>psf       | 0 psf                | 0 psf               | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>3 | -6.0307692<br>ft | 123.1954<br>ft  | -355.56477<br>psf | 82.51457<br>psf          | 59.950344<br>psf       | 0 psf                | 0 psf               | 1B Med. Dense to V. Dense Coarse- Grained Fil  |
| Slice<br>4 | -5.7230769<br>ft | 123.08572<br>ft | -348.71729<br>psf | 97.860875<br>psf         | 71.100088<br>psf       | 0 psf                | 0 psf               | 1B Med. Dense to V. Dense Coarse- Grained Fil  |
| Slice      | -5.4153846       | 122.99415       | -343.00063        | 107.52192                | 78.11925               | 0 psf                | 0 psf               | 1B Med.  |

| , 12.06 PW  | 1                |                 |                   | Static           | - Spencer        |       |       |  |
|-------------|------------------|-----------------|-------------------|------------------|------------------|-------|-------|--|
| 5           | ft               | ft              | psf               | psf              | psf              |       |       | Dense to V. Dense Coarse- Grained Fill         |
| Slice<br>6  | -5.1076923<br>ft | 122.91985<br>ft | -338.36251<br>psf | 112.92261<br>psf | 82.043081<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>7  | -4.8 ft          | 122.8622<br>ft  | -334.76288<br>psf | 114.98584<br>psf | 83.542104<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>8  | -4.4923077<br>ft | 122.8207<br>ft  | -332.17202<br>psf | 114.34018<br>psf | 83.073006<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>9  | -4.1846154<br>ft | 122.79502<br>ft | -330.56925<br>psf | 111.43213<br>psf | 80.960185<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>10 | -3.8769231<br>ft | 122.78498<br>ft | -329.94203<br>psf | 106.59038<br>psf | 77.442445<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>11 | -3.5692308<br>ft | 122.79048<br>ft | -330.28555<br>psf | 100.06453<br>psf | 72.701137<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>12 | -3.2615385<br>ft | 122.81157<br>ft | -331.60243<br>psf | 92.049521<br>psf | 66.877892<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>13 | -2.9538462<br>ft | 122.84842<br>ft | -333.90292<br>psf | 82.701669<br>psf | 60.086279<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>14 | -2.65 ft         | 122.90045<br>ft | -337.15136<br>psf | 261.60728<br>psf | 190.06882<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>15 | -2.35 ft         | 122.96768<br>ft | -341.34845<br>psf | 604.73684<br>psf | 439.36703<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>16 | -2.05 ft         | 123.05111<br>ft | -346.557<br>psf   | 743.25263<br>psf | 540.00464<br>psf | 0 psf | 0 psf | 1B Med.<br>Dense to V.                         |

| , 12.001 1  |                   |                 | ı                 |                  | ропост           |       |       | 1  |
|-------------|-------------------|-----------------|-------------------|------------------|------------------|-------|-------|--|
|             |                   |                 |                   |                  |                  |       |       | Dense<br>Coarse-<br>Grained Fill               |
| Slice<br>17 | -1.75 ft          | 123.15145<br>ft | -352.8213<br>psf  | 701.01914<br>psf | 509.32022<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>18 | -1.45 ft          | 123.26962<br>ft | -360.19818<br>psf | 658.83006<br>psf | 478.66805<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>19 | -1.279444 ft      | 123.34275<br>ft | -364.7641<br>psf  | 571.43575<br>psf | 415.17238<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>20 | -1.229444 ft      | 123.36612<br>ft | -366.22281<br>psf | 483.58869<br>psf | 351.34775<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>21 | -1.15 ft          | 123.40449<br>ft | -368.61858<br>psf | 425.91465<br>psf | 309.4451<br>psf  | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>22 | -0.95795805<br>ft | 123.5049<br>ft  | -374.88686<br>psf | 374.74493<br>psf | 272.26813<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>23 | -0.67387415<br>ft | 123.66684<br>ft | -384.99679<br>psf | 343.89899<br>psf | 249.85724<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>24 | -0.38979025<br>ft | 123.85002<br>ft | -396.4331<br>psf  | 312.45317<br>psf | 227.01052<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>25 | -0.10570635<br>ft | 124.05689<br>ft | -409.34775<br>psf | 280.32498<br>psf | 203.66802<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>26 | 0.17837754<br>ft  | 124.29066<br>ft | -423.94199<br>psf | 247.4273<br>psf  | 179.76646<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>27 | 0.46246144<br>ft  | 124.55573<br>ft | -440.49053<br>psf | 213.66587<br>psf | 155.23734<br>psf | 0 psf | 0 psf | 1B Med.<br>Dense to V.<br>Dense                |

| 12:00 PW    | Static - Spencer |                 |                   |                  |                  |       |       |  |
|-------------|------------------|-----------------|-------------------|------------------|------------------|-------|-------|--|
|             |                  |                 |                   |                  |                  |       |       | Coarse-<br>Grained Fill                        |
| Slice<br>28 | 0.74654534<br>ft | 124.85837<br>ft | -459.38421<br>psf | 178.93709<br>psf | 130.00541<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>29 | 1.0306292 ft     | 125.208 ft      | -481.21217<br>psf | 143.1273<br>psf  | 103.98807<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>30 | 1.3147131 ft     | 125.62013<br>ft | -506.94151<br>psf | 106.11802<br>psf | 77.099253<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>31 | 1.598797 ft      | 126.12397<br>ft | -538.39583<br>psf | 67.813543<br>psf | 49.269423<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>32 | 1.8828809 ft     | 126.79211<br>ft | -580.10825<br>psf | 28.250688<br>psf | 20.525326<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>33 | 2.0694223 ft     | 127.35223<br>ft | -615.07671<br>psf | 5.4652441<br>psf | 3.4150635<br>psf | 0 psf | 0 psf | Common<br>Borrow                               |

1/11/22, 12:06 PM Static - MP

# Static - MP

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## **File Information**

File Version: 10.02 Title: 05.33R

Created By: Yi Tyan Tsai Last Edited By: Bo Zhang Revision Number: 54 Date: 08/03/2021 Time: 12:34:15 PM

Tool Version: 10.2.1.19666 File Name: 05.33R (2020.04).gsz

Directory: \\geoengineers.com\WAN\Projects\0\0180366\01\Analysis\05.33R\

Last Solved Date: 08/03/2021 Last Solved Time: 12:34:28 PM

# **Project Settings**

Unit System: U.S. Customary Units

# **Analysis Settings**

#### Static - MP

Kind: SLOPE/W

Method: Morgenstern-Price

Settings

**Side Function** 

Interslice force function option: Half-Sine

PWP Conditions from: Piezometric Line Apply Phreatic Correction: No Use Staged Rapid Drawdown: No Unit Weight of Water: 62.430189 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 1

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

**Factor of Safety Convergence Settings** 

Maximum Number of Iterations: 100 Tolerable difference in F of S: 0.001

**Solution Settings** 

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3 Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

## **Materials**

### 4B Dense to V. Dense Sand/Gravel

Model: Mohr-Coulomb Unit Weight: 130 pcf Cohesion': 0 psf Phi': 43 ° Phi-B: 0 °

Pore Water Pressure Piezometric Line: 1

#### **Barrier**

Model: High Strength
Unit Weight: 150 pcf
Pore Water Pressure
Piezometric Line: 1

#### 1B Med. Dense to V. Dense Coarse-Grained Fill

Model: Mohr-Coulomb Unit Weight: 120 pcf Cohesion': 0 psf Phi': 36 °

Phi-B: 0 ° Pore Water Pressure

Piezometric Line: 1

1C V. Soft to Med. Stiff/V. Loose to Loose Fine-Grained Fill

Model: Mohr-Coulomb Unit Weight: 115 pcf Cohesion': 0 psf

Phi': 27 ° Phi-B: 0 °

Pore Water Pressure Piezometric Line: 1

#### **Common Borrow**

Model: Mohr-Coulomb Unit Weight: 120 pcf Cohesion': 0 psf Phi': 32 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

# **Slip Surface Entry and Exit**

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Left Type: Range

Left-Zone Left Coordinate: (-12.8, 123.63441) ft Left-Zone Right Coordinate: (-2.8, 123.5) ft

Left-Zone Increment: 10 Right Type: Range

Right-Zone Left Coordinate: (-1, 127.47616) ft Right-Zone Right Coordinate: (11, 130.16923) ft

Right-Zone Increment: 12 Radius Increments: 10

# **Slip Surface Limits**

Left Coordinate: (-40, 124) ft Right Coordinate: (80, 125.5) ft

## **Piezometric Lines**

#### Piezometric Line 1

#### **Coordinates**

|              | Х      | Υ        |
|--------------|--------|----------|
| Coordinate 1 | -40 ft | 117.5 ft |
| Coordinate 2 | 80 ft  | 117.5 ft |

# Geometry

Name: 2D Geometry

# **Settings**

View: 2D

Element Thickness: 1 ft

#### **Points**

|          | X                   | Υ        |  |  |  |
|----------|---------------------|----------|--|--|--|
| Point 1  | -40 ft              | 124 ft   |  |  |  |
| Point 2  | -1.1 ft             | 123.5 ft |  |  |  |
| Point 3  | -1.2 ft             | 126 ft   |  |  |  |
| Point 4  | 10 ft               | 130.1 ft |  |  |  |
| Point 5  | 23 ft               | 131 ft   |  |  |  |
| Point 6  | 80 ft               | 125.5 ft |  |  |  |
| Point 7  | 80 ft               | 95 ft    |  |  |  |
| Point 8  | -40 ft              | 95 ft    |  |  |  |
| Point 9  | -2.8 ft             | 123.5 ft |  |  |  |
| Point 10 | -2.2 ft             | 128.5 ft |  |  |  |
| Point 11 | -1.3 ft             | 128.5 ft |  |  |  |
| Point 12 | -40 ft              | 115 ft   |  |  |  |
| Point 13 | 80 ft               | 115 ft   |  |  |  |
| Point 14 | -40 ft              | 100 ft   |  |  |  |
| Point 15 | int 15 80 ft 100 ft |          |  |  |  |
|          |                     |          |  |  |  |

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| Point 16   -1.258888 ft |      | 127.47219 ft |  |  |
|-------------------------|------|--------------|--|--|
| Point 17                | 3 ft | 127.5375 ft  |  |  |

## **Regions**

|          | Material   | Points                 | Area                    |
|----------|--|------------------------|-------------------------|
| Region 1 | 1B Med. Dense to V. Dense Coarse-Grained Fill                | 1,9,2,3,17,4,5,6,13,12 | 1,442.5 ft <sup>2</sup> |
| Region 2 | Barrier  | 9,10,11,16,3,2         | 6.5 ft <sup>2</sup>     |
| Region 3 | 4B Dense to V. Dense Sand/Gravel                             | 7,8,14,15              | 600 ft <sup>2</sup>     |
| Region 4 | 1C V. Soft to Med. Stiff/V. Loose to Loose Fine-Grained Fill | 12,13,15,14            | 1,800 ft <sup>2</sup>   |
| Region 5 | Common Borrow  | 16,17,3                | 3.1369 ft <sup>2</sup>  |

# **Slip Results**

Slip Surfaces Analysed: 617 of 1573 converged

# **Current Slip Surface**

Slip Surface: 900 Factor of Safety: 1.69 Volume: 18.210888 ft<sup>3</sup> Weight: 2,380.3065 lbf

Resisting Moment: 10,261.094 lbf·ft Activating Moment: 6,064.1791 lbf·ft Resisting Force: 1,460.2611 lbf Activating Force: 862.80966 lbf Slip Rank: 1 of 1,573 slip surfaces

Exit: (-6.8, 123.55376) ft

Entry: (2.1139218, 127.52391) ft

Radius: 6.0990083 ft

Center: (-3.831987, 128.88188) ft

# Slip Slices

|            | X                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base<br>Material                             |
|------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|--|
| Slice<br>1 | -6.6461539<br>ft | 123.47371<br>ft | -372.93977<br>psf | 12.96744<br>psf          | 9.4213967<br>psf       | 0 psf                | 0 psf               | 1B Med. Dense to V Dense Coarse- Grained Fil |
| Slice<br>2 | -6.3384615<br>ft | 123.32427<br>ft | -363.61026<br>psf | 38.998734<br>psf         | 28.334239<br>psf       | 0 psf                | 0 psf               | 1B Med. Dense to V Dense Coarse- Grained Fi  |
| Slice<br>3 | -6.0307692<br>ft | 123.1954<br>ft  | -355.56477<br>psf | 63.877597<br>psf         | 46.409791<br>psf       | 0 psf                | 0 psf               | 1B Med. Dense to \ Dense Coarse- Grained Fi  |
| Slice<br>4 | -5.7230769<br>ft | 123.08572<br>ft | -348.71729<br>psf | 86.568582<br>psf         | 62.895757<br>psf       | 0 psf                | 0 psf               | 1B Med.<br>Dense to \<br>Dense               |

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|             |                  |                 |                   |                  |                  |       |       | Coarse                                      |
|-------------|------------------|-----------------|-------------------|------------------|------------------|-------|-------|---|
|             |                  |                 |                   |                  |                  |       |       | Graine                                      |
| Slice<br>5  | -5.4153846<br>ft | 122.99415<br>ft | -343.00063<br>psf | 105.9731<br>psf  | 76.993965<br>psf | 0 psf | 0 psf | 1B Me<br>Dense<br>Dense<br>Coarse<br>Graine |
| Slice<br>6  | -5.1076923<br>ft | 122.91985<br>ft | -338.36251<br>psf | 121.10881<br>psf | 87.990699<br>psf | 0 psf | 0 psf | 1B Me<br>Dense<br>Dense<br>Coarse<br>Graine |
| Slice<br>7  | -4.8 ft          | 122.8622<br>ft  | -334.76288<br>psf | 131.27502<br>psf | 95.376886<br>psf | 0 psf | 0 psf | 1B Me<br>Dense<br>Dense<br>Coarse<br>Graine |
| Slice<br>8  | -4.4923077<br>ft | 122.8207<br>ft  | -332.17202<br>psf | 136.15967<br>psf | 98.925791<br>psf | 0 psf | 0 psf | 1B Me<br>Dense<br>Dense<br>Coarse<br>Graine |
| Slice<br>9  | -4.1846154<br>ft | 122.79502<br>ft | -330.56925<br>psf | 135.86395<br>psf | 98.710941<br>psf | 0 psf | 0 psf | 1B Me<br>Dense<br>Dense<br>Coarse<br>Graine |
| Slice<br>10 | -3.8769231<br>ft | 122.78498<br>ft | -329.94203<br>psf | 130.84807<br>psf | 95.06669<br>psf  | 0 psf | 0 psf | 1B Me<br>Dense<br>Dense<br>Coarse<br>Graine |
| Slice<br>11 | -3.5692308<br>ft | 122.79048<br>ft | -330.28555<br>psf | 121.82277<br>psf | 88.509425<br>psf | 0 psf | 0 psf | 1B Me<br>Dense<br>Dense<br>Coars<br>Graine  |
| Slice<br>12 | -3.2615385<br>ft | 122.81157<br>ft | -331.60243<br>psf | 109.62064<br>psf | 79.64406<br>psf  | 0 psf | 0 psf | 1B Me<br>Dense<br>Dense<br>Coarse<br>Graine |
| Slice<br>13 | -2.9538462<br>ft | 122.84842<br>ft | -333.90292<br>psf | 95.077677<br>psf | 69.077976<br>psf | 0 psf | 0 psf | 1B Me<br>Dense<br>Dense<br>Coarse<br>Graine |
| Slice<br>14 | -2.65 ft         | 122.90045<br>ft | -337.15136<br>psf | 274.50558<br>psf | 199.43998<br>psf | 0 psf | 0 psf | 1B Me<br>Dense<br>Dense<br>Coarse<br>Graine |
| Slice<br>15 | -2.35 ft         | 122.96768<br>ft | -341.34845<br>psf | 618.99812<br>psf | 449.72846<br>psf | 0 psf | 0 psf | 1B Me<br>Dense<br>Dense                     |

1/11/22, 12:06 PM Static - MP

| 2:06 PM     |                   |                 |                   | Sta              | tic - MP         |       |       |  |
|-------------|-------------------|-----------------|-------------------|------------------|------------------|-------|-------|--|
|             |                   |                 |                   |                  |                  |       |       | Coarse-<br>Grained Fill                        |
| Slice<br>16 | -2.05 ft          | 123.05111<br>ft | -346.557<br>psf   | 749.33883<br>psf | 544.42653<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>17 | -1.75 ft          | 123.15145<br>ft | -352.8213<br>psf  | 695.52588<br>psf | 505.32913<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>18 | -1.45 ft          | 123.26962<br>ft | -360.19818<br>psf | 643.88876<br>psf | 467.81257<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>19 | -1.279444 ft      | 123.34275<br>ft | -364.7641<br>psf  | 552.46877<br>psf | 401.39205<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>20 | -1.229444 ft      | 123.36612<br>ft | -366.22281<br>psf | 463.90043<br>psf | 337.04339<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>21 | -1.15 ft          | 123.40449<br>ft | -368.61858<br>psf | 405.12122<br>psf | 294.33779<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>22 | -0.95795805<br>ft | 123.5049<br>ft  | -374.88686<br>psf | 351.87095<br>psf | 255.64921<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>23 | -0.67387415<br>ft | 123.66684<br>ft | -384.99679<br>psf | 319.56762<br>psf | 232.17947<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>24 | -0.38979025<br>ft | 123.85002<br>ft | -396.4331<br>psf  | 288.87275<br>psf | 209.87834<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>25 | -0.10570635<br>ft | 124.05689<br>ft | -409.34775<br>psf | 259.5312<br>psf  | 188.56046<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>26 | 0.17837754<br>ft  | 124.29066<br>ft | -423.94199<br>psf | 231.17086<br>psf | 167.95546<br>psf | 0 psf | 0 psf | 1B Med.<br>Dense to V.<br>Dense                |

1/11/22, 12:06 PM Static - MP

| 12.06 PW    |                  |                 |                   | Sia              | uc - MP          |       |       |  |
|-------------|------------------|-----------------|-------------------|------------------|------------------|-------|-------|--|
|             |                  |                 |                   |                  |                  |       |       | Coarse-<br>Grained Fill                        |
| Slice<br>27 | 0.46246144<br>ft | 124.55573<br>ft | -440.49053<br>psf | 203.29655<br>psf | 147.70359<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>28 | 0.74654534<br>ft | 124.85837<br>ft | -459.38421<br>psf | 175.26255<br>psf | 127.3357<br>psf  | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>29 | 1.0306292 ft     | 125.208 ft      | -481.21217<br>psf | 146.21092<br>psf | 106.22845<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>30 | 1.3147131 ft     | 125.62013<br>ft | -506.94151<br>psf | 114.94547<br>psf | 83.512773<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>31 | 1.598797 ft      | 126.12397<br>ft | -538.39583<br>psf | 79.659364<br>psf | 57.875916<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>32 | 1.8828809 ft     | 126.79211<br>ft | -580.10825<br>psf | 37.211468<br>psf | 27.035714<br>psf | 0 psf | 0 psf | 1B Med. Dense to V. Dense Coarse- Grained Fill |
| Slice<br>33 | 2.0694223 ft     | 127.35223<br>ft | -615.07671<br>psf | 8.2645668<br>psf | 5.1642745<br>psf | 0 psf | 0 psf | Common<br>Borrow                               |

# 1.1 Static (Spencer)

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### **File Information**

File Version: 11.01 Title: 05.55L

Created By: Bo Zhang Last Edited By: Yi Tyan Tsai Revision Number: 114 Date: 11/17/2021 Time: 03:29:15 PM

Tool Version: 11.1.3.22085 File Name: Wall 05.55L.gsz

Directory: P:\0\0180366\01\Analysis\Wall 05.55L\

Last Solved Date: 11/17/2021 Last Solved Time: 03:29:20 PM

## **Project Settings**

Unit System: U.S. Customary Units

## **Analysis Settings**

### 1.1 Static (Spencer)

Kind: SLOPE/W

Analysis Type: Spencer

Settings

PWP Conditions from: (none)

Critical Slip Surface Source from: (none) Unit Weight of Water: 62.430189 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 1

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

**Factor of Safety Convergence Settings** 

Maximum Number of Iterations: 100 Tolerable difference in F of S: 0.001

**Solution Settings** 

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20 Max Absolute Lambda: 2

### **Materials**

### **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

#### **Barrier**

Material Model: High Strength

Unit Weight: 150 pcf

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

#### **ESU 1B Medium Dense to Very Dense Coarse-Grained Fill**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 40 °

Phi-B: 0°

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32°

Phi-B: 0°

## **Slip Surface Entry and Exit**

Left Type: Range

Left-Zone Left Coordinate: (-20, 164.01845) ft Left-Zone Right Coordinate: (-5, 168.2) ft

Left-Zone Increment: 10 Right Type: Range

Right-Zone Left Coordinate: (-3, 173.2) ft

Right-Zone Right Coordinate: (20.000081, 172.52168) ft

Right-Zone Increment: 10 Radius Increments: 25

## **Slip Surface Limits**

Left Coordinate: (-40, 159) ft

Right Coordinate: (40, 173.3) ft

## **Surcharge Loads**

## **Surcharge Load 1**

Surcharge (Unit Weight): 250 pcf

Direction: Vertical

#### **Coordinates**

| Х       | Υ        |
|---------|----------|
| -1.9 ft | 174.2 ft |
| 6 ft    | 173.9 ft |
| 20.7 ft | 173.5 ft |

## **Geometry**

Name: 2D Geometry

## **Settings**

View: 2D

Element Thickness: 1 ft

#### **Points**

|          | Х        | Υ        |  |
|----------|----------|----------|--|
| Point 1  | -40 ft   | 150 ft   |  |
| Point 2  | 40 ft    | 150 ft   |  |
| Point 3  | 40 ft    | 155.5 ft |  |
| Point 4  | -40 ft   | 156 ft   |  |
| Point 5  | 40 ft    | 172.5 ft |  |
| Point 6  | 37.7 ft  | 172 ft   |  |
| Point 7  | -3.5 ft  | 171.7 ft |  |
| Point 8  | -3.5 ft  | 167.2 ft |  |
| Point 9  | -4.5 ft  | 167.2 ft |  |
| Point 10 | -12.9 ft | 165.8 ft |  |
| Point 11 | -40 ft   | 159 ft   |  |
| Point 12 | 40 ft    | 173.3 ft |  |
| Point 13 | 32.4 ft  | 173.3 ft |  |
| Point 14 | 24.8 ft  | 172.4 ft |  |
| Point 15 | -4 ft    | 176.2 ft |  |
| Point 16 | -4.5 ft  | 168.2 ft |  |
| Point 17 | -3.5 ft  | 176.2 ft |  |
| Point 18 | -3 ft    | 173.2 ft |  |
| Point 19 | -1.9 ft  | 173.2 ft |  |
| Point 20 | 20.7 ft  | 172.5 ft |  |
| Point 21 | -8.5 ft  | 168.2 ft |  |
| Point 22 | -4.5 ft  | 173.2 ft |  |
| Point 23 | -4.5 ft  | 166.2 ft |  |
| Point 24 | 2.5 ft   | 166.2 ft |  |
|          |          |          |  |

|          | Point 25 | 2.5 ft  | 167.2 ft     |  |  |
|----------|----------|---------|--------------|--|--|
|          | Point 26 | -3 ft   | 172.2 ft     |  |  |
| Point 27 |          | 12.2 ft | 172.76327 ft |  |  |

### **Regions**

|             | Material  | Points                               | Area                     |
|-------------|---|--------------------------------------|--------------------------|
| Region<br>1 | ESU 4B Dense to Very Dense Sand/Gravel                    | 1,2,3,4                              | 460 ft²                  |
| Region<br>2 | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill | 10,11,4,3,5,6,14,20,27,24,23,9,16,21 | 947.98<br>ft²            |
| Region 3    | Gravel Borrow   | 5,12,13,14,6                         | 13.185<br>ft²            |
| Region<br>4 | Barrier   | 15,22,16,9,8,7,26,18,17              | 9.625<br>ft <sup>2</sup> |
| Region<br>5 | Barrier   | 8,9,23,24,25                         | 7 ft²                    |
| Region<br>6 | Common Borrow   | 19,18,26,7,8,25,24,27                | 68.364<br>ft²            |

## **Slip Results**

Slip Surfaces Analysed: 939 of 3146 converged

## **Current Slip Surface**

Slip Surface: 717 Factor of Safety: 2.5 Volume: 132.3351 ft<sup>3</sup> Weight: 16,947.146 lbf

Resisting Moment: 303,263.89 lbf·ft Activating Moment: 121,007.24 lbf·ft Resisting Force: 14,386.138 lbf Activating Force: 5,739.9102 lbf Slip Rank: 1 of 3,146 slip surfaces Exit: (-16.928791, 164.78909) ft Entry: (8.500304, 172.87786) ft

Radius: 19.169378 ft

Center: (-8.3864687, 181.94991) ft

### **Slip Slices**

|            | X                | Y               | PWP   | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material   |
|------------|------------------|-----------------|-------|--------------------------|------------------------|----------------------|---------------------|---|
| Slice<br>1 | -16.525912<br>ft | 164.60008<br>ft | 0 psf | 65.085873<br>psf         | 54.613532<br>psf       | 0 psf                | 0 psf               | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>2 | -15.720154<br>ft | 164.2442<br>ft  | 0 psf | 179.05322<br>psf         | 150.24349<br>psf       | 0 psf                | 0 psf               | ESU 1B Medium<br>Dense to Very<br>Dense Coarse-<br>Grained Fill |
| Slice<br>3 | -14.914396<br>ft | 163.93137<br>ft | 0 psf | 272.55945<br>psf         | 228.70454<br>psf       | 0 psf                | 0 psf               | ESU 1B Medium<br>Dense to Very                                  |

| 10.207411   |                  |                 |       |                   | Tit Otatio (Oponi | 001)  |       |   |
|-------------|------------------|-----------------|-------|-------------------|-------------------|-------|-------|---|
|             |                  |                 |       |                   |                   |       |       | Dense Coarse-<br>Grained Fill                                   |
| Slice<br>4  | -14.108637<br>ft | 163.65937<br>ft | 0 psf | 349.75001<br>psf  | 293.4751<br>psf   | 0 psf | 0 psf | ESU 1B Medium<br>Dense to Very<br>Dense Coarse-<br>Grained Fill |
| Slice<br>5  | -13.302879<br>ft | 163.4264<br>ft  | 0 psf | 413.55151<br>psf  | 347.01092<br>psf  | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>6  | -12.46 ft        | 163.22376<br>ft | 0 psf | 490.70543<br>psf  | 411.75075<br>psf  | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>7  | -11.58 ft        | 163.05368<br>ft | 0 psf | 579.01877<br>psf  | 485.85444<br>psf  | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>8  | -10.7 ft         | 162.92581<br>ft | 0 psf | 654.15989<br>psf  | 548.90533<br>psf  | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>9  | -9.82 ft         | 162.8393<br>ft  | 0 psf | 717.74647<br>psf  | 602.2608<br>psf   | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>10 | -8.94 ft         | 162.79358<br>ft | 0 psf | 771.02299<br>psf  | 646.96511<br>psf  | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>11 | -8.1 ft          | 162.78684<br>ft | 0 psf | 781.76992<br>psf  | 655.98285<br>psf  | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>12 | -7.3 ft          | 162.81554<br>ft | 0 psf | 754.39416<br>psf  | 633.01186<br>psf  | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>13 | -6.5 ft          | 162.87781<br>ft | 0 psf | 723.88739<br>psf  | 607.41364<br>psf  | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>14 | -5.7 ft          | 162.97401<br>ft | 0 psf | 690.38431<br>psf  | 579.30122<br>psf  | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>15 | -4.9 ft          | 163.10464<br>ft | 0 psf | 653.99959<br>psf  | 548.77082<br>psf  | 0 psf | 0 psf | ESU 1B Medium<br>Dense to Very<br>Dense Coarse-<br>Grained Fill |
| Slice<br>16 | -4.25 ft         | 163.23389<br>ft | 0 psf | 1,601.8067<br>psf | 1,344.0754<br>psf | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice       | -3.75 ft         | 163.35147       | 0 psf | 1,772.0636        | 1,486.9379        | 0 psf | 0 psf | ESU 1B Medium   |

| U.Za AIVI   |                 |                 |       |                   | 1.1 Static (Spen  | cei)  |       |   |
|-------------|-----------------|-----------------|-------|-------------------|-------------------|-------|-------|---|
| 17          |                 | ft              |       | psf               | psf               |       |       | Dense to Very<br>Dense Coarse-<br>Grained Fill                  |
| Slice<br>18 | -3.25 ft        | 163.48333<br>ft | 0 psf | 1,382.5782<br>psf | 1,160.1209<br>psf | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>19 | -2.45 ft        | 163.73209<br>ft | 0 psf | 1,076.5243<br>psf | 903.31116<br>psf  | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>20 | -1.46 ft        | 164.08188<br>ft | 0 psf | 1,214.3017<br>psf | 1,018.9201<br>psf | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>21 | -0.58 ft        | 164.44871<br>ft | 0 psf | 1,130.3973<br>psf | 948.51596<br>psf  | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>22 | 0.3 ft          | 164.86873<br>ft | 0 psf | 1,043.8454<br>psf | 875.89031<br>psf  | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>23 | 1.18 ft         | 165.346 ft      | 0 psf | 954.51991<br>psf  | 800.9373<br>psf   | 0 psf | 0 psf | ESU 1B Medium<br>Dense to Very<br>Dense Coarse-<br>Grained Fill |
| Slice<br>24 | 2.06 ft         | 165.88563<br>ft | 0 psf | 862.28825<br>psf  | 723.54576<br>psf  | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>25 | 2.8198253<br>ft | 166.40228<br>ft | 0 psf | 760.35977<br>psf  | 638.01761<br>psf  | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>26 | 3.6163754<br>ft | 167.01596<br>ft | 0 psf | 695.96506<br>psf  | 434.88724<br>psf  | 0 psf | 0 psf | Common Borrow   |
| Slice<br>27 | 4.5698253<br>ft | 167.83677<br>ft | 0 psf | 592.64722<br>psf  | 370.32709<br>psf  | 0 psf | 0 psf | Common Borrow   |
| Slice<br>28 | 5.5232751<br>ft | 168.77784<br>ft | 0 psf | 484.43254<br>psf  | 302.70705<br>psf  | 0 psf | 0 psf | Common Borrow   |
| Slice<br>29 | 6.4167173<br>ft | 169.7885<br>ft  | 0 psf | 379.4826<br>psf   | 237.12704<br>psf  | 0 psf | 0 psf | Common Borrow   |
| Slice<br>30 | 7.250152<br>ft  | 170.88461<br>ft | 0 psf | 277.5586<br>psf   | 173.43787<br>psf  | 0 psf | 0 psf | Common Borrow   |
| Slice<br>31 | 8.0835867<br>ft | 172.17567<br>ft | 0 psf | 171.38997<br>psf  | 107.09634<br>psf  | 0 psf | 0 psf | Common Borrow   |

1/11/22, 10:29 AM 1.2 Static (M-P)

# 1.2 Static (M-P)

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### **File Information**

File Version: 11.01 Title: 05.55L

Created By: Bo Zhang Last Edited By: Yi Tyan Tsai Revision Number: 114 Date: 11/17/2021 Time: 03:29:15 PM

Tool Version: 11.1.3.22085 File Name: Wall 05.55L.gsz

Directory: P:\0\0180366\01\Analysis\Wall 05.55L\

Last Solved Date: 11/17/2021 Last Solved Time: 03:29:22 PM

## **Project Settings**

Unit System: U.S. Customary Units

## **Analysis Settings**

### 1.2 Static (M-P)

Kind: SLOPE/W

Analysis Type: Morgenstern-Price

Settings

Side Function

Interslice force function option: Half-Sine

PWP Conditions from: (none)

Critical Slip Surface Source from: (none) Unit Weight of Water: 62.430189 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 1

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

**Factor of Safety Convergence Settings** 

Maximum Number of Iterations: 100

Tolerable difference in F of S: 0.001

Solution Settings

1/11/22, 10:29 AM 1.2 Static (M-P)

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3 Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

### **Materials**

### **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

#### **Barrier**

Material Model: High Strength

Unit Weight: 150 pcf

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

#### **ESU 1B Medium Dense to Very Dense Coarse-Grained Fill**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 40 °

Phi-B: 0°

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

## **Slip Surface Entry and Exit**

Left Type: Range

Left-Zone Left Coordinate: (-20, 164.01845) ft Left-Zone Right Coordinate: (-5, 168.2) ft

Left-Zone Increment: 10 Right Type: Range

Right-Zone Left Coordinate: (-3, 173.2) ft

Right-Zone Right Coordinate: (20.000081, 172.52168) ft

Right-Zone Increment: 10
Radius Increments: 25

1/11/22, 10:29 AM 1.2 Static (M-P)

## **Slip Surface Limits**

Left Coordinate: (-40, 159) ft Right Coordinate: (40, 173.3) ft

## **Surcharge Loads**

### **Surcharge Load 1**

Surcharge (Unit Weight): 250 pcf

Direction: Vertical

#### Coordinates

| Χ       | Υ        |
|---------|----------|
| -1.9 ft | 174.2 ft |
| 6 ft    | 173.9 ft |
| 20.7 ft | 173.5 ft |

## Geometry

Name: 2D Geometry

### **Settings**

View: 2D

Element Thickness: 1 ft

### **Points**

| LS       |          |          |
|----------|----------|----------|
|          | Х        | Υ        |
| Point 1  | -40 ft   | 150 ft   |
| Point 2  | 40 ft    | 150 ft   |
| Point 3  | 40 ft    | 155.5 ft |
| Point 4  | -40 ft   | 156 ft   |
| Point 5  | 40 ft    | 172.5 ft |
| Point 6  | 37.7 ft  | 172 ft   |
| Point 7  | -3.5 ft  | 171.7 ft |
| Point 8  | -3.5 ft  | 167.2 ft |
| Point 9  | -4.5 ft  | 167.2 ft |
| Point 10 | -12.9 ft | 165.8 ft |
| Point 11 | -40 ft   | 159 ft   |
| Point 12 | 40 ft    | 173.3 ft |
| Point 13 | 32.4 ft  | 173.3 ft |
| Point 14 | 24.8 ft  | 172.4 ft |
| Point 15 | -4 ft    | 176.2 ft |
| Point 16 | -4.5 ft  | 168.2 ft |
| Point 17 | -3.5 ft  | 176.2 ft |
| Point 18 | -3 ft    | 173.2 ft |
| Point 19 | -1.9 ft  | 173.2 ft |
| Point 20 | 20.7 ft  | 172.5 ft |
| Point 21 | -8.5 ft  | 168.2 ft |
| Point 22 | -4.5 ft  | 173.2 ft |
|          |          |          |

| Point 23 | -4.5 ft | 166.2 ft     |
|----------|---------|--------------|
| Point 24 | 2.5 ft  | 166.2 ft     |
| Point 25 | 2.5 ft  | 167.2 ft     |
| Point 26 | -3 ft   | 172.2 ft     |
| Point 27 | 12.2 ft | 172.76327 ft |

### **Regions**

|             | Material  | Points                               | Area          |
|-------------|---|--------------------------------------|---------------|
| Region<br>1 | ESU 4B Dense to Very Dense Sand/Gravel                    | 1,2,3,4                              | 460 ft²       |
| Region<br>2 | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill | 10,11,4,3,5,6,14,20,27,24,23,9,16,21 | 947.98<br>ft² |
| Region<br>3 | Gravel Borrow   | 5,12,13,14,6                         | 13.185<br>ft² |
| Region<br>4 | Barrier   | 15,22,16,9,8,7,26,18,17              | 9.625<br>ft²  |
| Region<br>5 | Barrier   | 8,9,23,24,25                         | 7 ft²         |
| Region<br>6 | Common Borrow   | 19,18,26,7,8,25,24,27                | 68.364<br>ft² |

## **Slip Results**

Slip Surfaces Analysed: 945 of 3146 converged

## **Current Slip Surface**

Slip Surface: 717 Factor of Safety: 2.5 Volume: 132.3351 ft<sup>3</sup> Weight: 16,947.146 lbf

Resisting Moment: 303,216.01 lbf·ft Activating Moment: 121,007.24 lbf·ft Resisting Force: 14,380.328 lbf Activating Force: 5,738.3023 lbf Slip Rank: 1 of 3,146 slip surfaces Exit: (-16.928791, 164.78909) ft

Radius: 19.169378 ft

Center: (-8.3864687, 181.94991) ft

Entry: (8.500304, 172.87786) ft

## **Slip Slices**

|            | х                | Y               | PWP   | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material   |
|------------|------------------|-----------------|-------|--------------------------|------------------------|----------------------|---------------------|---|
| Slice<br>1 | -16.525912<br>ft | 164.60008<br>ft | 0 psf | 46.618237<br>psf         | 39.117346<br>psf       | 0 psf                | 0 psf               | ESU 1B Medium<br>Dense to Very<br>Dense Coarse-<br>Grained Fill |
| Slice<br>2 | -15.720154<br>ft | 164.2442<br>ft  | 0 psf | 140.0721<br>psf          | 117.53445<br>psf       | 0 psf                | 0 psf               | ESU 1B Medium<br>Dense to Very                                  |

| 10.20 7 1111 |                  |                 |       |                  | 1.2 Otatio (W 1  | ,     |       |   |
|--------------|------------------|-----------------|-------|------------------|------------------|-------|-------|---|
|              |                  |                 |       |                  |                  |       |       | Dense Coarse-<br>Grained Fill                                   |
| Slice<br>3   | -14.914396<br>ft | 163.93137<br>ft | 0 psf | 231.25932<br>psf | 194.04961<br>psf | 0 psf | 0 psf | ESU 1B Medium<br>Dense to Very<br>Dense Coarse-<br>Grained Fill |
| Slice<br>4   | -14.108637<br>ft | 163.65937<br>ft | 0 psf | 318.22116<br>psf | 267.01926<br>psf | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>5   | -13.302879<br>ft | 163.4264<br>ft  | 0 psf | 398.88356<br>psf | 334.70305<br>psf | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>6   | -12.46 ft        | 163.22376<br>ft | 0 psf | 495.46126<br>psf | 415.74136<br>psf | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>7   | -11.58 ft        | 163.05368<br>ft | 0 psf | 604.74308<br>psf | 507.43969<br>psf | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>8   | -10.7 ft         | 162.92581<br>ft | 0 psf | 699.66418<br>psf | 587.08796<br>psf | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>9   | -9.82 ft         | 162.8393<br>ft  | 0 psf | 778.44549<br>psf | 653.19332<br>psf | 0 psf | 0 psf | ESU 1B Medium<br>Dense to Very<br>Dense Coarse-<br>Grained Fill |
| Slice<br>10  | -8.94 ft         | 162.79358<br>ft | 0 psf | 840.31702<br>psf | 705.1097<br>psf  | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>11  | -8.1 ft          | 162.78684<br>ft | 0 psf | 851.78391<br>psf | 714.73156<br>psf | 0 psf | 0 psf | ESU 1B Medium<br>Dense to Very<br>Dense Coarse-<br>Grained Fill |
| Slice<br>12  | -7.3 ft          | 162.81554<br>ft | 0 psf | 818.03566<br>psf | 686.41342<br>psf | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>13  | -6.5 ft          | 162.87781<br>ft | 0 psf | 776.17952<br>psf | 651.29195<br>psf | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>14  | -5.7 ft          | 162.97401<br>ft | 0 psf | 727.98932<br>psf | 610.85557<br>psf | 0 psf | 0 psf | ESU 1B Medium<br>Dense to Very<br>Dense Coarse-<br>Grained Fill |
| Slice<br>15  | -4.9 ft          | 163.10464<br>ft | 0 psf | 675.10853<br>psf | 566.48332<br>psf | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice        | -4.25 ft         | 163.23389       | 0 psf | 1,619.7106       | 1,359.0985       | 0 psf | 0 psf | ESU 1B Medium   |

| 10.29 AW    |                 |                 |       |                   | 1.2 Static (IVI-F | ,     |       |   |
|-------------|-----------------|-----------------|-------|-------------------|-------------------|-------|-------|---|
| 16          |                 | ft              |       | psf               | psf               |       |       | Dense to Very<br>Dense Coarse-<br>Grained Fill                  |
| Slice<br>17 | -3.75 ft        | 163.35147<br>ft | 0 psf | 1,777.9702<br>psf | 1,491.8941<br>psf | 0 psf | 0 psf | ESU 1B Medium<br>Dense to Very<br>Dense Coarse-<br>Grained Fill |
| Slice<br>18 | -3.25 ft        | 163.48333<br>ft | 0 psf | 1,372.7566<br>psf | 1,151.8796<br>psf | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>19 | -2.45 ft        | 163.73209<br>ft | 0 psf | 1,047.5916<br>psf | 879.0337<br>psf   | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>20 | -1.46 ft        | 164.08188<br>ft | 0 psf | 1,166.581<br>psf  | 978.87766<br>psf  | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>21 | -0.58 ft        | 164.44871<br>ft | 0 psf | 1,071.2753<br>psf | 898.90675<br>psf  | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>22 | 0.3 ft          | 164.86873<br>ft | 0 psf | 979.03828<br>psf  | 821.51066<br>psf  | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>23 | 1.18 ft         | 165.346 ft      | 0 psf | 889.85921<br>psf  | 746.68054<br>psf  | 0 psf | 0 psf | ESU 1B Medium<br>Dense to Very<br>Dense Coarse-<br>Grained Fill |
| Slice<br>24 | 2.06 ft         | 165.88563<br>ft | 0 psf | 803.31836<br>psf  | 674.06414<br>psf  | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>25 | 2.8198253<br>ft | 166.40228<br>ft | 0 psf | 709.77306<br>psf  | 595.57031<br>psf  | 0 psf | 0 psf | ESU 1B Medium<br>Dense to Very<br>Dense Coarse-<br>Grained Fill |
| Slice<br>26 | 3.6163754<br>ft | 167.01596<br>ft | 0 psf | 661.85679<br>psf  | 413.57402<br>psf  | 0 psf | 0 psf | Common Borrow   |
| Slice<br>27 | 4.5698253<br>ft | 167.83677<br>ft | 0 psf | 580.29782<br>psf  | 362.61032<br>psf  | 0 psf | 0 psf | Common Borrow   |
| Slice<br>28 | 5.5232751<br>ft | 168.77784<br>ft | 0 psf | 495.14958<br>psf  | 309.4038<br>psf   | 0 psf | 0 psf | Common Borrow   |
| Slice<br>29 | 6.4167173<br>ft | 169.7885<br>ft  | 0 psf | 410.14666<br>psf  | 256.28808<br>psf  | 0 psf | 0 psf | Common Borrow   |
| Slice<br>30 | 7.250152<br>ft  | 170.88461<br>ft | 0 psf | 321.72718<br>psf  | 201.03745<br>psf  | 0 psf | 0 psf | Common Borrow   |
| Slice<br>31 | 8.0835867<br>ft | 172.17567<br>ft | 0 psf | 218.45784<br>psf  | 136.50761<br>psf  | 0 psf | 0 psf | Common Borrow   |

# 2A.1 Global - Static (Spencer)

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## **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 651 Date: 01/17/2022 Time: 02:02:35 PM

Tool Version: 11.1.1.22085

Last Solved Date: 01/17/2022 Last Solved Time: 02:11:18 PM

### **Project Settings**

Unit System: U.S. Customary Units

## **Analysis Settings**

### 2A.1 Global - Static (Spencer)

Kind: SLOPE/W

Parent: 2. Steady State (Global)

Analysis Type: Spencer

Settings

PWP Conditions from Parent Analysis: 2. Steady State (Global) [(last)]

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 20

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

Factor of Safety Convergence Settings

Maximum Number of Iterations: 100 Tolerable difference in F of S: 0.001

**Solution Settings** 

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

### **Materials**

#### **ESU 2A Very Loose to Loose Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **ESU 2B Medium Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

### **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

## ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **SEW Wall**

Material Model: High Strength

Unit Weight: 130 pcf

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

## Slip Surface Entry and Exit

Left Type: Range

Left-Zone Left Coordinate: (-50, 180.86613) ft

Left-Zone Right Coordinate: (0, 195) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15, 218.535) ft Right-Zone Right Coordinate: (70, 223.39933) ft

Right-Zone Increment: 30 Radius Increments: 20

## **Slip Surface Limits**

Left Coordinate: (-100, 170.1) ft Right Coordinate: (100, 223.6) ft

## **Surcharge Loads**

### **Surcharge Load 1**

Surcharge (Unit Weight): 250 pcf

Direction: Vertical

#### Coordinates

| X       | Υ         |
|---------|-----------|
| 35.9 ft | 224.15 ft |
| 40.2 ft | 224.2 ft  |
| 100 ft  | 224.6 ft  |

## Geometry

Name: Default Geometry

## **Settings**

View: 2D

Element Thickness: 1 ft

### **Points**

| TS       |             |              |
|----------|-------------|--------------|
|          | X           | Y            |
| Point 1  | 100 ft      | 160 ft       |
| Point 2  | 100 ft      | 185.5 ft     |
| Point 3  | 0.9 ft      | 160 ft       |
| Point 4  | 100 ft      | 211.1475 ft  |
| Point 5  | 3.8 ft      | 183 ft       |
| Point 6  | -20.1275 ft | 160 ft       |
| Point 7  | 100 ft      | 219.64 ft    |
| Point 8  | 42.5825 ft  | 219.8525 ft  |
| Point 9  | 40.2 ft     | 223.2 ft     |
| Point 10 | 100 ft      | 223.6 ft     |
| Point 11 | 0 ft        | 211.7 ft     |
| Point 12 | 0 ft        | 192 ft       |
| Point 13 | 13 ft       | 192 ft       |
| Point 14 | 24.5 ft     | 213.8 ft     |
| Point 15 | 24.5 ft     | 192 ft       |
| Point 16 | 24.5 ft     | 203 ft       |
| Point 17 | 24.5 ft     | 205 ft       |
| Point 18 | 41.8 ft     | 220.7 ft     |
| Point 19 | 26.6 ft     | 215.4 ft     |
| Point 20 | 37.9 ft     | 223.2 ft     |
| Point 21 | 6.13959 ft  | 185.3 ft     |
| Point 22 | 8.9 ft      | 192 ft       |
| Point 23 | -100 ft     | 160 ft       |
| Point 24 | -100 ft     | 170.1 ft     |
| Point 25 | -91.8 ft    | 174.4 ft     |
| Point 26 | -88.3 ft    | 176.5 ft     |
| Point 27 | -85.7 ft    | 177.8 ft     |
| Point 28 | -83.4 ft    | 178.4 ft     |
| Point 29 | -76 ft      | 178.9 ft     |
| Point 30 | -74 ft      | 179.7 ft     |
| Point 31 | -55.9 ft    | 180.2 ft     |
| Point 32 | -37.3 ft    | 182.3 ft     |
| Point 33 | -30.3 ft    | 182.9 ft     |
| Point 34 | -13.6 ft    | 190.2 ft     |
| Point 35 | 7 ft        | 223 ft       |
| Point 36 | 15 ft       | 223 ft       |
| Point 37 | 15 ft       | 211.7 ft     |
| Point 38 | 7 ft        | 211.7 ft     |
| Point 39 | -6 ft       | 195 ft       |
| Point 40 | -37.3275 ft | 162.2725 ft  |
| Point 41 | -47.26 ft   | 160 ft       |
| Point 42 | -5.125 ft   | 182.98095 ft |
| Point 43 | 80.7025 ft  | 160 ft       |
| Point 44 | -100 ft     | 129.8675 ft  |
| Point 45 | 100 ft      | 129.8675 ft  |
| Point 46 | -100 ft     | 147.8625 ft  |
|          |             | 1            |

| (-F      | ,           |              |
|----------|-------------|--------------|
| Point 47 | -27.95 ft   | 152.3875 ft  |
| Point 48 | -100 ft     | 133.97 ft    |
| Point 49 | 16.5 ft     | 197.3 ft     |
| Point 50 | 100 ft      | 209.9025 ft  |
| Point 51 | 95.42762 ft | 209.80965 ft |
| Point 52 | 3.915 ft    | 160.77581 ft |
| Point 53 | 17.7925 ft  | 187.09412 ft |
| Point 54 | 28.7 ft     | 129.8675 ft  |
| Point 55 | 0 ft        | 198.7 ft     |
| Point 56 | 47.15 ft    | 195.68393 ft |
| Point 57 | 42.67 ft    | 194.37311 ft |
| Point 58 | 0 ft        | 195 ft       |
| Point 59 | -32.3 ft    | 165.4 ft     |
| Point 60 | -16 ft      | 164.1 ft     |
| Point 61 | -100 ft     | 150.0525 ft  |
| Point 62 | 15 ft       | 218.535 ft   |
| Point 63 | 24 ft       | 223 ft       |
| Point 64 | 7 ft        | 214.495 ft   |
| Point 65 | 1.355 ft    | 211.7 ft     |
| Point 66 | 25.9 ft     | 223 ft       |
| Point 67 | 22 ft       | 192 ft       |
| Point 68 | 15.0117 ft  | 208.01106 ft |
| Point 69 | 21.5 ft     | 192 ft       |
| Point 70 | 15.5 ft     | 192 ft       |
| Point 71 | 15.5 ft     | 211.7 ft     |
| Point 72 | 15.5 ft     | 194.35 ft    |
| Point 73 | 15.5 ft     | 197.3 ft     |
| Point 74 | 15.5 ft     | 208.29 ft    |
| Point 75 | 18.50702 ft | 197.3 ft     |
| Point 76 | 15.5 ft     | 196.43333 ft |
| Point 77 | 21.5 ft     | 211.7 ft     |
| Point 78 | 20 ft       | 197.3 ft     |
| Point 79 | 20 ft       | 192 ft       |
| Point 80 | 21.5 ft     | 202 ft       |
| Point 81 | 21.5 ft     | 200 ft       |
| Point 82 | 21.5 ft     | 208.29 ft    |
| Point 83 | 31.9 ft     | 223.1 ft     |
| Point 84 | 31.9 ft     | 219.08 ft    |
|          |             |              |

## Regions

|             | Material  | Points                          | Area                       |
|-------------|---|---------------------------------|----------------------------|
| Region 1    | ESU 4B Dense to Very Dense<br>Sand/Gravel                           | 1,2,52,3,43                     | 1,263.5<br>ft <sup>2</sup> |
| Region 2    | ESU 5B Very Stiff to Hard Silt and<br>Clay/Dense to Very Dense Silt | 52,2,50,51,56,57,53,5,60,6,47,3 | 2,656.9<br>ft <sup>2</sup> |
| Region 3    | Gravel Borrow   | 9,18,8,7,10                     | 214.55<br>ft <sup>2</sup>  |
| Region<br>4 | SEW Wall  | 38,65,11,55,68,74,71,37         | 127 ft²                    |

| Region<br>5  | ESU 2B Medium Dense Sand/Gravel           | 8,16,17,18   | 31.556<br>ft <sup>2</sup>  |
|--------------|---|--|----------------------------|
| Region<br>6  | ESU 2A Very Loose to Loose<br>Sand/Gravel | 18,17,14,19,84,20,9                                      | 115.05<br>ft <sup>2</sup>  |
| Region<br>7  | Common Borrow                             | 38,37,62,64  | 38.52<br>ft <sup>2</sup>   |
| Region<br>8  | Common Borrow                             | 14,19,84,83,66,63,62,37,71,77                            | 132.58<br>ft <sup>2</sup>  |
| Region<br>9  | ESU 2B Medium Dense Sand/Gravel           | 22,42,59,40,60,5,21,13                                   | 332.37<br>ft <sup>2</sup>  |
| Region<br>10 | ESU 4B Dense to Very Dense<br>Sand/Gravel | 44,54,45,1,43,3,47,48                                    | 4,704.7<br>ft <sup>2</sup> |
| Region<br>11 | ESU 2B Medium Dense Sand/Gravel           | 41,46,48,47,6,60,40                                      | 992.46<br>ft <sup>2</sup>  |
| Region<br>12 | ESU 4B Dense to Very Dense<br>Sand/Gravel | 56,51,50,4,7,8,16,15,67,69,79,70,13,21,5,53,57           | 1,417.8<br>ft <sup>2</sup> |
| Region<br>13 | ESU 2A Very Loose to Loose<br>Sand/Gravel | 34,33,32,31,30,29,28,27,26,25,24,23,40,59,42,22,12,58,39 | 1,656.2<br>ft <sup>2</sup> |
| Region<br>14 | ESU 2A Very Loose to Loose<br>Sand/Gravel | 40,23,61,46,41   | 379.99<br>ft <sup>2</sup>  |
| Region<br>15 |   | 63,36,62   | 20.093<br>ft <sup>2</sup>  |
| Region<br>16 |   | 36,35,64,62  | 51.88<br>ft <sup>2</sup>   |
| Region<br>17 | Common Borrow                             | 64,65,38   | 7.8889<br>ft <sup>2</sup>  |
| Region<br>18 | ESU 4B Dense to Very Dense<br>Sand/Gravel | 15,16,81,69,67   | 28.5 ft <sup>2</sup>       |
| Region<br>19 | SEW Wall                                  | 72,76,22,13  | 11.692<br>ft <sup>2</sup>  |
| Region<br>20 | SEW Wall                                  | 70,72,13   | 2.9375<br>ft <sup>2</sup>  |
| Region<br>21 | SEW Wall                                  | 70,79,78,75,72   | 19.415<br>ft <sup>2</sup>  |
| Region<br>22 | Gravel Borrow                             | 81,75,78,79,69   | 11.991<br>ft <sup>2</sup>  |
| Region<br>23 | Gravel Borrow                             | 49,75,81,80  | 7.7095<br>ft <sup>2</sup>  |
| Region<br>24 | SEW Wall                                  | 49,76,72,75  | 4.002<br>ft <sup>2</sup>   |
| Region<br>25 | SEW Wall                                  | 73,76,49   | 0.43333<br>ft <sup>2</sup> |
| Region<br>26 | SEW Wall                                  | 76,73,74,68,55,58,12,22                                  | 163.72<br>ft <sup>2</sup>  |
| Region<br>27 | ESU 2B Medium Dense Sand/Gravel           | 80,81,16,17  | 6 ft²                      |
| Region<br>28 | Gravel Borrow                             | 74,82,77   | 10.23<br>ft <sup>2</sup>   |
| Region<br>29 | Gravel Borrow                             | 77,71,74   | 10.23<br>ft <sup>2</sup>   |
| Region<br>30 | ESU 2A Very Loose to Loose<br>Sand/Gravel | 77,82,80,17,14   | 27.75<br>ft²               |

| Region<br>31 | Gravel Borrow | 73,49,80,82,74 | 54.19<br>ft <sup>2</sup> |
|--------------|---------------|----------------|--------------------------|
| Region<br>32 | Common Borrow | 20,83,84       | 12.06<br>ft²             |
| Region<br>33 |               | 55,39,58       | 11.1 ft²                 |

## **Slip Results**

Slip Surfaces Analysed: 3694 of 16926 converged

## **Current Slip Surface**

Slip Surface: 3,605 Factor of Safety: 1.6 Volume: 1,345.1625 ft<sup>3</sup> Weight: 161,577.02 lbf

Resisting Moment: 8,321,638.7 lbf·ft Activating Moment: 5,136,113.9 lbf·ft

Resisting Force: 102,958.48 lbf Activating Force: 63,559.906 lbf Slip Rank: 1 of 16,926 slip surfaces Exit: (-39.462739, 182.05582) ft Entry: (43.844369, 223.22438) ft

Radius: 68.051682 ft

Center: (-19.83779, 247.21634) ft

#### Slip Slices

|            | X                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material                                |
|------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|--|
| Slice<br>1 | -38.381369<br>ft | 181.74952<br>ft | -184.72699<br>psf | 85.153074<br>psf         | 53.209546<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>2 | -36.133333<br>ft | 181.15543<br>ft | -184.12592<br>psf | 233.74644<br>psf         | 146.06098<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>3 | -33.8 ft         | 180.62304<br>ft | -182.80161<br>psf | 351.61963<br>psf         | 219.71633<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>4 | -31.466667<br>ft | 180.17606<br>ft | -181.52704<br>psf | 443.63975<br>psf         | 277.21688<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>5 | -28.908333<br>ft | 179.78648<br>ft | -179.6421<br>psf  | 597.47714<br>psf         | 373.34515<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>6 | -26.125 ft       | 179.47013<br>ft | -178.87824<br>psf | 800.23138<br>psf         | 500.04007<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice      | -23.341667       | 179.26921       | -178.19734        | 966.95761                | 604.22217              |                      |                     | ESU 2A Very                                  |

| 7           | ft               | ft              | psf               | psf               | psf               | 0 psf | 0 psf | Loose to Loose<br>Sand/Gravel                |
|-------------|------------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>8  | -20.558333<br>ft | 179.1827<br>ft  | -178.33075<br>psf | 1,102.7889<br>psf | 689.09898<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>9  | -17.775 ft       | 179.21018<br>ft | -185.68001<br>psf | 1,211.6969<br>psf | 757.15227<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>10 | -14.991667<br>ft | 179.35177<br>ft | -198.74798<br>psf | 1,296.8009<br>psf | 810.33113<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>11 | -11.747559<br>ft | 179.67303<br>ft | -344.90271<br>psf | 1,411.3099<br>psf | 881.88429<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>12 | -7.9475589<br>ft | 180.24066<br>ft | -400.29183<br>psf | 1,545.199<br>psf  | 965.5475<br>psf   | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>13 | -5.5625 ft       | 180.68028<br>ft | -362.75844<br>psf | 1,581.3298<br>psf | 988.12451<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>14 | -3.84375 ft      | 181.08401<br>ft | -337.22185<br>psf | 1,500.122<br>psf  | 937.38029<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>15 | -1.28125 ft      | 181.75709<br>ft | -299.62191<br>psf | 1,377.5004<br>psf | 860.75779<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>16 | 0.6775 ft        | 182.33452<br>ft | -271.81281<br>psf | 3,335.2082<br>psf | 2,084.0694<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>17 | 2.9086702<br>ft  | 183.09994<br>ft | -242.27377<br>psf | 3,240.2196<br>psf | 2,024.7139<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>18 | 5.3009652<br>ft  | 183.98454<br>ft | -201.86945<br>psf | 3,238.2228<br>psf | 3,019.6916<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>19 | 6.569795 ft      | 184.49909<br>ft | -177.12016<br>psf | 3,196.286<br>psf  | 2,980.5849<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>20 | 7.95 ft          | 185.10525<br>ft | -156.36495<br>psf | 3,146.2619<br>psf | 2,933.9367<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>21 | 10.95 ft         | 186.57099<br>ft | -102.19168<br>psf | 3,022.9419<br>psf | 2,818.939<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>22 | 14 ft            | 188.18493<br>ft | -68.87008<br>psf  | 2,873.1038<br>psf | 2,679.2126<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>23 | 15.25 ft         | 188.90859<br>ft | -61.372977<br>psf | 2,794.2124<br>psf | 2,605.6452<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>24 | 16 ft            | 189.36879<br>ft | -57.617279<br>psf | 2,744.318<br>psf  | 2,559.1179<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |

| oui Stuti   | ic (Spelicel)   |                 |                   |                   |                   |       |       |  |
|-------------|-----------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>25 | 17.50351 ft     | 190.33736<br>ft | -50.046546<br>psf | 2,641.3325<br>psf | 2,463.0824<br>psf | 0 psf | 0 psf | Very Dense<br>Sand/Gravel                    |
| Slice<br>26 | 19.25351 ft     | 191.52011<br>ft | -43.065855<br>psf | 2,519.3206<br>psf | 2,349.3044<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>27 | 20.75 ft        | 192.60142<br>ft | -38.792586<br>psf | 2,446.7349<br>psf | 1,911.5988<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>28 | 22.75 ft        | 194.16219<br>ft | -34.625819<br>psf | 2,121.175<br>psf  | 1,978.0277<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>29 | 24.25 ft        | 195.37822<br>ft | -32.143761<br>psf | 2,014.5071<br>psf | 1,878.5582<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>30 | 25.2 ft         | 196.20892<br>ft | -31.270669<br>psf | 1,913.6562<br>psf | 1,784.5133<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>31 | 26.25 ft        | 197.14917<br>ft | -30.956212<br>psf | 1,803.5273<br>psf | 1,681.8164<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>32 | 27.925 ft       | 198.77787<br>ft | -32.204416<br>psf | 1,625.0242<br>psf | 1,515.3596<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>33 | 30.575 ft       | 201.54701<br>ft | -38.262027<br>psf | 1,346.0204<br>psf | 1,255.1844<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>34 | 33.9 ft         | 205.59165<br>ft | -58.81759<br>psf  | 988.41951<br>psf  | 921.7161<br>psf   | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>35 | 36.9 ft         | 209.68543<br>ft | -104.92924<br>psf | 782.53479<br>psf  | 729.72549<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>36 | 39.05 ft        | 213.18728<br>ft | -190.04655<br>psf | 548.63795<br>psf  | 511.61317<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>37 | 41 ft           | 216.77626<br>ft | -345.23437<br>psf | 353.24361<br>psf  | 329.40499<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>38 | 42.095707<br>ft | 219.02478<br>ft | -491.37336<br>psf | 250.9148<br>psf   | 233.98184<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>39 | 42.448792<br>ft | 219.80479<br>ft | -545.92821<br>psf | 240.97156<br>psf  | 150.57574<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>40 | 43.17527 ft     | 221.57977<br>ft | 0 psf             | 144.59561<br>psf  | 112.97047<br>psf  | 0 psf | 0 psf | Gravel Borrow                                |

# 2A.2 Global - Static (M-P)

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## **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 651 Date: 01/17/2022 Time: 02:02:35 PM

Tool Version: 11.1.1.22085

Last Solved Date: 01/17/2022 Last Solved Time: 02:03:52 PM

## **Project Settings**

Unit System: U.S. Customary Units

## **Analysis Settings**

### 2A.2 Global - Static (M-P)

Kind: SLOPE/W

Parent: 2. Steady State (Global) Analysis Type: Morgenstern-Price

Settings

Side Function

Interslice force function option: Half-Sine

PWP Conditions from Parent Analysis: 2. Steady State (Global) [(last)]

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 20

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

Factor of Safety Convergence Settings

Maximum Number of Iterations: 100 Tolerable difference in F of S: 0.001

**Solution Settings** 

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

### **Materials**

### ESU 2A Very Loose to Loose Sand/Gravel

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **ESU 2B Medium Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

### **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **SEW Wall**

Material Model: High Strength

Unit Weight: 130 pcf

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

## **Slip Surface Entry and Exit**

Left Type: Range

Left-Zone Left Coordinate: (-50, 180.86613) ft

Left-Zone Right Coordinate: (0, 195) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15, 218.535) ft Right-Zone Right Coordinate: (70, 223.39933) ft

Right-Zone Increment: 30 Radius Increments: 20

## **Slip Surface Limits**

Left Coordinate: (-100, 170.1) ft Right Coordinate: (100, 223.6) ft

## **Surcharge Loads**

### **Surcharge Load 1**

Surcharge (Unit Weight): 250 pcf

Direction: Vertical

#### Coordinates

| X       | Υ         |
|---------|-----------|
| 35.9 ft | 224.15 ft |
| 40.2 ft | 224.2 ft  |
| 100 ft  | 224.6 ft  |

## Geometry

Name: Default Geometry

### **Settings**

View: 2D

Element Thickness: 1 ft

### **Points**

| 113      | ı           |              |
|----------|-------------|--------------|
|          | X           | Y            |
| Point 1  | 100 ft      | 160 ft       |
| Point 2  | 100 ft      | 185.5 ft     |
| Point 3  | 0.9 ft      | 160 ft       |
| Point 4  | 100 ft      | 211.1475 ft  |
| Point 5  | 3.8 ft      | 183 ft       |
| Point 6  | -20.1275 ft | 160 ft       |
| Point 7  | 100 ft      | 219.64 ft    |
| Point 8  | 42.5825 ft  | 219.8525 ft  |
| Point 9  | 40.2 ft     | 223.2 ft     |
| Point 10 | 100 ft      | 223.6 ft     |
| Point 11 | 0 ft        | 211.7 ft     |
| Point 12 | 0 ft        | 192 ft       |
| Point 13 | 13 ft       | 192 ft       |
| Point 14 | 24.5 ft     | 213.8 ft     |
| Point 15 | 24.5 ft     | 192 ft       |
| Point 16 | 24.5 ft     | 203 ft       |
| Point 17 | 24.5 ft     | 205 ft       |
| Point 18 | 41.8 ft     | 220.7 ft     |
| Point 19 | 26.6 ft     | 215.4 ft     |
| Point 20 | 37.9 ft     | 223.2 ft     |
| Point 21 | 6.13959 ft  | 185.3 ft     |
| Point 22 | 8.9 ft      | 192 ft       |
| Point 23 | -100 ft     | 160 ft       |
| Point 24 | -100 ft     | 170.1 ft     |
| Point 25 | -91.8 ft    | 174.4 ft     |
| Point 26 | -88.3 ft    | 176.5 ft     |
| Point 27 | -85.7 ft    | 177.8 ft     |
| Point 28 | -83.4 ft    | 178.4 ft     |
| Point 29 | -76 ft      | 178.9 ft     |
| Point 30 | -74 ft      | 179.7 ft     |
| Point 31 | -55.9 ft    | 180.2 ft     |
| Point 32 | -37.3 ft    | 182.3 ft     |
| Point 33 | -30.3 ft    | 182.9 ft     |
| Point 34 | -13.6 ft    | 190.2 ft     |
| Point 35 | 7 ft        | 223 ft       |
| Point 36 | 15 ft       | 223 ft       |
| Point 37 | 15 ft       | 211.7 ft     |
| Point 38 | 7 ft        | 211.7 ft     |
| Point 39 | -6 ft       | 195 ft       |
| Point 40 | -37.3275 ft | 162.2725 ft  |
| Point 41 | -47.26 ft   | 160 ft       |
| Point 42 | -5.125 ft   | 182.98095 ft |
| Point 43 | 80.7025 ft  | 160 ft       |
| Point 44 | -100 ft     | 129.8675 ft  |
|          | I           | 1            |

| 100 (       | 1 400 0075 0  |
|-------------|---|
|             | 129.8675 ft   |
|             | 147.8625 ft   |
|             | 152.3875 ft   |
| -100 ft     | 133.97 ft   |
| 16.5 ft     | 197.3 ft  |
| 100 ft      | 209.9025 ft   |
| 95.42762 ft | 209.80965 ft  |
| 3.915 ft    | 160.77581 ft  |
| 17.7925 ft  | 187.09412 ft  |
| 28.7 ft     | 129.8675 ft   |
| 0 ft        | 198.7 ft  |
| 47.15 ft    | 195.68393 ft  |
| 42.67 ft    | 194.37311 ft  |
| 0 ft        | 195 ft  |
| -32.3 ft    | 165.4 ft  |
| -16 ft      | 164.1 ft  |
| -100 ft     | 150.0525 ft   |
| 15 ft       | 218.535 ft  |
| 24 ft       | 223 ft  |
| 7 ft        | 214.495 ft  |
| 1.355 ft    | 211.7 ft  |
| 25.9 ft     | 223 ft  |
| 22 ft       | 192 ft  |
| 15.0117 ft  | 208.01106 ft  |
| 21.5 ft     | 192 ft  |
| 15.5 ft     | 192 ft  |
| 15.5 ft     | 211.7 ft  |
| 15.5 ft     | 194.35 ft   |
| 15.5 ft     | 197.3 ft  |
| 15.5 ft     | 208.29 ft   |
| 18.50702 ft | 197.3 ft  |
| 15.5 ft     | 196.43333 ft  |
| 21.5 ft     | 211.7 ft  |
| 20 ft       | 197.3 ft  |
| 20 ft       | 192 ft  |
| 21.5 ft     | 202 ft  |
| 21.5 ft     | 200 ft  |
| 21.5 ft     | 208.29 ft   |
| 31.9 ft     | 223.1 ft  |
| 31.9 ft     | 219.08 ft   |
|             | 100 ft  95.42762 ft  3.915 ft  17.7925 ft  28.7 ft  0 ft  47.15 ft  42.67 ft  0 ft  -32.3 ft  -16 ft  -100 ft  15 ft  24 ft  7 ft  1.355 ft  25.9 ft  22 ft  15.0117 ft  21.5 ft  15.5 ft  15.5 ft  15.5 ft  15.5 ft  15.5 ft  15.5 ft  21.5 ft |

## Regions

|             | Material   | Points                          | Area                       |
|-------------|--|---------------------------------|----------------------------|
| Region<br>1 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 1,2,52,3,43                     | 1,263.5<br>ft <sup>2</sup> |
| Region 2    | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 52,2,50,51,56,57,53,5,60,6,47,3 | 2,656.9<br>ft <sup>2</sup> |
| Region 3    | Gravel Borrow  | 9,18,8,7,10                     | 214.55<br>ft <sup>2</sup>  |

| Region<br>4  | SEW Wall                                  | 38,65,11,55,68,74,71,37                                  | 127 ft <sup>2</sup>        |
|--------------|---|--|----------------------------|
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel           | 8,16,17,18   | 31.556<br>ft <sup>2</sup>  |
| Region<br>6  | ESU 2A Very Loose to Loose<br>Sand/Gravel | 18,17,14,19,84,20,9                                      | 115.05<br>ft <sup>2</sup>  |
| Region<br>7  | Common Borrow                             | 38,37,62,64  | 38.52<br>ft <sup>2</sup>   |
| Region<br>8  | Common Borrow                             | 14,19,84,83,66,63,62,37,71,77                            | 132.58<br>ft <sup>2</sup>  |
| Region<br>9  | ESU 2B Medium Dense Sand/Gravel           | 22,42,59,40,60,5,21,13                                   | 332.37<br>ft <sup>2</sup>  |
| Region<br>10 | ESU 4B Dense to Very Dense<br>Sand/Gravel | 44,54,45,1,43,3,47,48                                    | 4,704.7<br>ft <sup>2</sup> |
| Region<br>11 | ESU 2B Medium Dense Sand/Gravel           | 41,46,48,47,6,60,40                                      | 992.46<br>ft <sup>2</sup>  |
| Region<br>12 | ESU 4B Dense to Very Dense<br>Sand/Gravel | 56,51,50,4,7,8,16,15,67,69,79,70,13,21,5,53,57           | 1,417.8<br>ft <sup>2</sup> |
| Region<br>13 | ESU 2A Very Loose to Loose<br>Sand/Gravel | 34,33,32,31,30,29,28,27,26,25,24,23,40,59,42,22,12,58,39 | 1,656.2<br>ft <sup>2</sup> |
| Region<br>14 | ESU 2A Very Loose to Loose<br>Sand/Gravel | 40,23,61,46,41   | 379.99<br>ft <sup>2</sup>  |
| Region<br>15 |   | 63,36,62   | 20.093<br>ft <sup>2</sup>  |
| Region<br>16 |   | 36,35,64,62  | 51.88<br>ft <sup>2</sup>   |
| Region<br>17 | Common Borrow                             | 64,65,38   | 7.8889<br>ft <sup>2</sup>  |
| Region<br>18 | ESU 4B Dense to Very Dense<br>Sand/Gravel | 15,16,81,69,67   | 28.5 ft <sup>2</sup>       |
| Region<br>19 | SEW Wall                                  | 72,76,22,13  | 11.692<br>ft <sup>2</sup>  |
| Region<br>20 | SEW Wall                                  | 70,72,13   | 2.9375<br>ft <sup>2</sup>  |
| Region<br>21 | SEW Wall                                  | 70,79,78,75,72   | 19.415<br>ft <sup>2</sup>  |
| Region<br>22 | Gravel Borrow                             | 81,75,78,79,69   | 11.991<br>ft <sup>2</sup>  |
| Region<br>23 | Gravel Borrow                             | 49,75,81,80  | 7.7095<br>ft <sup>2</sup>  |
| Region<br>24 | SEW Wall                                  | 49,76,72,75  | 4.002<br>ft <sup>2</sup>   |
| Region 25    | SEW Wall                                  | 73,76,49   | 0.43333<br>ft <sup>2</sup> |
| Region<br>26 | SEW Wall                                  | 76,73,74,68,55,58,12,22                                  | 163.72<br>ft <sup>2</sup>  |
| Region<br>27 | ESU 2B Medium Dense Sand/Gravel           | 80,81,16,17  | 6 ft <sup>2</sup>          |
| Region 28    | Gravel Borrow                             | 74,82,77   | 10.23<br>ft <sup>2</sup>   |
| Region<br>29 | Gravel Borrow                             | 77,71,74   | 10.23<br>ft <sup>2</sup>   |

| Region<br>30 | ESU 2A Very Loose to Loose<br>Sand/Gravel | 77,82,80,17,14 | 27.75<br>ft <sup>2</sup> |
|--------------|---|----------------|--------------------------|
| Region<br>31 | Gravel Borrow                             | 73,49,80,82,74 | 54.19<br>ft <sup>2</sup> |
| Region<br>32 | Common Borrow                             | 20,83,84       | 12.06<br>ft <sup>2</sup> |
| Region<br>33 |   | 55,39,58       | 11.1 ft²                 |

## **Slip Results**

Slip Surfaces Analysed: 3990 of 16926 converged

## **Current Slip Surface**

Slip Surface: 3,605 Factor of Safety: 1.6 Volume: 1,345.1625 ft<sup>3</sup> Weight: 161,577.02 lbf

Resisting Moment: 8,294,301.6 lbf·ft Activating Moment: 5,136,113.9 lbf·ft

Resisting Force: 102,467.85 lbf Activating Force: 63,467.659 lbf Slip Rank: 1 of 16,926 slip surfaces Exit: (-39.462739, 182.05582) ft Entry: (43.844369, 223.22438) ft

Radius: 68.051682 ft

Center: (-19.83779, 247.21634) ft

### **Slip Slices**

|            | The control of the co |                 |                   |                          |                        |                      |                     |  |
|------------|--|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|--|
|            | X  | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material                                |
| Slice<br>1 | -38.381369<br>ft   | 181.74952<br>ft | -184.72699<br>psf | 55.134939<br>psf         | 34.452134<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>2 | -36.133333<br>ft   | 181.15543<br>ft | -184.12592<br>psf | 166.39382<br>psf         | 103.9744<br>psf        | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>3 | -33.8 ft   | 180.62304<br>ft | -182.80161<br>psf | 275.0371<br>psf          | 171.86226<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>4 | -31.466667<br>ft   | 180.17606<br>ft | -181.52704<br>psf | 377.71346<br>psf         | 236.02156<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>5 | -28.908333<br>ft   | 179.78648<br>ft | -179.6421<br>psf  | 546.6349<br>psf          | 341.5754<br>psf        | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>6 | -26.125 ft   | 179.47013<br>ft | -178.87824<br>psf | 778.29808<br>psf         | 486.33462<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose                |

|             |                  |                 |                   |                   |                   |       |       | Sand/Gravel                                  |
|-------------|------------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>7  | -23.341667<br>ft | 179.26921<br>ft | -178.19734<br>psf | 989.83978<br>psf  | 618.52054<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>8  | -20.558333<br>ft | 179.1827<br>ft  | -178.33075<br>psf | 1,173.2366<br>psf | 733.11961<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>9  | -17.775 ft       | 179.21018<br>ft | -185.68001<br>psf | 1,322.5478<br>psf | 826.41956<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>10 | -14.991667<br>ft | 179.35177<br>ft | -198.74798<br>psf | 1,434.5316<br>psf | 896.39484<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>11 | -11.747559<br>ft | 179.67303<br>ft | -344.90271<br>psf | 1,560.1621<br>psf | 974.8975<br>psf   | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>12 | -7.9475589<br>ft | 180.24066<br>ft | -400.29183<br>psf | 1,681.5315<br>psf | 1,050.7375<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>13 | -5.5625 ft       | 180.68028<br>ft | -362.75844<br>psf | 1,697.3454<br>psf | 1,060.6191<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>14 | -3.84375 ft      | 181.08401<br>ft | -337.22185<br>psf | 1,593.6516<br>psf | 995.82402<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>15 | -1.28125 ft      | 181.75709<br>ft | -299.62191<br>psf | 1,434.6402<br>psf | 896.46269<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>16 | 0.6775 ft        | 182.33452<br>ft | -271.81281<br>psf | 3,384.3579<br>psf | 2,114.7815<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>17 | 2.9086702<br>ft  | 183.09994<br>ft | -242.27377<br>psf | 3,246.5967<br>psf | 2,028.6988<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>18 | 5.3009652<br>ft  | 183.98454<br>ft | -201.86945<br>psf | 3,279.2817<br>psf | 3,057.9797<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>19 | 6.569795 ft      | 184.49909<br>ft | -177.12016<br>psf | 3,207.5758<br>psf | 2,991.1129<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>20 | 7.95 ft          | 185.10525<br>ft | -156.36495<br>psf | 3,125.9893<br>psf | 2,915.0322<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>21 | 10.95 ft         | 186.57099<br>ft | -102.19168<br>psf | 2,941.985<br>psf  | 2,743.4454<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>22 | 14 ft            | 188.18493<br>ft | -68.87008<br>psf  | 2,745.3553<br>psf | 2,560.0852<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>23 | 15.25 ft         | 188.90859<br>ft | -61.372977<br>psf | 2,652.9618<br>psf | 2,473.9269<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice       | 16 ft            | 189.36879       | -57.617279        | 2,596.9434        | 2,421.6889        | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense                |

| 24          |                 | ft              | psf               | psf               | psf               |       |       | Sand/Gravel                                  |
|-------------|-----------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>25 | 17.50351 ft     | 190.33736<br>ft | -50.046546<br>psf | 2,485.9406<br>psf | 2,318.1771<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>26 | 19.25351 ft     | 191.52011<br>ft | -43.065855<br>psf | 2,361.0743<br>psf | 2,201.7374<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>27 | 20.75 ft        | 192.60142<br>ft | -38.792586<br>psf | 2,292.4167<br>psf | 1,791.0322<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>28 | 22.75 ft        | 194.16219<br>ft | -34.625819<br>psf | 1,982.5396<br>psf | 1,848.7481<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>29 | 24.25 ft        | 195.37822<br>ft | -32.143761<br>psf | 1,889.7296<br>psf | 1,762.2013<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>30 | 25.2 ft         | 196.20892<br>ft | -31.270669<br>psf | 1,800.0051<br>psf | 1,678.5319<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>31 | 26.25 ft        | 197.14917<br>ft | -30.956212<br>psf | 1,703.3399<br>psf | 1,588.3902<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>32 | 27.925 ft       | 198.77787<br>ft | -32.204416<br>psf | 1,549.6208<br>psf | 1,445.0448<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>33 | 30.575 ft       | 201.54701<br>ft | -38.262027<br>psf | 1,312.7484<br>psf | 1,224.1577<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>34 | 33.9 ft         | 205.59165<br>ft | -58.81759<br>psf  | 1,006.4394<br>psf | 938.51993<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>35 | 36.9 ft         | 209.68543<br>ft | -104.92924<br>psf | 851.40818<br>psf  | 793.95097<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>36 | 39.05 ft        | 213.18728<br>ft | -190.04655<br>psf | 631.90823<br>psf  | 589.26396<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>37 | 41 ft           | 216.77626<br>ft | -345.23437<br>psf | 434.73126<br>psf  | 405.39346<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>38 | 42.095707<br>ft | 219.02478<br>ft | -491.37336<br>psf | 323.29333<br>psf  | 301.47591<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>39 | 42.448792<br>ft | 219.80479<br>ft | -545.92821<br>psf | 347.36838<br>psf  | 217.05985<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>40 | 43.17527 ft     | 221.57977<br>ft | 0 psf             | 205.53779<br>psf  | 160.58372<br>psf  | 0 psf | 0 psf | Gravel Borrow                                |

# 2A.3 Global - Pseudo-Static (Spencer)

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## **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 651 Date: 01/17/2022 Time: 02:02:35 PM

Tool Version: 11.1.1.22085

Last Solved Date: 01/17/2022 Last Solved Time: 02:08:05 PM

### **Project Settings**

Unit System: U.S. Customary Units

## **Analysis Settings**

#### 2A.3 Global - Pseudo-Static (Spencer)

Kind: SLOPE/W

Parent: 2. Steady State (Global)

Analysis Type: Spencer

Settings

PWP Conditions from Parent Analysis: 2. Steady State (Global) [(last)]

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 20

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

Factor of Safety Convergence Settings

Maximum Number of Iterations: 100 Tolerable difference in F of S: 0.001

**Solution Settings** 

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

### **Materials**

#### **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **SEW Wall**

Material Model: High Strength

Unit Weight: 130 pcf

### **ESU 2A Very Loose to Loose Sand/Gravel (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 ° Phi-B: 0°

### **ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 200 psf

Effective Friction Angle: 32°

Phi-B: 0°

## Slip Surface Entry and Exit

Left Type: Range

Left-Zone Left Coordinate: (-50, 180.86613) ft

Left-Zone Right Coordinate: (0, 195) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15, 218.535) ft Right-Zone Right Coordinate: (70, 223.39933) ft

Right-Zone Increment: 30 Radius Increments: 20

## **Slip Surface Limits**

Left Coordinate: (-100, 170.1) ft Right Coordinate: (100, 223.6) ft

## **Seismic Coefficients**

Horz Seismic Coef.: 0.19

## **Surcharge Loads**

## **Surcharge Load 1**

Surcharge (Unit Weight): 125 pcf

Direction: Vertical

#### Coordinates

| X       | Υ         |
|---------|-----------|
| 35.9 ft | 224.15 ft |
| 39.4 ft | 224.2 ft  |
| 40.2 ft | 224.2 ft  |
| 100 ft  | 224.6 ft  |

## Geometry

Name: Default Geometry

### **Settings**

View: 2D

Element Thickness: 1 ft

#### **Points**

|          | Х           | Υ           |
|----------|-------------|-------------|
| Point 1  | 100 ft      | 160 ft      |
| Point 2  | 100 ft      | 185.5 ft    |
| Point 3  | 0.9 ft      | 160 ft      |
| Point 4  | 100 ft      | 211.1475 ft |
| Point 5  | 3.8 ft      | 183 ft      |
| Point 6  | -20.1275 ft | 160 ft      |
| Point 7  | 100 ft      | 219.64 ft   |
| Point 8  | 42.5825 ft  | 219.8525 ft |
| Point 9  | 40.2 ft     | 223.2 ft    |
| Point 10 | 100 ft      | 223.6 ft    |
| Point 11 | 0 ft        | 211.7 ft    |
| Point 12 | 0 ft        | 192 ft      |
| Point 13 | 13 ft       | 192 ft      |
| Point 14 | 24.5 ft     | 213.8 ft    |
| Point 15 | 24.5 ft     | 192 ft      |
| Point 16 | 24.5 ft     | 203 ft      |
| Point 17 | 24.5 ft     | 205 ft      |
| Point 18 | 41.8 ft     | 220.7 ft    |
| Point 19 | 26.6 ft     | 215.4 ft    |
| Point 20 | 37.9 ft     | 223.2 ft    |
| Point 21 | 6.13959 ft  | 185.3 ft    |
| Point 22 | 8.9 ft      | 192 ft      |
| Point 23 | -100 ft     | 160 ft      |
| Point 24 | -100 ft     | 170.1 ft    |
| Point 25 | -91.8 ft    | 174.4 ft    |
| Point 26 | -88.3 ft    | 176.5 ft    |
| Point 27 | -85.7 ft    | 177.8 ft    |
| Point 28 | -83.4 ft    | 178.4 ft    |
| Point 29 | -76 ft      | 178.9 ft    |
| Point 30 | -74 ft      | 179.7 ft    |
| Point 31 | -55.9 ft    | 180.2 ft    |
| Point 32 | -37.3 ft    | 182.3 ft    |
| Point 33 | -30.3 ft    | 182.9 ft    |
| Point 34 | -13.6 ft    | 190.2 ft    |
| Point 35 | 7 ft        | 223 ft      |
| Point 36 | 15 ft       | 223 ft      |
| Point 37 | 15 ft       | 211.7 ft    |
| Point 38 | 7 ft        | 211.7 ft    |
| Point 39 | -6 ft       | 195 ft      |
| Point 40 | -37.3275 ft | 162.2725 ft |
|          |             |             |

| Point 42 | -5.125 ft   | 182.98095 ft |
|----------|-------------|--------------|
| Point 43 | 80.7025 ft  | 160 ft       |
| Point 44 | -100 ft     | 129.8675 ft  |
| Point 45 | 100 ft      | 129.8675 ft  |
| Point 46 | -100 ft     | 147.8625 ft  |
| Point 47 | -27.95 ft   | 152.3875 ft  |
| Point 48 | -100 ft     | 133.97 ft    |
| Point 49 | 16.5 ft     | 197.3 ft     |
| Point 50 | 100 ft      | 209.9025 ft  |
| Point 51 | 95.42762 ft | 209.80965 ft |
| Point 52 | 3.915 ft    | 160.77581 ft |
| Point 53 | 17.7925 ft  | 187.09412 ft |
| Point 54 | 28.7 ft     | 129.8675 ft  |
| Point 55 | 0 ft        | 198.7 ft     |
| Point 56 | 47.15 ft    | 195.68393 ft |
| Point 57 | 42.67 ft    | 194.37311 ft |
| Point 58 | 0 ft        | 195 ft       |
| Point 59 | -32.3 ft    | 165.4 ft     |
| Point 60 | -16 ft      | 164.1 ft     |
| Point 61 | -100 ft     | 150.0525 ft  |
| Point 62 | 15 ft       | 218.535 ft   |
| Point 63 | 24 ft       | 223 ft       |
| Point 64 | 7 ft        | 214.495 ft   |
| Point 65 | 1.355 ft    | 211.7 ft     |
| Point 66 | 25.9 ft     | 223 ft       |
| Point 67 | 22 ft       | 192 ft       |
| Point 68 | 15.0117 ft  | 208.01106 ft |
| Point 69 | 21.5 ft     | 192 ft       |
| Point 70 | 15.5 ft     | 192 ft       |
| Point 71 | 15.5 ft     | 211.7 ft     |
| Point 72 | 15.5 ft     | 194.35 ft    |
| Point 73 | 15.5 ft     | 197.3 ft     |
| Point 74 | 15.5 ft     | 208.29 ft    |
| Point 75 | 18.50702 ft | 197.3 ft     |
| Point 76 | 15.5 ft     | 196.43333 ft |
| Point 77 | 21.5 ft     | 211.7 ft     |
| Point 78 | 20 ft       | 197.3 ft     |
| Point 79 | 20 ft       | 192 ft       |
| Point 80 | 21.5 ft     | 202 ft       |
| Point 81 | 21.5 ft     | 200 ft       |
| Point 82 | 21.5 ft     | 208.29 ft    |
| Point 83 | 31.9 ft     | 223.1 ft     |
| Point 84 | 31.9 ft     | 219.08 ft    |

# Regions

|             | Material                                  | Points      | Area                       |
|-------------|---|-------------|----------------------------|
| Region<br>1 | ESU 4B Dense to Very Dense<br>Sand/Gravel | 1,2,52,3,43 | 1,263.5<br>ft <sup>2</sup> |
| 1           | Saria, Gravei                             |             | <u> </u>                   |

| Region<br>2  | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 52,2,50,51,56,57,53,5,60,6,47,3                          | 2,656.9<br>ft <sup>2</sup> |
|--------------|--|--|----------------------------|
| Region<br>3  | Gravel Borrow  | 9,18,8,7,10  | 214.55<br>ft <sup>2</sup>  |
| Region<br>4  | SEW Wall   | 38,65,11,55,68,74,71,37                                  | 127 ft <sup>2</sup>        |
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)              | 8,16,17,18   | 31.556<br>ft <sup>2</sup>  |
| Region<br>6  | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion)    | 18,17,14,19,84,20,9                                      | 115.05<br>ft²              |
| Region<br>7  | Common Borrow  | 38,37,62,64  | 38.52<br>ft <sup>2</sup>   |
| Region<br>8  | Common Borrow  | 14,19,84,83,66,63,62,37,71,77                            | 132.58<br>ft²              |
| Region<br>9  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)              | 22,42,59,40,60,5,21,13                                   | 332.37<br>ft²              |
| Region<br>10 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 44,54,45,1,43,3,47,48                                    | 4,704.7<br>ft <sup>2</sup> |
| Region<br>11 | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)              | 41,46,48,47,6,60,40                                      | 992.46<br>ft²              |
| Region<br>12 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 56,51,50,4,7,8,16,15,67,69,79,70,13,21,5,53,57           | 1,417.8<br>ft <sup>2</sup> |
| Region<br>13 | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion)    | 34,33,32,31,30,29,28,27,26,25,24,23,40,59,42,22,12,58,39 | 1,656.2<br>ft²             |
| Region<br>14 | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion)    | 40,23,61,46,41   | 379.99<br>ft²              |
| Region<br>15 |  | 63,36,62   | 20.093<br>ft <sup>2</sup>  |
| Region<br>16 |  | 36,35,64,62  | 51.88<br>ft <sup>2</sup>   |
| Region<br>17 | Common Borrow  | 64,65,38   | 7.8889<br>ft <sup>2</sup>  |
| Region<br>18 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 15,16,81,69,67   | 28.5 ft                    |
| Region<br>19 | SEW Wall   | 72,76,22,13  | 11.692<br>ft²              |
| Region<br>20 | SEW Wall   | 70,72,13   | 2.9375<br>ft <sup>2</sup>  |
| Region<br>21 | SEW Wall   | 70,79,78,75,72   | 19.415<br>ft <sup>2</sup>  |
| Region<br>22 | Gravel Borrow  | 81,75,78,79,69   | 11.991<br>ft²              |
| Region<br>23 | Gravel Borrow  | 49,75,81,80  | 7.7095<br>ft <sup>2</sup>  |
| Region<br>24 | SEW Wall   | 49,76,72,75  | 4.002<br>ft <sup>2</sup>   |
| Region<br>25 | SEW Wall   | 73,76,49   | 0.4333<br>ft <sup>2</sup>  |
| Region<br>26 | SEW Wall   | 76,73,74,68,55,58,12,22                                  | 163.72<br>ft²              |
| Region<br>27 | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)              | 80,81,16,17  | 6 ft <sup>2</sup>          |

| Region<br>28 | Gravel Borrow   | 74,82,77       | 10.23<br>ft <sup>2</sup> |
|--------------|---|----------------|--------------------------|
| Region<br>29 | Gravel Borrow   | 77,71,74       | 10.23<br>ft <sup>2</sup> |
| Region<br>30 | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion) | 77,82,80,17,14 | 27.75<br>ft <sup>2</sup> |
| Region<br>31 | Gravel Borrow   | 73,49,80,82,74 | 54.19<br>ft <sup>2</sup> |
| Region<br>32 | Common Borrow   | 20,83,84       | 12.06<br>ft²             |
| Region<br>33 |   | 55,39,58       | 11.1 ft²                 |

# **Slip Results**

Slip Surfaces Analysed: 2795 of 16926 converged

# **Current Slip Surface**

Slip Surface: 2,323 Factor of Safety: 1.2 Volume: 1,399.3073 ft<sup>3</sup> Weight: 168,087.67 lbf

Resisting Moment: 9,239,657.7 lbf·ft Activating Moment: 7,442,258.5 lbf·ft

Resisting Force: 107,452.66 lbf Activating Force: 86,547.964 lbf Slip Rank: 1 of 16,926 slip surfaces Exit: (-43.677643, 181.57994) ft Entry: (45.712628, 223.23687) ft

Radius: 74.84631 ft

Center: (-22.766519, 253.44576) ft

### **Slip Slices**

|            | Х                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material  |
|------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|--|
| Slice<br>1 | -42.083232<br>ft | 181.15391<br>ft | -184.13636<br>psf | 460.20823<br>psf         | 287.57002<br>psf       | 100 psf              | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>2 | -38.894411<br>ft | 180.37596<br>ft | -184.76666<br>psf | 686.3869<br>psf          | 428.90213<br>psf       | 100 psf              | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>3 | -35.55 ft        | 179.7206<br>ft  | -183.58842<br>psf | 810.84854<br>psf         | 506.6744<br>psf        | 100 psf              | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent              |

|             |                  |                 |                   |                   |                  |         |       | Cohesion)  |
|-------------|------------------|-----------------|-------------------|-------------------|------------------|---------|-------|--|
| Slice<br>4  | -32.05 ft        | 179.19835<br>ft | -181.7637<br>psf  | 866.65457<br>psf  | 541.54588<br>psf | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>5  | -28.908333<br>ft | 178.86494<br>ft | -179.59703<br>psf | 970.36327<br>psf  | 606.35027<br>psf | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>6  | -26.125 ft       | 178.68781<br>ft | -178.59656<br>psf | 1,117.4093<br>psf | 698.2348<br>psf  | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>7  | -23.341667<br>ft | 178.6146<br>ft  | -175.945<br>psf   | 1,226.2843<br>psf | 766.26746<br>psf | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>8  | -20.558333<br>ft | 178.64498<br>ft | -179.69973<br>psf | 1,304.9008<br>psf | 815.39252<br>psf | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>9  | -17.775 ft       | 178.7791<br>ft  | -188.75781<br>psf | 1,358.9118<br>psf | 849.14232<br>psf | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>10 | -14.991667<br>ft | 179.01751<br>ft | -202.18527<br>psf | 1,392.4532<br>psf | 870.10132<br>psf | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>11 | -11.937442<br>ft | 179.40605<br>ft | -360.02514<br>psf | 1,446.5051<br>psf | 903.87668<br>psf | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>12 | -8.1374419<br>ft | 180.07539<br>ft | -400.40609<br>psf | 1,569.1649<br>psf | 980.52305<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                    |
| Slice<br>13 | -5.5625 ft       | 180.6049<br>ft  | -361.0774<br>psf  | 1,568.3015<br>psf | 979.98353<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                    |
| Slice<br>14 | -3.84375 ft      | 181.0431<br>ft  | -336.29385<br>psf | 1,468.5305<br>psf | 917.63971<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent                     |

|             |                 |                 |                   |                   |                   |         |       | Cohesion)   |
|-------------|-----------------|-----------------|-------------------|-------------------|-------------------|---------|-------|---|
| Slice<br>15 | -1.28125 ft     | 181.76198<br>ft | -299.7325<br>psf  | 1,323.7474<br>psf | 827.1692<br>psf   | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>16 | 0.6775 ft       | 182.36946<br>ft | -272.60257<br>psf | 3,062.9853<br>psf | 1,913.9656<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>17 | 2.9736904<br>ft | 183.18595<br>ft | -242.8472<br>psf  | 2,933.2119<br>psf | 1,832.8742<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>18 | 5.3659854<br>ft | 184.09278<br>ft | -204.08884<br>psf | 3,016.9193<br>psf | 2,813.3227<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                    |
| Slice<br>19 | 6.569795 ft     | 184.58988<br>ft | -180.68259<br>psf | 2,955.4642<br>psf | 2,756.015<br>psf  | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                    |
| Slice<br>20 | 7.95 ft         | 185.20075<br>ft | -159.86935<br>psf | 2,883.3759<br>psf | 2,688.7915<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                    |
| Slice<br>21 | 10.95 ft        | 186.66333<br>ft | -103.45834<br>psf | 2,721.2616<br>psf | 2,537.6175<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                    |
| Slice<br>22 | 14 ft           | 188.26236<br>ft | -70.070927<br>psf | 2,544.5355<br>psf | 2,372.8177<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                    |
| Slice<br>23 | 15.25 ft        | 188.97382<br>ft | -62.340785<br>psf | 2,459.5919<br>psf | 2,293.6065<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                    |
| Slice<br>24 | 16 ft           | 189.424 ft      | -58.384012<br>psf | 2,407.2906<br>psf | 2,244.8348<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                    |
| Slice<br>25 | 17.50351 ft     | 190.36741<br>ft | -50.390413<br>psf | 2,301.8296<br>psf | 2,146.4908<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                    |
| Slice<br>26 | 19.25351 ft     | 191.51456<br>ft | -43.009401<br>psf | 2,180.2859<br>psf | 2,033.1495<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                    |
| Slice<br>27 | 20.75 ft        | 192.55706<br>ft | -38.324338<br>psf | 2,069.9059<br>psf | 1,617.1878<br>psf | 0 psf   | 0 psf | Gravel Borrow   |
| Slice<br>28 | 22.75 ft        | 194.051 ft      | -33.503747<br>psf | 1,815.8883<br>psf | 1,693.3432<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                    |
| Slice<br>29 | 24.25 ft        | 195.21077<br>ft | -30.511031<br>psf | 1,718.5617<br>psf | 1,602.5848<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                    |
| Slice<br>30 | 25.2 ft         | 195.99707<br>ft | -29.171505<br>psf | 1,630.1664<br>psf | 1,520.1548<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                    |

| Slice<br>31 | 26.25 ft        | 196.88485<br>ft | -28.172489<br>psf | 1,534.6787<br>psf | 1,431.111<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
|-------------|-----------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>32 | 27.925 ft       | 198.40854<br>ft | -28.272026<br>psf | 1,383.1063<br>psf | 1,289.7675<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>33 | 30.575 ft       | 200.97593<br>ft | -31.384334<br>psf | 1,152.0352<br>psf | 1,074.2902<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>34 | 33.9 ft         | 204.64532<br>ft | -45.385097<br>psf | 867.58574<br>psf  | 809.0368<br>psf   | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>35 | 36.9 ft         | 208.28902<br>ft | -72.810031<br>psf | 678.82745<br>psf  | 633.01684<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>36 | 38.65 ft        | 210.68762<br>ft | -107.55797<br>psf | 539.99438<br>psf  | 503.55291<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>37 | 39.8 ft         | 212.37424<br>ft | -144.69408<br>psf | 452.25506<br>psf  | 421.73467<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>38 | 41 ft           | 214.28629<br>ft | -201.88589<br>psf | 367.78123<br>psf  | 342.96154<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>39 | 42.19125 ft     | 216.27268<br>ft | -285.31739<br>psf | 289.77867<br>psf  | 270.22298<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>40 | 43.348543<br>ft | 218.4016<br>ft  | -399.23263<br>psf | 202.98331<br>psf  | 189.285<br>psf    | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>41 | 44.913607<br>ft | 221.54185<br>ft | 0 psf             | 91.151408<br>psf  | 71.215285<br>psf  | 0 psf | 0 psf | Gravel Borrow                                |

# 2A.4 Global - Pseudo-Static (M-P)

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### **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 651 Date: 01/17/2022 Time: 02:02:35 PM

Tool Version: 11.1.1.22085

Last Solved Date: 01/17/2022 Last Solved Time: 02:10:23 PM

### **Project Settings**

Unit System: U.S. Customary Units

# **Analysis Settings**

#### 2A.4 Global - Pseudo-Static (M-P)

Description: Project Num: 00180-366-01 Wall: 05.85L-A Station: 1+90

Kind: SLOPE/W

Parent: 2. Steady State (Global) Analysis Type: Morgenstern-Price

Settings

Side Function

Interslice force function option: Half-Sine

PWP Conditions from Parent Analysis: 2. Steady State (Global) [(last)]

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 20

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

Factor of Safety Convergence Settings

Maximum Number of Iterations: 100 Tolerable difference in F of S: 0.001

Solution Settings

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

#### **Materials**

#### **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

#### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **SEW Wall**

Material Model: High Strength

Unit Weight: 130 pcf

### **ESU 2A Very Loose to Loose Sand/Gravel (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 100 psf

Effective Friction Angle: 32 °

Phi-B: 0°

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

#### 2A.4 Global - Pseudo-Static (M-P)

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

### **ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf

Effective Cohesion: 200 psf Effective Friction Angle: 32 °

Phi-B: 0°

# **Slip Surface Entry and Exit**

Left Type: Range

Left-Zone Left Coordinate: (-50, 180.86613) ft

Left-Zone Right Coordinate: (0, 195) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15, 218.535) ft Right-Zone Right Coordinate: (70, 223.39933) ft

Right-Zone Increment: 30 Radius Increments: 20

# **Slip Surface Limits**

Left Coordinate: (-100, 170.1) ft Right Coordinate: (100, 223.6) ft

### **Seismic Coefficients**

Horz Seismic Coef.: 0.19

### **Surcharge Loads**

#### **Surcharge Load 1**

Surcharge (Unit Weight): 125 pcf

Direction: Vertical

#### Coordinates

| Х       | Υ         |
|---------|-----------|
| 35.9 ft | 224.15 ft |
| 39.4 ft | 224.2 ft  |
| 40.2 ft | 224.2 ft  |
| 100 ft  | 224.6 ft  |

# **Geometry**

Name: Default Geometry

# Settings

View: 2D

Element Thickness: 1 ft

#### **Points**

| ts       |             |             |
|----------|-------------|-------------|
|          | Х           | Y           |
| Point 1  | 100 ft      | 160 ft      |
| Point 2  | 100 ft      | 185.5 ft    |
| Point 3  | 0.9 ft      | 160 ft      |
| Point 4  | 100 ft      | 211.1475 ft |
| Point 5  | 3.8 ft      | 183 ft      |
| Point 6  | -20.1275 ft | 160 ft      |
| Point 7  | 100 ft      | 219.64 ft   |
| Point 8  | 42.5825 ft  | 219.8525 ft |
| Point 9  | 40.2 ft     | 223.2 ft    |
| Point 10 | 100 ft      | 223.6 ft    |
| Point 11 | 0 ft        | 211.7 ft    |
| Point 12 | 0 ft        | 192 ft      |
| Point 13 | 13 ft       | 192 ft      |
| Point 14 | 24.5 ft     | 213.8 ft    |
| Point 15 | 24.5 ft     | 192 ft      |
| Point 16 | 24.5 ft     | 203 ft      |
| Point 17 | 24.5 ft     | 205 ft      |
| Point 18 | 41.8 ft     | 220.7 ft    |
| Point 19 | 26.6 ft     | 215.4 ft    |
| Point 20 | 37.9 ft     | 223.2 ft    |
| Point 21 | 6.13959 ft  | 185.3 ft    |
| Point 22 | 8.9 ft      | 192 ft      |
| Point 23 | -100 ft     | 160 ft      |
| Point 24 | -100 ft     | 170.1 ft    |
| Point 25 | -91.8 ft    | 174.4 ft    |
| Point 26 | -88.3 ft    | 176.5 ft    |
| Point 27 | -85.7 ft    | 177.8 ft    |
| Point 28 | -83.4 ft    | 178.4 ft    |
| Point 29 | -76 ft      | 178.9 ft    |
| Point 30 | -74 ft      | 179.7 ft    |
| Point 31 | -55.9 ft    | 180.2 ft    |
| Point 32 | -37.3 ft    | 182.3 ft    |
| Point 33 | -30.3 ft    | 182.9 ft    |
| Point 34 | -13.6 ft    | 190.2 ft    |
| Point 35 | 7 ft        | 223 ft      |
| Point 36 | 15 ft       | 223 ft      |
| Point 37 | 15 ft       | 211.7 ft    |
| Point 38 | 7 ft        | 211.7 ft    |
|          |             |             |

| Point 39-6 ft195 ftPoint 40-37.3275 ft162.2725 ftPoint 41-47.26 ft160 ftPoint 42-5.125 ft182.98095 ftPoint 4380.7025 ft160 ftPoint 44-100 ft129.8675 ftPoint 45100 ft129.8675 ftPoint 46-100 ft147.8625 ftPoint 47-27.95 ft152.3875 ftPoint 48-100 ft133.97 ftPoint 4916.5 ft197.3 ftPoint 50100 ft209.9025 ftPoint 5195.42762 ft209.80965 ftPoint 523.915 ft160.77581 ft |
|---|
| Point 41-47.26 ft160 ftPoint 42-5.125 ft182.98095 ftPoint 4380.7025 ft160 ftPoint 44-100 ft129.8675 ftPoint 45100 ft129.8675 ftPoint 46-100 ft147.8625 ftPoint 47-27.95 ft152.3875 ftPoint 48-100 ft133.97 ftPoint 4916.5 ft197.3 ftPoint 50100 ft209.9025 ftPoint 5195.42762 ft209.80965 ft  |
| Point 42-5.125 ft182.98095 ftPoint 4380.7025 ft160 ftPoint 44-100 ft129.8675 ftPoint 45100 ft129.8675 ftPoint 46-100 ft147.8625 ftPoint 47-27.95 ft152.3875 ftPoint 48-100 ft133.97 ftPoint 4916.5 ft197.3 ftPoint 50100 ft209.9025 ftPoint 5195.42762 ft209.80965 ft   |
| Point 44-100 ft129.8675 ftPoint 45100 ft129.8675 ftPoint 46-100 ft147.8625 ftPoint 47-27.95 ft152.3875 ftPoint 48-100 ft133.97 ftPoint 4916.5 ft197.3 ftPoint 50100 ft209.9025 ftPoint 5195.42762 ft209.80965 ft  |
| Point 45       100 ft       129.8675 ft         Point 46       -100 ft       147.8625 ft         Point 47       -27.95 ft       152.3875 ft         Point 48       -100 ft       133.97 ft         Point 49       16.5 ft       197.3 ft         Point 50       100 ft       209.9025 ft         Point 51       95.42762 ft       209.80965 ft                            |
| Point 46-100 ft147.8625 ftPoint 47-27.95 ft152.3875 ftPoint 48-100 ft133.97 ftPoint 4916.5 ft197.3 ftPoint 50100 ft209.9025 ftPoint 5195.42762 ft209.80965 ft   |
| Point 47       -27.95 ft       152.3875 ft         Point 48       -100 ft       133.97 ft         Point 49       16.5 ft       197.3 ft         Point 50       100 ft       209.9025 ft         Point 51       95.42762 ft       209.80965 ft   |
| Point 48       -100 ft       133.97 ft         Point 49       16.5 ft       197.3 ft         Point 50       100 ft       209.9025 ft         Point 51       95.42762 ft       209.80965 ft  |
| Point 49       16.5 ft       197.3 ft         Point 50       100 ft       209.9025 ft         Point 51       95.42762 ft       209.80965 ft   |
| Point 50         100 ft         209.9025 ft           Point 51         95.42762 ft         209.80965 ft   |
| Point 51 95.42762 ft 209.80965 ft   |
|   |
| Point 52 3.915 ft 160.77581 ft  |
|   |
| Point 53 17.7925 ft 187.09412 ft  |
| Point 54 28.7 ft 129.8675 ft  |
| Point 55 0 ft 198.7 ft  |
| Point 56 47.15 ft 195.68393 ft  |
| Point 57 42.67 ft 194.37311 ft  |
| Point 58 0 ft 195 ft  |
| Point 59 -32.3 ft 165.4 ft  |
| Point 60 -16 ft 164.1 ft  |
| Point 61 -100 ft 150.0525 ft  |
| Point 62 15 ft 218.535 ft   |
| Point 63 24 ft 223 ft   |
| Point 64 7 ft 214.495 ft  |
| Point 65   1.355 ft   211.7 ft  |
| Point 66 25.9 ft 223 ft   |
| Point 67   22 ft   192 ft   |
| Point 68   15.0117 ft   208.01106 ft  |
| Point 69 21.5 ft 192 ft   |
| Point 70   15.5 ft   192 ft   |
| Point 71   15.5 ft   211.7 ft   |
| Point 72   15.5 ft   194.35 ft  |
| Point 73   15.5 ft   197.3 ft   |
| Point 74 15.5 ft 208.29 ft  |
| Point 75   18.50702 ft   197.3 ft   |
| Point 76   15.5 ft   196.43333 ft   |
| Point 77 21.5 ft 211.7 ft   |
| Point 78   20 ft   197.3 ft   |
| Point 79   20 ft   192 ft   |
| Point 80 21.5 ft 202 ft   |
| Point 81 21.5 ft 200 ft   |
| Point 82 21.5 ft 208.29 ft  |
| Point 83 31.9 ft 223.1 ft   |
| Point 84   31.9 ft   219.08 ft  |

### Regions

|              | Material   | Points   | Area                       |
|--------------|--|--|----------------------------|
| Region<br>1  | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 1,2,52,3,43  | 1,263.5<br>ft <sup>2</sup> |
| Region<br>2  | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 52,2,50,51,56,57,53,5,60,6,47,3                          | 2,656.9<br>ft <sup>2</sup> |
| Region<br>3  | Gravel Borrow  | 9,18,8,7,10  | 214.55<br>ft <sup>2</sup>  |
| Region<br>4  | SEW Wall   | 38,65,11,55,68,74,71,37                                  | 127 ft²                    |
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)              | 8,16,17,18   | 31.556<br>ft <sup>2</sup>  |
| Region<br>6  | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion)    | 18,17,14,19,84,20,9                                      | 115.05<br>ft <sup>2</sup>  |
| Region<br>7  | Common Borrow  | 38,37,62,64  | 38.52<br>ft <sup>2</sup>   |
| Region<br>8  | Common Borrow  | 14,19,84,83,66,63,62,37,71,77                            | 132.58<br>ft <sup>2</sup>  |
| Region<br>9  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)              | 22,42,59,40,60,5,21,13                                   | 332.37<br>ft <sup>2</sup>  |
| Region<br>10 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 44,54,45,1,43,3,47,48                                    | 4,704.7<br>ft <sup>2</sup> |
| Region<br>11 | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)              | 41,46,48,47,6,60,40                                      | 992.46<br>ft <sup>2</sup>  |
| Region<br>12 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 56,51,50,4,7,8,16,15,67,69,79,70,13,21,5,53,57           | 1,417.8<br>ft <sup>2</sup> |
| Region<br>13 | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion)    | 34,33,32,31,30,29,28,27,26,25,24,23,40,59,42,22,12,58,39 | 1,656.2<br>ft <sup>2</sup> |
| Region<br>14 | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion)    | 40,23,61,46,41   | 379.99<br>ft <sup>2</sup>  |
| Region<br>15 |  | 63,36,62   | 20.093<br>ft <sup>2</sup>  |
| Region<br>16 |  | 36,35,64,62  | 51.88<br>ft <sup>2</sup>   |
| Region<br>17 | Common Borrow  | 64,65,38   | 7.8889<br>ft <sup>2</sup>  |
| Region<br>18 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 15,16,81,69,67   | 28.5 ft <sup>2</sup>       |
| Region<br>19 | SEW Wall   | 72,76,22,13  | 11.692<br>ft <sup>2</sup>  |
| Region<br>20 | SEW Wall   | 70,72,13   | 2.9375<br>ft <sup>2</sup>  |
| Region<br>21 | SEW Wall   | 70,79,78,75,72   | 19.415<br>ft <sup>2</sup>  |
| Region<br>22 | Gravel Borrow  | 81,75,78,79,69   | 11.991<br>ft <sup>2</sup>  |
| Region<br>23 | Gravel Borrow  | 49,75,81,80  | 7.7095<br>ft <sup>2</sup>  |
| Region<br>24 | SEW Wall   | 49,76,72,75  | 4.002<br>ft <sup>2</sup>   |
| Region 25    | SEW Wall   | 73,76,49   | 0.43333<br>ft <sup>2</sup> |
| Region       | SEW Wall   | 76,73,74,68,55,58,12,22                                  | 163.72                     |

| 26           |   |                | ft²                      |
|--------------|---|----------------|--------------------------|
| Region<br>27 | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)           | 80,81,16,17    | 6 ft²                    |
| Region<br>28 | Gravel Borrow   | 74,82,77       | 10.23<br>ft <sup>2</sup> |
| Region<br>29 | Gravel Borrow   | 77,71,74       | 10.23<br>ft <sup>2</sup> |
| Region<br>30 | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion) | 77,82,80,17,14 | 27.75<br>ft <sup>2</sup> |
| Region<br>31 | Gravel Borrow   | 73,49,80,82,74 | 54.19<br>ft <sup>2</sup> |
| Region<br>32 | Common Borrow   | 20,83,84       | 12.06<br>ft <sup>2</sup> |
| Region<br>33 |   | 55,39,58       | 11.1 ft²                 |

# **Slip Results**

Slip Surfaces Analysed: 3928 of 16926 converged

# **Current Slip Surface**

Slip Surface: 2,323 Factor of Safety: 1.2 Volume: 1,399.3073 ft³ Weight: 168,087.67 lbf

Resisting Moment: 9,146,728.7 lbf·ft Activating Moment: 7,442,258.5 lbf·ft

Resisting Force: 106,365.34 lbf Activating Force: 86,538.675 lbf Slip Rank: 1 of 16,926 slip surfaces Exit: (-43.677643, 181.57994) ft Entry: (45.712628, 223.23687) ft

Radius: 74.84631 ft

Center: (-22.766519, 253.44576) ft

### **Slip Slices**

|            | X                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material  |
|------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|--|
| Slice<br>1 | -42.083232<br>ft | 181.15391<br>ft | -184.13636<br>psf | 122.58598<br>psf         | 76.600224<br>psf       | 100 psf              | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>2 | -38.894411<br>ft | 180.37596<br>ft | -184.76666<br>psf | 323.13446<br>psf         | 201.91682<br>psf       | 100 psf              | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |

| Slice<br>3  | -35.55 ft        | 179.7206<br>ft  | -183.58842<br>psf | 534.14846<br>psf  | 333.773<br>psf    | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
|-------------|------------------|-----------------|-------------------|-------------------|-------------------|---------|-------|--|
| Slice<br>4  | -32.05 ft        | 179.19835<br>ft | -181.7637<br>psf  | 741.94699<br>psf  | 463.61994<br>psf  | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>5  | -28.908333<br>ft | 178.86494<br>ft | -179.59703<br>psf | 980.874<br>psf    | 612.9181<br>psf   | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>6  | -26.125 ft       | 178.68781<br>ft | -178.59656<br>psf | 1,244.466<br>psf  | 777.62864<br>psf  | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>7  | -23.341667<br>ft | 178.6146<br>ft  | -175.945<br>psf   | 1,466.958<br>psf  | 916.65707<br>psf  | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>8  | -20.558333<br>ft | 178.64498<br>ft | -179.69973<br>psf | 1,635.2007<br>psf | 1,021.7868<br>psf | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>9  | -17.775 ft       | 178.7791<br>ft  | -188.75781<br>psf | 1,742.2077<br>psf | 1,088.6522<br>psf | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>10 | -14.991667<br>ft | 179.01751<br>ft | -202.18527<br>psf | 1,787.9213<br>psf | 1,117.2172<br>psf | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>11 | -11.937442<br>ft | 179.40605<br>ft | -360.02514<br>psf | 1,812.6945<br>psf | 1,132.6972<br>psf | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>12 | -8.1374419<br>ft | 180.07539<br>ft | -400.40609<br>psf | 1,874.0357<br>psf | 1,171.0275<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                    |
| Slice<br>13 | -5.5625 ft       | 180.6049<br>ft  | -361.0774<br>psf  | 1,802.2847<br>psf | 1,126.1925<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                    |

| Slice<br>14 | -3.84375 ft     | 181.0431<br>ft  | -336.29385<br>psf | 1,646.2977<br>psf | 1,028.721<br>psf  | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
|-------------|-----------------|-----------------|-------------------|-------------------|-------------------|---------|-------|---|
| Slice<br>15 | -1.28125 ft     | 181.76198<br>ft | -299.7325<br>psf  | 1,418.7764<br>psf | 886.54988<br>psf  | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>16 | 0.6775 ft       | 182.36946<br>ft | -272.60257<br>psf | 3,081.3621<br>psf | 1,925.4487<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>17 | 2.9736904<br>ft | 183.18595<br>ft | -242.8472<br>psf  | 2,872.2802<br>psf | 1,794.7999<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>18 | 5.3659854<br>ft | 184.09278<br>ft | -204.08884<br>psf | 2,991.3639<br>psf | 2,789.492<br>psf  | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                    |
| Slice<br>19 | 6.569795 ft     | 184.58988<br>ft | -180.68259<br>psf | 2,880.9486<br>psf | 2,686.528<br>psf  | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                    |
| Slice<br>20 | 7.95 ft         | 185.20075<br>ft | -159.86935<br>psf | 2,758.9157<br>psf | 2,572.7305<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                    |
| Slice<br>21 | 10.95 ft        | 186.66333<br>ft | -103.45834<br>psf | 2,514.3397<br>psf | 2,344.6597<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                    |
| Slice<br>22 | 14 ft           | 188.26236<br>ft | -70.070927<br>psf | 2,288.0101<br>psf | 2,133.6039<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                    |
| Slice<br>23 | 15.25 ft        | 188.97382<br>ft | -62.340785<br>psf | 2,193.4649<br>psf | 2,045.4391<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                    |
| Slice<br>24 | 16 ft           | 189.424 ft      | -58.384012<br>psf | 2,138.6447<br>psf | 1,994.3184<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                    |
| Slice<br>25 | 17.50351 ft     | 190.36741<br>ft | -50.390413<br>psf | 2,034.4752<br>psf | 1,897.1788<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                    |
| Slice<br>26 | 19.25351 ft     | 191.51456<br>ft | -43.009401<br>psf | 1,923.2735<br>psf | 1,793.4816<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                    |
| Slice<br>27 | 20.75 ft        | 192.55706<br>ft | -38.324338<br>psf | 1,834.1667<br>psf | 1,433.0081<br>psf | 0 psf   | 0 psf | Gravel Borrow   |
| Slice<br>28 | 22.75 ft        | 194.051 ft      | -33.503747<br>psf | 1,610.1985<br>psf | 1,501.5344<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                    |
| Slice<br>29 | 24.25 ft        | 195.21077<br>ft | -30.511031<br>psf | 1,539.9531<br>psf | 1,436.0295<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense                                   |

|             |                 | I               |                   |                   | l                 |       | I     | Sand/Gravel                                  |
|-------------|-----------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>30 | 25.2 ft         | 195.99707<br>ft | -29.171505<br>psf | 1,470.7603<br>psf | 1,371.5062<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>31 | 26.25 ft        | 196.88485<br>ft | -28.172489<br>psf | 1,397.2738<br>psf | 1,302.9789<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>32 | 27.925 ft       | 198.40854<br>ft | -28.272026<br>psf | 1,283.1098<br>psf | 1,196.5192<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>33 | 30.575 ft       | 200.97593<br>ft | -31.384334<br>psf | 1,111.1906<br>psf | 1,036.202<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>34 | 33.9 ft         | 204.64532<br>ft | -45.385097<br>psf | 894.06429<br>psf  | 833.72844<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>35 | 36.9 ft         | 208.28902<br>ft | -72.810031<br>psf | 756.51958<br>psf  | 705.46592<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>36 | 38.65 ft        | 210.68762<br>ft | -107.55797<br>psf | 634.61828<br>psf  | 591.79112<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>37 | 39.8 ft         | 212.37424<br>ft | -144.69408<br>psf | 552.38594<br>psf  | 515.10823<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>38 | 41 ft           | 214.28629<br>ft | -201.88589<br>psf | 469.51281<br>psf  | 437.82778<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>39 | 42.19125 ft     | 216.27268<br>ft | -285.31739<br>psf | 388.30696<br>psf  | 362.1021<br>psf   | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>40 | 43.348543<br>ft | 218.4016<br>ft  | -399.23263<br>psf | 284.55685<br>psf  | 265.35356<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>41 | 44.913607<br>ft | 221.54185<br>ft | 0 psf             | 141.02731<br>psf  | 110.18261<br>psf  | 0 psf | 0 psf | Gravel Borrow                                |

# 2A.5 Global - Post-Seismic (Spencer)

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### **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 651 Date: 01/17/2022 Time: 02:02:35 PM

Tool Version: 11.1.1.22085

Last Solved Date: 01/17/2022 Last Solved Time: 02:12:26 PM

### **Project Settings**

Unit System: U.S. Customary Units

# **Analysis Settings**

#### 2A.5 Global - Post-Seismic (Spencer)

Description: Project Num: 00180-366-01 Wall: 05.85L-A Station: 1+90

Kind: SLOPE/W

Parent: 2. Steady State (Global)

Analysis Type: Spencer

Settings

PWP Conditions from Parent Analysis: 2. Steady State (Global) [(last)]

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 20

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

Factor of Safety Convergence Settings

Maximum Number of Iterations: 100

Tolerable difference in F of S: 0.001

Solution Settings

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3 Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

#### **Materials**

### **ESU 2A Very Loose to Loose Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **ESU 2B Medium Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

### **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

#### Common Borrow

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **SEW Wall**

Material Model: High Strength

Unit Weight: 130 pcf

### **ESU 2B Medium Dense Sand/Gravel (Residual Strength)**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 497 psf Effective Friction Angle: 0 °

Phi-B: 0°

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

### **Slip Surface Entry and Exit**

Left Type: Range

Left-Zone Left Coordinate: (-50, 180.86613) ft

Left-Zone Right Coordinate: (0, 195) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15, 218.535) ft Right-Zone Right Coordinate: (70, 223.39933) ft

Right-Zone Increment: 30 Radius Increments: 20

# **Slip Surface Limits**

Left Coordinate: (-100, 170.1) ft Right Coordinate: (100, 223.6) ft

# **Surcharge Loads**

### Surcharge Load 1

Surcharge (Unit Weight): 125 pcf

Direction: Vertical

#### Coordinates

| X       | Υ         |
|---------|-----------|
| 35.9 ft | 224.15 ft |
| 39.4 ft | 224.2 ft  |
| 40.2 ft | 224.2 ft  |
| 100 ft  | 224.6 ft  |

# **Geometry**

Name: Default Geometry

### **Settings**

View: 2D

Element Thickness: 1 ft

#### **Points**

| ITS      |             |             |
|----------|-------------|-------------|
|          | X           | Y           |
| Point 1  | 100 ft      | 160 ft      |
| Point 2  | 100 ft      | 185.5 ft    |
| Point 3  | 0.9 ft      | 160 ft      |
| Point 4  | 100 ft      | 211.1475 ft |
| Point 5  | 3.8 ft      | 183 ft      |
| Point 6  | -20.1275 ft | 160 ft      |
| Point 7  | 100 ft      | 219.64 ft   |
| Point 8  | 42.5825 ft  | 219.8525 ft |
| Point 9  | 40.2 ft     | 223.2 ft    |
| Point 10 | 100 ft      | 223.6 ft    |
| Point 11 | 0 ft        | 211.7 ft    |
| Point 12 | 0 ft        | 192 ft      |
| Point 13 | 13 ft       | 192 ft      |
| Point 14 | 24.5 ft     | 213.8 ft    |
| Point 15 | 24.5 ft     | 192 ft      |
| Point 16 | 24.5 ft     | 203 ft      |
| Point 17 | 24.5 ft     | 205 ft      |
| Point 18 | 41.8 ft     | 220.7 ft    |
| Point 19 | 26.6 ft     | 215.4 ft    |
| Point 20 | 37.9 ft     | 223.2 ft    |
| Point 21 | 6.13959 ft  | 185.3 ft    |
| Point 22 | 8.9 ft      | 192 ft      |
| Point 23 | -100 ft     | 160 ft      |
| Point 24 | -100 ft     | 170.1 ft    |
| Point 25 | -91.8 ft    | 174.4 ft    |
| Point 26 | -88.3 ft    | 176.5 ft    |
| Point 27 | -85.7 ft    | 177.8 ft    |
| Point 28 | -83.4 ft    | 178.4 ft    |
| Point 29 | -76 ft      | 178.9 ft    |
| Point 30 | -74 ft      | 179.7 ft    |
| Point 31 | -55.9 ft    | 180.2 ft    |
| Point 32 | -37.3 ft    | 182.3 ft    |
| Point 33 | -30.3 ft    | 182.9 ft    |
| Point 34 | -13.6 ft    | 190.2 ft    |
| Point 35 | 7 ft        | 223 ft      |
| Point 36 | 15 ft       | 223 ft      |
| Point 37 | 15 ft       | 211.7 ft    |
| Point 38 | 7 ft        | 211.7 ft    |

| Point 39 | -6 ft       | 195 ft       |
|----------|-------------|--------------|
| Point 40 | -37.3275 ft | 162.2725 ft  |
| Point 41 | -47.26 ft   | 160 ft       |
| Point 42 | -5.125 ft   | 182.98095 ft |
| Point 43 | 80.7025 ft  | 160 ft       |
| Point 44 | -100 ft     | 129.8675 ft  |
| Point 45 | 100 ft      | 129.8675 ft  |
| Point 46 | -100 ft     | 147.8625 ft  |
| Point 47 | -27.95 ft   | 152.3875 ft  |
| Point 48 | -100 ft     | 133.97 ft    |
| Point 49 | 16.5 ft     | 197.3 ft     |
| Point 50 | 100 ft      | 209.9025 ft  |
| Point 51 | 95.42762 ft | 209.80965 ft |
| Point 52 | 3.915 ft    | 160.77581 ft |
| Point 53 | 17.7925 ft  | 187.09412 ft |
| Point 54 | 28.7 ft     | 129.8675 ft  |
| Point 55 | 0 ft        | 198.7 ft     |
| Point 56 | 47.15 ft    | 195.68393 ft |
| Point 57 | 42.67 ft    | 194.37311 ft |
| Point 58 | 0 ft        | 195 ft       |
| Point 59 | -32.3 ft    | 165.4 ft     |
| Point 60 | -16 ft      | 164.1 ft     |
| Point 61 | -100 ft     | 150.0525 ft  |
| Point 62 | 15 ft       | 218.535 ft   |
| Point 63 | 24 ft       | 223 ft       |
| Point 64 | 7 ft        | 214.495 ft   |
| Point 65 | 1.355 ft    | 211.7 ft     |
| Point 66 | 25.9 ft     | 223 ft       |
| Point 67 | 22 ft       | 192 ft       |
| Point 68 | 15.0117 ft  | 208.01106 ft |
| Point 69 | 21.5 ft     | 192 ft       |
| Point 70 | 15.5 ft     | 192 ft       |
| Point 71 | 15.5 ft     | 211.7 ft     |
| Point 72 | 15.5 ft     | 194.35 ft    |
| Point 73 | 15.5 ft     | 197.3 ft     |
| Point 74 | 15.5 ft     | 208.29 ft    |
| Point 75 | 18.50702 ft | 197.3 ft     |
| Point 76 | 15.5 ft     | 196.43333 ft |
| Point 77 | 21.5 ft     | 211.7 ft     |
| Point 78 | 20 ft       | 197.3 ft     |
| Point 79 | 20 ft       | 192 ft       |
| Point 80 | 21.5 ft     | 202 ft       |
| Point 81 | 21.5 ft     | 200 ft       |
| Point 82 | 21.5 ft     | 208.29 ft    |
| Point 83 | 31.9 ft     | 223.1 ft     |
| Point 84 | 31.9 ft     | 219.08 ft    |
|          |             |              |

# Regions

|              | Material   | Points   | Area                       |
|--------------|--|--|----------------------------|
| Region<br>1  | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 1,2,52,3,43  | 1,263.5<br>ft <sup>2</sup> |
| Region<br>2  | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 52,2,50,51,56,57,53,5,60,6,47,3                          | 2,656.9<br>ft <sup>2</sup> |
| Region<br>3  | Gravel Borrow  | 9,18,8,7,10  | 214.55<br>ft <sup>2</sup>  |
| Region<br>4  | SEW Wall   | 38,65,11,55,68,74,71,37                                  | 127 ft <sup>2</sup>        |
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel                                  | 8,16,17,18   | 31.556<br>ft <sup>2</sup>  |
| Region<br>6  | ESU 2A Very Loose to Loose<br>Sand/Gravel                        | 18,17,14,19,84,20,9                                      | 115.05<br>ft <sup>2</sup>  |
| Region<br>7  | Common Borrow  | 38,37,62,64  | 38.52<br>ft <sup>2</sup>   |
| Region<br>8  | Common Borrow  | 14,19,84,83,66,63,62,37,71,77                            | 132.58<br>ft <sup>2</sup>  |
| Region<br>9  | ESU 2B Medium Dense Sand/Gravel                                  | 22,42,59,40,60,5,21,13                                   | 332.37<br>ft <sup>2</sup>  |
| Region<br>10 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 44,54,45,1,43,3,47,48                                    | 4,704.7<br>ft <sup>2</sup> |
| Region<br>11 | ESU 2B Medium Dense Sand/Gravel (Residual Strength)              | 41,46,48,47,6,60,40                                      | 992.46<br>ft <sup>2</sup>  |
| Region<br>12 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 56,51,50,4,7,8,16,15,67,69,79,70,13,21,5,53,57           | 1,417.8<br>ft <sup>2</sup> |
| Region<br>13 | ESU 2A Very Loose to Loose<br>Sand/Gravel                        | 34,33,32,31,30,29,28,27,26,25,24,23,40,59,42,22,12,58,39 | 1,656.2<br>ft <sup>2</sup> |
| Region<br>14 | ESU 2A Very Loose to Loose<br>Sand/Gravel                        | 40,23,61,46,41   | 379.99<br>ft <sup>2</sup>  |
| Region<br>15 |  | 63,36,62   | 20.093<br>ft <sup>2</sup>  |
| Region<br>16 |  | 36,35,64,62  | 51.88<br>ft <sup>2</sup>   |
| Region<br>17 | Common Borrow  | 64,65,38   | 7.8889<br>ft <sup>2</sup>  |
| Region<br>18 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 15,16,81,69,67   | 28.5 ft <sup>2</sup>       |
| Region<br>19 | SEW Wall   | 72,76,22,13  | 11.692<br>ft <sup>2</sup>  |
| Region<br>20 | SEW Wall   | 70,72,13   | 2.9375<br>ft <sup>2</sup>  |
| Region<br>21 | SEW Wall   | 70,79,78,75,72   | 19.415<br>ft <sup>2</sup>  |
| Region<br>22 | Gravel Borrow  | 81,75,78,79,69   | 11.991<br>ft <sup>2</sup>  |
| Region<br>23 | Gravel Borrow  | 49,75,81,80  | 7.7095<br>ft <sup>2</sup>  |
| Region<br>24 | SEW Wall   | 49,76,72,75  | 4.002<br>ft <sup>2</sup>   |
| Region<br>25 | SEW Wall   | 73,76,49   | 0.43333<br>ft <sup>2</sup> |
| Region       | SEW Wall   | 76,73,74,68,55,58,12,22                                  | 163.72                     |

| 26           |   |                | ft²                      |
|--------------|---|----------------|--------------------------|
| Region<br>27 | ESU 2B Medium Dense Sand/Gravel           | 80,81,16,17    | 6 ft²                    |
| Region<br>28 | Gravel Borrow                             | 74,82,77       | 10.23<br>ft <sup>2</sup> |
| Region<br>29 | Gravel Borrow                             | 77,71,74       | 10.23<br>ft <sup>2</sup> |
| Region<br>30 | ESU 2A Very Loose to Loose<br>Sand/Gravel | 77,82,80,17,14 | 27.75<br>ft <sup>2</sup> |
| Region<br>31 | Gravel Borrow                             | 73,49,80,82,74 | 54.19<br>ft <sup>2</sup> |
| Region<br>32 | Common Borrow                             | 20,83,84       | 12.06<br>ft <sup>2</sup> |
| Region<br>33 |   | 55,39,58       | 11.1 ft <sup>2</sup>     |

# **Slip Results**

Slip Surfaces Analysed: 3713 of 16926 converged

# **Current Slip Surface**

Slip Surface: 3,605 Factor of Safety: 1.6 Volume: 1,345.2449 ft<sup>3</sup> Weight: 161,587.73 lbf

Resisting Moment: 8,274,980.4 lbf·ft Activating Moment: 5,077,988.3 lbf·ft

Resisting Force: 102,599.41 lbf Activating Force: 62,974.195 lbf Slip Rank: 1 of 16,926 slip surfaces Exit: (-39.462739, 182.05582) ft Entry: (43.844369, 223.22438) ft

Radius: 68.051682 ft

Center: (-19.83779, 247.21634) ft

### **Slip Slices**

|            | Х                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material                                |
|------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|--|
| Slice<br>1 | -38.381369<br>ft | 181.74952<br>ft | -184.72699<br>psf | 84.179661<br>psf         | 52.601291<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>2 | -36.133333<br>ft | 181.15543<br>ft | -184.12592<br>psf | 231.34168<br>psf         | 144.55832<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>3 | -33.8 ft         | 180.62304<br>ft | -182.80161<br>psf | 348.37297<br>psf         | 217.68759<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice      | -31.466667       | 180.17606       | -181.52704        | 439.96106                | 274.91818              |                      |                     | ESU 2A Very                                  |

| 4           | ft               | ft              | psf               | psf               | psf               | 0 psf | 0 psf | Loose to Loose<br>Sand/Gravel                |
|-------------|------------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>5  | -28.908333<br>ft | 179.78648<br>ft | -179.6421<br>psf  | 593.07459<br>psf  | 370.59414<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>6  | -26.125 ft       | 179.47013<br>ft | -178.87824<br>psf | 795.0535<br>psf   | 496.80457<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>7  | -23.341667<br>ft | 179.26921<br>ft | -178.19734<br>psf | 961.48033<br>psf  | 600.79959<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>8  | -20.558333<br>ft | 179.1827<br>ft  | -178.33075<br>psf | 1,097.3473<br>psf | 685.69868<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>9  | -17.775 ft       | 179.21018<br>ft | -185.68001<br>psf | 1,206.526<br>psf  | 753.92113<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>10 | -14.991667<br>ft | 179.35177<br>ft | -198.74798<br>psf | 1,292.0634<br>psf | 807.37084<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>11 | -11.747559<br>ft | 179.67303<br>ft | -344.90271<br>psf | 1,407.0872<br>psf | 879.24565<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>12 | -7.9475589<br>ft | 180.24066<br>ft | -400.29183<br>psf | 1,541.6773<br>psf | 963.3469<br>psf   | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>13 | -5.5625 ft       | 180.68028<br>ft | -362.75844<br>psf | 1,578.3879<br>psf | 986.2862<br>psf   | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>14 | -3.84375 ft      | 181.08401<br>ft | -337.22185<br>psf | 1,497.7687<br>psf | 935.90976<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>15 | -1.28125 ft      | 181.75709<br>ft | -299.62191<br>psf | 1,375.917<br>psf  | 859.76834<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>16 | 0.6775 ft        | 182.33452<br>ft | -271.81281<br>psf | 3,332.4068<br>psf | 2,082.3189<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>17 | 2.9086702<br>ft  | 183.09994<br>ft | -242.27377<br>psf | 3,238.6145<br>psf | 2,023.7109<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>18 | 5.3009652<br>ft  | 183.98454<br>ft | -201.86945<br>psf | 3,233.626<br>psf  | 3,015.4051<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>19 | 6.569795 ft      | 184.49909<br>ft | -177.12016<br>psf | 3,192.5145<br>psf | 2,977.068<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>20 | 7.95 ft          | 185.10525<br>ft | -156.36495<br>psf | 3,143.3566<br>psf | 2,931.2274<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>21 | 10.95 ft         | 186.57099<br>ft | -102.19168<br>psf | 3,021.7952<br>psf | 2,817.8697<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |

| Slice<br>22 | 14 ft           | 188.18493<br>ft | -68.87008<br>psf  | 2,873.5417<br>psf | 2,679.621<br>psf  | 0 psf | 0 psf | Very Dense<br>Sand/Gravel                    |
|-------------|-----------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>23 | 15.25 ft        | 188.90859<br>ft | -61.372977<br>psf | 2,795.2376<br>psf | 2,606.6012<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>24 | 16 ft           | 189.36879<br>ft | -57.617279<br>psf | 2,745.6778<br>psf | 2,560.3859<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>25 | 17.50351 ft     | 190.33736<br>ft | -50.046546<br>psf | 2,643.3197<br>psf | 2,464.9355<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>26 | 19.25351 ft     | 191.52011<br>ft | -43.065855<br>psf | 2,521.9621<br>psf | 2,351.7677<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>27 | 20.75 ft        | 192.60142<br>ft | -38.792586<br>psf | 2,450.846<br>psf  | 1,914.8108<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>28 | 22.75 ft        | 194.16219<br>ft | -34.625819<br>psf | 2,124.6577<br>psf | 1,981.2753<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>29 | 24.25 ft        | 195.37822<br>ft | -32.143761<br>psf | 2,018.3257<br>psf | 1,882.1191<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>30 | 25.2 ft         | 196.20892<br>ft | -31.270669<br>psf | 1,917.5968<br>psf | 1,788.1879<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>31 | 26.25 ft        | 197.14917<br>ft | -30.956212<br>psf | 1,807.5674<br>psf | 1,685.5839<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>32 | 27.925 ft       | 198.77787<br>ft | -32.204416<br>psf | 1,629.146<br>psf  | 1,519.2032<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>33 | 30.575 ft       | 201.54701<br>ft | -38.262027<br>psf | 1,350.0783<br>psf | 1,258.9684<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>34 | 33.9 ft         | 205.59165<br>ft | -58.81759<br>psf  | 992.03567<br>psf  | 925.08823<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>35 | 36.9 ft         | 209.68543<br>ft | -104.92924<br>psf | 733.61111<br>psf  | 684.10343<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>36 | 38.65 ft        | 212.45926<br>ft | -167.01043<br>psf | 548.27386<br>psf  | 511.27365<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>37 | 39.8 ft         | 214.44935<br>ft | -233.4533<br>psf  | 429.34405<br>psf  | 400.36981<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>38 | 41 ft           | 216.77626<br>ft | -345.23437<br>psf | 311.36094<br>psf  | 290.34878<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>39 | 42.095707<br>ft | 219.02478<br>ft | -491.37336<br>psf | 211.62726<br>psf  | 197.34562<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice       | 42.448792       | 219.80479       | -545.92821        | 198.62307         | 124.11347         |       |       | ESU 2B Medium                                |

#### 2A.5 Global - Post-Seismic (Spencer)

| 40          | ft          | ft              | psf   | psf              | psf              | 0 psf | 0 psf | Dense<br>Sand/Gravel |
|-------------|-------------|-----------------|-------|------------------|------------------|-------|-------|----------------------|
| Slice<br>41 | 43.17527 ft | 221.57977<br>ft | 0 psf | 106.26164<br>psf | 83.020691<br>psf | 0 psf | 0 psf | Gravel Borrow        |

# 2A.6 Global - Post-Seismic (M-P)

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### **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 651 Date: 01/17/2022 Time: 02:02:35 PM

Tool Version: 11.1.1.22085

Last Solved Date: 01/17/2022 Last Solved Time: 02:12:43 PM

### **Project Settings**

Unit System: U.S. Customary Units

# **Analysis Settings**

#### 2A.6 Global - Post-Seismic (M-P)

Description: Project Num: 00180-366-01 Wall: 05.85L-A Station: 1+90

Kind: SLOPE/W

Parent: 2. Steady State (Global) Analysis Type: Morgenstern-Price

Settings

Side Function

Interslice force function option: Half-Sine

PWP Conditions from Parent Analysis: 2. Steady State (Global) [(last)]

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 20

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

Factor of Safety Convergence Settings

Maximum Number of Iterations: 100 Tolerable difference in F of S: 0.001

Solution Settings

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

#### **Materials**

#### **ESU 2A Very Loose to Loose Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **ESU 2B Medium Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

### **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **SEW Wall**

Material Model: High Strength

Unit Weight: 130 pcf

### **ESU 2B Medium Dense Sand/Gravel (Residual Strength)**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 497 psf Effective Friction Angle: 0 °

Phi-B: 0°

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

# **Slip Surface Entry and Exit**

Left Type: Range

Left-Zone Left Coordinate: (-50, 180.86613) ft

Left-Zone Right Coordinate: (0, 195) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15, 218.535) ft Right-Zone Right Coordinate: (70, 223.39933) ft

Right-Zone Increment: 30 Radius Increments: 20

### **Slip Surface Limits**

Left Coordinate: (-100, 170.1) ft Right Coordinate: (100, 223.6) ft

# **Surcharge Loads**

#### Surcharge Load 1

Surcharge (Unit Weight): 125 pcf

Direction: Vertical

#### Coordinates

| X       | Y         |
|---------|-----------|
| 35.9 ft | 224.15 ft |
| 39.4 ft | 224.2 ft  |
| 40.2 ft | 224.2 ft  |

100 ft | 224.6 ft

# **Geometry**

Name: Default Geometry

### **Settings**

View: 2D

Element Thickness: 1 ft

#### **Points**

|          | Х           | Υ           |
|----------|-------------|-------------|
| Point 1  | 100 ft      | 160 ft      |
| Point 2  | 100 ft      | 185.5 ft    |
| Point 3  | 0.9 ft      | 160 ft      |
| Point 4  | 100 ft      | 211.1475 ft |
| Point 5  | 3.8 ft      | 183 ft      |
| Point 6  | -20.1275 ft | 160 ft      |
| Point 7  | 100 ft      | 219.64 ft   |
| Point 8  | 42.5825 ft  | 219.8525 ft |
| Point 9  | 40.2 ft     | 223.2 ft    |
| Point 10 | 100 ft      | 223.6 ft    |
| Point 11 | 0 ft        | 211.7 ft    |
| Point 12 | 0 ft        | 192 ft      |
| Point 13 | 13 ft       | 192 ft      |
| Point 14 | 24.5 ft     | 213.8 ft    |
| Point 15 | 24.5 ft     | 192 ft      |
| Point 16 | 24.5 ft     | 203 ft      |
| Point 17 | 24.5 ft     | 205 ft      |
| Point 18 | 41.8 ft     | 220.7 ft    |
| Point 19 | 26.6 ft     | 215.4 ft    |
| Point 20 | 37.9 ft     | 223.2 ft    |
| Point 21 | 6.13959 ft  | 185.3 ft    |
| Point 22 | 8.9 ft      | 192 ft      |
| Point 23 | -100 ft     | 160 ft      |
| Point 24 | -100 ft     | 170.1 ft    |
| Point 25 | -91.8 ft    | 174.4 ft    |
| Point 26 | -88.3 ft    | 176.5 ft    |
| Point 27 | -85.7 ft    | 177.8 ft    |
| Point 28 | -83.4 ft    | 178.4 ft    |
| Point 29 | -76 ft      | 178.9 ft    |
| Point 30 | -74 ft      | 179.7 ft    |
| Point 31 | -55.9 ft    | 180.2 ft    |
| Point 32 | -37.3 ft    | 182.3 ft    |
| Point 33 | -30.3 ft    | 182.9 ft    |
| Point 34 | -13.6 ft    | 190.2 ft    |
| Point 35 | 7 ft        | 223 ft      |
| Point 36 | 15 ft       | 223 ft      |
|          | I           | 1           |

| l p. :   | 1 4 5 6     | 244 7 (4     |
|----------|-------------|--------------|
| Point 37 | 15 ft       | 211.7 ft     |
| Point 38 | 7 ft        | 211.7 ft     |
| Point 39 | -6 ft       | 195 ft       |
| Point 40 | -37.3275 ft | 162.2725 ft  |
| Point 41 | -47.26 ft   | 160 ft       |
| Point 42 | -5.125 ft   | 182.98095 ft |
| Point 43 | 80.7025 ft  | 160 ft       |
| Point 44 | -100 ft     | 129.8675 ft  |
| Point 45 | 100 ft      | 129.8675 ft  |
| Point 46 | -100 ft     | 147.8625 ft  |
| Point 47 | -27.95 ft   | 152.3875 ft  |
| Point 48 | -100 ft     | 133.97 ft    |
| Point 49 | 16.5 ft     | 197.3 ft     |
| Point 50 | 100 ft      | 209.9025 ft  |
| Point 51 | 95.42762 ft | 209.80965 ft |
| Point 52 | 3.915 ft    | 160.77581 ft |
| Point 53 | 17.7925 ft  | 187.09412 ft |
| Point 54 | 28.7 ft     | 129.8675 ft  |
| Point 55 | 0 ft        | 198.7 ft     |
| Point 56 | 47.15 ft    | 195.68393 ft |
| Point 57 | 42.67 ft    | 194.37311 ft |
| Point 58 | 0 ft        | 195 ft       |
| Point 59 | -32.3 ft    | 165.4 ft     |
| Point 60 | -16 ft      | 164.1 ft     |
| Point 61 | -100 ft     | 150.0525 ft  |
| Point 62 | 15 ft       | 218.535 ft   |
| Point 63 | 24 ft       | 223 ft       |
| Point 64 | 7 ft        | 214.495 ft   |
| Point 65 | 1.355 ft    | 211.7 ft     |
| Point 66 | 25.9 ft     | 223 ft       |
| Point 67 | 22 ft       | 192 ft       |
| Point 68 | 15.0117 ft  | 208.01106 ft |
| Point 69 | 21.5 ft     | 192 ft       |
| Point 70 | 15.5 ft     | 192 ft       |
| Point 71 | 15.5 ft     | 211.7 ft     |
| Point 72 | 15.5 ft     | 194.35 ft    |
| Point 73 | 15.5 ft     | 197.3 ft     |
| Point 74 | 15.5 ft     | 208.29 ft    |
| Point 75 | 18.50702 ft | 197.3 ft     |
| Point 76 | 15.5 ft     | 196.43333 ft |
| Point 77 | 21.5 ft     | 211.7 ft     |
| Point 78 | 20 ft       | 197.3 ft     |
| Point 79 | 20 ft       | 192 ft       |
| Point 80 | 21.5 ft     | 202 ft       |
| Point 81 | 21.5 ft     | 200 ft       |
| Point 82 | 21.5 ft     | 208.29 ft    |
| Point 83 | 31.9 ft     | 223.1 ft     |
| Point 84 | 31.9 ft     | 219.08 ft    |
|          | 1           |              |

### Regions

|              | Material   | Points   | Area                       |
|--------------|--|--|----------------------------|
| Region<br>1  | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 1,2,52,3,43  | 1,263.5<br>ft <sup>2</sup> |
| Region<br>2  | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 52,2,50,51,56,57,53,5,60,6,47,3                          | 2,656.9<br>ft <sup>2</sup> |
| Region 3     | Gravel Borrow  | 9,18,8,7,10  | 214.55<br>ft <sup>2</sup>  |
| Region<br>4  | SEW Wall   | 38,65,11,55,68,74,71,37                                  | 127 ft <sup>2</sup>        |
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel                                  | 8,16,17,18   | 31.556<br>ft <sup>2</sup>  |
| Region<br>6  | ESU 2A Very Loose to Loose<br>Sand/Gravel                        | 18,17,14,19,84,20,9                                      | 115.05<br>ft <sup>2</sup>  |
| Region<br>7  | Common Borrow  | 38,37,62,64  | 38.52<br>ft <sup>2</sup>   |
| Region<br>8  | Common Borrow  | 14,19,84,83,66,63,62,37,71,77                            | 132.58<br>ft <sup>2</sup>  |
| Region<br>9  | ESU 2B Medium Dense Sand/Gravel                                  | 22,42,59,40,60,5,21,13                                   | 332.37<br>ft <sup>2</sup>  |
| Region<br>10 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 44,54,45,1,43,3,47,48                                    | 4,704.7<br>ft <sup>2</sup> |
| Region<br>11 | ESU 2B Medium Dense Sand/Gravel (Residual Strength)              | 41,46,48,47,6,60,40                                      | 992.46<br>ft <sup>2</sup>  |
| Region<br>12 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 56,51,50,4,7,8,16,15,67,69,79,70,13,21,5,53,57           | 1,417.8<br>ft <sup>2</sup> |
| Region<br>13 | ESU 2A Very Loose to Loose<br>Sand/Gravel                        | 34,33,32,31,30,29,28,27,26,25,24,23,40,59,42,22,12,58,39 | 1,656.2<br>ft <sup>2</sup> |
| Region<br>14 | ESU 2A Very Loose to Loose<br>Sand/Gravel                        | 40,23,61,46,41   | 379.99<br>ft <sup>2</sup>  |
| Region<br>15 |  | 63,36,62   | 20.093<br>ft <sup>2</sup>  |
| Region<br>16 |  | 36,35,64,62  | 51.88<br>ft²               |
| Region<br>17 | Common Borrow  | 64,65,38   | 7.8889<br>ft <sup>2</sup>  |
| Region<br>18 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 15,16,81,69,67   | 28.5 ft <sup>2</sup>       |
| Region<br>19 | SEW Wall   | 72,76,22,13  | 11.692<br>ft²              |
| Region<br>20 | SEW Wall   | 70,72,13   | 2.9375<br>ft <sup>2</sup>  |
| Region<br>21 | SEW Wall   | 70,79,78,75,72   | 19.415<br>ft <sup>2</sup>  |
| Region<br>22 | Gravel Borrow  | 81,75,78,79,69   | 11.991<br>ft <sup>2</sup>  |
| Region<br>23 | Gravel Borrow  | 49,75,81,80  | 7.7095<br>ft <sup>2</sup>  |
| Region<br>24 | SEW Wall   | 49,76,72,75  | 4.002<br>ft <sup>2</sup>   |
| Region<br>25 | SEW Wall   | 73,76,49   | 0.43333<br>ft <sup>2</sup> |

| Region<br>26 | SEW Wall                                  | 76,73,74,68,55,58,12,22 | 163.72<br>ft²            |
|--------------|---|-------------------------|--------------------------|
| Region<br>27 | ESU 2B Medium Dense Sand/Gravel           | 80,81,16,17             | 6 ft²                    |
| Region<br>28 | Gravel Borrow                             | 74,82,77                | 10.23<br>ft <sup>2</sup> |
| Region<br>29 | Gravel Borrow                             | 77,71,74                | 10.23<br>ft <sup>2</sup> |
| Region<br>30 | ESU 2A Very Loose to Loose<br>Sand/Gravel | 77,82,80,17,14          | 27.75<br>ft <sup>2</sup> |
| Region<br>31 | Gravel Borrow                             | 73,49,80,82,74          | 54.19<br>ft <sup>2</sup> |
| Region<br>32 | Common Borrow                             | 20,83,84                | 12.06<br>ft <sup>2</sup> |
| Region<br>33 |   | 55,39,58                | 11.1 ft²                 |

# **Slip Results**

Slip Surfaces Analysed: 3986 of 16926 converged

# **Current Slip Surface**

Slip Surface: 3,565 Factor of Safety: 1.6 Volume: 1,324.6782 ft<sup>3</sup> Weight: 158,551.65 lbf

Resisting Moment: 7,224,518.2 lbf·ft Activating Moment: 4,447,222.2 lbf·ft

Resisting Force: 99,458.321 lbf Activating Force: 61,253.09 lbf Slip Rank: 1 of 16,926 slip surfaces Exit: (-39.462739, 182.05582) ft Entry: (40.107848, 223.2) ft

Radius: 60.629231 ft

Center: (-18.446374, 238.92599) ft

### **Slip Slices**

|            | X                | Υ               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material                                |
|------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|--|
| Slice      | -38.381369<br>ft | 181.67926<br>ft | -184.7297<br>psf  | 66.443221<br>psf         | 41.518332<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>2 | -36.133333<br>ft | 180.94679<br>ft | -184.09026<br>psf | 202.22966<br>psf         | 126.36712<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice      | -33.8 ft         | 180.28543<br>ft | -182.76023<br>psf | 336.93437<br>psf         | 210.53996<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
|            | -33.8 ft         |                 |                   |                          | _                      | 0 p                  | sf                  | osf 0 psf                                    |

| -31.466667<br>ft | 179.72338<br>ft   | -181.47672<br>psf   | 465.23465<br>psf   | 290.71087<br>psf   | 0 psf   | 0 psf   | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel  |
|------------------|---|---|--|--|---|---|---|
| -28.908333<br>ft | 179.22293<br>ft   | -179.60891<br>psf   | 662.84438<br>psf   | 414.19114<br>psf   | 0 psf   | 0 psf   | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel  |
| -26.125 ft       | 178.80133<br>ft   | -178.61864<br>psf   | 923.91702<br>psf   | 577.32743<br>psf   | 0 psf   | 0 psf   | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel  |
| -23.341667<br>ft | 178.51084<br>ft   | -175.61288<br>psf   | 1,157.8436<br>psf  | 723.501<br>psf   | 0 psf   | 0 psf   | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel  |
| -20.558333<br>ft | 178.34956<br>ft   | -180.54345<br>psf   | 1,354.3699<br>psf  | 846.30423<br>psf   | 0 psf   | 0 psf   | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel  |
| -17.775 ft       | 178.31645<br>ft   | -192.10306<br>psf   | 1,506.6088<br>psf  | 941.43367<br>psf   | 0 psf   | 0 psf   | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel  |
| -14.991667<br>ft | 178.41132<br>ft   | -250.32815<br>psf   | 1,611.7546<br>psf  | 1,007.1361<br>psf  | 0 psf   | 0 psf   | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel  |
| -12.700355<br>ft | 178.57642<br>ft   | -392.05384<br>psf   | 1,687.5171<br>psf  | 1,054.4777<br>psf  | 0 psf   | 0 psf   | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel  |
| -10.350532<br>ft | 178.85753<br>ft   | -415.05091<br>psf   | 1,764.0149<br>psf  | 1,102.2788<br>psf  | 0 psf   | 0 psf   | ESU 2B Medium<br>Dense<br>Sand/Gravel   |
| -7.4501774<br>ft | 179.32051<br>ft   | -369.72616<br>psf   | 1,818.5854<br>psf  | 1,136.3783<br>psf  | 0 psf   | 0 psf   | ESU 2B Medium<br>Dense<br>Sand/Gravel   |
| -5.5625 ft       | 179.68319<br>ft   | -340.41286<br>psf   | 1,803.6886<br>psf  | 1,127.0697<br>psf  | 0 psf   | 0 psf   | ESU 2B Medium<br>Dense<br>Sand/Gravel   |
| -3.84375 ft      | 180.09637<br>ft   | -314.78325<br>psf   | 1,683.7745<br>psf  | 1,052.1391<br>psf  | 0 psf   | 0 psf   | ESU 2B Medium<br>Dense<br>Sand/Gravel   |
| -1.28125 ft      | 180.79272<br>ft   | -277.77774<br>psf   | 1,502.4471<br>psf  | 938.83317<br>psf   | 0 psf   | 0 psf   | ESU 2B Medium<br>Dense<br>Sand/Gravel   |
| 0.6775 ft        | 181.39625<br>ft   | -250.59007<br>psf   | 3,402.9843<br>psf  | 2,126.4206<br>psf  | 0 psf   | 0 psf   | ESU 2B Medium<br>Dense<br>Sand/Gravel   |
| 2.1603505<br>ft  | 181.91254<br>ft   | -231.23046<br>psf   | 3,284.394<br>psf   | 2,052.3171<br>psf  | 0 psf   | 0 psf   | ESU 2B Medium<br>Dense<br>Sand/Gravel   |
| 3.3828505<br>ft  | 182.36462<br>ft   | -212.67007<br>psf   | 3,362.6885<br>psf  | 3,135.7577<br>psf  | 0 psf   | 0 psf   | ESU 5B Very Stiff<br>to Hard Silt and<br>Clay/Dense to<br>Very Dense Silt   |
| 4.969795 ft      | 183.01554<br>ft   | -179.14105<br>psf   | 3,252.7731<br>psf  | 3,033.26<br>psf  | 0 psf   | 0 psf   | ESU 5B Very Stiff<br>to Hard Silt and<br>Clay/Dense to<br>Very Dense Silt<br>ESU 5B Very Stiff  |
|                  | ft  -28.908333 ft  -26.125 ft  -23.341667 ft  -17.775 ft  -14.991667 ft  -12.700355 ft  -10.350532 ft  -7.4501774 ft  -5.5625 ft  -3.84375 ft  -1.28125 ft  0.6775 ft  2.1603505 ft  3.3828505 ft | ft         -28.9083333 ft       1779.22293 ft         -26.125 ft       1778.80133         -23.341667 ft       178.51084 ft         -20.558333 ft       178.34956 ft         -17.775 ft       178.31645         ft       178.57642 ft         -12.700355 ft       178.57642 ft         ft       179.32051 ft         -7.4501774 ft       179.32051 ft         -3.84375 ft       180.09637 ft         -1.28125 ft       180.79272 ft         0.6775 ft       181.39625 ft         ft       181.39625 ft         ft       182.36462 ft         4 969795 ft       183.01554 | ft         psf           -28.908333   ft         179.22293   -179.60891   psf           -26.125 ft         178.80133   -178.61864   psf           -23.341667   178.51084   ft         -175.61288   psf           -20.558333   178.34956   ft         -180.54345   psf           -17.775 ft         178.31645   -192.10306   psf           ft         178.41132   -250.32815   psf           ft         178.57642   -392.05384   psf           ft         178.857642   -392.05384   psf           ft         179.32051   -369.72616   psf           -7.4501774   179.32051   -369.72616   psf         -340.41286   psf           -3.84375 ft         180.09637   -314.78325   psf           -1.28125 ft         180.79272   -277.77774   psf           0.6775 ft         181.39625   -250.59007   psf           2.1603505   181.91254   -231.23046   psf           3.3828505   182.36462   -212.67007   psf           4.969735 ft         1883.01554   -179.14105 | ft         psf         psf           28.908333 ft         179.22293 psf         179.60891 psf         662.84438 psf           -26.125 ft         178.80133 psf         178.61864 psf         923.91702 psf           -23.341667 ft         178.51084 psf         175.61288 psf         1,157.8436 psf           -17.775 ft         178.34956 psf         180.54345 psf         1,506.6088 psf           -17.775 ft         178.41132 psf         192.10306 psf         1,506.6088 psf           -14.991667 psf         178.41132 psf         192.10306 psf         1,6611.7546 psf           -12.700355 psf         178.857642 psf         192.05384 psf         1,6611.7546 psf           -10.350532 psf         178.857642 psf         1,390.72614 psf         1,818.5854 psf           -1.4501774 psf         179.68319 psf         -340.41286 psf         1,803.6886 psf           -3.84375 psf         180.09637 psf         -314.78325 psf         1,683.7745 psf           -1.28125 psf         180.79272 psf         -277.77774 psf         1,502.4471 psf           0.6775 psf         181.39625 psf         -250.59007 psf         3,402.9843 psf           1.603505 psf         181.91254 psf         -231.23046 psf         3,284.394 psf           1.4999735 psf         183.01554 psf         -179.14105 p | ft         ft         psf         psf         psf           -28.908333         179.22293         -179.60891         662.84438         414.19114           -26.125 ft         178.80133         -178.61864         923.91702         577.32743           -23.341667         178.51084         -175.61288         1,157.8436         723.501           -20.558333         178.34956         -180.54345         1,354.3699         846.30423           -17.775 ft         178.31645         -192.10306         1,506.6088         941.43367           -14.991667         178.41132         -250.32815         1,611.7546         1,007.1361           ft         psf         psf         psf         psf           -12.700355         178.57642         -392.05384         1,687.5171         1,054.4777           psf         psf         psf         psf         psf           -7.4501774         179.32051         -369.72616         1,818.5854         1,136.3783           ft         psf         psf         psf         psf           -3.84375 ft         180.09637         -314.78325         1,683.7745         1,052.1391           -1.28125 ft         181.93625         -2777.77774         1,502.4471         psf< | ft         psf         psf         psf         Opsf           -28.908333         179.22293         -179.60891         662.84438         414.19114         0 psf           -26.125 ft         178.80133         -178.61864         923.91702         577.32743         0 psf           -23.341667         178.51084         -175.61288         1,157.8436         723.501         0 psf           -20.558333         178.34956         -180.54345         1,354.3699         846.30423         0 psf           -17.775 ft         178.41132         -192.10306         1,506.6088         941.43367         0 psf           -14.991667         178.41132         -250.32815         1,611.7546         1,007.1361         0 psf           -12.700355         178.57642         -392.05384         1,687.5171         1,054.4777         0 psf           -10.350532         178.85753         -415.05091         1,764.0149         1,102.2788         0 psf           -7.4501774         179.32051         -369.72616         1,818.5854         1,136.3783         0 psf           -5.5625 ft         179.68319         -340.41286         1,803.6886         1,127.0697         0 psf           -1.28125 ft         180.09637         -714.78325         1,683.7745 <td>ft         psf         psf         psf         Opsf         Opsf           -28.908333         ft         psf         psf         0 psf         0 psf           -26.125 ft         ft         psf         223.91702         577.32743         0 psf         0 psf           -26.125 ft         ft         psf         223.91702         577.32743         0 psf         0 psf           -23.341667         ft         psf         -175.61288         1,157.8436         723.501         0 psf         0 psf           -20.558333         ft         178.31645         -180.54345         1,354.3699         846.30423         0 psf         0 psf           -17.775 ft         ft         ft         psf         1,506.6088         941.43367         0 psf         0 psf           -12.700355         ft         ft         psf         1,6611.7546         1,007.1361         0 psf         0 psf           -12.700355         ft         ft         psf         1,687.5171         1,007.1361         0 psf         0 psf           -10.350532         ft         psf         psf         1,764.0149         1,102.2788         0 psf         0 psf           -7.4501774         ft         psf         <t< td=""></t<></td> | ft         psf         psf         psf         Opsf         Opsf           -28.908333         ft         psf         psf         0 psf         0 psf           -26.125 ft         ft         psf         223.91702         577.32743         0 psf         0 psf           -26.125 ft         ft         psf         223.91702         577.32743         0 psf         0 psf           -23.341667         ft         psf         -175.61288         1,157.8436         723.501         0 psf         0 psf           -20.558333         ft         178.31645         -180.54345         1,354.3699         846.30423         0 psf         0 psf           -17.775 ft         ft         ft         psf         1,506.6088         941.43367         0 psf         0 psf           -12.700355         ft         ft         psf         1,6611.7546         1,007.1361         0 psf         0 psf           -12.700355         ft         ft         psf         1,687.5171         1,007.1361         0 psf         0 psf           -10.350532         ft         psf         psf         1,764.0149         1,102.2788         0 psf         0 psf           -7.4501774         ft         psf <t< td=""></t<> |

| Slice<br>21 | 6.569795 ft     | 183.70034<br>ft | -145.27789<br>psf | 3,142.6751<br>psf | 2,930.592<br>psf  | 0 psf | 0 psf | to Hard Silt and<br>Clay/Dense to<br>Very Dense Silt                      |
|-------------|-----------------|-----------------|-------------------|-------------------|-------------------|-------|-------|---|
| Slice<br>22 | 7.1191192<br>ft | 183.95061<br>ft | -136.31103<br>psf | 3,104.158<br>psf  | 2,894.6742<br>psf | 0 psf | 0 psf | ESU 5B Very Stiff<br>to Hard Silt and<br>Clay/Dense to<br>Very Dense Silt |
| Slice<br>23 | 8.0691192<br>ft | 184.41013<br>ft | -125.52094<br>psf | 3,036.6881<br>psf | 2,831.7574<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                              |
| Slice<br>24 | 9.925 ft        | 185.35712<br>ft | -101.58276<br>psf | 2,906.0488<br>psf | 2,709.9344<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                              |
| Slice<br>25 | 11.975 ft       | 186.49471<br>ft | -83.542116<br>psf | 2,763.3895<br>psf | 2,576.9024<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                              |
| Slice<br>26 | 14 ft           | 187.72311<br>ft | -65.252821<br>psf | 2,610.9188<br>psf | 2,434.7212<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                              |
| Slice<br>27 | 15.25 ft        | 188.52393<br>ft | -55.654776<br>psf | 2,511.1937<br>psf | 2,341.726<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                              |
| Slice<br>28 | 16 ft           | 189.03629<br>ft | -52.935826<br>psf | 2,450.9936<br>psf | 2,285.5885<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                              |
| Slice<br>29 | 17.50351 ft     | 190.1207<br>ft  | -47.576163<br>psf | 2,332.021<br>psf  | 2,174.6448<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                              |
| Slice<br>30 | 19.25351 ft     | 191.45269<br>ft | -42.381173<br>psf | 2,198.6677<br>psf | 2,050.2908<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                              |
| Slice<br>31 | 20.75 ft        | 192.68119<br>ft | -39.635688<br>psf | 2,137.6769<br>psf | 1,670.1363<br>psf | 0 psf | 0 psf | Gravel Borrow   |
| Slice<br>32 | 22.75 ft        | 194.47537<br>ft | -37.787964<br>psf | 1,811.0101<br>psf | 1,688.7942<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                              |
| Slice<br>33 | 24.25 ft        | 195.88183<br>ft | -37.053605<br>psf | 1,709.937<br>psf  | 1,594.542<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                              |
| Slice<br>34 | 25.2 ft         | 196.85604<br>ft | -37.707094<br>psf | 1,615.7578<br>psf | 1,506.7185<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                              |
| Slice<br>35 | 26.25 ft        | 197.96418<br>ft | -39.450437<br>psf | 1,513.9555<br>psf | 1,411.7863<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                              |
| Slice<br>36 | 27.925 ft       | 199.92134<br>ft | -45.186409<br>psf | 1,348.2056<br>psf | 1,257.222<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                              |
| Slice<br>37 | 30.575 ft       | 203.32086<br>ft | -62.748622<br>psf | 1,087.0422<br>psf | 1,013.6833<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                              |
| Slice<br>38 | 32.9 ft         | 206.74046<br>ft | -93.98265<br>psf  | 849.49406<br>psf  | 792.16603<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                              |

| Slice<br>39 | 34.9 ft         | 210.19237<br>ft | -158.39432<br>psf | 627.76051<br>psf | 585.39614<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
|-------------|-----------------|-----------------|-------------------|------------------|------------------|-------|-------|--|
| Slice<br>40 | 36.542942<br>ft | 213.43596<br>ft | -282.44568<br>psf | 486.43747<br>psf | 453.61028<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>41 | 37.542942<br>ft | 215.68308<br>ft | -383.52709<br>psf | 442.4543<br>psf  | 276.47613<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>42 | 38.084547<br>ft | 217.01942<br>ft | -430.69764<br>psf | 367.71312<br>psf | 229.77266<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>43 | 38.834547<br>ft | 219.13199<br>ft | -346.48104<br>psf | 253.48764<br>psf | 158.39666<br>psf | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>44 | 39.753924<br>ft | 221.98416<br>ft | -329.47457<br>psf | 108.89079<br>psf | 68.042515<br>psf | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |

# 2B.1 Global - Static FC Wall (Spencer)

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## **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 652 Date: 01/17/2022 Time: 02:07:09 PM

Tool Version: 11.1.1.22085

Last Solved Date: 01/17/2022 Last Solved Time: 02:17:01 PM

## **Project Settings**

Unit System: U.S. Customary Units

# **Analysis Settings**

#### 2B.1 Global - Static FC Wall (Spencer)

Description: With Forward Compatible Wall

Kind: SLOPE/W

Parent: 2. Steady State (Global)

Analysis Type: Spencer

Settings

PWP Conditions from Parent Analysis: 2. Steady State (Global) [(last)]

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 20

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

Factor of Safety Convergence Settings

Maximum Number of Iterations: 100

Tolerable difference in F of S: 0.001

Solution Settings

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3 Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

## **Materials**

## **ESU 2A Very Loose to Loose Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **ESU 2B Medium Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

## **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

# ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

#### Common Borrow

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **SEW Wall**

Material Model: High Strength

Unit Weight: 130 pcf

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

#### **Forward Compatible Wall**

Material Model: High Strength

Unit Weight: 130 pcf

#### **Lightweight EPS**

Material Model: Mohr-Coulomb

Unit Weight: 5 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 0 °

Phi-B: 0°

# **Slip Surface Entry and Exit**

Left Type: Range

Left-Zone Left Coordinate: (-40, 181.99516) ft Left-Zone Right Coordinate: (0, 196.3) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15, 223) ft

Right-Zone Right Coordinate: (70, 223.39933) ft

Right-Zone Increment: 30 Radius Increments: 20

## **Slip Surface Limits**

Left Coordinate: (-100, 170.1) ft Right Coordinate: (100, 223.6) ft

# **Surcharge Loads**

## Surcharge Load 1

Surcharge (Unit Weight): 250 pcf

Direction: Vertical

#### Coordinates



| 9 ft |      | 224 ft   |
|------|------|----------|
| 37.  | 9 ft | 224.2 ft |
| 40.  | 2 ft | 224.2 ft |
| 100  | ) ft | 224.6 ft |

# **Geometry**

Name: Default Geometry

# **Settings**

View: 2D

Element Thickness: 1 ft

#### **Points**

| 115      |             |             |
|----------|-------------|-------------|
|          | X           | Y           |
| Point 1  | 100 ft      | 160 ft      |
| Point 2  | 100 ft      | 185.5 ft    |
| Point 3  | 0.9 ft      | 160 ft      |
| Point 4  | 100 ft      | 211.1475 ft |
| Point 5  | 3.8 ft      | 183 ft      |
| Point 6  | -20.1275 ft | 160 ft      |
| Point 7  | 100 ft      | 219.64 ft   |
| Point 8  | 42.5825 ft  | 219.8525 ft |
| Point 9  | 40.2 ft     | 223.2 ft    |
| Point 10 | 100 ft      | 223.6 ft    |
| Point 11 | 0 ft        | 211.7 ft    |
| Point 12 | 0 ft        | 192 ft      |
| Point 13 | 13 ft       | 192 ft      |
| Point 14 | 24.5 ft     | 213.8 ft    |
| Point 15 | 24.5 ft     | 192 ft      |
| Point 16 | 24.5 ft     | 203 ft      |
| Point 17 | 24.5 ft     | 205 ft      |
| Point 18 | 41.8 ft     | 220.7 ft    |
| Point 19 | 26.6 ft     | 215.4 ft    |
| Point 20 | 37.9 ft     | 223.2 ft    |
| Point 21 | 6.13959 ft  | 185.3 ft    |
| Point 22 | 8.9 ft      | 192 ft      |
| Point 23 | -100 ft     | 160 ft      |
| Point 24 | -100 ft     | 170.1 ft    |
| Point 25 | -91.8 ft    | 174.4 ft    |
| Point 26 | -88.3 ft    | 176.5 ft    |
| Point 27 | -85.7 ft    | 177.8 ft    |
| Point 28 | -83.4 ft    | 178.4 ft    |
| Point 29 | -76 ft      | 178.9 ft    |
| Point 30 | -74 ft      | 179.7 ft    |
| Point 31 | -55.9 ft    | 180.2 ft    |
| Point 32 | -37.3 ft    | 182.3 ft    |
| Point 33 | -30.3 ft    | 182.9 ft    |
|          |             |             |

|          | 1           | 1            |
|----------|-------------|--------------|
| Point 34 | -13.6 ft    | 190.2 ft     |
| Point 35 | 7 ft        | 223 ft       |
| Point 36 | 15 ft       | 223 ft       |
| Point 37 | 15 ft       | 211.7 ft     |
| Point 38 | 7 ft        | 211.7 ft     |
| Point 39 | -6 ft       | 195 ft       |
| Point 40 | -37.3275 ft | 162.2725 ft  |
| Point 41 | -47.26 ft   | 160 ft       |
| Point 42 | -5.125 ft   | 182.98095 ft |
| Point 43 | 80.7025 ft  | 160 ft       |
| Point 44 | -100 ft     | 129.8675 ft  |
| Point 45 | 100 ft      | 129.8675 ft  |
| Point 46 | -100 ft     | 147.8625 ft  |
| Point 47 | -27.95 ft   | 152.3875 ft  |
| Point 48 | -100 ft     | 133.97 ft    |
| Point 49 | 16.5 ft     | 197.3 ft     |
| Point 50 | 100 ft      | 209.9025 ft  |
| Point 51 | 95.42762 ft | 209.80965 ft |
| Point 52 | 3.915 ft    | 160.77581 ft |
| Point 53 | 17.7925 ft  | 187.09412 ft |
| Point 54 | 28.7 ft     | 129.8675 ft  |
| Point 55 | 0 ft        | 198.7 ft     |
| Point 56 | 47.15 ft    | 195.68393 ft |
| Point 57 | 42.67 ft    | 194.37311 ft |
| Point 58 | 0 ft        | 195 ft       |
| Point 59 | -32.3 ft    | 165.4 ft     |
| Point 60 | -16 ft      | 164.1 ft     |
| Point 61 | -100 ft     | 150.0525 ft  |
| Point 62 | 15 ft       | 218.535 ft   |
| Point 63 | 24 ft       | 223 ft       |
| Point 64 | 7 ft        | 214.495 ft   |
| Point 65 | 1.355 ft    | 211.7 ft     |
| Point 66 | 25.9 ft     | 223 ft       |
| Point 67 | 22 ft       | 192 ft       |
| Point 68 | 15.0117 ft  | 208.01106 ft |
| Point 69 | 21.5 ft     | 192 ft       |
| Point 70 | 15.5 ft     | 192 ft       |
| Point 71 | 15.5 ft     | 211.7 ft     |
| Point 72 | 15.5 ft     | 194.35 ft    |
| Point 73 | 15.5 ft     | 197.3 ft     |
| Point 74 | 15.5 ft     | 208.29 ft    |
| Point 75 | 18.50702 ft | 197.3 ft     |
| Point 76 | 15.5 ft     | 196.43333 ft |
| Point 77 | 21.5 ft     | 211.7 ft     |
| Point 78 | 20 ft       | 197.3 ft     |
| Point 79 | 20 ft       | 192 ft       |
| Point 80 | 21.5 ft     | 202 ft       |
| Point 81 | 21.5 ft     | 200 ft       |
| . 5///01 |             |              |

| Point 82 | 21.5 ft | 208.29 ft |
|----------|---------|-----------|
| Point 83 | 31.9 ft | 223.1 ft  |
| Point 84 | 31.9 ft | 219.08 ft |

# Regions

|              | Material  | Points   | Area                       |
|--------------|---|--|----------------------------|
| Region<br>1  | ESU 4B Dense to Very Dense<br>Sand/Gravel                           | 1,2,52,3,43  | 1,263.5<br>ft <sup>2</sup> |
| Region<br>2  | ESU 5B Very Stiff to Hard Silt and<br>Clay/Dense to Very Dense Silt | 52,2,50,51,56,57,53,5,60,6,47,3                          | 2,656.9<br>ft <sup>2</sup> |
| Region<br>3  | Gravel Borrow   | 9,18,8,7,10  | 214.55<br>ft <sup>2</sup>  |
| Region<br>4  | SEW Wall  | 38,65,11,55,68,74,71,37                                  | 127 ft <sup>2</sup>        |
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel                                     | 8,16,17,18   | 31.556<br>ft <sup>2</sup>  |
| Region<br>6  | ESU 2A Very Loose to Loose<br>Sand/Gravel                           | 18,17,14,19,84,20,9                                      | 115.05<br>ft <sup>2</sup>  |
| Region<br>7  | Forward Compatible Wall   | 38,37,62,64  | 38.52<br>ft <sup>2</sup>   |
| Region<br>8  | Lightweight EPS   | 14,19,84,83,66,63,62,37,71,77                            | 132.58<br>ft <sup>2</sup>  |
| Region<br>9  | ESU 2B Medium Dense Sand/Gravel                                     | 22,42,59,40,60,5,21,13                                   | 332.37<br>ft <sup>2</sup>  |
| Region<br>10 | ESU 4B Dense to Very Dense<br>Sand/Gravel                           | 44,54,45,1,43,3,47,48                                    | 4,704.7<br>ft <sup>2</sup> |
| Region<br>11 | ESU 2B Medium Dense Sand/Gravel                                     | 41,46,48,47,6,60,40                                      | 992.46<br>ft <sup>2</sup>  |
| Region<br>12 | ESU 4B Dense to Very Dense<br>Sand/Gravel                           | 56,51,50,4,7,8,16,15,67,69,79,70,13,21,5,53,57           | 1,417.8<br>ft <sup>2</sup> |
| Region<br>13 | ESU 2A Very Loose to Loose<br>Sand/Gravel                           | 34,33,32,31,30,29,28,27,26,25,24,23,40,59,42,22,12,58,39 | 1,656.2<br>ft <sup>2</sup> |
| Region<br>14 | ESU 2A Very Loose to Loose<br>Sand/Gravel                           | 40,23,61,46,41   | 379.99<br>ft <sup>2</sup>  |
| Region<br>15 | Lightweight EPS   | 63,36,62   | 20.093<br>ft <sup>2</sup>  |
| Region<br>16 | Forward Compatible Wall   | 36,35,64,62  | 51.88<br>ft <sup>2</sup>   |
| Region<br>17 |   | 64,65,38   | 7.8889<br>ft <sup>2</sup>  |
| Region<br>18 | ESU 4B Dense to Very Dense<br>Sand/Gravel                           | 15,16,81,69,67   | 28.5 ft <sup>2</sup>       |
| Region<br>19 | SEW Wall  | 72,76,22,13  | 11.692<br>ft <sup>2</sup>  |
| Region<br>20 | SEW Wall  | 70,72,13   | 2.9375<br>ft <sup>2</sup>  |
| Region<br>21 | SEW Wall  | 70,79,78,75,72   | 19.415<br>ft <sup>2</sup>  |
| Region<br>22 | Gravel Borrow   | 81,75,78,79,69   | 11.991<br>ft <sup>2</sup>  |
| Region<br>23 | Gravel Borrow   | 49,75,81,80  | 7.7095<br>ft <sup>2</sup>  |

| Region<br>24 | SEW Wall                                  | 49,76,72,75             | 4.002<br>ft <sup>2</sup>   |
|--------------|---|-------------------------|----------------------------|
| Region<br>25 | SEW Wall                                  | 73,76,49                | 0.43333<br>ft <sup>2</sup> |
| Region<br>26 | SEW Wall                                  | 76,73,74,68,55,58,12,22 | 163.72<br>ft <sup>2</sup>  |
| Region<br>27 | ESU 2B Medium Dense Sand/Gravel           | 80,81,16,17             | 6 ft²                      |
| Region<br>28 | Gravel Borrow                             | 74,82,77                | 10.23<br>ft <sup>2</sup>   |
| Region<br>29 | Gravel Borrow                             | 77,71,74                | 10.23<br>ft <sup>2</sup>   |
| Region<br>30 | ESU 2A Very Loose to Loose<br>Sand/Gravel | 77,82,80,17,14          | 27.75<br>ft <sup>2</sup>   |
| Region<br>31 | Gravel Borrow                             | 73,49,80,82,74          | 54.19<br>ft <sup>2</sup>   |
| Region<br>32 | Common Borrow                             | 20,83,84                | 12.06<br>ft <sup>2</sup>   |
| Region<br>33 |   | 55,39,58                | 11.1 ft²                   |

# **Slip Results**

Slip Surfaces Analysed: 3242 of 16926 converged

# **Current Slip Surface**

Slip Surface: 1,021 Factor of Safety: 1.7 Volume: 1,418.7634 ft<sup>3</sup> Weight: 154,405.55 lbf

Resisting Moment: 8,919,144.1 lbf·ft Activating Moment: 5,346,275.2 lbf·ft

Resisting Force: 105,234.7 lbf Activating Force: 63,084.426 lbf Slip Rank: 1 of 16,926 slip surfaces Exit: (-38.240876, 182.19377) ft Entry: (46.166189, 223.23991) ft

Radius: 72.22526 ft

Center: (-20.046856, 252.08988) ft

## **Slip Slices**

|            | X                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material                                |
|------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|--|
| Slice<br>1 | -37.770438<br>ft | 182.07469<br>ft | -184.85613<br>psf | 32.647615<br>psf         | 20.400494<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>2 | -35.55 ft        | 181.57087<br>ft | -183.87843<br>psf | 158.60209<br>psf         | 99.105582<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose                |

|             |                  |                 |                   |                   |                   |       |       | Sand/Gravel                                  |
|-------------|------------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>3  | -32.05 ft        | 180.89112<br>ft | -181.90896<br>psf | 312.02985<br>psf  | 194.97789<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>4  | -28.908333<br>ft | 180.42402<br>ft | -179.6982<br>psf  | 487.91756<br>psf  | 304.88473<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>5  | -26.125 ft       | 180.13438<br>ft | -179.0209<br>psf  | 691.45366<br>psf  | 432.0682<br>psf   | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>6  | -23.341667<br>ft | 179.95326<br>ft | -180.28457<br>psf | 861.1649<br>psf   | 538.11555<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>7  | -20.558333<br>ft | 179.87984<br>ft | -178.0415<br>psf  | 1,001.5771<br>psf | 625.85485<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>8  | -17.775 ft       | 179.91379<br>ft | -180.73923<br>psf | 1,116.2529<br>psf | 697.51225<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>9  | -14.991667<br>ft | 180.05526<br>ft | -190.1224<br>psf  | 1,208.0335<br>psf | 754.86312<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>10 | -12.326997<br>ft | 180.28979<br>ft | -254.29877<br>psf | 1,307.044<br>psf  | 816.73175<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>11 | -9.780992<br>ft  | 180.60949<br>ft | -368.84527<br>psf | 1,413.6703<br>psf | 883.35927<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>12 | -7.2539947<br>ft | 181.01803<br>ft | -403.69014<br>psf | 1,501.3089<br>psf | 938.12194<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>13 | -5.5625 ft       | 181.33331<br>ft | -377.40593<br>psf | 1,520.8509<br>psf | 950.33311<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>14 | -3.84375 ft      | 181.71788<br>ft | -351.63392<br>psf | 1,444.7217<br>psf | 902.76229<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>15 | -1.28125 ft      | 182.35768<br>ft | -313.21625<br>psf | 1,329.5116<br>psf | 830.77108<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>16 | 0.6775 ft        | 182.90542<br>ft | -284.61599<br>psf | 3,318.5771<br>psf | 2,073.6771<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>17 | 3.3141258<br>ft  | 183.77835<br>ft | -248.89977<br>psf | 3,119.0069<br>psf | 1,948.9718<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>18 | 5.7064208<br>ft  | 184.61365<br>ft | -212.44256<br>psf | 3,013.5322<br>psf | 2,810.1642<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>19 | 6.569795 ft      | 184.94952<br>ft | -194.40709<br>psf | 2,947.8517<br>psf | 2,748.9162<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice       | 7.95 ft          | 185.5196        | -171.22478        | 4,104.4667        | 3,827.4771        | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense                |

| 20          |             | ft              | psf               | psf               | psf               |       |       | <br>  Sand/Gravel                            |
|-------------|-------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>21 | 8.95 ft     | 185.94105<br>ft | -152.7832<br>psf  | 4,008.0903<br>psf | 3,737.6047<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>22 | 11 ft       | 186.9157<br>ft  | -105.78401<br>psf | 4,010.2923<br>psf | 3,739.658<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>23 | 14 ft       | 188.40304<br>ft | -72.253284<br>psf | 3,698.7316<br>psf | 3,449.123<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>24 | 15.25 ft    | 189.07767<br>ft | -63.880304<br>psf | 2,480.6563<br>psf | 2,313.2495<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>25 | 16 ft       | 189.5057<br>ft  | -59.51264<br>psf  | 2,408.0477<br>psf | 2,245.5408<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>26 | 17.50351 ft | 190.40457<br>ft | -50.815986<br>psf | 2,262.1644<br>psf | 2,109.5025<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>27 | 19.25351 ft | 191.49963<br>ft | -42.857717<br>psf | 2,094.2702<br>psf | 1,952.9385<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>28 | 20.75 ft    | 192.49727<br>ft | -37.69367<br>psf  | 1,970.8238<br>psf | 1,539.7763<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>29 | 22.75 ft    | 193.93054<br>ft | -32.288402<br>psf | 1,679.1011<br>psf | 1,565.7871<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>30 | 24.25 ft    | 195.04449<br>ft | -28.88961<br>psf  | 1,630.2693<br>psf | 1,520.2508<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>31 | 25.2 ft     | 195.80131<br>ft | -27.371515<br>psf | 1,597.0866<br>psf | 1,489.3073<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>32 | 26.25 ft    | 196.6563<br>ft  | -26.087373<br>psf | 1,559.1239<br>psf | 1,453.9065<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>33 | 27.925 ft   | 198.1265<br>ft  | -25.620539<br>psf | 1,481.4122<br>psf | 1,381.4392<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>34 | 30.575 ft   | 200.60723<br>ft | -27.532663<br>psf | 1,347.6559<br>psf | 1,256.7095<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>35 | 33.4 ft     | 203.56213<br>ft | -35.750746<br>psf | 1,369.741<br>psf  | 1,277.3041<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>36 | 36.4 ft     | 207.096 ft      | -57.336715<br>psf | 1,053.7077<br>psf | 982.59829<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>37 | 39.05 ft    | 210.61649<br>ft | -100.14726<br>psf | 780.76011<br>psf  | 728.07058<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>38 | 41 ft       | 213.52142<br>ft | -170.16956<br>psf | 595.0236<br>psf   | 554.86849<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense                |

|             |                 |                 |                   |                  |                  |       |       | Sand/Gravel                                  |
|-------------|-----------------|-----------------|-------------------|------------------|------------------|-------|-------|--|
| Slice<br>39 | 42.19125 ft     | 215.45231<br>ft | -237.66118<br>psf | 489.20603<br>psf | 456.192<br>psf   | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>40 | 43.581761<br>ft | 217.98102<br>ft | -363.35006<br>psf | 342.19412<br>psf | 319.10118<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>41 | 45.373605<br>ft | 221.54251<br>ft | 0 psf             | 163.05805        | 127.39491<br>nsf | 0 psf | 0 psf | Gravel Borrow                                |

# 2B.2 Global - Static FC Wall (M-P)

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## **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 652 Date: 01/17/2022 Time: 02:07:09 PM

Tool Version: 11.1.1.22085

Last Solved Date: 01/17/2022 Last Solved Time: 02:24:47 PM

## **Project Settings**

Unit System: U.S. Customary Units

# **Analysis Settings**

#### 2B.2 Global - Static FC Wall (M-P)

Description: With Forward Compatible Wall

Kind: SLOPE/W

Parent: 2. Steady State (Global) Analysis Type: Morgenstern-Price

Settings

Side Function

Interslice force function option: Half-Sine

PWP Conditions from Parent Analysis: 2. Steady State (Global) [(last)]

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 20

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

Factor of Safety Convergence Settings

Maximum Number of Iterations: 100 Tolerable difference in F of S: 0.001

Tolerable difference in F of 5: 0.001

Solution Settings

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

#### **Materials**

## **ESU 2A Very Loose to Loose Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **ESU 2B Medium Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

## **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

## ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **SEW Wall**

Material Model: High Strength

Unit Weight: 130 pcf

## **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

#### **Forward Compatible Wall**

Material Model: High Strength

Unit Weight: 130 pcf

#### **Lightweight EPS**

Material Model: Mohr-Coulomb

Unit Weight: 5 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 0 °

Phi-B: 0°

# **Slip Surface Entry and Exit**

Left Type: Range

Left-Zone Left Coordinate: (-40, 181.99516) ft Left-Zone Right Coordinate: (0, 196.3) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15, 223) ft

Right-Zone Right Coordinate: (70, 223.39933) ft

Right-Zone Increment: 30
Radius Increments: 20

# **Slip Surface Limits**

Left Coordinate: (-100, 170.1) ft Right Coordinate: (100, 223.6) ft

# **Surcharge Loads**

## Surcharge Load 1

Surcharge (Unit Weight): 250 pcf

Direction: Vertical

#### **Coordinates**

| X       | Y        |
|---------|----------|
| 9 ft    | 224 ft   |
| 37.9 ft | 224.2 ft |
| 40.2 ft | 224.2 ft |
| 100 ft  | 224.6 ft |

# **Geometry**

Name: Default Geometry

# Settings

View: 2D

Element Thickness: 1 ft

#### **Points**

|          | Х           | Υ           |
|----------|-------------|-------------|
| Point 1  | 100 ft      | 160 ft      |
| Point 2  | 100 ft      | 185.5 ft    |
| Point 3  | 0.9 ft      | 160 ft      |
| Point 4  | 100 ft      | 211.1475 ft |
| Point 5  | 3.8 ft      | 183 ft      |
| Point 6  | -20.1275 ft | 160 ft      |
| Point 7  | 100 ft      | 219.64 ft   |
| Point 8  | 42.5825 ft  | 219.8525 ft |
| Point 9  | 40.2 ft     | 223.2 ft    |
| Point 10 | 100 ft      | 223.6 ft    |
| Point 11 | 0 ft        | 211.7 ft    |
| Point 12 | 0 ft        | 192 ft      |
| Point 13 | 13 ft       | 192 ft      |
| Point 14 | 24.5 ft     | 213.8 ft    |
| Point 15 | 24.5 ft     | 192 ft      |
| Point 16 | 24.5 ft     | 203 ft      |
| Point 17 | 24.5 ft     | 205 ft      |
| Point 18 | 41.8 ft     | 220.7 ft    |
| Point 19 | 26.6 ft     | 215.4 ft    |
| Point 20 | 37.9 ft     | 223.2 ft    |
| Point 21 | 6.13959 ft  | 185.3 ft    |
| Point 22 | 8.9 ft      | 192 ft      |
| Point 23 | -100 ft     | 160 ft      |
| Point 24 | -100 ft     | 170.1 ft    |
| Point 25 | -91.8 ft    | 174.4 ft    |
| Point 26 | -88.3 ft    | 176.5 ft    |
| Point 27 | -85.7 ft    | 177.8 ft    |
| Point 28 | -83.4 ft    | 178.4 ft    |
| Point 29 | -76 ft      | 178.9 ft    |
| Point 30 | -74 ft      | 179.7 ft    |
| Point 31 | -55.9 ft    | 180.2 ft    |
| Point 32 | -37.3 ft    | 182.3 ft    |
|          |             |             |

|          | l           |              |
|----------|-------------|--------------|
| Point 33 | -30.3 ft    | 182.9 ft     |
| Point 34 | -13.6 ft    | 190.2 ft     |
| Point 35 | 7 ft        | 223 ft       |
| Point 36 | 15 ft       | 223 ft       |
| Point 37 | 15 ft       | 211.7 ft     |
| Point 38 | 7 ft        | 211.7 ft     |
| Point 39 | -6 ft       | 195 ft       |
| Point 40 | -37.3275 ft | 162.2725 ft  |
| Point 41 | -47.26 ft   | 160 ft       |
| Point 42 | -5.125 ft   | 182.98095 ft |
| Point 43 | 80.7025 ft  | 160 ft       |
| Point 44 | -100 ft     | 129.8675 ft  |
| Point 45 | 100 ft      | 129.8675 ft  |
| Point 46 | -100 ft     | 147.8625 ft  |
| Point 47 | -27.95 ft   | 152.3875 ft  |
| Point 48 | -100 ft     | 133.97 ft    |
| Point 49 | 16.5 ft     | 197.3 ft     |
| Point 50 | 100 ft      | 209.9025 ft  |
| Point 51 | 95.42762 ft | 209.80965 ft |
| Point 52 | 3.915 ft    | 160.77581 ft |
| Point 53 | 17.7925 ft  | 187.09412 ft |
| Point 54 | 28.7 ft     | 129.8675 ft  |
| Point 55 | 0 ft        | 198.7 ft     |
| Point 56 | 47.15 ft    | 195.68393 ft |
| Point 57 | 42.67 ft    | 194.37311 ft |
| Point 58 | 0 ft        | 195 ft       |
| Point 59 | -32.3 ft    | 165.4 ft     |
| Point 60 | -16 ft      | 164.1 ft     |
| Point 61 | -100 ft     | 150.0525 ft  |
| Point 62 | 15 ft       | 218.535 ft   |
| Point 63 | 24 ft       | 223 ft       |
| Point 64 | 7 ft        | 214.495 ft   |
| Point 65 | 1.355 ft    | 211.7 ft     |
| Point 66 | 25.9 ft     | 223 ft       |
| Point 67 | 22 ft       | 192 ft       |
| Point 68 | 15.0117 ft  | 208.01106 ft |
| Point 69 | 21.5 ft     | 192 ft       |
| Point 70 | 15.5 ft     | 192 ft       |
| Point 70 | 15.5 ft     | 211.7 ft     |
| Point 72 | 15.5 ft     | 194.35 ft    |
| Point 73 | 15.5 ft     | 194.55 ft    |
| Point 73 | 15.5 ft     | 208.29 ft    |
|          | 18.50702 ft | 197.3 ft     |
| Point 75 |             |              |
| Point 76 | 15.5 ft     | 196.43333 ft |
| Point 77 | 21.5 ft     | 211.7 ft     |
| Point 78 | 20 ft       | 197.3 ft     |
| Point 79 | 20 ft       | 192 ft       |
| Point 80 | 21.5 ft     | 202 ft       |
|          |             |              |

| Point 81 | 21.5 ft | 200 ft    |
|----------|---------|-----------|
| Point 82 | 21.5 ft | 208.29 ft |
| Point 83 | 31.9 ft | 223.1 ft  |
| Point 84 | 31.9 ft | 219.08 ft |

# Regions

|              | Material  | Points   | Area                       |
|--------------|---|--|----------------------------|
| Region<br>1  | ESU 4B Dense to Very Dense<br>Sand/Gravel                           | 1,2,52,3,43  | 1,263.5<br>ft <sup>2</sup> |
| Region 2     | ESU 5B Very Stiff to Hard Silt and<br>Clay/Dense to Very Dense Silt | 52,2,50,51,56,57,53,5,60,6,47,3                          | 2,656.9<br>ft <sup>2</sup> |
| Region<br>3  | Gravel Borrow   | 9,18,8,7,10  | 214.55<br>ft <sup>2</sup>  |
| Region<br>4  | SEW Wall  | 38,65,11,55,68,74,71,37                                  | 127 ft²                    |
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel                                     | 8,16,17,18   | 31.556<br>ft <sup>2</sup>  |
| Region<br>6  | ESU 2A Very Loose to Loose<br>Sand/Gravel                           | 18,17,14,19,84,20,9                                      | 115.05<br>ft <sup>2</sup>  |
| Region<br>7  | Forward Compatible Wall   | 38,37,62,64  | 38.52<br>ft <sup>2</sup>   |
| Region<br>8  | Lightweight EPS   | 14,19,84,83,66,63,62,37,71,77                            | 132.58<br>ft <sup>2</sup>  |
| Region<br>9  | ESU 2B Medium Dense Sand/Gravel                                     | 22,42,59,40,60,5,21,13                                   | 332.37<br>ft <sup>2</sup>  |
| Region<br>10 | ESU 4B Dense to Very Dense<br>Sand/Gravel                           | 44,54,45,1,43,3,47,48                                    | 4,704.7<br>ft <sup>2</sup> |
| Region<br>11 | ESU 2B Medium Dense Sand/Gravel                                     | 41,46,48,47,6,60,40                                      | 992.46<br>ft <sup>2</sup>  |
| Region<br>12 | ESU 4B Dense to Very Dense<br>Sand/Gravel                           | 56,51,50,4,7,8,16,15,67,69,79,70,13,21,5,53,57           | 1,417.8<br>ft <sup>2</sup> |
| Region<br>13 | ESU 2A Very Loose to Loose<br>Sand/Gravel                           | 34,33,32,31,30,29,28,27,26,25,24,23,40,59,42,22,12,58,39 | 1,656.2<br>ft <sup>2</sup> |
| Region<br>14 | ESU 2A Very Loose to Loose<br>Sand/Gravel                           | 40,23,61,46,41   | 379.99<br>ft <sup>2</sup>  |
| Region<br>15 | Lightweight EPS   | 63,36,62   | 20.093<br>ft <sup>2</sup>  |
| Region<br>16 | Forward Compatible Wall   | 36,35,64,62  | 51.88<br>ft²               |
| Region<br>17 |   | 64,65,38   | 7.8889<br>ft <sup>2</sup>  |
| Region<br>18 | ESU 4B Dense to Very Dense<br>Sand/Gravel                           | 15,16,81,69,67   | 28.5 ft <sup>2</sup>       |
| Region<br>19 | SEW Wall  | 72,76,22,13  | 11.692<br>ft <sup>2</sup>  |
| Region<br>20 | SEW Wall  | 70,72,13   | 2.9375<br>ft <sup>2</sup>  |
| Region<br>21 | SEW Wall  | 70,79,78,75,72   | 19.415<br>ft <sup>2</sup>  |
| Region<br>22 | Gravel Borrow   | 81,75,78,79,69   | 11.991<br>ft <sup>2</sup>  |
| Region       |   |  | 7.7095                     |

| 23           | Gravel Borrow                             | 49,75,81,80             | ft²                        |
|--------------|---|-------------------------|----------------------------|
| Region<br>24 | SEW Wall                                  | 49,76,72,75             | 4.002<br>ft <sup>2</sup>   |
| Region<br>25 | SEW Wall                                  | 73,76,49                | 0.43333<br>ft <sup>2</sup> |
| Region<br>26 | SEW Wall                                  | 76,73,74,68,55,58,12,22 | 163.72<br>ft²              |
| Region<br>27 | ESU 2B Medium Dense Sand/Gravel           | 80,81,16,17             | 6 ft²                      |
| Region<br>28 | Gravel Borrow                             | 74,82,77                | 10.23<br>ft <sup>2</sup>   |
| Region<br>29 | Gravel Borrow                             | 77,71,74                | 10.23<br>ft <sup>2</sup>   |
| Region<br>30 | ESU 2A Very Loose to Loose<br>Sand/Gravel | 77,82,80,17,14          | 27.75<br>ft <sup>2</sup>   |
| Region<br>31 | Gravel Borrow                             | 73,49,80,82,74          | 54.19<br>ft <sup>2</sup>   |
| Region<br>32 | Common Borrow                             | 20,83,84                | 12.06<br>ft <sup>2</sup>   |
| Region<br>33 |   | 55,39,58                | 11.1 ft²                   |

# **Slip Results**

Slip Surfaces Analysed: 3668 of 16926 converged

# **Current Slip Surface**

Slip Surface: 1,021 Factor of Safety: 1.7 Volume: 1,418.7634 ft<sup>3</sup> Weight: 154,405.55 lbf

Resisting Moment: 8,893,411.3 lbf·ft Activating Moment: 5,346,275.2 lbf·ft

Resisting Force: 104,794.33 lbf Activating Force: 63,006.121 lbf Slip Rank: 1 of 16,926 slip surfaces Exit: (-38.240876, 182.19377) ft Entry: (46.166189, 223.23991) ft

Radius: 72.22526 ft

Center: (-20.046856, 252.08988) ft

## **Slip Slices**

|            | X                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material                                |
|------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|--|
| Slice<br>1 | -37.770438<br>ft | 182.07469<br>ft | -184.85613<br>psf | 21.278947<br>psf         | 13.296562<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
|            |                  |                 |                   |                          |                        |                      |                     |  |

| Slice<br>2  | -35.55 ft        | 181.57087<br>ft | -183.87843<br>psf | 113.91874<br>psf  | 71.184327<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
|-------------|------------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>3  | -32.05 ft        | 180.89112<br>ft | -181.90896<br>psf | 253.64302<br>psf  | 158.49375<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>4  | -28.908333<br>ft | 180.42402<br>ft | -179.6982<br>psf  | 433.13249<br>psf  | 270.65122<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>5  | -26.125 ft       | 180.13438<br>ft | -179.0209<br>psf  | 653.07406<br>psf  | 408.08597<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>6  | -23.341667<br>ft | 179.95326<br>ft | -180.28457<br>psf | 858.10305<br>psf  | 536.20229<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>7  | -20.558333<br>ft | 179.87984<br>ft | -178.0415<br>psf  | 1,040.7677<br>psf | 650.34386<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>8  | -17.775 ft       | 179.91379<br>ft | -180.73923<br>psf | 1,195.027<br>psf  | 746.73575<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>9  | -14.991667<br>ft | 180.05526<br>ft | -190.1224<br>psf  | 1,316.9287<br>psf | 822.90837<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>10 | -12.326997<br>ft | 180.28979<br>ft | -254.29877<br>psf | 1,432.8859<br>psf | 895.36647<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>11 | -9.780992<br>ft  | 180.60949<br>ft | -368.84527<br>psf | 1,544.3928<br>psf | 965.04376<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>12 | -7.2539947<br>ft | 181.01803<br>ft | -403.69014<br>psf | 1,625.7153<br>psf | 1,015.8597<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>13 | -5.5625 ft       | 181.33331<br>ft | -377.40593<br>psf | 1,634.9553<br>psf | 1,021.6335<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>14 | -3.84375 ft      | 181.71788<br>ft | -351.63392<br>psf | 1,541.8019<br>psf | 963.42476<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>15 | -1.28125 ft      | 182.35768<br>ft | -313.21625<br>psf | 1,397.1193<br>psf | 873.01701<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>16 | 0.6775 ft        | 182.90542<br>ft | -284.61599<br>psf | 3,384.6638<br>psf | 2,114.9727<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>17 | 3.3141258<br>ft  | 183.77835<br>ft | -248.89977<br>psf | 3,139.6029<br>psf | 1,961.8416<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>18 | 5.7064208<br>ft  | 184.61365<br>ft | -212.44256<br>psf | 3,071.487<br>psf  | 2,864.208<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>19 | 6.569795 ft      | 184.94952<br>ft | -194.40709<br>psf | 2,987.2701<br>psf | 2,785.6745<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |

| Slice<br>20 | 7.95 ft     | 185.5196<br>ft  | -171.22478<br>psf | 4,136.6538<br>psf | 3,857.4921<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
|-------------|-------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>21 | 8.95 ft     | 185.94105<br>ft | -152.7832<br>psf  | 4,015.1596<br>psf | 3,744.1969<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>22 | 11 ft       | 186.9157<br>ft  | -105.78401<br>psf | 3,971.5313<br>psf | 3,703.5128<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>23 | 14 ft       | 188.40304<br>ft | -72.253284<br>psf | 3,601.834<br>psf  | 3,358.7645<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>24 | 15.25 ft    | 189.07767<br>ft | -63.880304<br>psf | 2,365.6407<br>psf | 2,205.9956<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>25 | 16 ft       | 189.5057<br>ft  | -59.51264<br>psf  | 2,285.2301<br>psf | 2,131.0116<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>26 | 17.50351 ft | 190.40457<br>ft | -50.815986<br>psf | 2,127.174<br>psf  | 1,983.6218<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>27 | 19.25351 ft | 191.49963<br>ft | -42.857717<br>psf | 1,950.3184<br>psf | 1,818.7013<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>28 | 20.75 ft    | 192.49727<br>ft | -37.69367<br>psf  | 1,820.6147<br>psf | 1,422.4201<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>29 | 22.75 ft    | 193.93054<br>ft | -32.288402<br>psf | 1,536.6102<br>psf | 1,432.9122<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>30 | 24.25 ft    | 195.04449<br>ft | -28.88961<br>psf  | 1,492.612<br>psf  | 1,391.8832<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>31 | 25.2 ft     | 195.80131<br>ft | -27.371515<br>psf | 1,464.9356<br>psf | 1,366.0745<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>32 | 26.25 ft    | 196.6563<br>ft  | -26.087373<br>psf | 1,434.5725<br>psf | 1,337.7605<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>33 | 27.925 ft   | 198.1265<br>ft  | -25.620539<br>psf | 1,373.2823<br>psf | 1,280.6065<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>34 | 30.575 ft   | 200.60723<br>ft | -27.532663<br>psf | 1,272.7873<br>psf | 1,186.8934<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>35 | 33.4 ft     | 203.56213<br>ft | -35.750746<br>psf | 1,352.7872<br>psf | 1,261.4945<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>36 | 36.4 ft     | 207.096 ft      | -57.336715<br>psf | 1,086.0017<br>psf | 1,012.7129<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>37 | 39.05 ft    | 210.61649<br>ft | -100.14726<br>psf | 847.394<br>psf    | 790.20769<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
|             |             |                 |                   |                   |                   |       |       | ESU 4B Dense to                              |

| Slice<br>38 | 41 ft           | 213.52142<br>ft | -170.16956<br>psf | 678.63253<br>psf | 632.83507<br>psf | 0 psf | 0 psf | Very Dense<br>Sand/Gravel                    |
|-------------|-----------------|-----------------|-------------------|------------------|------------------|-------|-------|--|
| Slice<br>39 | 42.19125 ft     | 215.45231<br>ft | -237.66118<br>psf | 578.69343<br>psf | 539.64035<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>40 | 43.581761<br>ft | 217.98102<br>ft | -363.35006<br>psf | 423.9667<br>psf  | 395.35535<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice       | 45.373605<br>ft | 221.54251<br>ft | 0 psf             | 226.88037        | 177.25837        | 0 psf | 0 psf | Gravel Borrow                                |

# 2B.3 Global - Pseudo-Static FC Wall (Spencer)

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## **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 652 Date: 01/17/2022 Time: 02:07:09 PM

Tool Version: 11.1.1.22085

Last Solved Date: 01/17/2022 Last Solved Time: 02:32:27 PM

## **Project Settings**

Unit System: U.S. Customary Units

# **Analysis Settings**

#### 2B.3 Global - Pseudo-Static FC Wall (Spencer)

Description: With Forward Compatible Wall

Kind: SLOPE/W

Parent: 2. Steady State (Global)

Analysis Type: Spencer

Settings

PWP Conditions from Parent Analysis: 2. Steady State (Global) [(last)]

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 20

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

Factor of Safety Convergence Settings

Maximum Number of Iterations: 100

Tolerable difference in F of S: 0.001

Solution Settings

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3 Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

#### **Materials**

## **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

## ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **SEW Wall**

Material Model: High Strength

Unit Weight: 130 pcf

## **ESU 2A Very Loose to Loose Sand/Gravel (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 100 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

## **ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 200 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### Forward Compatible Wall

Material Model: High Strength

Unit Weight: 130 pcf

#### **Lightweight EPS**

Material Model: Mohr-Coulomb

Unit Weight: 5 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 0 °

Phi-B: 0°

# **Slip Surface Entry and Exit**

Left Type: Range

Left-Zone Left Coordinate: (-40, 181.99516) ft Left-Zone Right Coordinate: (0, 196.3) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15, 223) ft

Right-Zone Right Coordinate: (70, 223.39933) ft

Right-Zone Increment: 30 Radius Increments: 20

## **Slip Surface Limits**

Left Coordinate: (-100, 170.1) ft Right Coordinate: (100, 223.6) ft

## **Seismic Coefficients**

Horz Seismic Coef.: 0.191

# **Surcharge Loads**

## **Surcharge Load 1**

Surcharge (Unit Weight): 125 pcf

Direction: Vertical

#### Coordinates

| X       | Υ        |
|---------|----------|
| 9 ft    | 224 ft   |
| 26 ft   | 224 ft   |
| 39.4 ft | 224.2 ft |
| 40.2 ft | 224.2 ft |
| 100 ft  | 224.6 ft |

# **Geometry**

Name: Default Geometry

# **Settings**

View: 2D

Element Thickness: 1 ft

#### **Points**

|          | X           | Y           |
|----------|-------------|-------------|
| Point 1  | 100 ft      | 160 ft      |
| Point 2  | 100 ft      | 185.5 ft    |
| Point 3  | 0.9 ft      | 160 ft      |
| Point 4  | 100 ft      | 211.1475 ft |
| Point 5  | 3.8 ft      | 183 ft      |
| Point 6  | -20.1275 ft | 160 ft      |
| Point 7  | 100 ft      | 219.64 ft   |
| Point 8  | 42.5825 ft  | 219.8525 ft |
| Point 9  | 40.2 ft     | 223.2 ft    |
| Point 10 | 100 ft      | 223.6 ft    |
| Point 11 | 0 ft        | 211.7 ft    |
| Point 12 | 0 ft        | 192 ft      |
| Point 13 | 13 ft       | 192 ft      |
| Point 14 | 24.5 ft     | 213.8 ft    |
| Point 15 | 24.5 ft     | 192 ft      |
| Point 16 | 24.5 ft     | 203 ft      |
| Point 17 | 24.5 ft     | 205 ft      |
| Point 18 | 41.8 ft     | 220.7 ft    |
| Point 19 | 26.6 ft     | 215.4 ft    |
| Point 20 | 37.9 ft     | 223.2 ft    |
| Point 21 | 6.13959 ft  | 185.3 ft    |
| Point 22 | 8.9 ft      | 192 ft      |
| Point 23 | -100 ft     | 160 ft      |
| Point 24 | -100 ft     | 170.1 ft    |
| Point 25 | -91.8 ft    | 174.4 ft    |
| Point 26 | -88.3 ft    | 176.5 ft    |
| Point 27 | -85.7 ft    | 177.8 ft    |
| Point 28 | -83.4 ft    | 178.4 ft    |

| l p-:-+ 20 | 76.4        | 17006        |
|------------|-------------|--------------|
| Point 29   | -76 ft      | 178.9 ft     |
| Point 30   | -74 ft      | 179.7 ft     |
| Point 31   | -55.9 ft    | 180.2 ft     |
| Point 32   | -37.3 ft    | 182.3 ft     |
| Point 33   | -30.3 ft    | 182.9 ft     |
| Point 34   | -13.6 ft    | 190.2 ft     |
| Point 35   | 7 ft        | 223 ft       |
| Point 36   | 15 ft       | 223 ft       |
| Point 37   | 15 ft       | 211.7 ft     |
| Point 38   | 7 ft        | 211.7 ft     |
| Point 39   | -6 ft       | 195 ft       |
| Point 40   | -37.3275 ft | 162.2725 ft  |
| Point 41   | -47.26 ft   | 160 ft       |
| Point 42   | -5.125 ft   | 182.98095 ft |
| Point 43   | 80.7025 ft  | 160 ft       |
| Point 44   | -100 ft     | 129.8675 ft  |
| Point 45   | 100 ft      | 129.8675 ft  |
| Point 46   | -100 ft     | 147.8625 ft  |
| Point 47   | -27.95 ft   | 152.3875 ft  |
| Point 48   | -100 ft     | 133.97 ft    |
| Point 49   | 16.5 ft     | 197.3 ft     |
| Point 50   | 100 ft      | 209.9025 ft  |
| Point 51   | 95.42762 ft | 209.80965 ft |
| Point 52   | 3.915 ft    | 160.77581 ft |
| Point 53   | 17.7925 ft  | 187.09412 ft |
| Point 54   | 28.7 ft     | 129.8675 ft  |
| Point 55   | 0 ft        | 198.7 ft     |
| Point 56   | 47.15 ft    | 195.68393 ft |
| Point 57   | 42.67 ft    | 194.37311 ft |
| Point 58   | 0 ft        | 195 ft       |
| Point 59   | -32.3 ft    | 165.4 ft     |
| Point 60   | -16 ft      | 164.1 ft     |
| Point 61   | -100 ft     | 150.0525 ft  |
| Point 62   | 15 ft       | 218.535 ft   |
| Point 63   | 24 ft       | 223 ft       |
| Point 64   | 7 ft        | 214.495 ft   |
| Point 65   | 1.355 ft    | 211.7 ft     |
| Point 66   | 25.9 ft     | 223 ft       |
| Point 67   | 22 ft       | 192 ft       |
| Point 68   | 15.0117 ft  | 208.01106 ft |
| Point 69   | 21.5 ft     | 192 ft       |
| Point 70   | 15.5 ft     | 192 ft       |
| Point 71   | 15.5 ft     | 211.7 ft     |
| Point 72   | 15.5 ft     | 194.35 ft    |
| Point 73   | 15.5 ft     | 197.3 ft     |
| Point 74   | 15.5 ft     | 208.29 ft    |
| Point 75   | 18.50702 ft | 197.3 ft     |
| Point 76   | 15.5 ft     | 196.43333 ft |
| 1 01110 70 | 15.5 10     | 150.755511   |
|            |             |              |

| Point 77 | 21.5 ft | 211.7 ft  |
|----------|---------|-----------|
| Point 78 | 20 ft   | 197.3 ft  |
| Point 79 | 20 ft   | 192 ft    |
| Point 80 | 21.5 ft | 202 ft    |
| Point 81 | 21.5 ft | 200 ft    |
| Point 82 | 21.5 ft | 208.29 ft |
| Point 83 | 31.9 ft | 223.1 ft  |
| Point 84 | 31.9 ft | 219.08 ft |

# Regions

|              | Material   | Points   | Area                       |
|--------------|--|--|----------------------------|
| Region<br>1  | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 1,2,52,3,43  | 1,263.5<br>ft <sup>2</sup> |
| Region<br>2  | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 52,2,50,51,56,57,53,5,60,6,47,3                          | 2,656.9<br>ft <sup>2</sup> |
| Region<br>3  | Gravel Borrow  | 9,18,8,7,10  | 214.55<br>ft <sup>2</sup>  |
| Region<br>4  | SEW Wall   | 38,65,11,55,68,74,71,37                                  | 127 ft <sup>2</sup>        |
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)              | 8,16,17,18   | 31.556<br>ft <sup>2</sup>  |
| Region<br>6  | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion)    | 18,17,14,19,84,20,9                                      | 115.05<br>ft²              |
| Region<br>7  | Forward Compatible Wall  | 38,37,62,64  | 38.52<br>ft <sup>2</sup>   |
| Region<br>8  | Lightweight EPS  | 14,19,84,83,66,63,62,37,71,77                            | 132.58<br>ft²              |
| Region<br>9  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)              | 22,42,59,40,60,5,21,13                                   | 332.37<br>ft <sup>2</sup>  |
| Region<br>10 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 44,54,45,1,43,3,47,48                                    | 4,704.7<br>ft <sup>2</sup> |
| Region<br>11 | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)              | 41,46,48,47,6,60,40                                      | 992.46<br>ft²              |
| Region<br>12 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 56,51,50,4,7,8,16,15,67,69,79,70,13,21,5,53,57           | 1,417.8<br>ft²             |
| Region<br>13 | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion)    | 34,33,32,31,30,29,28,27,26,25,24,23,40,59,42,22,12,58,39 | 1,656.2<br>ft <sup>2</sup> |
| Region<br>14 | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion)    | 40,23,61,46,41   | 379.99<br>ft²              |
| Region<br>15 | Lightweight EPS  | 63,36,62   | 20.093<br>ft <sup>2</sup>  |
| Region<br>16 | Forward Compatible Wall  | 36,35,64,62  | 51.88<br>ft²               |
| Region<br>17 |  | 64,65,38   | 7.8889<br>ft <sup>2</sup>  |
| Region<br>18 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 15,16,81,69,67   | 28.5 ft <sup>2</sup>       |
| Region<br>19 | SEW Wall   | 72,76,22,13  | 11.692<br>ft²              |
| Region<br>20 | SEW Wall   | 70,72,13   | 2.9375<br>ft <sup>2</sup>  |

| Region<br>21 | SEW Wall  | 70,79,78,75,72          | 19.415<br>ft <sup>2</sup>  |
|--------------|---|-------------------------|----------------------------|
| Region<br>22 | Gravel Borrow   | 81,75,78,79,69          | 11.991<br>ft²              |
| Region<br>23 | Gravel Borrow   | 49,75,81,80             | 7.7095<br>ft <sup>2</sup>  |
| Region<br>24 | SEW Wall  | 49,76,72,75             | 4.002<br>ft <sup>2</sup>   |
| Region<br>25 | SEW Wall  | 73,76,49                | 0.43333<br>ft <sup>2</sup> |
| Region<br>26 | SEW Wall  | 76,73,74,68,55,58,12,22 | 163.72<br>ft <sup>2</sup>  |
| Region<br>27 | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)           | 80,81,16,17             | 6 ft <sup>2</sup>          |
| Region<br>28 | Gravel Borrow   | 74,82,77                | 10.23<br>ft <sup>2</sup>   |
| Region<br>29 | Gravel Borrow   | 77,71,74                | 10.23<br>ft <sup>2</sup>   |
| Region<br>30 | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion) | 77,82,80,17,14          | 27.75<br>ft <sup>2</sup>   |
| Region<br>31 | Gravel Borrow   | 73,49,80,82,74          | 54.19<br>ft <sup>2</sup>   |
| Region<br>32 | Common Borrow   | 20,83,84                | 12.06<br>ft <sup>2</sup>   |
| Region<br>33 |   | 55,39,58                | 11.1 ft²                   |
|              |   | ·                       |                            |

# **Slip Results**

Slip Surfaces Analysed: 2154 of 16926 converged

# **Current Slip Surface**

Slip Surface: 1,021 Factor of Safety: 1.3 Volume: 1,418.8147 ft<sup>3</sup> Weight: 154,412.22 lbf

Resisting Moment: 8,436,684.9 lbf·ft Activating Moment: 6,572,450.7 lbf·ft

Resisting Force: 102,643.9 lbf Activating Force: 79,937.615 lbf Slip Rank: 1 of 16,926 slip surfaces Exit: (-38.240876, 182.19377) ft Entry: (46.166189, 223.23991) ft

Radius: 72.22526 ft

Center: (-20.046856, 252.08988) ft

## **Slip Slices**

|  | X | Y | PWP | Base<br>Normal | Frictional | Cohesive | Suction | Base Material |  |
|--|---|---|-----|----------------|------------|----------|---------|---------------|--|
|--|---|---|-----|----------------|------------|----------|---------|---------------|--|

|             |                  |                 |                   | Stress            | Strength         | Strength | Strength |  |
|-------------|------------------|-----------------|-------------------|-------------------|------------------|----------|----------|--|
| Slice<br>1  | -37.770438<br>ft | 182.07469<br>ft | -184.85613<br>psf | 368.2252<br>psf   | 230.09264<br>psf | 100 psf  | 0 psf    | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>2  | -35.55 ft        | 181.57087<br>ft | -183.87843<br>psf | 527.83809<br>psf  | 329.82984<br>psf | 100 psf  | 0 psf    | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>3  | -32.05 ft        | 180.89112<br>ft | -181.90896<br>psf | 673.93747<br>psf  | 421.12287<br>psf | 100 psf  | 0 psf    | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>4  | -28.908333<br>ft | 180.42402<br>ft | -179.6982<br>psf  | 841.24531<br>psf  | 525.66841<br>psf | 100 psf  | 0 psf    | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>5  | -26.125 ft       | 180.13438<br>ft | -179.0209<br>psf  | 1,036.5562<br>psf | 647.71221<br>psf | 100 psf  | 0 psf    | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>6  | -23.341667<br>ft | 179.95326<br>ft | -180.28457<br>psf | 1,175.074<br>psf  | 734.26774<br>psf | 100 psf  | 0 psf    | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>7  | -20.558333<br>ft | 179.87984<br>ft | -178.0415<br>psf  | 1,271.8969<br>psf | 794.76937<br>psf | 100 psf  | 0 psf    | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>8  | -17.775 ft       | 179.91379<br>ft | -180.73923<br>psf | 1,337.0153<br>psf | 835.45987<br>psf | 100 psf  | 0 psf    | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>9  | -14.991667<br>ft | 180.05526<br>ft | -190.1224<br>psf  | 1,377.2287<br>psf | 860.58801<br>psf | 100 psf  | 0 psf    | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>10 | -12.326997<br>ft | 180.28979<br>ft | -254.29877<br>psf | 1,428.2837<br>psf | 892.49071<br>psf | 100 psf  | 0 psf    | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>11 | -9.780992<br>ft  | 180.60949<br>ft | -368.84527<br>psf | 1,489.1459<br>psf | 930.52164<br>psf | 100 psf  | 0 psf    | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel                           |

|             |                  |                 |                   |                   |                   |         |       | (Apparent<br>Cohesion)                              |
|-------------|------------------|-----------------|-------------------|-------------------|-------------------|---------|-------|---|
| Slice<br>12 | -7.2539947<br>ft | 181.01803<br>ft | -403.69014<br>psf | 1,593.2967<br>psf | 995.60225<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion) |
| Slice<br>13 | -5.5625 ft       | 181.33331<br>ft | -377.40593<br>psf | 1,579.1228<br>psf | 986.74544<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion) |
| Slice<br>14 | -3.84375 ft      | 181.71788<br>ft | -351.63392<br>psf | 1,475.1626<br>psf | 921.78389<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion) |
| Slice<br>15 | -1.28125 ft      | 182.35768<br>ft | -313.21625<br>psf | 1,325.9764<br>psf | 828.562<br>psf    | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion) |
| Slice<br>16 | 0.6775 ft        | 182.90542<br>ft | -284.61599<br>psf | 3,110.6219<br>psf | 1,943.7323<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion) |
| Slice<br>17 | 3.3141258<br>ft  | 183.77835<br>ft | -248.89977<br>psf | 2,859.1394<br>psf | 1,786.5886<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion) |
| Slice<br>18 | 5.7064208<br>ft  | 184.61365<br>ft | -212.44256<br>psf | 2,873.9393<br>psf | 2,679.9918<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel        |
| Slice<br>19 | 6.569795 ft      | 184.94952<br>ft | -194.40709<br>psf | 2,785.7289<br>psf | 2,597.7342<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel        |
| Slice<br>20 | 7.95 ft          | 185.5196<br>ft  | -171.22478<br>psf | 3,823.9648<br>psf | 3,565.9049<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel        |
| Slice<br>21 | 8.95 ft          | 185.94105<br>ft | -152.7832<br>psf  | 3,697.1477<br>psf | 3,447.646<br>psf  | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel        |
| Slice<br>22 | 11 ft            | 186.9157<br>ft  | -105.78401<br>psf | 3,548.9342<br>psf | 3,309.4347<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel        |
| Slice<br>23 | 14 ft            | 188.40304<br>ft | -72.253284<br>psf | 3,179.0081<br>psf | 2,964.473<br>psf  | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel        |
| Slice<br>24 | 15.25 ft         | 189.07767<br>ft | -63.880304<br>psf | 2,084.4722<br>psf | 1,943.8018<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel        |
| Slice       |                  | 189.5057        | -59.51264         | 2,008.2702        | 1,872.7422        |         |       | ESU 4B Dense to                                     |

| 25          | 16 ft           | ft              | psf               | psf               | psf               | 0 psf | 0 psf | Very Dense<br>Sand/Gravel                    |
|-------------|-----------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>26 | 17.50351 ft     | 190.40457<br>ft | -50.815986<br>psf | 1,858.3737<br>psf | 1,732.9615<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>27 | 19.25351 ft     | 191.49963<br>ft | -42.857717<br>psf | 1,690.6431<br>psf | 1,576.5502<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>28 | 20.75 ft        | 192.49727<br>ft | -37.69367<br>psf  | 1,531.4311<br>psf | 1,196.4851<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>29 | 22.75 ft        | 193.93054<br>ft | -32.288402<br>psf | 1,304.9752<br>psf | 1,216.9091<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>30 | 24.25 ft        | 195.04449<br>ft | -28.88961<br>psf  | 1,250.7663<br>psf | 1,166.3585<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>31 | 25.2 ft         | 195.80131<br>ft | -27.371515<br>psf | 1,215.2304<br>psf | 1,133.2207<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>32 | 25.95 ft        | 196.40529<br>ft | -26.439209<br>psf | 1,187.7917<br>psf | 1,107.6337<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>33 | 26.3 ft         | 196.6976<br>ft  | -26.013331<br>psf | 1,174.2929<br>psf | 1,095.0458<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>34 | 27.925 ft       | 198.1265<br>ft  | -25.620539<br>psf | 1,103.736<br>psf  | 1,029.2505<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>35 | 30.575 ft       | 200.60723<br>ft | -27.532663<br>psf | 984.229<br>psf    | 917.80839<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>36 | 33.4 ft         | 203.56213<br>ft | -35.750746<br>psf | 985.14407<br>psf  | 918.66171<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>37 | 36.4 ft         | 207.096 ft      | -57.336715<br>psf | 735.49241<br>psf  | 685.85777<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>38 | 38.65 ft        | 210.02434<br>ft | -90.418054<br>psf | 560.18954<br>psf  | 522.3852<br>psf   | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>39 | 39.8 ft         | 211.66302<br>ft | -120.70681<br>psf | 473.84035<br>psf  | 441.86328<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>40 | 41 ft           | 213.52142<br>ft | -170.16956<br>psf | 390.78162<br>psf  | 364.40975<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>41 | 42.19125 ft     | 215.45231<br>ft | -237.66118<br>psf | 314.14137<br>psf  | 292.94156<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>42 | 43.581761<br>ft | 217.98102<br>ft | -363.35006<br>psf | 210.48732<br>psf  | 196.2826<br>psf   | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>43 | 45.373605<br>ft | 221.54251<br>ft | 0 psf             | 86.935972<br>psf  | 67.921825<br>psf  | 0 psf | 0 psf | Gravel Borrow                                |



# 2B.4 Global - Pseudo-Static FC Walll (M-P)

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## **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 652 Date: 01/17/2022 Time: 02:07:09 PM

Tool Version: 11.1.1.22085

Last Solved Date: 01/17/2022 Last Solved Time: 02:21:21 PM

# **Project Settings**

Unit System: U.S. Customary Units

# **Analysis Settings**

#### 2B.4 Global - Pseudo-Static FC Walll (M-P)

Description: With Forward Compatible Wall

Kind: SLOPE/W

Parent: 2. Steady State (Global) Analysis Type: Morgenstern-Price

Settings

Side Function

Interslice force function option: Half-Sine

PWP Conditions from Parent Analysis: 2. Steady State (Global) [(last)]

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 20

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

Factor of Safety Convergence Settings

Maximum Number of Iterations: 100 Tolerable difference in F of S: 0.001

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Solution Settings

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

#### **Materials**

## **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

## ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **SEW Wall**

Material Model: High Strength

Unit Weight: 130 pcf

# **ESU 2A Very Loose to Loose Sand/Gravel (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 32°

Phi-B: 0°

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

## **ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 200 psf Effective Friction Angle: 32 °

Phi-B: 0°

## **Forward Compatible Wall**

Material Model: High Strength

Unit Weight: 130 pcf

#### **Lightweight EPS**

Material Model: Mohr-Coulomb

Unit Weight: 5 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 0 °

Phi-B: 0°

# **Slip Surface Entry and Exit**

Left Type: Range

Left-Zone Left Coordinate: (-40, 181.99516) ft Left-Zone Right Coordinate: (0, 196.3) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15, 223) ft

Right-Zone Right Coordinate: (70, 223.39933) ft

Right-Zone Increment: 30 Radius Increments: 20

# **Slip Surface Limits**

Left Coordinate: (-100, 170.1) ft Right Coordinate: (100, 223.6) ft

## **Seismic Coefficients**

Horz Seismic Coef.: 0.191

# **Surcharge Loads**

# **Surcharge Load 1**

Surcharge (Unit Weight): 125 pcf

Direction: Vertical

#### **Coordinates**

| X       | Y        |
|---------|----------|
| 9 ft    | 224 ft   |
| 26 ft   | 224 ft   |
| 39.4 ft | 224.2 ft |
| 40.2 ft | 224.2 ft |
| 100 ft  | 224.6 ft |

# **Geometry**

Name: Default Geometry

## **Settings**

View: 2D

Element Thickness: 1 ft

## **Points**

| 1.5      |             |             |  |  |
|----------|-------------|-------------|--|--|
|          | X           | Υ           |  |  |
| Point 1  | 100 ft      | 160 ft      |  |  |
| Point 2  | 100 ft      | 185.5 ft    |  |  |
| Point 3  | 0.9 ft      | 160 ft      |  |  |
| Point 4  | 100 ft      | 211.1475 ft |  |  |
| Point 5  | 3.8 ft      | 183 ft      |  |  |
| Point 6  | -20.1275 ft | 160 ft      |  |  |
| Point 7  | 100 ft      | 219.64 ft   |  |  |
| Point 8  | 42.5825 ft  | 219.8525 ft |  |  |
| Point 9  | 40.2 ft     | 223.2 ft    |  |  |
| Point 10 | 100 ft      | 223.6 ft    |  |  |
| Point 11 | 0 ft        | 211.7 ft    |  |  |
| Point 12 | 0 ft        | 192 ft      |  |  |
| Point 13 | 13 ft       | 192 ft      |  |  |
| Point 14 | 24.5 ft     | 213.8 ft    |  |  |
| Point 15 | 24.5 ft     | 192 ft      |  |  |
| Point 16 | 24.5 ft     | 203 ft      |  |  |
| Point 17 | 24.5 ft     | 205 ft      |  |  |
| Point 18 | 41.8 ft     | 220.7 ft    |  |  |
| Point 19 | 26.6 ft     | 215.4 ft    |  |  |
| Point 20 | 37.9 ft     | 223.2 ft    |  |  |
| Point 21 | 6.13959 ft  | 185.3 ft    |  |  |
| Point 22 | 8.9 ft      | 192 ft      |  |  |
| Point 23 | -100 ft     | 160 ft      |  |  |
| Point 24 | -100 ft     | 170.1 ft    |  |  |
| Point 25 | -91.8 ft    | 174.4 ft    |  |  |
|          |             |             |  |  |

| l 5 · · 66 | l           | 1 476 5 6    |
|------------|-------------|--------------|
| Point 26   | -88.3 ft    | 176.5 ft     |
| Point 27   | -85.7 ft    | 177.8 ft     |
| Point 28   | -83.4 ft    | 178.4 ft     |
| Point 29   | -76 ft      | 178.9 ft     |
| Point 30   | -74 ft      | 179.7 ft     |
| Point 31   | -55.9 ft    | 180.2 ft     |
| Point 32   | -37.3 ft    | 182.3 ft     |
| Point 33   | -30.3 ft    | 182.9 ft     |
| Point 34   | -13.6 ft    | 190.2 ft     |
| Point 35   | 7 ft        | 223 ft       |
| Point 36   | 15 ft       | 223 ft       |
| Point 37   | 15 ft       | 211.7 ft     |
| Point 38   | 7 ft        | 211.7 ft     |
| Point 39   | -6 ft       | 195 ft       |
| Point 40   | -37.3275 ft | 162.2725 ft  |
| Point 41   | -47.26 ft   | 160 ft       |
| Point 42   | -5.125 ft   | 182.98095 ft |
| Point 43   | 80.7025 ft  | 160 ft       |
| Point 44   | -100 ft     | 129.8675 ft  |
| Point 45   | 100 ft      | 129.8675 ft  |
| Point 46   | -100 ft     | 147.8625 ft  |
| Point 47   | -27.95 ft   | 152.3875 ft  |
| Point 48   | -100 ft     | 133.97 ft    |
| Point 49   | 16.5 ft     | 197.3 ft     |
| Point 50   | 100 ft      | 209.9025 ft  |
| Point 51   | 95.42762 ft | 209.80965 ft |
| Point 52   | 3.915 ft    | 160.77581 ft |
| Point 53   | 17.7925 ft  | 187.09412 ft |
| Point 54   | 28.7 ft     | 129.8675 ft  |
| Point 55   | 0 ft        | 198.7 ft     |
| Point 56   | 47.15 ft    | 195.68393 ft |
| Point 57   | 42.67 ft    | 194.37311 ft |
| Point 58   | 0 ft        | 195 ft       |
| Point 59   | -32.3 ft    | 165.4 ft     |
| Point 60   | -16 ft      | 164.1 ft     |
| Point 61   | -100 ft     | 150.0525 ft  |
| Point 62   | 15 ft       | 218.535 ft   |
| Point 63   | 24 ft       | 223 ft       |
| Point 64   | 7 ft        | 214.495 ft   |
| Point 65   | 1.355 ft    | 211.7 ft     |
| Point 66   | 25.9 ft     | 223 ft       |
| Point 67   | 22 ft       | 192 ft       |
| Point 68   | 15.0117 ft  | 208.01106 ft |
| Point 69   | 21.5 ft     | 192 ft       |
| Point 70   | 15.5 ft     | 192 ft       |
| Point 71   | 15.5 ft     | 211.7 ft     |
| Point 72   | 15.5 ft     | 194.35 ft    |
| Point 73   | 15.5 ft     | 197.3 ft     |
|            |             |              |

| Point 74 | 15.5 ft     | 208.29 ft    |
|----------|-------------|--------------|
| Point 75 | 18.50702 ft | 197.3 ft     |
| Point 76 | 15.5 ft     | 196.43333 ft |
| Point 77 | 21.5 ft     | 211.7 ft     |
| Point 78 | 20 ft       | 197.3 ft     |
| Point 79 | 20 ft       | 192 ft       |
| Point 80 | 21.5 ft     | 202 ft       |
| Point 81 | 21.5 ft     | 200 ft       |
| Point 82 | 21.5 ft     | 208.29 ft    |
| Point 83 | 31.9 ft     | 223.1 ft     |
| Point 84 | 31.9 ft     | 219.08 ft    |

## Regions

|              | Material   | Points   | Area                       |
|--------------|--|--|----------------------------|
| Region<br>1  | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 1,2,52,3,43  | 1,263.5<br>ft <sup>2</sup> |
| Region<br>2  | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 52,2,50,51,56,57,53,5,60,6,47,3                          | 2,656.9<br>ft <sup>2</sup> |
| Region<br>3  | Gravel Borrow  | 9,18,8,7,10  | 214.55<br>ft <sup>2</sup>  |
| Region<br>4  | SEW Wall   | 38,65,11,55,68,74,71,37                                  | 127 ft <sup>2</sup>        |
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)              | 8,16,17,18   | 31.556<br>ft <sup>2</sup>  |
| Region<br>6  | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion)    | 18,17,14,19,84,20,9                                      | 115.05<br>ft <sup>2</sup>  |
| Region<br>7  | Forward Compatible Wall  | 38,37,62,64  | 38.52<br>ft <sup>2</sup>   |
| Region<br>8  | Lightweight EPS  | 14,19,84,83,66,63,62,37,71,77                            | 132.58<br>ft <sup>2</sup>  |
| Region<br>9  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)              | 22,42,59,40,60,5,21,13                                   | 332.37<br>ft <sup>2</sup>  |
| Region<br>10 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 44,54,45,1,43,3,47,48                                    | 4,704.7<br>ft <sup>2</sup> |
| Region<br>11 | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)              | 41,46,48,47,6,60,40                                      | 992.46<br>ft²              |
| Region<br>12 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 56,51,50,4,7,8,16,15,67,69,79,70,13,21,5,53,57           | 1,417.8<br>ft <sup>2</sup> |
| Region<br>13 | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion)    | 34,33,32,31,30,29,28,27,26,25,24,23,40,59,42,22,12,58,39 | 1,656.2<br>ft <sup>2</sup> |
| Region<br>14 | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion)    | 40,23,61,46,41   | 379.99<br>ft <sup>2</sup>  |
| Region<br>15 | Lightweight EPS  | 63,36,62   | 20.093<br>ft <sup>2</sup>  |
| Region<br>16 | Forward Compatible Wall  | 36,35,64,62  | 51.88<br>ft²               |
| Region<br>17 |  | 64,65,38   | 7.8889<br>ft²              |
| Region<br>18 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 15,16,81,69,67   | 28.5 ft <sup>2</sup>       |
| Region       | SEW Wall   | 72,76,22,13  | 11.692                     |

| 19           |   |                         | ft²                        |
|--------------|---|-------------------------|----------------------------|
| Region<br>20 | SEW Wall  | 70,72,13                | 2.9375<br>ft <sup>2</sup>  |
| Region<br>21 | SEW Wall  | 70,79,78,75,72          | 19.415<br>ft <sup>2</sup>  |
| Region<br>22 | Gravel Borrow   | 81,75,78,79,69          | 11.991<br>ft²              |
| Region<br>23 | Gravel Borrow   | 49,75,81,80             | 7.7095<br>ft <sup>2</sup>  |
| Region<br>24 | SEW Wall  | 49,76,72,75             | 4.002<br>ft <sup>2</sup>   |
| Region<br>25 | SEW Wall  | 73,76,49                | 0.43333<br>ft <sup>2</sup> |
| Region<br>26 | SEW Wall  | 76,73,74,68,55,58,12,22 | 163.72<br>ft²              |
| Region<br>27 | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)           | 80,81,16,17             | 6 ft²                      |
| Region<br>28 | Gravel Borrow   | 74,82,77                | 10.23<br>ft <sup>2</sup>   |
| Region<br>29 | Gravel Borrow   | 77,71,74                | 10.23<br>ft <sup>2</sup>   |
| Region<br>30 | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion) | 77,82,80,17,14          | 27.75<br>ft <sup>2</sup>   |
| Region<br>31 | Gravel Borrow   | 73,49,80,82,74          | 54.19<br>ft <sup>2</sup>   |
| Region<br>32 | Common Borrow   | 20,83,84                | 12.06<br>ft <sup>2</sup>   |
| Region<br>33 |   | 55,39,58                | 11.1 ft²                   |

### **Slip Results**

Slip Surfaces Analysed: 3622 of 16926 converged

## **Current Slip Surface**

Slip Surface: 1,021 Factor of Safety: 1.3 Volume: 1,418.8147 ft<sup>3</sup> Weight: 154,412.22 lbf

Resisting Moment: 8,351,757.2 lbf·ft Activating Moment: 6,572,450.7 lbf·ft

Resisting Force: 101,586.31 lbf Activating Force: 79,948.783 lbf Slip Rank: 1 of 16,926 slip surfaces Exit: (-38.240876, 182.19377) ft Entry: (46.166189, 223.23991) ft

Radius: 72.22526 ft

Center: (-20.046856, 252.08988) ft

## Slip Slices

|             | X                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material  |
|-------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|--|
| Slice<br>1  | -37.770438<br>ft | 182.07469<br>ft | -184.85613<br>psf | 49.186123<br>psf         | 30.734901<br>psf       | 100 psf              | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>2  | -35.55 ft        | 181.57087<br>ft | -183.87843<br>psf | 168.26683<br>psf         | 105.14478<br>psf       | 100 psf              | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>3  | -32.05 ft        | 180.89112<br>ft | -181.90896<br>psf | 364.95917<br>psf         | 228.0518<br>psf        | 100 psf              | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>4  | -28.908333<br>ft | 180.42402<br>ft | -179.6982<br>psf  | 617.05079<br>psf         | 385.57613<br>psf       | 100 psf              | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>5  | -26.125 ft       | 180.13438<br>ft | -179.0209<br>psf  | 918.8684<br>psf          | 574.1727<br>psf        | 100 psf              | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>6  | -23.341667<br>ft | 179.95326<br>ft | -180.28457<br>psf | 1,205.2862<br>psf        | 753.14641<br>psf       | 100 psf              | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>7  | -20.558333<br>ft | 179.87984<br>ft | -178.0415<br>psf  | 1,453.7439<br>psf        | 908.39999<br>psf       | 100 psf              | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>8  | -17.775 ft       | 179.91379<br>ft | -180.73923<br>psf | 1,644.5562<br>psf        | 1,027.6327<br>psf      | 100 psf              | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>9  | -14.991667<br>ft | 180.05526<br>ft | -190.1224<br>psf  | 1,765.4905<br>psf        | 1,103.2009<br>psf      | 100 psf              | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>10 | -12.326997<br>ft | 180.28979<br>ft | -254.29877<br>psf | 1,845.9991<br>psf        | 1,153.5083<br>psf      | 100 psf              | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |

| Slice<br>11 | -9.780992<br>ft  | 180.60949<br>ft | -368.84527<br>psf | 1,893.909<br>psf  | 1,183.4457<br>psf | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
|-------------|------------------|-----------------|-------------------|-------------------|-------------------|---------|-------|--|
| Slice<br>12 | -7.2539947<br>ft | 181.01803<br>ft | -403.69014<br>psf | 1,972.5688<br>psf | 1,232.5978<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                    |
| Slice<br>13 | -5.5625 ft       | 181.33331<br>ft | -377.40593<br>psf | 1,917.4595<br>psf | 1,198.1617<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                    |
| Slice<br>14 | -3.84375 ft      | 181.71788<br>ft | -351.63392<br>psf | 1,758.2033<br>psf | 1,098.6473<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                    |
| Slice<br>15 | -1.28125 ft      | 182.35768<br>ft | -313.21625<br>psf | 1,520.192<br>psf  | 949.9214<br>psf   | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                    |
| Slice<br>16 | 0.6775 ft        | 182.90542<br>ft | -284.61599<br>psf | 3,225.7503<br>psf | 2,015.6725<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                    |
| Slice<br>17 | 3.3141258<br>ft  | 183.77835<br>ft | -248.89977<br>psf | 2,864.4527<br>psf | 1,789.9087<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                    |
| Slice<br>18 | 5.7064208<br>ft  | 184.61365<br>ft | -212.44256<br>psf | 2,926.828<br>psf  | 2,729.3113<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                           |
| Slice<br>19 | 6.569795 ft      | 184.94952<br>ft | -194.40709<br>psf | 2,794.2249<br>psf | 2,605.6569<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                           |
| Slice<br>20 | 7.95 ft          | 185.5196<br>ft  | -171.22478<br>psf | 3,790.252<br>psf  | 3,534.4672<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                           |
| Slice<br>21 | 8.95 ft          | 185.94105<br>ft | -152.7832<br>psf  | 3,613.2766<br>psf | 3,369.4349<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                           |
| Slice<br>22 | 11 ft            | 186.9157<br>ft  | -105.78401<br>psf | 3,387.812<br>psf  | 3,159.1858<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                           |
| Slice<br>23 | 14 ft            | 188.40304<br>ft | -72.253284<br>psf | 2,936.5307<br>psf | 2,738.3592<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel                           |
| Slice       |                  | 189.07767       | -63.880304        | 1,834.5576        | 1,710.7527        |         |       | ESU 4B Dense to  |

| 24          | 15.25 ft    | ft              | psf               | psf               | psf               | 0 psf | 0 psf | Very Dense<br>Sand/Gravel                    |
|-------------|-------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>25 | 16 ft       | 189.5057<br>ft  | -59.51264<br>psf  | 1,751.4628<br>psf | 1,633.2655<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>26 | 17.50351 ft | 190.40457<br>ft | -50.815986<br>psf | 1,594.4673<br>psf | 1,486.8648<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>27 | 19.25351 ft | 191.49963<br>ft | -42.857717<br>psf | 1,427.4886<br>psf | 1,331.1546<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>28 | 20.75 ft    | 192.49727<br>ft | -37.69367<br>psf  | 1,277.6965<br>psf | 998.24588<br>psf  | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>29 | 22.75 ft    | 193.93054<br>ft | -32.288402<br>psf | 1,071.0607<br>psf | 998.78023<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>30 | 24.25 ft    | 195.04449<br>ft | -28.88961<br>psf  | 1,034.2335<br>psf | 964.43833<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>31 | 25.2 ft     | 195.80131<br>ft | -27.371515<br>psf | 1,012.9065<br>psf | 944.55061<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>32 | 25.95 ft    | 196.40529<br>ft | -26.439209<br>psf | 997.58492<br>psf  | 930.26299<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>33 | 26.3 ft     | 196.6976<br>ft  | -26.013331<br>psf | 990.25308<br>psf  | 923.42594<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>34 | 27.925 ft   | 198.1265<br>ft  | -25.620539<br>psf | 951.32339<br>psf  | 887.12341<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>35 | 30.575 ft   | 200.60723<br>ft | -27.532663<br>psf | 889.45245<br>psf  | 829.42783<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>36 | 33.4 ft     | 203.56213<br>ft | -35.750746<br>psf | 981.34156<br>psf  | 915.11581<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>37 | 36.4 ft     | 207.096 ft      | -57.336715<br>psf | 795.97929<br>psf  | 742.2627<br>psf   | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>38 | 38.65 ft    | 210.02434<br>ft | -90.418054<br>psf | 654.49593<br>psf  | 610.32733<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>39 | 39.8 ft     | 211.66302<br>ft | -120.70681<br>psf | 578.6092<br>psf   | 539.56181<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>40 | 41 ft       | 213.52142<br>ft | -170.16956<br>psf | 502.2 psf         | 468.30907<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>41 | 42.19125 ft | 215.45231<br>ft | -237.66118<br>psf | 427.066<br>psf    | 398.24549<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice       | 43.581761   | 217.98102       | -363.35006        | 304.81326         | 284.24296         | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense                |

#### 2B.4 Global - Pseudo-Static FC Walll (M-P)

| 42          | ft              | ft              | psf   | psf              | psf              |       |       | <br>  Sand/Gravel |
|-------------|-----------------|-----------------|-------|------------------|------------------|-------|-------|-------------------|
| Slice<br>43 | 45.373605<br>ft | 221.54251<br>ft | 0 psf | 141.84265<br>psf | 110.81962<br>psf | 0 psf | 0 psf | Gravel Borrow     |

# 2B.5 Global - Post-Seismic FC Wall (Spencer)

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### **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 652 Date: 01/17/2022 Time: 02:07:09 PM

Tool Version: 11.1.1.22085

Last Solved Date: 01/17/2022 Last Solved Time: 02:26:28 PM

### **Project Settings**

Unit System: U.S. Customary Units

## **Analysis Settings**

#### 2B.5 Global - Post-Seismic FC Wall (Spencer)

Description: With Forward Compatible Wall

Kind: SLOPE/W

Parent: 2. Steady State (Global)

Analysis Type: Spencer

Settings

PWP Conditions from Parent Analysis: 2. Steady State (Global) [(last)]

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 20

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

Factor of Safety Convergence Settings Maximum Number of Iterations: 100 Tolerable difference in F of S: 0.001

Solution Settings

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3 Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

#### **Materials**

### **ESU 2A Very Loose to Loose Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **ESU 2B Medium Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

### **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

#### Common Borrow

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **SEW Wall**

Material Model: High Strength

Unit Weight: 130 pcf

#### **ESU 2B Medium Dense Sand/Gravel (Residual Strength)**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 497 psf Effective Friction Angle: 0 °

Phi-B: 0°

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

#### Forward Compatible Wall

Material Model: High Strength

Unit Weight: 130 pcf

#### **Lightweight EPS**

Material Model: Mohr-Coulomb

Unit Weight: 5 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 0 °

Phi-B: 0°

## **Slip Surface Entry and Exit**

Left Type: Range

Left-Zone Left Coordinate: (-40, 181.99516) ft Left-Zone Right Coordinate: (0, 196.3) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15, 223) ft

Right-Zone Right Coordinate: (70, 223.39933) ft

Right-Zone Increment: 30 Radius Increments: 20

## **Slip Surface Limits**

Left Coordinate: (-100, 170.1) ft Right Coordinate: (100, 223.6) ft

## **Surcharge Loads**

### **Surcharge Load 1**

Surcharge (Unit Weight): 125 pcf

Direction: Vertical

#### **Coordinates**

| X       | Υ        |
|---------|----------|
| 9 ft    | 224 ft   |
| 26 ft   | 224 ft   |
| 39.4 ft | 224.2 ft |
| 40.2 ft | 224.2 ft |
| 100 ft  | 224.6 ft |

## **Geometry**

Name: Default Geometry

### **Settings**

View: 2D

Element Thickness: 1 ft

#### **Points**

| 1.5      |             |             |
|----------|-------------|-------------|
|          | Х           | Υ           |
| Point 1  | 100 ft      | 160 ft      |
| Point 2  | 100 ft      | 185.5 ft    |
| Point 3  | 0.9 ft      | 160 ft      |
| Point 4  | 100 ft      | 211.1475 ft |
| Point 5  | 3.8 ft      | 183 ft      |
| Point 6  | -20.1275 ft | 160 ft      |
| Point 7  | 100 ft      | 219.64 ft   |
| Point 8  | 42.5825 ft  | 219.8525 ft |
| Point 9  | 40.2 ft     | 223.2 ft    |
| Point 10 | 100 ft      | 223.6 ft    |
| Point 11 | 0 ft        | 211.7 ft    |
| Point 12 | 0 ft        | 192 ft      |
| Point 13 | 13 ft       | 192 ft      |
| Point 14 | 24.5 ft     | 213.8 ft    |
| Point 15 | 24.5 ft     | 192 ft      |
| Point 16 | 24.5 ft     | 203 ft      |
| Point 17 | 24.5 ft     | 205 ft      |
| Point 18 | 41.8 ft     | 220.7 ft    |
| Point 19 | 26.6 ft     | 215.4 ft    |
| Point 20 | 37.9 ft     | 223.2 ft    |
| Point 21 | 6.13959 ft  | 185.3 ft    |
| Point 22 | 8.9 ft      | 192 ft      |
| Point 23 | -100 ft     | 160 ft      |
| Point 24 | -100 ft     | 170.1 ft    |
| Point 25 | -91.8 ft    | 174.4 ft    |
|          |             |             |

| l 5 · · 66 | l           | 1 470 5 6    |
|------------|-------------|--------------|
| Point 26   | -88.3 ft    | 176.5 ft     |
| Point 27   | -85.7 ft    | 177.8 ft     |
| Point 28   | -83.4 ft    | 178.4 ft     |
| Point 29   | -76 ft      | 178.9 ft     |
| Point 30   | -74 ft      | 179.7 ft     |
| Point 31   | -55.9 ft    | 180.2 ft     |
| Point 32   | -37.3 ft    | 182.3 ft     |
| Point 33   | -30.3 ft    | 182.9 ft     |
| Point 34   | -13.6 ft    | 190.2 ft     |
| Point 35   | 7 ft        | 223 ft       |
| Point 36   | 15 ft       | 223 ft       |
| Point 37   | 15 ft       | 211.7 ft     |
| Point 38   | 7 ft        | 211.7 ft     |
| Point 39   | -6 ft       | 195 ft       |
| Point 40   | -37.3275 ft | 162.2725 ft  |
| Point 41   | -47.26 ft   | 160 ft       |
| Point 42   | -5.125 ft   | 182.98095 ft |
| Point 43   | 80.7025 ft  | 160 ft       |
| Point 44   | -100 ft     | 129.8675 ft  |
| Point 45   | 100 ft      | 129.8675 ft  |
| Point 46   | -100 ft     | 147.8625 ft  |
| Point 47   | -27.95 ft   | 152.3875 ft  |
| Point 48   | -100 ft     | 133.97 ft    |
| Point 49   | 16.5 ft     | 197.3 ft     |
| Point 50   | 100 ft      | 209.9025 ft  |
| Point 51   | 95.42762 ft | 209.80965 ft |
| Point 52   | 3.915 ft    | 160.77581 ft |
| Point 53   | 17.7925 ft  | 187.09412 ft |
| Point 54   | 28.7 ft     | 129.8675 ft  |
| Point 55   | 0 ft        | 198.7 ft     |
| Point 56   | 47.15 ft    | 195.68393 ft |
| Point 57   | 42.67 ft    | 194.37311 ft |
| Point 58   | 0 ft        | 195 ft       |
| Point 59   | -32.3 ft    | 165.4 ft     |
| Point 60   | -16 ft      | 164.1 ft     |
| Point 61   | -100 ft     | 150.0525 ft  |
| Point 62   | 15 ft       | 218.535 ft   |
| Point 63   | 24 ft       | 223 ft       |
| Point 64   | 7 ft        | 214.495 ft   |
| Point 65   | 1.355 ft    | 211.7 ft     |
| Point 66   | 25.9 ft     | 223 ft       |
| Point 67   | 22 ft       | 192 ft       |
| Point 68   | 15.0117 ft  | 208.01106 ft |
| Point 69   | 21.5 ft     | 192 ft       |
| Point 70   | 15.5 ft     | 192 ft       |
| Point 71   | 15.5 ft     | 211.7 ft     |
| Point 72   | 15.5 ft     | 194.35 ft    |
| Point 73   | 15.5 ft     | 197.3 ft     |
|            |             |              |

| Point 74 | 15.5 ft     | 208.29 ft    |
|----------|-------------|--------------|
| Point 75 | 18.50702 ft | 197.3 ft     |
| Point 76 | 15.5 ft     | 196.43333 ft |
| Point 77 | 21.5 ft     | 211.7 ft     |
| Point 78 | 20 ft       | 197.3 ft     |
| Point 79 | 20 ft       | 192 ft       |
| Point 80 | 21.5 ft     | 202 ft       |
| Point 81 | 21.5 ft     | 200 ft       |
| Point 82 | 21.5 ft     | 208.29 ft    |
| Point 83 | 31.9 ft     | 223.1 ft     |
| Point 84 | 31.9 ft     | 219.08 ft    |

## Regions

|              | Material   | Points   | Area                       |
|--------------|--|--|----------------------------|
| Region<br>1  | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 1,2,52,3,43  | 1,263.5<br>ft <sup>2</sup> |
| Region<br>2  | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 52,2,50,51,56,57,53,5,60,6,47,3                          | 2,656.9<br>ft <sup>2</sup> |
| Region<br>3  | Gravel Borrow  | 9,18,8,7,10  | 214.55<br>ft <sup>2</sup>  |
| Region<br>4  | SEW Wall   | 38,65,11,55,68,74,71,37                                  | 127 ft <sup>2</sup>        |
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel                                  | 8,16,17,18   | 31.556<br>ft <sup>2</sup>  |
| Region<br>6  | ESU 2A Very Loose to Loose<br>Sand/Gravel                        | 18,17,14,19,84,20,9                                      | 115.05<br>ft <sup>2</sup>  |
| Region<br>7  | Forward Compatible Wall  | 38,37,62,64  | 38.52<br>ft <sup>2</sup>   |
| Region<br>8  | Lightweight EPS  | 14,19,84,83,66,63,62,37,71,77                            | 132.58<br>ft <sup>2</sup>  |
| Region<br>9  | ESU 2B Medium Dense Sand/Gravel                                  | 22,42,59,40,60,5,21,13                                   | 332.37<br>ft <sup>2</sup>  |
| Region<br>10 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 44,54,45,1,43,3,47,48                                    | 4,704.7<br>ft <sup>2</sup> |
| Region<br>11 | ESU 2B Medium Dense Sand/Gravel (Residual Strength)              | 41,46,48,47,6,60,40                                      | 992.46<br>ft²              |
| Region<br>12 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 56,51,50,4,7,8,16,15,67,69,79,70,13,21,5,53,57           | 1,417.8<br>ft <sup>2</sup> |
| Region<br>13 | ESU 2A Very Loose to Loose<br>Sand/Gravel                        | 34,33,32,31,30,29,28,27,26,25,24,23,40,59,42,22,12,58,39 | 1,656.2<br>ft <sup>2</sup> |
| Region<br>14 | ESU 2A Very Loose to Loose<br>Sand/Gravel                        | 40,23,61,46,41   | 379.99<br>ft²              |
| Region<br>15 | Lightweight EPS  | 63,36,62   | 20.093<br>ft <sup>2</sup>  |
| Region<br>16 | Forward Compatible Wall  | 36,35,64,62  | 51.88<br>ft²               |
| Region<br>17 |  | 64,65,38   | 7.8889<br>ft²              |
| Region<br>18 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 15,16,81,69,67   | 28.5 ft <sup>2</sup>       |
| Region       | SEW Wall   | 72,76,22,13  | 11.692                     |

| 19           |   |                         | ft²                        |
|--------------|---|-------------------------|----------------------------|
| Region<br>20 | SEW Wall                                  | 70,72,13                | 2.9375<br>ft <sup>2</sup>  |
| Region<br>21 | SEW Wall                                  | 70,79,78,75,72          | 19.415<br>ft <sup>2</sup>  |
| Region<br>22 | Gravel Borrow                             | 81,75,78,79,69          | 11.991<br>ft <sup>2</sup>  |
| Region<br>23 | Gravel Borrow                             | 49,75,81,80             | 7.7095<br>ft <sup>2</sup>  |
| Region<br>24 | SEW Wall                                  | 49,76,72,75             | 4.002<br>ft <sup>2</sup>   |
| Region<br>25 | SEW Wall                                  | 73,76,49                | 0.43333<br>ft <sup>2</sup> |
| Region<br>26 | SEW Wall                                  | 76,73,74,68,55,58,12,22 | 163.72<br>ft²              |
| Region<br>27 | ESU 2B Medium Dense Sand/Gravel           | 80,81,16,17             | 6 ft²                      |
| Region<br>28 | Gravel Borrow                             | 74,82,77                | 10.23<br>ft <sup>2</sup>   |
| Region<br>29 | Gravel Borrow                             | 77,71,74                | 10.23<br>ft <sup>2</sup>   |
| Region<br>30 | ESU 2A Very Loose to Loose<br>Sand/Gravel | 77,82,80,17,14          | 27.75<br>ft²               |
| Region<br>31 | Gravel Borrow                             | 73,49,80,82,74          | 54.19<br>ft <sup>2</sup>   |
| Region<br>32 | Common Borrow                             | 20,83,84                | 12.06<br>ft²               |
| Region<br>33 |   | 55,39,58                | 11.1 ft²                   |

## **Slip Results**

Slip Surfaces Analysed: 3261 of 16926 converged

## **Current Slip Surface**

Slip Surface: 1,021 Factor of Safety: 1.7 Volume: 1,418.8147 ft<sup>3</sup> Weight: 154,412.22 lbf

Resisting Moment: 8,641,474.2 lbf·ft Activating Moment: 5,105,467.4 lbf·ft

Resisting Force: 102,360.4 lbf Activating Force: 60,480.068 lbf Slip Rank: 1 of 16,926 slip surfaces Exit: (-38.240876, 182.19377) ft Entry: (46.166189, 223.23991) ft

Radius: 72.22526 ft

Center: (-20.046856, 252.08988) ft

## **Slip Slices**

| Sirces      | ı                | 1               | I                 | I                        | ı                      | 1                    | 1                   | T  |
|-------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|--|
|             | X                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material                                |
| Slice<br>1  | -37.770438<br>ft | 182.07469<br>ft | -184.85613<br>psf | 32.144229<br>psf         | 20.085944<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>2  | -35.55 ft        | 181.57087<br>ft | -183.87843<br>psf | 156.37913<br>psf         | 97.716526<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>3  | -32.05 ft        | 180.89112<br>ft | -181.90896<br>psf | 308.26356<br>psf         | 192.62445<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>4  | -28.908333<br>ft | 180.42402<br>ft | -179.6982<br>psf  | 482.76859<br>psf         | 301.6673<br>psf        | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>5  | -26.125 ft       | 180.13438<br>ft | -179.0209<br>psf  | 684.98481<br>psf         | 428.02601<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>6  | -23.341667<br>ft | 179.95326<br>ft | -180.28457<br>psf | 854.04199<br>psf         | 533.66466<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>7  | -20.558333<br>ft | 179.87984<br>ft | -178.0415<br>psf  | 994.28379<br>psf         | 621.29747<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>8  | -17.775 ft       | 179.91379<br>ft | -180.73923<br>psf | 1,109.1401<br>psf        | 693.06764<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>9  | -14.991667<br>ft | 180.05526<br>ft | -190.1224<br>psf  | 1,201.3536<br>psf        | 750.68907<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>10 | -12.326997<br>ft | 180.28979<br>ft | -254.29877<br>psf | 1,300.8011<br>psf        | 812.83073<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>11 | -9.780992<br>ft  | 180.60949<br>ft | -368.84527<br>psf | 1,407.8766<br>psf        | 879.73894<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>12 | -7.2539947<br>ft | 181.01803<br>ft | -403.69014<br>psf | 1,496.1144<br>psf        | 934.87606<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>13 | -5.5625 ft       | 181.33331<br>ft | -377.40593<br>psf | 1,516.2124<br>psf        | 947.43468<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>14 | -3.84375 ft      | 181.71788<br>ft | -351.63392<br>psf | 1,440.9011<br>psf        | 900.37493<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>15 | -1.28125 ft      | 182.35768<br>ft | -313.21625<br>psf | 1,326.7714<br>psf        | 829.0588<br>psf        | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>16 | 0.6775 ft        | 182.90542<br>ft | -284.61599<br>psf | 3,313.168<br>psf         | 2,070.2972<br>psf      | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice       | 3.3141258        | 183.77835       | -248.89977        | 3,115.6891               | 1,946.8986             |                      |                     | ESU 2B Medium                                |

| 17          | ft              | ft              | psf               | psf               | psf               | 0 psf | 0 psf | Dense<br>Sand/Gravel                         |
|-------------|-----------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>18 | 5.7064208<br>ft | 184.61365<br>ft | -212.44256<br>psf | 3,006.8752<br>psf | 2,803.9564<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>19 | 6.569795 ft     | 184.94952<br>ft | -194.40709<br>psf | 2,942.0427<br>psf | 2,743.4992<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>20 | 7.95 ft         | 185.5196<br>ft  | -171.22478<br>psf | 4,097.9205<br>psf | 3,821.3727<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>21 | 8.95 ft         | 185.94105<br>ft | -152.7832<br>psf  | 4,002.7668<br>psf | 3,732.6405<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>22 | 11 ft           | 186.9157<br>ft  | -105.78401<br>psf | 3,902.2017<br>psf | 3,638.8619<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>23 | 14 ft           | 188.40304<br>ft | -72.253284<br>psf | 3,594.7197<br>psf | 3,352.1303<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>24 | 15.25 ft        | 189.07767<br>ft | -63.880304<br>psf | 2,377.9467<br>psf | 2,217.4712<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>25 | 16 ft           | 189.5057<br>ft  | -59.51264<br>psf  | 2,306.0971<br>psf | 2,150.4703<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>26 | 17.50351 ft     | 190.40457<br>ft | -50.815986<br>psf | 2,161.709<br>psf  | 2,015.8263<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>27 | 19.25351 ft     | 191.49963<br>ft | -42.857717<br>psf | 1,995.4988<br>psf | 1,860.8327<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>28 | 20.75 ft        | 192.49727<br>ft | -37.69367<br>psf  | 1,873.1465<br>psf | 1,463.4624<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>29 | 22.75 ft        | 193.93054<br>ft | -32.288402<br>psf | 1,583.4613<br>psf | 1,476.6015<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>30 | 24.25 ft        | 195.04449<br>ft | -28.88961<br>psf  | 1,536.211<br>psf  | 1,432.5399<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>31 | 25.2 ft         | 195.80131<br>ft | -27.371515<br>psf | 1,504.0815<br>psf | 1,402.5787<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>32 | 25.95 ft        | 196.40529<br>ft | -26.439209<br>psf | 1,478.9735<br>psf | 1,379.1651<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>33 | 26.3 ft         | 196.6976<br>ft  | -26.013331<br>psf | 1,466.2908<br>psf | 1,367.3383<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>34 | 27.925 ft       | 198.1265<br>ft  | -25.620539<br>psf | 1,396.2447<br>psf | 1,302.0193<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice       | 30.575 ft       | 200.60723       | -27.532663        | 1,271.3916        | 1,185.5918        | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense                |

|             |                 | · •             |                   |                   |                  |       |       |  |
|-------------|-----------------|-----------------|-------------------|-------------------|------------------|-------|-------|--|
| 35          |                 | ft              | psf               | psf               | psf              |       |       | Sand/Gravel                                  |
| Slice<br>36 | 33.4 ft         | 203.56213<br>ft | -35.750746<br>psf | 1,303.3226<br>psf | 1,215.368<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>37 | 36.4 ft         | 207.096 ft      | -57.336715<br>psf | 995.67217<br>psf  | 928.47932<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>38 | 38.65 ft        | 210.02434<br>ft | -90.418054<br>psf | 771.12425<br>psf  | 719.085<br>psf   | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>39 | 39.8 ft         | 211.66302<br>ft | -120.70681<br>psf | 657.64023<br>psf  | 613.25944<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>40 | 41 ft           | 213.52142<br>ft | -170.16956<br>psf | 547.08975<br>psf  | 510.16945<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>41 | 42.19125 ft     | 215.45231<br>ft | -237.66118<br>psf | 443.27672<br>psf  | 413.36223<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>42 | 43.581761<br>ft | 217.98102<br>ft | -363.35006<br>psf | 298.61682<br>psf  | 278.46469<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>43 | 45.373605<br>ft | 221.54251<br>ft | 0 psf             | 120.72592<br>psf  | 94.321427<br>psf | 0 psf | 0 psf | Gravel Borrow                                |

# 2B.6 Global - Post-Seismic FC Wall (M-P)

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### **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 652 Date: 01/17/2022 Time: 02:07:09 PM

Tool Version: 11.1.1.22085

Last Solved Date: 01/17/2022 Last Solved Time: 02:25:15 PM

### **Project Settings**

Unit System: U.S. Customary Units

## **Analysis Settings**

#### 2B.6 Global - Post-Seismic FC Wall (M-P)

Description: With Forward Compatible Wall

Kind: SLOPE/W

Parent: 2. Steady State (Global) Analysis Type: Morgenstern-Price

Settings

Side Function

Interslice force function option: Half-Sine

PWP Conditions from Parent Analysis: 2. Steady State (Global) [(last)]

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 20

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

Factor of Safety Convergence Settings

Maximum Number of Iterations: 100 Tolerable difference in F of S: 0.001

Solution Settings

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

#### **Materials**

#### **ESU 2A Very Loose to Loose Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **ESU 2B Medium Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

### **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **SEW Wall**

Material Model: High Strength

Unit Weight: 130 pcf

#### **ESU 2B Medium Dense Sand/Gravel (Residual Strength)**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 497 psf Effective Friction Angle: 0 °

Phi-B: 0°

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

#### **Forward Compatible Wall**

Material Model: High Strength

Unit Weight: 130 pcf

#### **Lightweight EPS**

Material Model: Mohr-Coulomb

Unit Weight: 5 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 0 °

Phi-B: 0°

## **Slip Surface Entry and Exit**

Left Type: Range

Left-Zone Left Coordinate: (-40, 181.99516) ft Left-Zone Right Coordinate: (0, 196.3) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15, 223) ft

Right-Zone Right Coordinate: (70, 223.39933) ft

Right-Zone Increment: 30
Radius Increments: 20

## **Slip Surface Limits**

Left Coordinate: (-100, 170.1) ft Right Coordinate: (100, 223.6) ft

## **Surcharge Loads**

### **Surcharge Load 1**

Surcharge (Unit Weight): 125 pcf

Direction: Vertical

#### **Coordinates**

| X       | Υ        |
|---------|----------|
| 9 ft    | 224 ft   |
| 26 ft   | 224 ft   |
| 39.4 ft | 224.2 ft |
| 40.2 ft | 224.2 ft |
| 100 ft  | 224.6 ft |

## **Geometry**

Name: Default Geometry

### **Settings**

View: 2D

Element Thickness: 1 ft

#### **Points**

|          | X           | Υ           |
|----------|-------------|-------------|
| Point 1  | 100 ft      | 160 ft      |
| Point 2  | 100 ft      | 185.5 ft    |
| Point 3  | 0.9 ft      | 160 ft      |
| Point 4  | 100 ft      | 211.1475 ft |
| Point 5  | 3.8 ft      | 183 ft      |
| Point 6  | -20.1275 ft | 160 ft      |
| Point 7  | 100 ft      | 219.64 ft   |
| Point 8  | 42.5825 ft  | 219.8525 ft |
| Point 9  | 40.2 ft     | 223.2 ft    |
| Point 10 | 100 ft      | 223.6 ft    |
| Point 11 | 0 ft        | 211.7 ft    |
| Point 12 | 0 ft        | 192 ft      |
| Point 13 | 13 ft       | 192 ft      |
| Point 14 | 24.5 ft     | 213.8 ft    |
| Point 15 | 24.5 ft     | 192 ft      |
| Point 16 | 24.5 ft     | 203 ft      |
| Point 17 | 24.5 ft     | 205 ft      |
| Point 18 | 41.8 ft     | 220.7 ft    |
| Point 19 | 26.6 ft     | 215.4 ft    |
| Point 20 | 37.9 ft     | 223.2 ft    |
| Point 21 | 6.13959 ft  | 185.3 ft    |
| Point 22 | 8.9 ft      | 192 ft      |
| Point 23 | -100 ft     | 160 ft      |
|          |             |             |

| Doint 24 | 100 ft      | 170.1 ft     |
|----------|-------------|--------------|
| Point 24 | -100 ft     | 170.1 ft     |
| Point 25 | -91.8 ft    | 174.4 ft     |
| Point 26 | -88.3 ft    | 176.5 ft     |
| Point 27 | -85.7 ft    | 177.8 ft     |
| Point 28 | -83.4 ft    | 178.4 ft     |
| Point 29 | -76 ft      | 178.9 ft     |
| Point 30 | -74 ft      | 179.7 ft     |
| Point 31 | -55.9 ft    | 180.2 ft     |
| Point 32 | -37.3 ft    | 182.3 ft     |
| Point 33 | -30.3 ft    | 182.9 ft     |
| Point 34 | -13.6 ft    | 190.2 ft     |
| Point 35 | 7 ft        | 223 ft       |
| Point 36 | 15 ft       | 223 ft       |
| Point 37 | 15 ft       | 211.7 ft     |
| Point 38 | 7 ft        | 211.7 ft     |
| Point 39 | -6 ft       | 195 ft       |
| Point 40 | -37.3275 ft | 162.2725 ft  |
| Point 41 | -47.26 ft   | 160 ft       |
| Point 42 | -5.125 ft   | 182.98095 ft |
| Point 43 | 80.7025 ft  | 160 ft       |
| Point 44 | -100 ft     | 129.8675 ft  |
| Point 45 | 100 ft      | 129.8675 ft  |
| Point 46 | -100 ft     | 147.8625 ft  |
| Point 47 | -27.95 ft   | 152.3875 ft  |
| Point 48 | -100 ft     | 133.97 ft    |
| Point 49 | 16.5 ft     | 197.3 ft     |
| Point 50 | 100 ft      | 209.9025 ft  |
| Point 51 | 95.42762 ft | 209.80965 ft |
| Point 52 | 3.915 ft    | 160.77581 ft |
| Point 53 | 17.7925 ft  | 187.09412 ft |
| Point 54 | 28.7 ft     | 129.8675 ft  |
| Point 55 | 0 ft        | 198.7 ft     |
| Point 56 | 47.15 ft    | 195.68393 ft |
| Point 57 | 42.67 ft    | 194.37311 ft |
| Point 58 | 0 ft        | 195 ft       |
| Point 59 | -32.3 ft    | 165.4 ft     |
| Point 60 | -16 ft      | 164.1 ft     |
| Point 61 | -100 ft     | 150.0525 ft  |
| Point 62 | 15 ft       | 218.535 ft   |
| Point 63 | 24 ft       | 223 ft       |
| Point 64 | 7 ft        | 214.495 ft   |
| Point 65 | 1.355 ft    | 214.455 ft   |
| Point 66 | 25.9 ft     | 223 ft       |
| Point 67 | 23.9 ft     | 192 ft       |
| Point 68 | 15.0117 ft  | 208.01106 ft |
| Point 69 | 21.5 ft     | 192 ft       |
|          |             |              |
| Point 70 | 15.5 ft     | 192 ft       |
| Point 71 | 15.5 ft     | 211.7 ft     |
|          | I           | I            |

| Point 72 | 15.5 ft     | 194.35 ft    |
|----------|-------------|--------------|
| Point 73 | 15.5 ft     | 197.3 ft     |
| Point 74 | 15.5 ft     | 208.29 ft    |
| Point 75 | 18.50702 ft | 197.3 ft     |
| Point 76 | 15.5 ft     | 196.43333 ft |
| Point 77 | 21.5 ft     | 211.7 ft     |
| Point 78 | 20 ft       | 197.3 ft     |
| Point 79 | 20 ft       | 192 ft       |
| Point 80 | 21.5 ft     | 202 ft       |
| Point 81 | 21.5 ft     | 200 ft       |
| Point 82 | 21.5 ft     | 208.29 ft    |
| Point 83 | 31.9 ft     | 223.1 ft     |
| Point 84 | 31.9 ft     | 219.08 ft    |

## Regions

|              | Material   | Points   | Area                       |
|--------------|--|--|----------------------------|
| Region<br>1  | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 1,2,52,3,43  | 1,263.5<br>ft <sup>2</sup> |
| Region<br>2  | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 52,2,50,51,56,57,53,5,60,6,47,3                          | 2,656.9<br>ft <sup>2</sup> |
| Region<br>3  | Gravel Borrow  | 9,18,8,7,10  | 214.55<br>ft <sup>2</sup>  |
| Region<br>4  | SEW Wall   | 38,65,11,55,68,74,71,37                                  | 127 ft²                    |
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel                                  | 8,16,17,18   | 31.556<br>ft <sup>2</sup>  |
| Region<br>6  | ESU 2A Very Loose to Loose<br>Sand/Gravel                        | 18,17,14,19,84,20,9                                      | 115.05<br>ft <sup>2</sup>  |
| Region<br>7  | Forward Compatible Wall  | 38,37,62,64  | 38.52<br>ft <sup>2</sup>   |
| Region<br>8  | Lightweight EPS  | 14,19,84,83,66,63,62,37,71,77                            | 132.58<br>ft <sup>2</sup>  |
| Region<br>9  | ESU 2B Medium Dense Sand/Gravel                                  | 22,42,59,40,60,5,21,13                                   | 332.37<br>ft <sup>2</sup>  |
| Region<br>10 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 44,54,45,1,43,3,47,48                                    | 4,704.7<br>ft <sup>2</sup> |
| Region<br>11 | ESU 2B Medium Dense Sand/Gravel (Residual Strength)              | 41,46,48,47,6,60,40                                      | 992.46<br>ft²              |
| Region<br>12 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 56,51,50,4,7,8,16,15,67,69,79,70,13,21,5,53,57           | 1,417.8<br>ft <sup>2</sup> |
| Region<br>13 | ESU 2A Very Loose to Loose<br>Sand/Gravel                        | 34,33,32,31,30,29,28,27,26,25,24,23,40,59,42,22,12,58,39 | 1,656.2<br>ft <sup>2</sup> |
| Region<br>14 | ESU 2A Very Loose to Loose<br>Sand/Gravel                        | 40,23,61,46,41   | 379.99<br>ft <sup>2</sup>  |
| Region<br>15 | Lightweight EPS  | 63,36,62   | 20.093<br>ft <sup>2</sup>  |
| Region<br>16 | Forward Compatible Wall  | 36,35,64,62  | 51.88<br>ft <sup>2</sup>   |
| Region<br>17 |  | 64,65,38   | 7.8889<br>ft <sup>2</sup>  |
| Region       | ESU 4B Dense to Very Dense                                       |  |                            |

| 18           | <br>  Sand/Gravel                         | 15,16,81,69,67          | 28.5 ft <sup>2</sup>       |
|--------------|---|-------------------------|----------------------------|
| Region<br>19 | SEW Wall                                  | 72,76,22,13             | 11.692<br>ft <sup>2</sup>  |
| Region<br>20 | SEW Wall                                  | 70,72,13                | 2.9375<br>ft <sup>2</sup>  |
| Region<br>21 | SEW Wall                                  | 70,79,78,75,72          | 19.415<br>ft²              |
| Region<br>22 | Gravel Borrow                             | 81,75,78,79,69          | 11.991<br>ft <sup>2</sup>  |
| Region<br>23 | Gravel Borrow                             | 49,75,81,80             | 7.7095<br>ft <sup>2</sup>  |
| Region<br>24 | SEW Wall                                  | 49,76,72,75             | 4.002<br>ft <sup>2</sup>   |
| Region<br>25 | SEW Wall                                  | 73,76,49                | 0.43333<br>ft <sup>2</sup> |
| Region<br>26 | SEW Wall                                  | 76,73,74,68,55,58,12,22 | 163.72<br>ft²              |
| Region<br>27 | ESU 2B Medium Dense Sand/Gravel           | 80,81,16,17             | 6 ft²                      |
| Region<br>28 | Gravel Borrow                             | 74,82,77                | 10.23<br>ft <sup>2</sup>   |
| Region<br>29 | Gravel Borrow                             | 77,71,74                | 10.23<br>ft <sup>2</sup>   |
| Region<br>30 | ESU 2A Very Loose to Loose<br>Sand/Gravel | 77,82,80,17,14          | 27.75<br>ft <sup>2</sup>   |
| Region<br>31 | Gravel Borrow                             | 73,49,80,82,74          | 54.19<br>ft <sup>2</sup>   |
| Region<br>32 | Common Borrow                             | 20,83,84                | 12.06<br>ft²               |
| Region<br>33 |   | 55,39,58                | 11.1 ft²                   |

### **Slip Results**

Slip Surfaces Analysed: 3665 of 16926 converged

## **Current Slip Surface**

Slip Surface: 1,021 Factor of Safety: 1.7 Volume: 1,418.8147 ft<sup>3</sup> Weight: 154,412.22 lbf

Resisting Moment: 8,617,457.5 lbf·ft Activating Moment: 5,105,467.4 lbf·ft

Resisting Force: 101,951.55 lbf Activating Force: 60,409.582 lbf Slip Rank: 1 of 16,926 slip surfaces Exit: (-38.240876, 182.19377) ft Entry: (46.166189, 223.23991) ft

Radius: 72.22526 ft

Center: (-20.046856, 252.08988) ft

## **Slip Slices**

|             | Х                | Υ               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material                                |
|-------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|--|
| Slice<br>1  | -37.770438<br>ft | 182.07469<br>ft | -184.85613<br>psf | 21.235998<br>psf         | 13.269724<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>2  | -35.55 ft        | 181.57087<br>ft | -183.87843<br>psf | 113.49 psf               | 70.916425<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>3  | -32.05 ft        | 180.89112<br>ft | -181.90896<br>psf | 252.14037<br>psf         | 157.55479<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>4  | -28.908333<br>ft | 180.42402<br>ft | -179.6982<br>psf  | 429.91684<br>psf         | 268.64186<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>5  | -26.125 ft       | 180.13438<br>ft | -179.0209<br>psf  | 647.57948<br>psf         | 404.65257<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>6  | -23.341667<br>ft | 179.95326<br>ft | -180.28457<br>psf | 850.16156<br>psf         | 531.2399<br>psf        | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>7  | -20.558333<br>ft | 179.87984<br>ft | -178.0415<br>psf  | 1,030.5615<br>psf        | 643.96629<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>8  | -17.775 ft       | 179.91379<br>ft | -180.73923<br>psf | 1,183.0556<br>psf        | 739.25519<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>9  | -14.991667<br>ft | 180.05526<br>ft | -190.1224<br>psf  | 1,303.9219<br>psf        | 814.78086<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>10 | -12.326997<br>ft | 180.28979<br>ft | -254.29877<br>psf | 1,419.4794<br>psf        | 886.9892<br>psf        | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>11 | -9.780992<br>ft  | 180.60949<br>ft | -368.84527<br>psf | 1,531.1769<br>psf        | 956.78553<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>12 | -7.2539947<br>ft | 181.01803<br>ft | -403.69014<br>psf | 1,613.3893<br>psf        | 1,008.1575<br>psf      | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>13 | -5.5625 ft       | 181.33331<br>ft | -377.40593<br>psf | 1,623.691<br>psf         | 1,014.5948<br>psf      | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>14 | -3.84375 ft      | 181.71788<br>ft | -351.63392<br>psf | 1,532.2438<br>psf        | 957.45219<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>15 | -1.28125 ft      | 182.35768<br>ft | -313.21625<br>psf | 1,390.1552<br>psf        | 868.66536<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>16 | 0.6775 ft        | 182.90542<br>ft | -284.61599<br>psf | 3,373.7822<br>psf        | 2,108.1731<br>psf      | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense                       |

|             |                 |                 |                   |                   |                   |       |       | Sand/Gravel                                  |
|-------------|-----------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>17 | 3.3141258<br>ft | 183.77835<br>ft | -248.89977<br>psf | 3,133.1456<br>psf | 1,957.8067<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>18 | 5.7064208<br>ft | 184.61365<br>ft | -212.44256<br>psf | 3,059.2962<br>psf | 2,852.8399<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>19 | 6.569795 ft     | 184.94952<br>ft | -194.40709<br>psf | 2,977.0591<br>psf | 2,776.1526<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>20 | 7.95 ft         | 185.5196<br>ft  | -171.22478<br>psf | 4,125.3393<br>psf | 3,846.9412<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>21 | 8.95 ft         | 185.94105<br>ft | -152.7832<br>psf  | 4,006.651<br>psf  | 3,736.2625<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>22 | 11 ft           | 186.9157<br>ft  | -105.78401<br>psf | 3,862.4923<br>psf | 3,601.8323<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>23 | 14 ft           | 188.40304<br>ft | -72.253284<br>psf | 3,502.0013<br>psf | 3,265.669<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>24 | 15.25 ft        | 189.07767<br>ft | -63.880304<br>psf | 2,269.5402<br>psf | 2,116.3804<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>25 | 16 ft           | 189.5057<br>ft  | -59.51264<br>psf  | 2,190.7231<br>psf | 2,042.8823<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>26 | 17.50351 ft     | 190.40457<br>ft | -50.815986<br>psf | 2,035.6018<br>psf | 1,898.2294<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>27 | 19.25351 ft     | 191.49963<br>ft | -42.857717<br>psf | 1,861.73<br>psf   | 1,736.0913<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>28 | 20.75 ft        | 192.49727<br>ft | -37.69367<br>psf  | 1,734.3521<br>psf | 1,355.0244<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>29 | 22.75 ft        | 193.93054<br>ft | -32.288402<br>psf | 1,452.1565<br>psf | 1,354.1578<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>30 | 24.25 ft        | 195.04449<br>ft | -28.88961<br>psf  | 1,409.7894<br>psf | 1,314.6499<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>31 | 25.2 ft         | 195.80131<br>ft | -27.371515<br>psf | 1,383.0118<br>psf | 1,289.6793<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>32 | 25.95 ft        | 196.40529<br>ft | -26.439209<br>psf | 1,362.8862<br>psf | 1,270.9119<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>33 | 26.3 ft         | 196.6976<br>ft  | -26.013331<br>psf | 1,352.9229<br>psf | 1,261.621<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>34 | 27.925 ft       | 198.1265<br>ft  | -25.620539<br>psf | 1,298.1662<br>psf | 1,210.5596<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |

| Slice<br>35 | 30.575 ft       | 200.60723<br>ft | -27.532663<br>psf | 1,204.8632<br>psf | 1,123.5531<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
|-------------|-----------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>36 | 33.4 ft         | 203.56213<br>ft | -35.750746<br>psf | 1,292.3702<br>psf | 1,205.1547<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>37 | 36.4 ft         | 207.096 ft      | -57.336715<br>psf | 1,030.4465<br>psf | 960.90691<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>38 | 38.65 ft        | 210.02434<br>ft | -90.418054<br>psf | 833.05742<br>psf  | 776.83861<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>39 | 39.8 ft         | 211.66302<br>ft | -120.70681<br>psf | 729.37405<br>psf  | 680.15231<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>40 | 41 ft           | 213.52142<br>ft | -170.16956<br>psf | 626.26025<br>psf  | 583.99713<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>41 | 42.19125 ft     | 215.45231<br>ft | -237.66118<br>psf | 526.13212<br>psf  | 490.62614<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>42 | 43.581761<br>ft | 217.98102<br>ft | -363.35006<br>psf | 370.90105<br>psf  | 345.87083<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>43 | 45.373605<br>ft | 221.54251<br>ft | 0 psf             | 167.80031<br>psf  | 131.09997<br>psf  | 0 psf | 0 psf | Gravel Borrow                                |

# 2A.1 Global - Static (Spencer)

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### **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 318 Date: 01/13/2022 Time: 03:58:28 PM

Tool Version: 11.1.1.22085

File Name: Wall 05.85L-B Sta 2+60\_FC Wall (lightweight fill).gsz Directory: P:\0\0180366\01\Analysis\Wall 05.85L-B\22-01-13\

Last Solved Date: 01/13/2022 Last Solved Time: 04:01:16 PM

### **Project Settings**

Unit System: U.S. Customary Units

## **Analysis Settings**

### 2A.1 Global - Static (Spencer)

Kind: SLOPE/W

Analysis Type: Spencer

Settings

PWP Conditions from: Piezometric Line

Apply Phreatic Correction: No Use Staged Rapid Drawdown: No

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit

Critical slip surfaces saved: 1

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

**Factor of Safety Convergence Settings** 

Maximum Number of Iterations: 100

Tolerable difference in F of S: 0.001

**Solution Settings** 

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

#### **Materials**

#### **ESU 1B Medium Dense to Very Dense Coarse-Grained Fill**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 41 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **ESU 2B Medium Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 115 pcf Effective Cohesion: 0 psf Effective Friction Angle: 34 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **SEW Wall**

Material Model: High Strength

Unit Weight: 130 pcf
Pore Water Pressure
Piezometric Line: 1

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf

Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 42 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### Slip Surface Entry and Exit

Left Type: Range

Left-Zone Left Coordinate: (-40.9, 191.85458) ft Left-Zone Right Coordinate: (-0.9, 199.92697) ft

Left-Zone Increment: 20

Right Type: Range

Right-Zone Left Coordinate: (20.000001, 228.81169) ft

Right-Zone Right Coordinate: (65, 233.85753) ft

Right-Zone Increment: 25
Radius Increments: 20

### **Slip Surface Limits**

Left Coordinate: (-80, 186.2) ft Right Coordinate: (80, 234.2) ft

### **Piezometric Lines**

#### Piezometric Line 1

Coordinates

|               | X         | Υ          |
|---------------|-----------|------------|
| Coordinate 1  | -48.3 ft  | 180 ft     |
| Coordinate 2  | -4.1 ft   | 190.1 ft   |
| Coordinate 3  | 11.7 ft   | 193.8 ft   |
| Coordinate 4  | 17.165 ft | 194.87 ft  |
| Coordinate 5  | 24.11 ft  | 196.755 ft |
| Coordinate 6  | 29.52 ft  | 198.8 ft   |
| Coordinate 7  | 32.23 ft  | 199.83 ft  |
| Coordinate 8  | 60.885 ft | 211.35 ft  |
| Coordinate 9  | 70.775 ft | 215.12 ft  |
| Coordinate 10 | 74.125 ft | 216.15 ft  |
| Coordinate 11 | 80 ft     | 217.365 ft |

## **Surcharge Loads**

### **Surcharge Load 1**

Surcharge (Unit Weight): 250 pcf

Direction: Vertical

#### Coordinates

| Х       | Y        |  |  |
|---------|----------|--|--|
| 43 ft   | 234.5 ft |  |  |
| 45 ft   | 234.5 ft |  |  |
| 58.1 ft | 234.7 ft |  |  |
| 80 ft   | 235.2 ft |  |  |

## **Geometry**

Name: 2. Global Stability

**Settings** 

View: 2D

Element Thickness: 1 ft

#### **Points**

|          | Х        | Υ        |
|----------|----------|----------|
| Point 1  | 80 ft    | 199.4 ft |
| Point 2  | 58 ft    | 196.6 ft |
| Point 3  | 37.6 ft  | 191.9 ft |
| Point 4  | 42.1 ft  | 180 ft   |
| Point 5  | 80 ft    | 180 ft   |
| Point 6  | 80 ft    | 226 ft   |
| Point 7  | 58 ft    | 225.3 ft |
| Point 8  | 29.8 ft  | 195 ft   |
| Point 9  | 11.7 ft  | 193.8 ft |
| Point 10 | -48.3 ft | 180 ft   |
|          |          |          |

| مد د د د |          | 00456     |
|----------|----------|-----------|
| Point 11 | 80 ft    | 234.2 ft  |
| Point 12 | 58.1 ft  | 233.7 ft  |
| Point 13 | 26.5 ft  | 214.1 ft  |
| Point 14 | -10.8 ft | 197 ft    |
| Point 15 | -18.3 ft | 195.3 ft  |
| Point 16 | -21.1 ft | 194.7 ft  |
| Point 17 | -24.4 ft | 193.6 ft  |
| Point 18 | -32.1 ft | 193.1 ft  |
| Point 19 | -36.6 ft | 192.3 ft  |
| Point 20 | -61.7 ft | 189.7 ft  |
| Point 21 | -65.4 ft | 189.3 ft  |
| Point 22 | -73.2 ft | 188 ft    |
| Point 23 | -80 ft   | 186.2 ft  |
| Point 24 | -80 ft   | 180 ft    |
| Point 25 | -4.1 ft  | 190.1 ft  |
| Point 26 | 32 ft    | 197.4 ft  |
| Point 27 | -0.9 ft  | 219.4 ft  |
| Point 28 | -0.9 ft  | 196.3 ft  |
| Point 29 | -4.9 ft  | 199.8 ft  |
| Point 30 | -0.9 ft  | 199.8 ft  |
| Point 31 | -0.9 ft  | 199.4 ft  |
| Point 32 | 17.1 ft  | 196.3 ft  |
| Point 33 | 15.6 ft  | 219.4 ft  |
| Point 34 | 11.1 ft  | 196.3 ft  |
| Point 35 | 17.1 ft  | 214.2 ft  |
| Point 36 | 45 ft    | 233.5 ft  |
| Point 37 | 37.1 ft  | 228.2 ft  |
| Point 38 | 29.4 ft  | 222.3 ft  |
| Point 39 | 29.5 ft  | 233.5 ft  |
| Point 40 | 1.5 ft   | 219.4 ft  |
| Point 41 | 31.5 ft  | 233.5 ft  |
| Point 42 | 6.1 ft   | 233.5 ft  |
| Point 43 | 14.1 ft  | 233.5 ft  |
| Point 44 | 14.1 ft  | 219.4 ft  |
| Point 45 | 6.1 ft   | 219.4 ft  |
| Point 46 | 14.1 ft  | 225.9 ft  |
| Point 47 | 6.1 ft   | 221.74 ft |
| Point 48 | 15.6 ft  | 214.2 ft  |
| Point 49 | 15.6 ft  | 196.3 ft  |
| Point 50 | 17.1 ft  | 208.4 ft  |
| Point 51 | 17.1 ft  | 219.4 ft  |
| Point 52 | 6.1 ft   | 232 ft    |
| Point 53 | 14.1 ft  | 232 ft    |
| Point 54 | 39 ft    | 233.5 ft  |
| Point 55 | 39 ft    | 230.5 ft  |
|          |          |           |

## Regions

| Material | Points | Area |
|----------|--------|------|
|          |        |      |

| Region<br>1  | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 1,2,3,4,5                                       | 659.92<br>ft <sup>2</sup> |
|--------------|--|---|---------------------------|
| Region<br>2  | ESU 4B Dense to Very Dense Sand/Gravel                           | 1,6,7,26,8,9,25,10,4,3,2                        | 1,867.8<br>ft²            |
| Region<br>3  | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill        | 14,29,30,31                                     | 7.58 ft <sup>2</sup>      |
| Region<br>4  | SEW Wall   | 27,30,31,28,34,49,48,33,44,45,40                | 381.15<br>ft <sup>2</sup> |
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel                                  | 14,15,16,17,18,19,20,21,22,23,24,10,25,34,28,31 | 748.7<br>ft²              |
| Region<br>6  | ESU 2B Medium Dense Sand/Gravel                                  | 7,6,11,12,13,50,32,49,34,25,9,8,26              | 856.44<br>ft <sup>2</sup> |
| Region<br>7  | Common Borrow  | 45,44,46,47                                     | 35.36<br>ft <sup>2</sup>  |
| Region<br>8  | Common Borrow  | 36,55,51,35,38,37                               | 75.79<br>ft²              |
| Region<br>9  |  | 43,53,46,39                                     | 58.52<br>ft <sup>2</sup>  |
| Region<br>10 |  | 43,42,52,53                                     | 12 ft²                    |
| Region<br>11 | Common Borrow  | 47,40,45  | 5.382<br>ft²              |
| Region<br>12 | Gravel Borrow  | 32,50,35,48,49                                  | 26.85<br>ft²              |
| Region<br>13 | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill        | 35,50,13,12,36,37,38                            | 241.79<br>ft²             |
| Region<br>14 | Gravel Borrow  | 33,48,35,51                                     | 7.8 ft²                   |
| Region<br>15 |  | 47,46,53,52                                     | 65.44<br>ft <sup>2</sup>  |
| Region<br>16 | Common Borrow  | 41,39,46,44,33,51,55,54                         | 171.02<br>ft²             |
| Region<br>17 | Common Borrow  | 36,54,55  | 9 ft²                     |

### **Slip Results**

Slip Surfaces Analysed: 1551 of 11466 converged

## **Current Slip Surface**

Slip Surface: 2,555 Factor of Safety: 1.4 Volume: 1,414.2092 ft<sup>3</sup> Weight: 173,720.13 lbf

Resisting Moment: 7,586,863.7 lbf·ft Activating Moment: 5,287,280.8 lbf·ft

Resisting Force: 97,275.564 lbf
Activating Force: 67,817.027 lbf
Slip Rank: 1 of 11,466 slip surfaces

Exit: (-32.72383, 192.9891) ft Entry: (50.251608, 233.58018) ft

Radius: 67.426709 ft

Center: (-12.822974, 257.41205) ft

## Slip Slices

|             | X                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material                         |
|-------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|---------------------------------------|
| Slice<br>1  | -32.411915<br>ft | 192.89439<br>ft | -578.06471<br>psf | 35.98996<br>psf          | 24.275535<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>2  | -30.816667<br>ft | 192.44425<br>ft | -527.22959<br>psf | 168.3422<br>psf          | 113.54825<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>3  | -28.25 ft        | 191.78713<br>ft | -449.62762<br>psf | 330.05236<br>psf         | 222.62313<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>4  | -25.683333<br>ft | 191.23605<br>ft | -378.64246<br>psf | 449.61168<br>psf         | 303.26691<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>5  | -22.75 ft        | 190.74097<br>ft | -305.92389<br>psf | 625.52938<br>psf         | 421.92489<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>6  | -19.7 ft         | 190.35173<br>ft | -238.14544<br>psf | 796.52858<br>psf         | 537.26531<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>7  | -17.05 ft        | 190.12963<br>ft | -186.50044<br>psf | 884.36335<br>psf         | 596.51061<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>8  | -14.55 ft        | 190.01906<br>ft | -143.95418<br>psf | 946.55184<br>psf         | 638.45728<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>9  | -12.05 ft        | 190.00136<br>ft | -107.20267<br>psf | 989.48396<br>psf         | 667.41536<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>10 | -9.325 ft        | 190.09234<br>ft | -74.024233<br>psf | 1,074.0601<br>psf        | 724.4627<br>psf        | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>11 | -6.375 ft        | 190.31072<br>ft | -45.587566<br>psf | 1,190.8689<br>psf        | 803.25119<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>12 | -4.5 ft          | 190.50221<br>ft | -30.801475<br>psf | 1,224.4038<br>psf        | 825.87082<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>13 | -3.2452353<br>ft | 190.67464<br>ft | -23.366998<br>psf | 1,172.741<br>psf         | 791.02376<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>14 | -1.6452353<br>ft | 190.92259<br>ft | -15.459087<br>psf | 1,106.1046<br>psf        | 746.07699<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>15 | 0.3 ft           | 191.28602<br>ft | -9.7119652<br>psf | 3,728.8637<br>psf        | 2,515.1503<br>psf      | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense                |

|             |            |                 |                   |                   |                   |       |       | Sand/Gravel                           |
|-------------|------------|-----------------|-------------------|-------------------|-------------------|-------|-------|---------------------------------------|
| Slice<br>16 | 2.65 ft    | 191.79534<br>ft | -7.1540667<br>psf | 3,606.2622<br>psf | 2,432.4546<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>17 | 4.95 ft    | 192.38082<br>ft | -10.078507<br>psf | 3,551.2911<br>psf | 2,395.3761<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>18 | 7.35 ft    | 193.08713<br>ft | -19.081688<br>psf | 3,485.4792<br>psf | 2,350.9854<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>19 | 9.85 ft    | 193.92555<br>ft | -34.867853<br>psf | 3,408.1309<br>psf | 2,298.8133<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>20 | 11.4 ft    | 194.48745<br>ft | -47.280731<br>psf | 3,356.4002<br>psf | 2,263.9205<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>21 | 12.9 ft    | 195.09829<br>ft | -66.352671<br>psf | 3,299.4711<br>psf | 2,225.5214<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>22 | 14.85 ft   | 195.93123<br>ft | -94.504091<br>psf | 3,220.6856<br>psf | 2,172.3799<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>23 | 16.3825 ft | 196.64489<br>ft | -120.31334<br>psf | 3,148.7949<br>psf | 2,460.1082<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>24 | 18.3225 ft | 197.62395<br>ft | -152.2424<br>psf  | 2,870.5167<br>psf | 1,936.1879<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>25 | 20.6375 ft | 198.88872<br>ft | -191.95627<br>psf | 2,753.5574<br>psf | 1,857.2979<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>26 | 22.9525 ft | 200.27527<br>ft | -239.26898<br>psf | 2,628.0994<br>psf | 1,772.6754<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>27 | 25.305 ft  | 201.81961<br>ft | -287.84498<br>psf | 2,491.6453<br>psf | 1,680.636<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>28 | 28 ft      | 203.78098<br>ft | -346.66576<br>psf | 2,322.9323<br>psf | 1,566.8376<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>29 | 29.51 ft   | 204.93081<br>ft | -382.79865<br>psf | 2,226.4936<br>psf | 1,501.7889<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>30 | 30.51 ft   | 205.76958<br>ft | -411.42266<br>psf | 2,120.1432<br>psf | 1,430.0546<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>31 | 31.865 ft  | 206.92335<br>ft | -451.28187<br>psf | 1,978.975<br>psf  | 1,334.8355<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>32 | 33.4475 ft | 208.39572<br>ft | -503.95806<br>psf | 1,809.6168<br>psf | 1,220.602<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>33 | 35.8825 ft | 210.81767<br>ft | -594.00316<br>psf | 1,550.9471<br>psf | 1,046.1271<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |

| Slice<br>34 | 38.05 ft        | 213.18304<br>ft | -687.22762<br>psf  | 1,319.9733<br>psf | 890.33322<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                  |
|-------------|-----------------|-----------------|--------------------|-------------------|------------------|-------|-------|--|
| Slice<br>35 | 41 ft           | 216.93519<br>ft | -847.35724<br>psf  | 994.04806<br>psf  | 670.49389<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                  |
| Slice<br>36 | 44 ft           | 221.16217<br>ft | -1,035.8619<br>psf | 786.76265<br>psf  | 530.67811<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                  |
| Slice<br>37 | 46.190983<br>ft | 224.89091<br>ft | -1,213.5712<br>psf | 536.90588<br>psf  | 362.14759<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                  |
| Slice<br>38 | 48.816787<br>ft | 230.31614<br>ft | -1,486.2341<br>psf | 209.84439<br>psf  | 182.41494<br>psf | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill |

# 2A.2 Global - Static (M-P)

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## **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 318 Date: 01/13/2022 Time: 03:58:28 PM

Tool Version: 11.1.1.22085

File Name: Wall 05.85L-B Sta 2+60\_FC Wall (lightweight fill).gsz Directory: P:\0\0180366\01\Analysis\Wall 05.85L-B\22-01-13\

Last Solved Date: 01/13/2022 Last Solved Time: 04:01:18 PM

## **Project Settings**

Unit System: U.S. Customary Units

# **Analysis Settings**

## 2A.2 Global - Static (M-P)

Kind: SLOPE/W

Analysis Type: Morgenstern-Price

Settings

**Side Function** 

Interslice force function option: Half-Sine

PWP Conditions from: Piezometric Line

Apply Phreatic Correction: No
Use Staged Rapid Drawdown: No
Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 1

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

**Factor of Safety Convergence Settings** 

Maximum Number of Iterations: 100
Tolerable difference in F of S: 0.001

**Solution Settings** 

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

### **Materials**

### **ESU 1B Medium Dense to Very Dense Coarse-Grained Fill**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 41 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

## **ESU 2B Medium Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 115 pcf Effective Cohesion: 0 psf Effective Friction Angle: 34 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **SEW Wall**

Material Model: High Strength

Unit Weight: 130 pcf
Pore Water Pressure
Piezometric Line: 1

**Gravel Borrow** 

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 42 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

# **Slip Surface Entry and Exit**

Left Type: Range

Left-Zone Left Coordinate: (-40.9, 191.85458) ft Left-Zone Right Coordinate: (-0.9, 199.92697) ft

Left-Zone Increment: 20

Right Type: Range

Right-Zone Left Coordinate: (20.000001, 228.81169) ft

Right-Zone Right Coordinate: (65, 233.85753) ft

Right-Zone Increment: 25 Radius Increments: 20

# **Slip Surface Limits**

Left Coordinate: (-80, 186.2) ft Right Coordinate: (80, 234.2) ft

## **Piezometric Lines**

#### Piezometric Line 1

### Coordinates

|               | Х         | Υ          |
|---------------|-----------|------------|
| Coordinate 1  | -48.3 ft  | 180 ft     |
| Coordinate 2  | -4.1 ft   | 190.1 ft   |
| Coordinate 3  | 11.7 ft   | 193.8 ft   |
| Coordinate 4  | 17.165 ft | 194.87 ft  |
| Coordinate 5  | 24.11 ft  | 196.755 ft |
| Coordinate 6  | 29.52 ft  | 198.8 ft   |
| Coordinate 7  | 32.23 ft  | 199.83 ft  |
| Coordinate 8  | 60.885 ft | 211.35 ft  |
| Coordinate 9  | 70.775 ft | 215.12 ft  |
| Coordinate 10 | 74.125 ft | 216.15 ft  |
| Coordinate 11 | 80 ft     | 217.365 ft |

# **Surcharge Loads**

## **Surcharge Load 1**

Surcharge (Unit Weight): 250 pcf

Direction: Vertical

#### Coordinates

| Х       | Υ        |
|---------|----------|
| 43 ft   | 234.5 ft |
| 45 ft   | 234.5 ft |
| 58.1 ft | 234.7 ft |
| 80 ft   | 235.2 ft |

# **Geometry**

Name: 2. Global Stability

Settings

View: 2D

Element Thickness: 1 ft

### **Points**

|         | Х       | Υ        |
|---------|---------|----------|
| Point 1 | 80 ft   | 199.4 ft |
| Point 2 | 58 ft   | 196.6 ft |
| Point 3 | 37.6 ft | 191.9 ft |
| Point 4 | 42.1 ft | 180 ft   |
| Point 5 | 80 ft   | 180 ft   |
| Point 6 | 80 ft   | 226 ft   |
| Point 7 | 58 ft   | 225.3 ft |
| Point 8 | 29.8 ft | 195 ft   |
| Point 9 | 11.7 ft | 193.8 ft |
|         |         |          |

| Point 10 | -48.3 ft | 180 ft    |
|----------|----------|-----------|
| Point 11 | 80 ft    | 234.2 ft  |
| Point 12 | 58.1 ft  | 233.7 ft  |
| Point 13 | 26.5 ft  | 214.1 ft  |
| Point 14 | -10.8 ft | 197 ft    |
| Point 15 | -18.3 ft | 195.3 ft  |
| Point 16 | -21.1 ft | 194.7 ft  |
| Point 17 | -24.4 ft | 193.6 ft  |
| Point 18 | -32.1 ft | 193.1 ft  |
| Point 19 | -36.6 ft | 192.3 ft  |
| Point 20 | -61.7 ft | 189.7 ft  |
| Point 21 | -65.4 ft | 189.3 ft  |
| Point 22 | -73.2 ft | 188 ft    |
| Point 23 | -80 ft   | 186.2 ft  |
| Point 24 | -80 ft   | 180 ft    |
| Point 25 | -4.1 ft  | 190.1 ft  |
| Point 26 | 32 ft    | 197.4 ft  |
| Point 27 | -0.9 ft  | 219.4 ft  |
| Point 28 | -0.9 ft  | 196.3 ft  |
| Point 29 | -4.9 ft  | 199.8 ft  |
| Point 30 | -0.9 ft  | 199.8 ft  |
| Point 31 | -0.9 ft  | 199.4 ft  |
| Point 32 | 17.1 ft  | 196.3 ft  |
| Point 33 | 15.6 ft  | 219.4 ft  |
| Point 34 | 11.1 ft  | 196.3 ft  |
| Point 35 | 17.1 ft  | 214.2 ft  |
| Point 36 | 45 ft    | 233.5 ft  |
| Point 37 | 37.1 ft  | 228.2 ft  |
| Point 38 | 29.4 ft  | 222.3 ft  |
| Point 39 | 29.5 ft  | 233.5 ft  |
| Point 40 | 1.5 ft   | 219.4 ft  |
| Point 41 | 31.5 ft  | 233.5 ft  |
| Point 42 | 6.1 ft   | 233.5 ft  |
| Point 43 | 14.1 ft  | 233.5 ft  |
| Point 44 | 14.1 ft  | 219.4 ft  |
| Point 45 | 6.1 ft   | 219.4 ft  |
| Point 46 | 14.1 ft  | 225.9 ft  |
| Point 47 | 6.1 ft   | 221.74 ft |
| Point 48 | 15.6 ft  | 214.2 ft  |
| Point 49 | 15.6 ft  | 196.3 ft  |
| Point 50 | 17.1 ft  | 208.4 ft  |
| Point 51 | 17.1 ft  | 219.4 ft  |
| Point 52 | 6.1 ft   | 232 ft    |
| Point 53 | 14.1 ft  | 232 ft    |
| Point 54 | 39 ft    | 233.5 ft  |
| Point 55 | 39 ft    | 230.5 ft  |
|          |          |           |

## **Regions**

|                            | Material   | Points  | Area                       |
|----------------------------|--|---|----------------------------|
| Region<br>1                | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 1,2,3,4,5                                       | 659.92<br>ft <sup>2</sup>  |
| Region<br>2                | ESU 4B Dense to Very Dense Sand/Gravel                           | 1,6,7,26,8,9,25,10,4,3,2                        | 1,867.8<br>ft <sup>2</sup> |
| Region<br>3                | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill        | 14,29,30,31                                     | 7.58 ft <sup>2</sup>       |
| Region<br>4                | SEW Wall   | 27,30,31,28,34,49,48,33,44,45,40                | 381.15<br>ft <sup>2</sup>  |
| Region<br>5                | ESU 2B Medium Dense Sand/Gravel                                  | 14,15,16,17,18,19,20,21,22,23,24,10,25,34,28,31 | 748.7<br>ft <sup>2</sup>   |
| Region<br>6                | ESU 2B Medium Dense Sand/Gravel                                  | 7,6,11,12,13,50,32,49,34,25,9,8,26              | 856.44<br>ft <sup>2</sup>  |
| Region 7 Common Borrow     |  | 45,44,46,47                                     | 35.36<br>ft <sup>2</sup>   |
| Region<br>8                | Common Borrow  | 36,55,51,35,38,37                               |                            |
| Region<br>9                |  | 43,53,46,39                                     | 58.52<br>ft <sup>2</sup>   |
| Region<br>10               |  | 43,42,52,53                                     | 12 ft²                     |
| Region<br>11               | Common Borrow  | 47,40,45  | 5.382<br>ft <sup>2</sup>   |
| Region<br>12               | Gravel Borrow  | 32,50,35,48,49                                  | 26.85<br>ft <sup>2</sup>   |
| Region<br>13               | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill        | 35,50,13,12,36,37,38                            | 241.79<br>ft <sup>2</sup>  |
| Region<br>14               | Gravel Borrow  | 33,48,35,51                                     | 7.8 ft <sup>2</sup>        |
| Region<br>15               |  | 47,46,53,52                                     | 65.44<br>ft <sup>2</sup>   |
| Region<br>16               | Common Borrow  | 41,39,46,44,33,51,55,54                         | 171.02<br>ft <sup>2</sup>  |
| Region<br>17 Common Borrow |  | 36,54,55  | 9 ft²                      |

# **Slip Results**

Slip Surfaces Analysed: 1726 of 11466 converged

# **Current Slip Surface**

Slip Surface: 2,555 Factor of Safety: 1.4 Volume: 1,414.2092 ft<sup>3</sup> Weight: 173,720.13 lbf

Resisting Moment: 7,600,603.5 lbf·ft Activating Moment: 5,287,280.8 lbf·ft

Resisting Force: 97,347.4 lbf Activating Force: 67,744.006 lbf Slip Rank: 1 of 11,466 slip surfaces Exit: (-32.72383, 192.9891) ft Entry: (50.251608, 233.58018) ft

Radius: 67.426709 ft

Center: (-12.822974, 257.41205) ft

## **Slip Slices**

|             | X                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material                         |
|-------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|---------------------------------------|
| Slice<br>1  | -32.411915<br>ft | 192.89439<br>ft | -578.06471<br>psf | 20.408067<br>psf         | 13.765415<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>2  | -30.816667<br>ft | 192.44425<br>ft | -527.22959<br>psf | 104.73335<br>psf         | 70.643535<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>3  | -28.25 ft        | 191.78713<br>ft | -449.62762<br>psf | 232.46507<br>psf         | 156.79967<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>4  | -25.683333<br>ft | 191.23605<br>ft | -378.64246<br>psf | 354.76529<br>psf         | 239.29221<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>5  | -22.75 ft        | 190.74097<br>ft | -305.92389<br>psf | 547.95018<br>psf         | 369.59707<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>6  | -19.7 ft         | 190.35173<br>ft | -238.14544<br>psf | 762.16029<br>psf         | 514.08361<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>7  | -17.05 ft        | 190.12963<br>ft | -186.50044<br>psf | 904.20074<br>psf         | 609.8911<br>psf        | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>8  | -14.55 ft        | 190.01906<br>ft | -143.95418<br>psf | 1,015.9524<br>psf        | 685.26855<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>9  | -12.05 ft        | 190.00136<br>ft | -107.20267<br>psf | 1,100.4928<br>psf        | 742.29174<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>10 | -9.325 ft        | 190.09234<br>ft | -74.024233<br>psf | 1,216.6636<br>psf        | 820.64998<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>11 | -6.375 ft        | 190.31072<br>ft | -45.587566<br>psf | 1,352.7804<br>psf        | 912.46191<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>12 | -4.5 ft          | 190.50221<br>ft | -30.801475<br>psf | 1,389.6256<br>psf        | 937.31434<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>13 | -3.2452353<br>ft | 190.67464<br>ft | -23.366998<br>psf | 1,333.1144<br>psf        | 899.19704<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>14 | -1.6452353<br>ft | 190.92259<br>ft | -15.459087<br>psf | 1,255.3738<br>psf        | 846.7603<br>psf        | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
|             |                  |                 |                   |                          |                        |                      |                     | ESU 2B Medium                         |

| Slice<br>15 | 0.3 ft     | 191.28602<br>ft | -9.7119652<br>psf | 3,945.2118<br>psf | 2,661.079<br>psf  | 0 psf | 0 psf | Dense<br>Sand/Gravel                  |
|-------------|------------|-----------------|-------------------|-------------------|-------------------|-------|-------|---------------------------------------|
| Slice<br>16 | 2.65 ft    | 191.79534<br>ft | -7.1540667<br>psf | 3,795.1301<br>psf | 2,559.8476<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>17 | 4.95 ft    | 192.38082<br>ft | -10.078507<br>psf | 3,697.8451<br>psf | 2,494.228<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>18 | 7.35 ft    | 193.08713<br>ft | -19.081688<br>psf | 3,576.4818<br>psf | 2,412.3674<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>19 | 9.85 ft    | 193.92555<br>ft | -34.867853<br>psf | 3,436.0636<br>psf | 2,317.6542<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>20 | 11.4 ft    | 194.48745<br>ft | -47.280731<br>psf | 3,345.3873<br>psf | 2,256.4923<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>21 | 12.9 ft    | 195.09829<br>ft | -66.352671<br>psf | 3,252.1416<br>psf | 2,193.5972<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>22 | 14.85 ft   | 195.93123<br>ft | -94.504091<br>psf | 3,130.1189<br>psf | 2,111.2919<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>23 | 16.3825 ft | 196.64489<br>ft | -120.31334<br>psf | 3,047.6272<br>psf | 2,381.0673<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>24 | 18.3225 ft | 197.62395<br>ft | -152.2424<br>psf  | 2,717.8975<br>psf | 1,833.245<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>25 | 20.6375 ft | 198.88872<br>ft | -191.95627<br>psf | 2,574.8219<br>psf | 1,736.7393<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>26 | 22.9525 ft | 200.27527<br>ft | -239.26898<br>psf | 2,435.8948<br>psf | 1,643.0318<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>27 | 25.305 ft  | 201.81961<br>ft | -287.84498<br>psf | 2,299.3103<br>psf | 1,550.9044<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>28 | 28 ft      | 203.78098<br>ft | -346.66576<br>psf | 2,147.5572<br>psf | 1,448.5456<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>29 | 29.51 ft   | 204.93081<br>ft | -382.79865<br>psf | 2,066.9522<br>psf | 1,394.1769<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>30 | 30.51 ft   | 205.76958<br>ft | -411.42266<br>psf | 1,974.3681<br>psf | 1,331.7281<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>31 | 31.865 ft  | 206.92335<br>ft | -451.28187<br>psf | 1,853.5571<br>psf | 1,250.2401<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>32 | 33.4475 ft | 208.39572<br>ft | -503.95806<br>psf | 1,711.8631<br>psf | 1,154.6663<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice       |            | 210.81767       | -594.00316        | 1,499.3279        | 1,011.3094        |       |       | ESU 2B Medium                         |

| 33          | 35.8825 ft      | ft              | psf                | psf               | psf              | 0 psf | 0 psf | Dense<br>Sand/Gravel  |
|-------------|-----------------|-----------------|--------------------|-------------------|------------------|-------|-------|---|
| Slice<br>34 | 38.05 ft        | 213.18304<br>ft | -687.22762<br>psf  | 1,310.7504<br>psf | 884.11234<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                           |
| Slice<br>35 | 41 ft           | 216.93519<br>ft | -847.35724<br>psf  | 1,037.5984<br>psf | 699.86894<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                           |
| Slice<br>36 | 44 ft           | 221.16217<br>ft | -1,035.8619<br>psf | 891.13166<br>psf  | 601.0759<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                           |
| Slice<br>37 | 46.190983<br>ft | 224.89091<br>ft | -1,213.5712<br>psf | 654.26939<br>psf  | 441.31027<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                           |
| Slice<br>38 | 48.816787<br>ft | 230.31614<br>ft | -1,486.2341<br>psf | 269.81641<br>psf  | 234.54782<br>psf | 0 psf | 0 psf | ESU 1B Medium<br>Dense to Very<br>Dense Coarse-<br>Grained Fill |

# 2A.3 Global - Pseudo-Static (Spencer)

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## **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 318 Date: 01/13/2022 Time: 03:58:28 PM

Tool Version: 11.1.1.22085

File Name: Wall 05.85L-B Sta 2+60\_FC Wall (lightweight fill).gsz Directory: P:\0\0180366\01\Analysis\Wall 05.85L-B\22-01-13\

Last Solved Date: 01/13/2022 Last Solved Time: 04:01:28 PM

## **Project Settings**

Unit System: U.S. Customary Units

# **Analysis Settings**

### 2A.3 Global - Pseudo-Static (Spencer)

Kind: SLOPE/W

Analysis Type: Spencer

Settings

**PWP Conditions from: Piezometric Line** 

Apply Phreatic Correction: No Use Staged Rapid Drawdown: No

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit

Critical slip surfaces saved: 1

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

**Factor of Safety Convergence Settings** 

Maximum Number of Iterations: 100
Tolerable difference in F of S: 0.001

**Solution Settings** 

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

### **Materials**

## **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **SEW Wall**

Material Model: High Strength

Unit Weight: 130 pcf
Pore Water Pressure
Piezometric Line: 1

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

## ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 42 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

## **ESU 1B Medium Dense to Very Dense Coarse-Grained Fill (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 41°

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

## **ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 115 pcf

Effective Cohesion: 200 psf Effective Friction Angle: 34 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### **Common Borrow (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 50 psf Effective Friction Angle: 32 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

## Slip Surface Entry and Exit

Left Type: Range

Left-Zone Left Coordinate: (-40.9, 191.85458) ft Left-Zone Right Coordinate: (-0.9, 199.92697) ft

Left-Zone Increment: 20

Right Type: Range

Right-Zone Left Coordinate: (21.860569, 229.72989) ft

Right-Zone Right Coordinate: (65, 233.85753) ft

Right-Zone Increment: 25
Radius Increments: 20

# **Slip Surface Limits**

Left Coordinate: (-80, 186.2) ft Right Coordinate: (80, 234.2) ft

## **Piezometric Lines**

#### Piezometric Line 1

Coordinates

|               | X         | Υ          |
|---------------|-----------|------------|
| Coordinate 1  | -48.3 ft  | 180 ft     |
| Coordinate 2  | -4.1 ft   | 190.1 ft   |
| Coordinate 3  | 11.7 ft   | 193.8 ft   |
| Coordinate 4  | 17.165 ft | 194.87 ft  |
| Coordinate 5  | 24.11 ft  | 196.755 ft |
| Coordinate 6  | 29.52 ft  | 198.8 ft   |
| Coordinate 7  | 32.23 ft  | 199.83 ft  |
| Coordinate 8  | 60.885 ft | 211.35 ft  |
| Coordinate 9  | 70.775 ft | 215.12 ft  |
| Coordinate 10 | 74.125 ft | 216.15 ft  |
| Coordinate 11 | 80 ft     | 217.365 ft |

## **Seismic Coefficients**

Horz Seismic Coef.: 0.196

# **Surcharge Loads**

# **Surcharge Load 1**

Surcharge (Unit Weight): 125 pcf

Direction: Vertical

### **Coordinates**

| Х       | Υ        |
|---------|----------|
| 43 ft   | 234.5 ft |
| 45 ft   | 234.5 ft |
| 58.1 ft | 234.7 ft |
| 80 ft   | 235.2 ft |

# **Geometry**

Name: 2. Global Stability

Settings

View: 2D

Element Thickness: 1 ft

### **Points**

|         | Х       | Υ        |
|---------|---------|----------|
| Point 1 | 80 ft   | 199.4 ft |
| Point 2 | 58 ft   | 196.6 ft |
| Point 3 | 37.6 ft | 191.9 ft |
| Point 4 | 42.1 ft | 180 ft   |
| Point 5 | 80 ft   | 180 ft   |
| Point 6 | 80 ft   | 226 ft   |
|         |         |          |

| Point 7  | 58 ft    | 225.3 ft  |
|----------|----------|-----------|
| Point 8  | 29.8 ft  | 195 ft    |
| Point 9  | 11.7 ft  | 193.8 ft  |
| Point 10 | -48.3 ft | 180 ft    |
| Point 11 | 80 ft    | 234.2 ft  |
| Point 12 | 58.1 ft  | 233.7 ft  |
| Point 13 | 26.5 ft  | 214.1 ft  |
| Point 14 | -10.8 ft | 197 ft    |
| Point 15 | -18.3 ft | 195.3 ft  |
| Point 16 | -21.1 ft | 194.7 ft  |
| Point 17 | -24.4 ft | 193.6 ft  |
| Point 18 | -32.1 ft | 193.1 ft  |
| Point 19 | -36.6 ft | 192.3 ft  |
| Point 20 | -61.7 ft | 189.7 ft  |
| Point 21 | -65.4 ft | 189.3 ft  |
| Point 22 | -73.2 ft | 188 ft    |
| Point 23 | -80 ft   | 186.2 ft  |
| Point 24 | -80 ft   | 180 ft    |
| Point 25 | -4.1 ft  | 190.1 ft  |
| Point 26 | 32 ft    | 197.4 ft  |
| Point 27 | -0.9 ft  | 219.4 ft  |
| Point 28 | -0.9 ft  | 196.3 ft  |
| Point 29 | -4.9 ft  | 199.8 ft  |
| Point 30 | -0.9 ft  | 199.8 ft  |
| Point 31 | -0.9 ft  | 199.4 ft  |
| Point 32 | 17.1 ft  | 196.3 ft  |
| Point 33 | 15.6 ft  | 219.4 ft  |
| Point 34 | 11.1 ft  | 196.3 ft  |
| Point 35 | 17.1 ft  | 214.2 ft  |
| Point 36 | 45 ft    | 233.5 ft  |
| Point 37 | 37.1 ft  | 228.2 ft  |
| Point 38 | 29.4 ft  | 222.3 ft  |
| Point 39 | 29.5 ft  | 233.5 ft  |
| Point 40 | 1.5 ft   | 219.4 ft  |
| Point 41 | 31.5 ft  | 233.5 ft  |
| Point 42 | 6.1 ft   | 233.5 ft  |
| Point 43 | 14.1 ft  | 233.5 ft  |
| Point 44 | 14.1 ft  | 219.4 ft  |
| Point 45 | 6.1 ft   | 219.4 ft  |
| Point 46 | 14.1 ft  | 225.9 ft  |
| Point 47 | 6.1 ft   | 221.74 ft |
| Point 48 | 15.6 ft  | 214.2 ft  |
| Point 49 | 15.6 ft  | 196.3 ft  |
| Point 50 | 17.1 ft  | 208.4 ft  |
| Point 51 | 17.1 ft  | 219.4 ft  |
| Point 52 | 6.1 ft   | 232 ft    |
| Point 53 | 14.1 ft  | 232 ft    |
| Point 54 | 39 ft    | 233.5 ft  |
|          |          |           |

Point 55 | 39 ft | 230.5 ft

## **Regions**

|              | Material  | Points  | Area                       |
|--------------|---|---|----------------------------|
| Region<br>1  | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt              | 1,2,3,4,5                                       | 659.92<br>ft <sup>2</sup>  |
| Region<br>2  | ESU 4B Dense to Very Dense Sand/Gravel  | 1,6,7,26,8,9,25,10,4,3,2                        | 1,867.8<br>ft <sup>2</sup> |
| Region<br>3  | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill (Apparent Cohesion) | 14,29,30,31                                     | 7.58 ft <sup>2</sup>       |
| Region<br>4  | SEW Wall  | 27,30,31,28,34,49,48,33,44,45,40                | 381.15<br>ft <sup>2</sup>  |
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                           | 14,15,16,17,18,19,20,21,22,23,24,10,25,34,28,31 | 748.7<br>ft <sup>2</sup>   |
| Region<br>6  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                           | 7,6,11,12,13,50,32,49,34,25,9,8,26              | 856.44<br>ft <sup>2</sup>  |
| Region<br>7  | Common Borrow (Apparent Cohesion)   | 45,44,46,47                                     | 35.36<br>ft <sup>2</sup>   |
| Region<br>8  | Common Borrow (Apparent Cohesion)   | 36,55,51,35,38,37                               | 75.79<br>ft²               |
| Region<br>9  |   | 43,53,46,39                                     | 58.52<br>ft <sup>2</sup>   |
| Region<br>10 |   | 43,42,52,53                                     | 12 ft²                     |
| Region<br>11 | Common Borrow (Apparent Cohesion)   | 47,40,45  | 5.382<br>ft <sup>2</sup>   |
| Region<br>12 | Gravel Borrow   | 32,50,35,48,49                                  | 26.85<br>ft <sup>2</sup>   |
| Region<br>13 | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill (Apparent Cohesion) | 35,50,13,12,36,37,38                            | 241.79<br>ft <sup>2</sup>  |
| Region<br>14 | Gravel Borrow   | 33,48,35,51                                     | 7.8 ft <sup>2</sup>        |
| Region<br>15 |   | 47,46,53,52                                     | 65.44<br>ft <sup>2</sup>   |
| Region<br>16 | Common Borrow (Apparent Cohesion)   | 41,39,46,44,33,51,55,54                         | 171.02<br>ft <sup>2</sup>  |
| Region<br>17 | Common Borrow (Apparent Cohesion)   | 36,54,55  | 9 ft²                      |

# **Slip Results**

Slip Surfaces Analysed: 1204 of 11466 converged

# **Current Slip Surface**

Slip Surface: 2,029 Factor of Safety: 1.3 Volume: 1,472.3511 ft<sup>3</sup> Weight: 180,599.67 lbf

Resisting Moment: 9,582,424.3 lbf·ft

Activating Moment: 7,661,581.3 lbf·ft

Resisting Force: 115,203.84 lbf Activating Force: 92,086.539 lbf Slip Rank: 1 of 11,466 slip surfaces Exit: (-34.756941, 192.62766) ft Entry: (52.676158, 233.61719) ft

Radius: 73.426209 ft

Center: (-14.522295, 263.21071) ft

# **Slip Slices**

|            | x                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material   |
|------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|---|
| Slice<br>1 | -33.42847<br>ft  | 192.27359<br>ft | -553.82155<br>psf | 707.30569<br>psf         | 477.08371<br>psf       | 200 psf              | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>2 | -30.816667<br>ft | 191.6274<br>ft  | -476.25824<br>psf | 879.27764<br>psf         | 593.08025<br>psf       | 200 psf              | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>3 | -28.25 ft        | 191.091 ft      | -406.18922<br>psf | 945.72893<br>psf         | 637.90222<br>psf       | 200 psf              | 0 psf               | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>4 | -25.683333<br>ft | 190.64933<br>ft | -342.03114<br>psf | 976.60911<br>psf         | 658.73116<br>psf       | 200 psf              | 0 psf               | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>5 | -22.75 ft        | 190.26582<br>ft | -276.27452<br>psf | 1,071.5176<br>psf        | 722.74776<br>psf       | 200 psf              | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>6 | -19.7 ft         | 189.98073<br>ft | -214.99513<br>psf | 1,166.1583<br>psf        | 786.58371<br>psf       | 200 psf              | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>7 | -17.05 ft        | 189.83868<br>ft | -168.34534<br>psf | 1,190.1523<br>psf        | 802.76786<br>psf       | 200 psf              | 0 psf               | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>8 | -14.55 ft        | 189.79514<br>ft | -129.98171<br>psf | 1,197.8351<br>psf        | 807.94999<br>psf       | 200 psf              | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |

| Slice<br>9  | -12.05 ft        | 189.83679<br>ft | -96.933383<br>psf | 1,191.6619<br>psf | 803.78611<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
|-------------|------------------|-----------------|-------------------|-------------------|-------------------|---------|-------|---|
| Slice<br>10 | -9.325 ft        | 189.9836<br>ft  | -67.238796<br>psf | 1,228.6053<br>psf | 828.70474<br>psf  | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>11 | -6.375 ft        | 190.253 ft      | -41.986049<br>psf | 1,297.4536<br>psf | 875.14353<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>12 | -4.5 ft          | 190.47283<br>ft | -28.968148<br>psf | 1,303.1065<br>psf | 878.95641<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>13 | -3.2527955<br>ft | 190.65954<br>ft | -22.535558<br>psf | 1,237.1528<br>psf | 834.4701<br>psf   | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>14 | -1.6527955<br>ft | 190.92517<br>ft | -15.730192<br>psf | 1,154.1055<br>psf | 778.45399<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>15 | 0.3 ft           | 191.30656<br>ft | -10.993582<br>psf | 3,608.7289<br>psf | 2,434.1184<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>16 | 2.65 ft          | 191.83059<br>ft | -9.3532554<br>psf | 3,444.0982<br>psf | 2,323.0736<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>17 | 4.95 ft          | 192.42359<br>ft | -12.747745<br>psf | 3,349.6031<br>psf | 2,259.3358<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>18 | 7.35 ft          | 193.13007<br>ft | -21.761226<br>psf | 3,248.2018<br>psf | 2,190.9398<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>19 | 9.85 ft          | 193.96012<br>ft | -37.025116<br>psf | 3,139.5522<br>psf | 2,117.6547<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |

| Slice<br>20 | 11.4 ft     | 194.51325<br>ft | -48.890895<br>psf | 3,071.116<br>psf  | 2,071.4939<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
|-------------|-------------|-----------------|-------------------|-------------------|-------------------|---------|-------|---|
| Slice<br>21 | 12.9 ft     | 195.10966<br>ft | -67.062023<br>psf | 3,000.5369<br>psf | 2,023.8877<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>22 | 14.85 ft    | 195.92024<br>ft | -93.818311<br>psf | 2,906.8082<br>psf | 1,960.6669<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>23 | 15.65809 ft | 196.27381<br>ft | -106.00813<br>psf | 2,866.1545<br>psf | 1,933.2456<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>24 | 16.44059 ft | 196.63692<br>ft | -119.10598<br>psf | 2,838.0823<br>psf | 2,217.3529<br>psf | 0 psf   | 0 psf | Gravel Borrow   |
| Slice<br>25 | 18.90125 ft | 197.86186<br>ft | -157.28615<br>psf | 2,529.8275<br>psf | 1,706.3902<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>26 | 22.37375 ft | 199.7595<br>ft  | -216.88657<br>psf | 2,344.0122<br>psf | 1,581.0562<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>27 | 25.305 ft   | 201.54085<br>ft | -270.45014<br>psf | 2,181.7896<br>psf | 1,471.6357<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>28 | 28 ft       | 203.37864<br>ft | -321.56009<br>psf | 2,024.3266<br>psf | 1,365.4255<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>29 | 29.51 ft    | 204.45218<br>ft | -352.93164<br>psf | 1,936.1394<br>psf | 1,305.9425<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>30 | 30.51 ft    | 205.22856<br>ft | -377.66276<br>psf | 1,842.5701<br>psf | 1,242.8292<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice       | 31.865 ft   | 206.29493       | -412.0684         | 1,719.1526        | 1,159.5831        | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                           |

| 70a1 - 1 SCC | ido-static (spence | 1)              |                    |                   |                   |         |       |  |
|--------------|--------------------|-----------------|--------------------|-------------------|-------------------|---------|-------|--|
| 31           |                    | ft              | psf                | psf               | psf               |         |       | (Apparent Cohesion)  |
| Slice<br>32  | 33.4475 ft         | 207.64345<br>ft | -457.01677<br>psf  | 1,573.4456<br>psf | 1,061.3024<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                        |
| Slice<br>33  | 35.8825 ft         | 209.84442<br>ft | -533.27235<br>psf  | 1,354.1603<br>psf | 913.39265<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                        |
| Slice<br>34  | 38.05 ft           | 211.96903<br>ft | -611.47318<br>psf  | 1,161.8184<br>psf | 783.65642<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                        |
| Slice<br>35  | 41 ft              | 215.25948<br>ft | -742.79274<br>psf  | 897.48883<br>psf  | 605.36386<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                        |
| Slice<br>36  | 44 ft              | 218.89587<br>ft | -894.44424<br>psf  | 698.70246<br>psf  | 471.28076<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                        |
| Slice<br>37  | 46.352659<br>ft    | 222.22556<br>ft | -1,043.1979<br>psf | 491.90271<br>psf  | 331.79256<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                        |
| Slice<br>38  | 49.057978<br>ft    | 226.58265<br>ft | -1,247.2139<br>psf | 260.81775<br>psf  | 175.92379<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                        |
| Slice<br>39  | 51.543398<br>ft    | 231.27392<br>ft | -1,477.5989<br>psf | 81.431429<br>psf  | 70.787261<br>psf  | 100 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill (Apparent Cohesion) |

# 2A.4 Global - Pseudo-Static (M-P)

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## **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 318 Date: 01/13/2022 Time: 03:58:28 PM

Tool Version: 11.1.1.22085

File Name: Wall 05.85L-B Sta 2+60\_FC Wall (lightweight fill).gsz Directory: P:\0\0180366\01\Analysis\Wall 05.85L-B\22-01-13\

Last Solved Date: 01/13/2022 Last Solved Time: 04:01:32 PM

## **Project Settings**

Unit System: U.S. Customary Units

# **Analysis Settings**

### 2A.4 Global - Pseudo-Static (M-P)

Kind: SLOPE/W

Analysis Type: Morgenstern-Price

Settings

**Side Function** 

Interslice force function option: Half-Sine

PWP Conditions from: Piezometric Line

Apply Phreatic Correction: No
Use Staged Rapid Drawdown: No
Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 1

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

**Factor of Safety Convergence Settings** 

Maximum Number of Iterations: 100
Tolerable difference in F of S: 0.001

**Solution Settings** 

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

## **Materials**

### **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **SEW Wall**

Material Model: High Strength

Unit Weight: 130 pcf
Pore Water Pressure
Piezometric Line: 1

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

## ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 42 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

## **ESU 1B Medium Dense to Very Dense Coarse-Grained Fill (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 41°

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

## ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)

Material Model: Mohr-Coulomb

Unit Weight: 115 pcf Effective Cohesion: 200 psf Effective Friction Angle: 34 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### **Common Borrow (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 50 psf Effective Friction Angle: 32 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

# **Slip Surface Entry and Exit**

Left Type: Range

Left-Zone Left Coordinate: (-40.9, 191.85458) ft Left-Zone Right Coordinate: (-0.9, 199.92697) ft

Left-Zone Increment: 20

Right Type: Range

Right-Zone Left Coordinate: (23.356756, 230.46827) ft

Right-Zone Right Coordinate: (65, 233.85753) ft

Right-Zone Increment: 25 Radius Increments: 20

# **Slip Surface Limits**

Left Coordinate: (-80, 186.2) ft Right Coordinate: (80, 234.2) ft

## **Piezometric Lines**

#### Piezometric Line 1

#### **Coordinates**

|               | Х         | Υ          |
|---------------|-----------|------------|
| Coordinate 1  | -48.3 ft  | 180 ft     |
| Coordinate 2  | -4.1 ft   | 190.1 ft   |
| Coordinate 3  | 11.7 ft   | 193.8 ft   |
| Coordinate 4  | 17.165 ft | 194.87 ft  |
| Coordinate 5  | 24.11 ft  | 196.755 ft |
| Coordinate 6  | 29.52 ft  | 198.8 ft   |
| Coordinate 7  | 32.23 ft  | 199.83 ft  |
| Coordinate 8  | 60.885 ft | 211.35 ft  |
| Coordinate 9  | 70.775 ft | 215.12 ft  |
| Coordinate 10 | 74.125 ft | 216.15 ft  |
| Coordinate 11 | 80 ft     | 217.365 ft |

## **Seismic Coefficients**

Horz Seismic Coef.: 0.196

# **Surcharge Loads**

## **Surcharge Load 1**

Surcharge (Unit Weight): 125 pcf

Direction: Vertical

#### **Coordinates**

| X       | Υ        |
|---------|----------|
| 43 ft   | 234.5 ft |
| 45 ft   | 234.5 ft |
| 58.1 ft | 234.7 ft |
| 80 ft   | 235.2 ft |

# Geometry

Name: 2. Global Stability

Settings

View: 2D

Element Thickness: 1 ft

## **Points**

|         | X       | Y        |
|---------|---------|----------|
| Point 1 | 80 ft   | 199.4 ft |
| Point 2 | 58 ft   | 196.6 ft |
| Point 3 | 37.6 ft | 191.9 ft |
| Point 4 | 42.1 ft | 180 ft   |
| Point 5 | 80 ft   | 180 ft   |
| 1       | 1       | l .      |

| Point 6         80 ft         226 ft           Point 7         58 ft         225.3 ft           Point 8         29.8 ft         195 ft           Point 9         11.7 ft         193.8 ft           Point 10         -48.3 ft         180 ft           Point 11         80 ft         234.2 ft           Point 12         58.1 ft         233.7 ft           Point 13         26.5 ft         214.1 ft           Point 14         -10.8 ft         197 ft           Point 15         -18.3 ft         195.3 ft           Point 16         -21.1 ft         194.7 ft           Point 17         -24.4 ft         193.6 ft           Point 18         -32.1 ft         193.1 ft           Point 29         -36.6 ft         192.3 ft           Point 20         -61.7 ft         189.7 ft           Point 21         -65.4 ft         189.3 ft           Point 22         -73.2 ft         188 ft           Point 23         -80 ft         186.2 ft           Point 24         -80 ft         180 ft           Point 25         -4.1 ft         190.1 ft           Point 26         32 ft         197.4 ft           Point 27         <   | l        | 1        | l        |
|--|----------|----------|----------|
| Point 8         29.8 ft         195 ft           Point 9         11.7 ft         193.8 ft           Point 10         -48.3 ft         180 ft           Point 11         80 ft         234.2 ft           Point 12         58.1 ft         233.7 ft           Point 13         26.5 ft         214.1 ft           Point 14         -10.8 ft         197 ft           Point 15         -18.3 ft         195.3 ft           Point 16         -21.1 ft         194.7 ft           Point 17         -24.4 ft         193.6 ft           Point 18         -32.1 ft         193.1 ft           Point 19         -36.6 ft         192.3 ft           Point 20         -61.7 ft         189.7 ft           Point 21         -65.4 ft         189.3 ft           Point 22         -73.2 ft         188 ft           Point 23         -80 ft         186.2 ft           Point 24         -80 ft         180 ft           Point 25         -4.1 ft         190.1 ft           Point 26         32 ft         197.4 ft           Point 27         -0.9 ft         196.3 ft           Point 30         -0.9 ft         199.8 ft           Point 31   | Point 6  | 80 ft    | 226 ft   |
| Point 9         11.7 ft         193.8 ft           Point 10         -48.3 ft         180 ft           Point 11         80 ft         234.2 ft           Point 12         58.1 ft         233.7 ft           Point 13         26.5 ft         214.1 ft           Point 14         -10.8 ft         197 ft           Point 15         -18.3 ft         195.3 ft           Point 16         -21.1 ft         194.7 ft           Point 17         -24.4 ft         193.6 ft           Point 18         -32.1 ft         193.1 ft           Point 19         -36.6 ft         192.3 ft           Point 20         -61.7 ft         189.7 ft           Point 21         -65.4 ft         189.3 ft           Point 22         -73.2 ft         188 ft           Point 23         -80 ft         186.2 ft           Point 24         -80 ft         180 ft           Point 25         -4.1 ft         190.1 ft           Point 26         32 ft         197.4 ft           Point 27         -0.9 ft         196.3 ft           Point 28         -0.9 ft         199.8 ft           Point 30         -0.9 ft         199.8 ft           Point 31 <td></td> <td></td> <td></td>                              |          |          |          |
| Point 10         -48.3 ft         180 ft           Point 11         80 ft         234.2 ft           Point 12         58.1 ft         233.7 ft           Point 13         26.5 ft         214.1 ft           Point 14         -10.8 ft         197 ft           Point 15         -18.3 ft         195.3 ft           Point 16         -21.1 ft         194.7 ft           Point 17         -24.4 ft         193.6 ft           Point 18         -32.1 ft         193.1 ft           Point 19         -36.6 ft         192.3 ft           Point 20         -61.7 ft         189.7 ft           Point 21         -65.4 ft         189.3 ft           Point 22         -73.2 ft         188 ft           Point 23         -80 ft         186.2 ft           Point 24         -80 ft         180 ft           Point 25         -4.1 ft         190.1 ft           Point 26         32 ft         197.4 ft           Point 27         -0.9 ft         199.4 ft           Point 28         -0.9 ft         199.8 ft           Point 30         -0.9 ft         199.8 ft           Point 31         -0.9 ft         199.8 ft           Point 32 <td></td> <td></td> <td></td>                             |          |          |          |
| Point 11         80 ft         234.2 ft           Point 12         58.1 ft         233.7 ft           Point 13         26.5 ft         214.1 ft           Point 14         -10.8 ft         197 ft           Point 15         -18.3 ft         195.3 ft           Point 16         -21.1 ft         194.7 ft           Point 17         -24.4 ft         193.6 ft           Point 18         -32.1 ft         193.1 ft           Point 19         -36.6 ft         192.3 ft           Point 20         -61.7 ft         189.7 ft           Point 21         -65.4 ft         189.3 ft           Point 22         -73.2 ft         188 ft           Point 23         -80 ft         186.2 ft           Point 24         -80 ft         180 ft           Point 25         -4.1 ft         190.1 ft           Point 26         32 ft         197.4 ft           Point 27         -0.9 ft         196.3 ft           Point 28         -0.9 ft         199.8 ft           Point 30         -0.9 ft         199.8 ft           Point 31         -0.9 ft         199.8 ft           Point 32         17.1 ft         196.3 ft           Point 33 </td <td></td> <td>_</td> <td>193.8 ft</td>              |          | _        | 193.8 ft |
| Point 12         58.1 ft         233.7 ft           Point 13         26.5 ft         214.1 ft           Point 14         -10.8 ft         197 ft           Point 15         -18.3 ft         195.3 ft           Point 16         -21.1 ft         194.7 ft           Point 17         -24.4 ft         193.6 ft           Point 18         -32.1 ft         193.1 ft           Point 19         -36.6 ft         192.3 ft           Point 20         -61.7 ft         189.7 ft           Point 21         -65.4 ft         189.3 ft           Point 22         -73.2 ft         188 ft           Point 23         -80 ft         186.2 ft           Point 24         -80 ft         180 ft           Point 25         -4.1 ft         190.1 ft           Point 26         32 ft         197.4 ft           Point 27         -0.9 ft         199.8 ft           Point 28         -0.9 ft         199.8 ft           Point 30         -0.9 ft         199.8 ft           Point 31         -0.9 ft         199.8 ft           Point 32         17.1 ft         196.3 ft           Point 33         15.6 ft         219.4 ft           Point 34  | Point 10 | -48.3 ft |          |
| Point 13         26.5 ft         214.1 ft           Point 14         -10.8 ft         197 ft           Point 15         -18.3 ft         195.3 ft           Point 16         -21.1 ft         194.7 ft           Point 17         -24.4 ft         193.6 ft           Point 19         -36.6 ft         192.3 ft           Point 20         -61.7 ft         189.7 ft           Point 21         -65.4 ft         189.3 ft           Point 22         -73.2 ft         188 ft           Point 23         -80 ft         186.2 ft           Point 24         -80 ft         180 ft           Point 25         -4.1 ft         190.1 ft           Point 26         32 ft         197.4 ft           Point 27         -0.9 ft         190.3 ft           Point 28         -0.9 ft         199.8 ft           Point 29         -4.9 ft         199.8 ft           Point 30         -0.9 ft         199.8 ft           Point 31         -0.9 ft         199.8 ft           Point 32         17.1 ft         196.3 ft           Point 33         15.6 ft         219.4 ft           Point 34         11.1 ft         196.3 ft           Point 35<  | Point 11 | 80 ft    | 234.2 ft |
| Point 14         -10.8 ft         197 ft           Point 15         -18.3 ft         195.3 ft           Point 16         -21.1 ft         194.7 ft           Point 17         -24.4 ft         193.6 ft           Point 18         -32.1 ft         193.1 ft           Point 19         -36.6 ft         192.3 ft           Point 20         -61.7 ft         189.7 ft           Point 21         -65.4 ft         189.3 ft           Point 22         -73.2 ft         188 ft           Point 23         -80 ft         186.2 ft           Point 24         -80 ft         180 ft           Point 25         -4.1 ft         190.1 ft           Point 26         32 ft         197.4 ft           Point 27         -0.9 ft         196.3 ft           Point 28         -0.9 ft         199.8 ft           Point 29         -4.9 ft         199.8 ft           Point 30         -0.9 ft         199.8 ft           Point 31         -0.9 ft         199.8 ft           Point 32         17.1 ft         196.3 ft           Point 33         15.6 ft         219.4 ft           Point 34         11.1 ft         196.3 ft           Point 35  | Point 12 | 58.1 ft  | 233.7 ft |
| Point 15         -18.3 ft         195.3 ft           Point 16         -21.1 ft         194.7 ft           Point 17         -24.4 ft         193.6 ft           Point 18         -32.1 ft         193.1 ft           Point 19         -36.6 ft         192.3 ft           Point 20         -61.7 ft         189.7 ft           Point 21         -65.4 ft         189.3 ft           Point 22         -73.2 ft         188 ft           Point 23         -80 ft         186.2 ft           Point 24         -80 ft         180 ft           Point 25         -4.1 ft         190.1 ft           Point 26         32 ft         197.4 ft           Point 27         -0.9 ft         190.3 ft           Point 28         -0.9 ft         199.8 ft           Point 29         -4.9 ft         199.8 ft           Point 30         -0.9 ft         199.8 ft           Point 31         -0.9 ft         199.8 ft           Point 32         17.1 ft         196.3 ft           Point 33         15.6 ft         219.4 ft           Point 34         11.1 ft         196.3 ft           Point 35         17.1 ft         214.2 ft           Point 3  | Point 13 | 26.5 ft  | 214.1 ft |
| Point 16         -21.1 ft         194.7 ft           Point 17         -24.4 ft         193.6 ft           Point 18         -32.1 ft         193.1 ft           Point 19         -36.6 ft         192.3 ft           Point 20         -61.7 ft         189.7 ft           Point 21         -65.4 ft         189.3 ft           Point 22         -73.2 ft         188 ft           Point 23         -80 ft         186.2 ft           Point 24         -80 ft         180 ft           Point 25         -4.1 ft         190.1 ft           Point 26         32 ft         197.4 ft           Point 27         -0.9 ft         190.1 ft           Point 28         -0.9 ft         199.8 ft           Point 29         -4.9 ft         199.8 ft           Point 30         -0.9 ft         199.8 ft           Point 31         -0.9 ft         199.8 ft           Point 32         17.1 ft         196.3 ft           Point 33         15.6 ft         219.4 ft           Point 34         11.1 ft         196.3 ft           Point 35         17.1 ft         214.2 ft           Point 36         45 ft         233.5 ft           Point 37 </td <td>Point 14</td> <td>-10.8 ft</td> <td>197 ft</td> | Point 14 | -10.8 ft | 197 ft   |
| Point 17         -24.4 ft         193.6 ft           Point 18         -32.1 ft         193.1 ft           Point 19         -36.6 ft         192.3 ft           Point 20         -61.7 ft         189.7 ft           Point 21         -65.4 ft         189.3 ft           Point 22         -73.2 ft         188 ft           Point 23         -80 ft         186.2 ft           Point 24         -80 ft         180 ft           Point 25         -4.1 ft         190.1 ft           Point 26         32 ft         197.4 ft           Point 27         -0.9 ft         190.1 ft           Point 28         -0.9 ft         199.8 ft           Point 29         -4.9 ft         199.8 ft           Point 30         -0.9 ft         199.8 ft           Point 31         -0.9 ft         199.8 ft           Point 32         17.1 ft         196.3 ft           Point 33         15.6 ft         219.4 ft           Point 34         11.1 ft         196.3 ft           Point 35         17.1 ft         214.2 ft           Point 36         45 ft         233.5 ft           Point 37         37.1 ft         222.3 ft           Point 40 <td>Point 15</td> <td>-18.3 ft</td> <td>195.3 ft</td>     | Point 15 | -18.3 ft | 195.3 ft |
| Point 18         -32.1 ft         193.1 ft           Point 19         -36.6 ft         192.3 ft           Point 20         -61.7 ft         189.7 ft           Point 21         -65.4 ft         189.3 ft           Point 22         -73.2 ft         188 ft           Point 23         -80 ft         186.2 ft           Point 24         -80 ft         180 ft           Point 25         -4.1 ft         190.1 ft           Point 26         32 ft         197.4 ft           Point 27         -0.9 ft         199.4 ft           Point 28         -0.9 ft         199.8 ft           Point 30         -0.9 ft         199.8 ft           Point 31         -0.9 ft         199.8 ft           Point 32         17.1 ft         196.3 ft           Point 33         15.6 ft         219.4 ft           Point 34         11.1 ft         196.3 ft           Point 35         17.1 ft         219.4 ft           Point 36         45 ft         233.5 ft           Point 37         37.1 ft         228.2 ft           Point 38         29.4 ft         222.3 ft           Point 40         1.5 ft         219.4 ft           Point 41   | Point 16 | -21.1 ft | 194.7 ft |
| Point 19         -36.6 ft         192.3 ft           Point 20         -61.7 ft         189.7 ft           Point 21         -65.4 ft         189.3 ft           Point 22         -73.2 ft         188 ft           Point 23         -80 ft         186.2 ft           Point 24         -80 ft         180 ft           Point 25         -4.1 ft         190.1 ft           Point 26         32 ft         197.4 ft           Point 27         -0.9 ft         194 ft           Point 28         -0.9 ft         199.8 ft           Point 30         -0.9 ft         199.8 ft           Point 31         -0.9 ft         199.8 ft           Point 32         17.1 ft         196.3 ft           Point 31         -0.9 ft         199.4 ft           Point 32         17.1 ft         196.3 ft           Point 33         15.6 ft         219.4 ft           Point 34         11.1 ft         196.3 ft           Point 35         17.1 ft         214.2 ft           Point 36         45 ft         233.5 ft           Point 37         37.1 ft         222.3 ft           Point 40         1.5 ft         219.4 ft           Point 41  | Point 17 | -24.4 ft | 193.6 ft |
| Point 20         -61.7 ft         189.7 ft           Point 21         -65.4 ft         189.3 ft           Point 22         -73.2 ft         188 ft           Point 23         -80 ft         186.2 ft           Point 24         -80 ft         180 ft           Point 25         -4.1 ft         190.1 ft           Point 26         32 ft         197.4 ft           Point 27         -0.9 ft         194 ft           Point 28         -0.9 ft         199.8 ft           Point 29         -4.9 ft         199.8 ft           Point 30         -0.9 ft         199.8 ft           Point 31         -0.9 ft         199.8 ft           Point 32         17.1 ft         196.3 ft           Point 33         15.6 ft         219.4 ft           Point 34         11.1 ft         196.3 ft           Point 35         17.1 ft         214.2 ft           Point 36         45 ft         233.5 ft           Point 37         37.1 ft         228.2 ft           Point 38         29.4 ft         222.3 ft           Point 40         1.5 ft         219.4 ft           Point 41         31.5 ft         233.5 ft           Point 42   | Point 18 | -32.1 ft | 193.1 ft |
| Point 21         -65.4 ft         189.3 ft           Point 22         -73.2 ft         188 ft           Point 23         -80 ft         186.2 ft           Point 24         -80 ft         180 ft           Point 25         -4.1 ft         190.1 ft           Point 26         32 ft         197.4 ft           Point 27         -0.9 ft         219.4 ft           Point 28         -0.9 ft         196.3 ft           Point 29         -4.9 ft         199.8 ft           Point 30         -0.9 ft         199.8 ft           Point 31         -0.9 ft         199.8 ft           Point 32         17.1 ft         196.3 ft           Point 33         15.6 ft         219.4 ft           Point 34         11.1 ft         196.3 ft           Point 35         17.1 ft         196.3 ft           Point 36         45 ft         233.5 ft           Point 37         37.1 ft         24.2 ft           Point 38         29.4 ft         222.3 ft           Point 39         29.5 ft         233.5 ft           Point 40         1.5 ft         219.4 ft           Point 41         31.5 ft         233.5 ft           Point 42   | Point 19 | -36.6 ft | 192.3 ft |
| Point 22         -73.2 ft         188 ft           Point 23         -80 ft         186.2 ft           Point 24         -80 ft         180 ft           Point 25         -4.1 ft         190.1 ft           Point 26         32 ft         197.4 ft           Point 27         -0.9 ft         219.4 ft           Point 28         -0.9 ft         196.3 ft           Point 29         -4.9 ft         199.8 ft           Point 30         -0.9 ft         199.8 ft           Point 31         -0.9 ft         199.8 ft           Point 32         17.1 ft         196.3 ft           Point 32         17.1 ft         196.3 ft           Point 33         15.6 ft         219.4 ft           Point 34         11.1 ft         196.3 ft           Point 35         17.1 ft         214.2 ft           Point 36         45 ft         233.5 ft           Point 37         37.1 ft         228.2 ft           Point 38         29.4 ft         222.3 ft           Point 40         1.5 ft         219.4 ft           Point 41         31.5 ft         233.5 ft           Point 42         6.1 ft         233.5 ft           Point 43  | Point 20 | -61.7 ft | 189.7 ft |
| Point 23         -80 ft         186.2 ft           Point 24         -80 ft         180 ft           Point 25         -4.1 ft         190.1 ft           Point 26         32 ft         197.4 ft           Point 27         -0.9 ft         219.4 ft           Point 28         -0.9 ft         196.3 ft           Point 29         -4.9 ft         199.8 ft           Point 30         -0.9 ft         199.8 ft           Point 31         -0.9 ft         199.4 ft           Point 32         17.1 ft         196.3 ft           Point 33         15.6 ft         219.4 ft           Point 34         11.1 ft         196.3 ft           Point 35         17.1 ft         214.2 ft           Point 36         45 ft         233.5 ft           Point 37         37.1 ft         228.2 ft           Point 38         29.4 ft         222.3 ft           Point 39         29.5 ft         233.5 ft           Point 40         1.5 ft         219.4 ft           Point 41         31.5 ft         233.5 ft           Point 42         6.1 ft         233.5 ft           Point 43         14.1 ft         219.4 ft           Point 44   | Point 21 | -65.4 ft | 189.3 ft |
| Point 24         -80 ft         180 ft           Point 25         -4.1 ft         190.1 ft           Point 26         32 ft         197.4 ft           Point 27         -0.9 ft         219.4 ft           Point 28         -0.9 ft         196.3 ft           Point 29         -4.9 ft         199.8 ft           Point 30         -0.9 ft         199.8 ft           Point 31         -0.9 ft         199.4 ft           Point 32         17.1 ft         196.3 ft           Point 33         15.6 ft         219.4 ft           Point 34         11.1 ft         196.3 ft           Point 35         17.1 ft         214.2 ft           Point 36         45 ft         233.5 ft           Point 37         37.1 ft         228.2 ft           Point 38         29.4 ft         222.3 ft           Point 39         29.5 ft         233.5 ft           Point 40         1.5 ft         219.4 ft           Point 41         31.5 ft         233.5 ft           Point 42         6.1 ft         233.5 ft           Point 43         14.1 ft         219.4 ft           Point 44         14.1 ft         219.4 ft           Point 45  | Point 22 | -73.2 ft | 188 ft   |
| Point 25         -4.1 ft         190.1 ft           Point 26         32 ft         197.4 ft           Point 27         -0.9 ft         219.4 ft           Point 28         -0.9 ft         196.3 ft           Point 29         -4.9 ft         199.8 ft           Point 30         -0.9 ft         199.8 ft           Point 31         -0.9 ft         199.4 ft           Point 32         17.1 ft         196.3 ft           Point 33         15.6 ft         219.4 ft           Point 34         11.1 ft         196.3 ft           Point 35         17.1 ft         214.2 ft           Point 36         45 ft         233.5 ft           Point 37         37.1 ft         228.2 ft           Point 38         29.4 ft         222.3 ft           Point 39         29.5 ft         233.5 ft           Point 40         1.5 ft         219.4 ft           Point 41         31.5 ft         233.5 ft           Point 42         6.1 ft         233.5 ft           Point 43         14.1 ft         219.4 ft           Point 44         14.1 ft         219.4 ft           Point 45         6.1 ft         219.4 ft           Point 46  | Point 23 | -80 ft   | 186.2 ft |
| Point 26         32 ft         197.4 ft           Point 27         -0.9 ft         219.4 ft           Point 28         -0.9 ft         196.3 ft           Point 29         -4.9 ft         199.8 ft           Point 30         -0.9 ft         199.8 ft           Point 31         -0.9 ft         199.4 ft           Point 32         17.1 ft         196.3 ft           Point 33         15.6 ft         219.4 ft           Point 34         11.1 ft         196.3 ft           Point 35         17.1 ft         214.2 ft           Point 36         45 ft         233.5 ft           Point 37         37.1 ft         228.2 ft           Point 38         29.4 ft         222.3 ft           Point 39         29.5 ft         233.5 ft           Point 40         1.5 ft         219.4 ft           Point 41         31.5 ft         233.5 ft           Point 42         6.1 ft         233.5 ft           Point 43         14.1 ft         233.5 ft           Point 44         14.1 ft         219.4 ft           Point 45         6.1 ft         219.4 ft           Point 46         14.1 ft         221.74 ft           Point 47   | Point 24 | -80 ft   | 180 ft   |
| Point 27         -0.9 ft         219.4 ft           Point 28         -0.9 ft         196.3 ft           Point 29         -4.9 ft         199.8 ft           Point 30         -0.9 ft         199.8 ft           Point 31         -0.9 ft         199.4 ft           Point 32         17.1 ft         196.3 ft           Point 33         15.6 ft         219.4 ft           Point 34         11.1 ft         196.3 ft           Point 35         17.1 ft         214.2 ft           Point 36         45 ft         233.5 ft           Point 37         37.1 ft         228.2 ft           Point 38         29.4 ft         222.3 ft           Point 39         29.5 ft         233.5 ft           Point 40         1.5 ft         219.4 ft           Point 41         31.5 ft         233.5 ft           Point 42         6.1 ft         233.5 ft           Point 43         14.1 ft         233.5 ft           Point 44         14.1 ft         219.4 ft           Point 45         6.1 ft         219.4 ft           Point 46         14.1 ft         225.9 ft           Point 47         6.1 ft         221.74 ft           Point 49 <td>Point 25</td> <td>-4.1 ft</td> <td>190.1 ft</td>       | Point 25 | -4.1 ft  | 190.1 ft |
| Point 28         -0.9 ft         196.3 ft           Point 29         -4.9 ft         199.8 ft           Point 30         -0.9 ft         199.8 ft           Point 31         -0.9 ft         199.4 ft           Point 32         17.1 ft         196.3 ft           Point 33         15.6 ft         219.4 ft           Point 34         11.1 ft         196.3 ft           Point 35         17.1 ft         214.2 ft           Point 36         45 ft         233.5 ft           Point 37         37.1 ft         228.2 ft           Point 38         29.4 ft         222.3 ft           Point 39         29.5 ft         233.5 ft           Point 40         1.5 ft         219.4 ft           Point 41         31.5 ft         233.5 ft           Point 42         6.1 ft         233.5 ft           Point 43         14.1 ft         233.5 ft           Point 44         14.1 ft         219.4 ft           Point 45         6.1 ft         219.4 ft           Point 46         14.1 ft         219.4 ft           Point 47         6.1 ft         221.74 ft           Point 48         15.6 ft         196.3 ft           Point 50 <td>Point 26</td> <td>32 ft</td> <td>197.4 ft</td>         | Point 26 | 32 ft    | 197.4 ft |
| Point 29         -4.9 ft         199.8 ft           Point 30         -0.9 ft         199.4 ft           Point 31         -0.9 ft         199.4 ft           Point 32         17.1 ft         196.3 ft           Point 33         15.6 ft         219.4 ft           Point 34         11.1 ft         196.3 ft           Point 35         17.1 ft         214.2 ft           Point 36         45 ft         233.5 ft           Point 37         37.1 ft         228.2 ft           Point 38         29.4 ft         222.3 ft           Point 39         29.5 ft         233.5 ft           Point 40         1.5 ft         219.4 ft           Point 41         31.5 ft         233.5 ft           Point 42         6.1 ft         233.5 ft           Point 43         14.1 ft         233.5 ft           Point 44         14.1 ft         219.4 ft           Point 45         6.1 ft         219.4 ft           Point 46         14.1 ft         225.9 ft           Point 47         6.1 ft         221.74 ft           Point 48         15.6 ft         196.3 ft           Point 50         17.1 ft         208.4 ft           Point 51 <td>Point 27</td> <td>-0.9 ft</td> <td>219.4 ft</td>       | Point 27 | -0.9 ft  | 219.4 ft |
| Point 30         -0.9 ft         199.8 ft           Point 31         -0.9 ft         199.4 ft           Point 32         17.1 ft         196.3 ft           Point 33         15.6 ft         219.4 ft           Point 34         11.1 ft         196.3 ft           Point 35         17.1 ft         214.2 ft           Point 36         45 ft         233.5 ft           Point 37         37.1 ft         228.2 ft           Point 38         29.4 ft         222.3 ft           Point 39         29.5 ft         233.5 ft           Point 40         1.5 ft         219.4 ft           Point 41         31.5 ft         233.5 ft           Point 42         6.1 ft         233.5 ft           Point 43         14.1 ft         233.5 ft           Point 44         14.1 ft         219.4 ft           Point 45         6.1 ft         219.4 ft           Point 46         14.1 ft         225.9 ft           Point 47         6.1 ft         221.74 ft           Point 48         15.6 ft         196.3 ft           Point 50         17.1 ft         208.4 ft           Point 51         17.1 ft         219.4 ft           Point 52 <td>Point 28</td> <td>-0.9 ft</td> <td>196.3 ft</td>       | Point 28 | -0.9 ft  | 196.3 ft |
| Point 31         -0.9 ft         199.4 ft           Point 32         17.1 ft         196.3 ft           Point 33         15.6 ft         219.4 ft           Point 34         11.1 ft         196.3 ft           Point 35         17.1 ft         214.2 ft           Point 36         45 ft         233.5 ft           Point 37         37.1 ft         228.2 ft           Point 38         29.4 ft         222.3 ft           Point 39         29.5 ft         233.5 ft           Point 40         1.5 ft         219.4 ft           Point 41         31.5 ft         233.5 ft           Point 42         6.1 ft         233.5 ft           Point 43         14.1 ft         219.4 ft           Point 44         14.1 ft         219.4 ft           Point 45         6.1 ft         219.4 ft           Point 46         14.1 ft         225.9 ft           Point 47         6.1 ft         221.74 ft           Point 48         15.6 ft         214.2 ft           Point 50         17.1 ft         208.4 ft           Point 51         17.1 ft         219.4 ft           Point 52         6.1 ft         232 ft  | Point 29 | -4.9 ft  | 199.8 ft |
| Point 32         17.1 ft         196.3 ft           Point 33         15.6 ft         219.4 ft           Point 34         11.1 ft         196.3 ft           Point 35         17.1 ft         214.2 ft           Point 36         45 ft         233.5 ft           Point 37         37.1 ft         228.2 ft           Point 38         29.4 ft         222.3 ft           Point 39         29.5 ft         233.5 ft           Point 40         1.5 ft         219.4 ft           Point 41         31.5 ft         233.5 ft           Point 42         6.1 ft         233.5 ft           Point 43         14.1 ft         233.5 ft           Point 44         14.1 ft         219.4 ft           Point 45         6.1 ft         219.4 ft           Point 46         14.1 ft         225.9 ft           Point 47         6.1 ft         221.74 ft           Point 48         15.6 ft         214.2 ft           Point 50         17.1 ft         208.4 ft           Point 51         17.1 ft         219.4 ft           Point 52         6.1 ft         232 ft  | Point 30 | -0.9 ft  | 199.8 ft |
| Point 33         15.6 ft         219.4 ft           Point 34         11.1 ft         196.3 ft           Point 35         17.1 ft         214.2 ft           Point 36         45 ft         233.5 ft           Point 37         37.1 ft         228.2 ft           Point 38         29.4 ft         222.3 ft           Point 39         29.5 ft         233.5 ft           Point 40         1.5 ft         219.4 ft           Point 41         31.5 ft         233.5 ft           Point 42         6.1 ft         233.5 ft           Point 43         14.1 ft         233.5 ft           Point 44         14.1 ft         219.4 ft           Point 45         6.1 ft         219.4 ft           Point 46         14.1 ft         225.9 ft           Point 47         6.1 ft         221.74 ft           Point 48         15.6 ft         214.2 ft           Point 50         17.1 ft         208.4 ft           Point 51         17.1 ft         219.4 ft           Point 52         6.1 ft         232 ft  | Point 31 | -0.9 ft  | 199.4 ft |
| Point 34         11.1 ft         196.3 ft           Point 35         17.1 ft         214.2 ft           Point 36         45 ft         233.5 ft           Point 37         37.1 ft         228.2 ft           Point 38         29.4 ft         222.3 ft           Point 39         29.5 ft         233.5 ft           Point 40         1.5 ft         219.4 ft           Point 41         31.5 ft         233.5 ft           Point 42         6.1 ft         233.5 ft           Point 43         14.1 ft         219.4 ft           Point 44         14.1 ft         219.4 ft           Point 45         6.1 ft         219.4 ft           Point 46         14.1 ft         225.9 ft           Point 47         6.1 ft         221.74 ft           Point 48         15.6 ft         214.2 ft           Point 49         15.6 ft         196.3 ft           Point 50         17.1 ft         208.4 ft           Point 51         17.1 ft         219.4 ft           Point 52         6.1 ft         232 ft  | Point 32 | 17.1 ft  | 196.3 ft |
| Point 35         17.1 ft         214.2 ft           Point 36         45 ft         233.5 ft           Point 37         37.1 ft         228.2 ft           Point 38         29.4 ft         222.3 ft           Point 39         29.5 ft         233.5 ft           Point 40         1.5 ft         219.4 ft           Point 41         31.5 ft         233.5 ft           Point 42         6.1 ft         233.5 ft           Point 43         14.1 ft         219.4 ft           Point 44         14.1 ft         219.4 ft           Point 45         6.1 ft         219.4 ft           Point 46         14.1 ft         225.9 ft           Point 47         6.1 ft         221.74 ft           Point 48         15.6 ft         214.2 ft           Point 49         15.6 ft         196.3 ft           Point 50         17.1 ft         208.4 ft           Point 51         17.1 ft         219.4 ft           Point 52         6.1 ft         232 ft  | Point 33 | 15.6 ft  | 219.4 ft |
| Point 36         45 ft         233.5 ft           Point 37         37.1 ft         228.2 ft           Point 38         29.4 ft         222.3 ft           Point 39         29.5 ft         233.5 ft           Point 40         1.5 ft         219.4 ft           Point 41         31.5 ft         233.5 ft           Point 42         6.1 ft         233.5 ft           Point 43         14.1 ft         219.4 ft           Point 44         14.1 ft         219.4 ft           Point 45         6.1 ft         219.4 ft           Point 46         14.1 ft         225.9 ft           Point 47         6.1 ft         221.74 ft           Point 48         15.6 ft         214.2 ft           Point 49         15.6 ft         196.3 ft           Point 50         17.1 ft         208.4 ft           Point 51         17.1 ft         219.4 ft           Point 52         6.1 ft         232 ft  | Point 34 | 11.1 ft  | 196.3 ft |
| Point 37       37.1 ft       228.2 ft         Point 38       29.4 ft       222.3 ft         Point 39       29.5 ft       233.5 ft         Point 40       1.5 ft       219.4 ft         Point 41       31.5 ft       233.5 ft         Point 42       6.1 ft       233.5 ft         Point 43       14.1 ft       219.4 ft         Point 44       14.1 ft       219.4 ft         Point 45       6.1 ft       219.4 ft         Point 46       14.1 ft       225.9 ft         Point 47       6.1 ft       221.74 ft         Point 48       15.6 ft       214.2 ft         Point 49       15.6 ft       196.3 ft         Point 50       17.1 ft       208.4 ft         Point 51       17.1 ft       219.4 ft         Point 52       6.1 ft       232 ft  | Point 35 | 17.1 ft  | 214.2 ft |
| Point 38         29.4 ft         222.3 ft           Point 39         29.5 ft         233.5 ft           Point 40         1.5 ft         219.4 ft           Point 41         31.5 ft         233.5 ft           Point 42         6.1 ft         233.5 ft           Point 43         14.1 ft         233.5 ft           Point 44         14.1 ft         219.4 ft           Point 45         6.1 ft         219.4 ft           Point 46         14.1 ft         225.9 ft           Point 47         6.1 ft         221.74 ft           Point 48         15.6 ft         214.2 ft           Point 49         15.6 ft         196.3 ft           Point 50         17.1 ft         208.4 ft           Point 51         17.1 ft         219.4 ft           Point 52         6.1 ft         232 ft  | Point 36 | 45 ft    | 233.5 ft |
| Point 38         29.4 ft         222.3 ft           Point 39         29.5 ft         233.5 ft           Point 40         1.5 ft         219.4 ft           Point 41         31.5 ft         233.5 ft           Point 42         6.1 ft         233.5 ft           Point 43         14.1 ft         233.5 ft           Point 44         14.1 ft         219.4 ft           Point 45         6.1 ft         219.4 ft           Point 46         14.1 ft         225.9 ft           Point 47         6.1 ft         221.74 ft           Point 48         15.6 ft         214.2 ft           Point 49         15.6 ft         196.3 ft           Point 50         17.1 ft         208.4 ft           Point 51         17.1 ft         219.4 ft           Point 52         6.1 ft         232 ft  | Point 37 | 37.1 ft  | 228.2 ft |
| Point 40       1.5 ft       219.4 ft         Point 41       31.5 ft       233.5 ft         Point 42       6.1 ft       233.5 ft         Point 43       14.1 ft       233.5 ft         Point 44       14.1 ft       219.4 ft         Point 45       6.1 ft       219.4 ft         Point 46       14.1 ft       225.9 ft         Point 47       6.1 ft       221.74 ft         Point 48       15.6 ft       214.2 ft         Point 49       15.6 ft       196.3 ft         Point 50       17.1 ft       208.4 ft         Point 51       17.1 ft       219.4 ft         Point 52       6.1 ft       232 ft  | Point 38 | 29.4 ft  | 222.3 ft |
| Point 4131.5 ft233.5 ftPoint 426.1 ft233.5 ftPoint 4314.1 ft233.5 ftPoint 4414.1 ft219.4 ftPoint 456.1 ft219.4 ftPoint 4614.1 ft225.9 ftPoint 476.1 ft221.74 ftPoint 4815.6 ft214.2 ftPoint 4915.6 ft196.3 ftPoint 5017.1 ft208.4 ftPoint 5117.1 ft219.4 ftPoint 526.1 ft232 ft  | Point 39 | 29.5 ft  | 233.5 ft |
| Point 426.1 ft233.5 ftPoint 4314.1 ft233.5 ftPoint 4414.1 ft219.4 ftPoint 456.1 ft219.4 ftPoint 4614.1 ft225.9 ftPoint 476.1 ft221.74 ftPoint 4815.6 ft214.2 ftPoint 4915.6 ft196.3 ftPoint 5017.1 ft208.4 ftPoint 5117.1 ft219.4 ftPoint 526.1 ft232 ft   | Point 40 | 1.5 ft   | 219.4 ft |
| Point 426.1 ft233.5 ftPoint 4314.1 ft233.5 ftPoint 4414.1 ft219.4 ftPoint 456.1 ft219.4 ftPoint 4614.1 ft225.9 ftPoint 476.1 ft221.74 ftPoint 4815.6 ft214.2 ftPoint 4915.6 ft196.3 ftPoint 5017.1 ft208.4 ftPoint 5117.1 ft219.4 ftPoint 526.1 ft232 ft   | Point 41 | 31.5 ft  | 233.5 ft |
| Point 4414.1 ft219.4 ftPoint 456.1 ft219.4 ftPoint 4614.1 ft225.9 ftPoint 476.1 ft221.74 ftPoint 4815.6 ft214.2 ftPoint 4915.6 ft196.3 ftPoint 5017.1 ft208.4 ftPoint 5117.1 ft219.4 ftPoint 526.1 ft232 ft  | Point 42 | 6.1 ft   |          |
| Point 4414.1 ft219.4 ftPoint 456.1 ft219.4 ftPoint 4614.1 ft225.9 ftPoint 476.1 ft221.74 ftPoint 4815.6 ft214.2 ftPoint 4915.6 ft196.3 ftPoint 5017.1 ft208.4 ftPoint 5117.1 ft219.4 ftPoint 526.1 ft232 ft  | Point 43 | 14.1 ft  | 233.5 ft |
| Point 456.1 ft219.4 ftPoint 4614.1 ft225.9 ftPoint 476.1 ft221.74 ftPoint 4815.6 ft214.2 ftPoint 4915.6 ft196.3 ftPoint 5017.1 ft208.4 ftPoint 5117.1 ft219.4 ftPoint 526.1 ft232 ft   | Point 44 | 14.1 ft  |          |
| Point 4614.1 ft225.9 ftPoint 476.1 ft221.74 ftPoint 4815.6 ft214.2 ftPoint 4915.6 ft196.3 ftPoint 5017.1 ft208.4 ftPoint 5117.1 ft219.4 ftPoint 526.1 ft232 ft   |          |          |          |
| Point 476.1 ft221.74 ftPoint 4815.6 ft214.2 ftPoint 4915.6 ft196.3 ftPoint 5017.1 ft208.4 ftPoint 5117.1 ft219.4 ftPoint 526.1 ft232 ft  |          |          |          |
| Point 48       15.6 ft       214.2 ft         Point 49       15.6 ft       196.3 ft         Point 50       17.1 ft       208.4 ft         Point 51       17.1 ft       219.4 ft         Point 52       6.1 ft       232 ft   |          |          |          |
| Point 49       15.6 ft       196.3 ft         Point 50       17.1 ft       208.4 ft         Point 51       17.1 ft       219.4 ft         Point 52       6.1 ft       232 ft   |          |          |          |
| Point 50         17.1 ft         208.4 ft           Point 51         17.1 ft         219.4 ft           Point 52         6.1 ft         232 ft   |          |          |          |
| Point 51 17.1 ft 219.4 ft Point 52 6.1 ft 232 ft   |          |          |          |
| Point 52 6.1 ft 232 ft   |          |          |          |
|  |          |          |          |
| 25210  |          |          |          |
|  |          |          |          |

| Point 54 | 39 ft | 233.5 ft |
|----------|-------|----------|
| Point 55 | 39 ft | 230.5 ft |

## **Regions**

|              | Material  | Points  | Area                       |
|--------------|---|---|----------------------------|
| Region<br>1  | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt              | 1,2,3,4,5                                       | 659.92<br>ft <sup>2</sup>  |
| Region<br>2  | ESU 4B Dense to Very Dense Sand/Gravel  | 1,6,7,26,8,9,25,10,4,3,2                        | 1,867.8<br>ft <sup>2</sup> |
| Region<br>3  | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill (Apparent Cohesion) | 14,29,30,31                                     | 7.58 ft <sup>2</sup>       |
| Region<br>4  | SEW Wall  | 27,30,31,28,34,49,48,33,44,45,40                | 381.15<br>ft <sup>2</sup>  |
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                           | 14,15,16,17,18,19,20,21,22,23,24,10,25,34,28,31 | 748.7<br>ft <sup>2</sup>   |
| Region<br>6  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                           | 7,6,11,12,13,50,32,49,34,25,9,8,26              | 856.44<br>ft <sup>2</sup>  |
| Region<br>7  | Common Borrow (Apparent Cohesion)   | 45,44,46,47                                     | 35.36<br>ft <sup>2</sup>   |
| Region<br>8  | Common Borrow (Apparent Cohesion)   | 36,55,51,35,38,37                               | 75.79<br>ft²               |
| Region<br>9  |   | 43,53,46,39                                     | 58.52<br>ft <sup>2</sup>   |
| Region<br>10 |   | 43,42,52,53                                     | 12 ft²                     |
| Region<br>11 | Common Borrow (Apparent Cohesion)   | 47,40,45  | 5.382<br>ft <sup>2</sup>   |
| Region<br>12 | Gravel Borrow   | 32,50,35,48,49                                  | 26.85<br>ft <sup>2</sup>   |
| Region<br>13 | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill (Apparent Cohesion) | 35,50,13,12,36,37,38                            | 241.79<br>ft <sup>2</sup>  |
| Region<br>14 | Gravel Borrow   | 33,48,35,51                                     | 7.8 ft <sup>2</sup>        |
| Region<br>15 |   | 47,46,53,52                                     | 65.44<br>ft <sup>2</sup>   |
| Region<br>16 | Common Borrow (Apparent Cohesion)   | 41,39,46,44,33,51,55,54                         | 171.02<br>ft <sup>2</sup>  |
| Region<br>17 | Common Borrow (Apparent Cohesion)   | 36,54,55  | 9 ft²                      |

# **Slip Results**

Slip Surfaces Analysed: 1837 of 11466 converged

# **Current Slip Surface**

Slip Surface: 2,575 Factor of Safety: 1.3 Volume: 1,463.8667 ft<sup>3</sup> Weight: 179,655.51 lbf Resisting Moment: 9,369,898.3 lbf·ft Activating Moment: 7,486,242.8 lbf·ft

Resisting Force: 114,533.43 lbf Activating Force: 91,449.07 lbf Slip Rank: 1 of 11,466 slip surfaces Exit: (-32.72383, 192.9891) ft Entry: (53.143274, 233.62432) ft

Radius: 72.452532 ft

Center: (-13.193045, 262.75956) ft

## **Slip Slices**

|            | X                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material   |
|------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|---|
| Slice<br>1 | -32.411915<br>ft | 192.90328<br>ft | -578.61944<br>psf | 76.106242<br>psf         | 51.334308<br>psf       | 200 psf              | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>2 | -30.816667<br>ft | 192.49558<br>ft | -530.4326<br>psf  | 178.95001<br>psf         | 120.70331<br>psf       | 200 psf              | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>3 | -28.25 ft        | 191.901 ft      | -456.73283<br>psf | 344.47359<br>psf         | 232.35037<br>psf       | 200 psf              | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>4 | -25.683333<br>ft | 191.40366<br>ft | -389.10136<br>psf | 515.29602<br>psf         | 347.57156<br>psf       | 200 psf              | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>5 | -22.75 ft        | 190.9594<br>ft  | -319.55363<br>psf | 778.31133<br>psf         | 524.97762<br>psf       | 200 psf              | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>6 | -19.7 ft         | 190.61351<br>ft | -254.48061<br>psf | 1,072.9331<br>psf        | 723.70254<br>psf       | 200 psf              | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>7 | -17.05 ft        | 190.42059<br>ft | -204.65682<br>psf | 1,280.3088<br>psf        | 863.57921<br>psf       | 200 psf              | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>8 | -14.55 ft        | 190.33053<br>ft | -163.38964<br>psf | 1,441.4971<br>psf        | 972.3021<br>psf        | 200 psf              | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent              |

|             |                  |                 |                   |                   |                   |         |       | Cohesion)   |
|-------------|------------------|-----------------|-------------------|-------------------|-------------------|---------|-------|---|
| Slice<br>9  | -12.05 ft        | 190.32684<br>ft | -127.51216<br>psf | 1,556.4548<br>psf | 1,049.842<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion) |
| Slice<br>10 | -9.325 ft        | 190.42544<br>ft | -94.809576<br>psf | 1,680.8729<br>psf | 1,133.7631<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion) |
| Slice<br>11 | -6.375 ft        | 190.64376<br>ft | -66.369596<br>psf | 1,793.3564<br>psf | 1,209.6342<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion) |
| Slice<br>12 | -4.5 ft          | 190.83156<br>ft | -51.352647<br>psf | 1,798.669<br>psf  | 1,213.2176<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion) |
| Slice<br>13 | -2.6006305<br>ft | 191.10153<br>ft | -40.585987<br>psf | 1,664.8875<br>psf | 1,122.9808<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion) |
| Slice<br>14 | -1.0006305<br>ft | 191.34035<br>ft | -32.107758<br>psf | 1,547.2417<br>psf | 1,043.6277<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion) |
| Slice<br>15 | 0.3 ft           | 191.58502<br>ft | -28.369589<br>psf | 4,146.2205<br>psf | 2,796.661<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion) |
| Slice<br>16 | 2.65 ft          | 192.07025<br>ft | -24.308367<br>psf | 3,885.4234<br>psf | 2,620.7512<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion) |
| Slice<br>17 | 4.95 ft          | 192.62549<br>ft | -25.345922<br>psf | 3,679.1315<br>psf | 2,481.6056<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion) |
| Slice<br>18 | 7.35 ft          | 193.29264<br>ft | -31.905682<br>psf | 3,452.6177<br>psf | 2,328.82<br>psf   | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion) |
| Slice<br>19 | 9.85 ft          | 194.0817<br>ft  | -44.61136<br>psf  | 3,217.2005<br>psf | 2,170.0291<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent  |

|             |             |                 |                   |                   |                   |         |       | Cohesion)   |
|-------------|-------------|-----------------|-------------------|-------------------|-------------------|---------|-------|---|
| Slice<br>20 | 11.4 ft     | 194.60936<br>ft | -54.887981<br>psf | 3,076.1891<br>psf | 2,074.9157<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>21 | 12.9 ft     | 195.18096<br>ft | -71.510939<br>psf | 2,941.9737<br>psf | 1,984.3863<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>22 | 14.85 ft    | 195.95915<br>ft | -96.24606<br>psf  | 2,776.5637<br>psf | 1,872.8159<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>23 | 16.3825 ft  | 196.62393<br>ft | -119.00538<br>psf | 2,675.3048<br>psf | 2,090.1772<br>psf | 0 psf   | 0 psf | Gravel Borrow   |
| Slice<br>24 | 18.90125 ft | 197.83211<br>ft | -155.42947<br>psf | 2,301.0995<br>psf | 1,552.1112<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>25 | 22.37375 ft | 199.66915<br>ft | -211.24909<br>psf | 2,079.5704<br>psf | 1,402.6879<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>26 | 25.305 ft   | 201.39769<br>ft | -261.51667<br>psf | 1,921.074<br>psf  | 1,295.7808<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>27 | 28 ft       | 203.1846<br>ft  | -309.45164<br>psf | 1,793.9106<br>psf | 1,210.008<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>28 | 29.51 ft    | 204.22906<br>ft | -339.0095<br>psf  | 1,730.6803<br>psf | 1,167.3586<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>29 | 30.51 ft    | 204.98524<br>ft | -362.47954<br>psf | 1,657.5688<br>psf | 1,118.0443<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>30 | 31.865 ft   | 206.02399<br>ft | -395.16179<br>psf | 1,563.5425<br>psf | 1,054.6227<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
|             |             |                 |                   |                   |                   |         |       | ESU 2B Medium<br>Dense  |

| ouar - 1 scu | ai - rseudo-static (M-r) |                 |                    |                   |                  |         |       |  |  |
|--------------|--------------------------|-----------------|--------------------|-------------------|------------------|---------|-------|--|--|
| Slice<br>31  | 33.4475 ft               | 207.33848<br>ft | -437.98633<br>psf  | 1,455.9412<br>psf | 982.04475<br>psf | 200 psf | 0 psf | Sand/Gravel<br>(Apparent<br>Cohesion)                                      |  |
| Slice<br>32  | 35.8825 ft               | 209.48461<br>ft | -510.82019<br>psf  | 1,297.8562<br>psf | 875.41503<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                        |  |
| Slice<br>33  | 38.05 ft                 | 211.55689<br>ft | -585.75588<br>psf  | 1,159.9169<br>psf | 782.37383<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                        |  |
| Slice<br>34  | 41 ft                    | 214.76599<br>ft | -711.99882<br>psf  | 962.14614<br>psf  | 648.97576<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                        |  |
| Slice<br>35  | 44 ft                    | 218.31106<br>ft | -857.9524<br>psf   | 823.45292<br>psf  | 555.42601<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                        |  |
| Slice<br>36  | 46.525357<br>ft          | 221.82298<br>ft | -1,013.7444<br>psf | 618.46375<br>psf  | 417.15906<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                        |  |
| Slice<br>37  | 49.576072<br>ft          | 226.70365<br>ft | -1,241.7667<br>psf | 328.57709<br>psf  | 221.62805<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                        |  |
| Slice<br>38  | 52.122352<br>ft          | 231.49172<br>ft | -1,476.6657<br>psf | 92.340339<br>psf  | 80.270232<br>psf | 100 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill (Apparent Cohesion) |  |

# 2B.1 Global - Static FC Wall (Spencer)

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## **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Bo Zhang Revision Number: 314 Date: 01/12/2022

Tool Version: 11.1.1.22700

Time: 10:44:22 AM

File Name: Wall 05.85L-B Sta 2+60\_FC Wall (lightweight fill).gsz Directory: P:\0\0180366\01\Analysis\Wall 05.85L-B\22-01-13\

Last Solved Date: 01/12/2022 Last Solved Time: 10:49:10 AM

# **Project Settings**

Unit System: U.S. Customary Units

# **Analysis Settings**

## 2B.1 Global - Static FC Wall (Spencer)

Description: With Forward Compatible Wall

Kind: SLOPE/W

Analysis Type: Spencer

Settings

PWP Conditions from: Piezometric Line

Apply Phreatic Correction: No
Use Staged Rapid Drawdown: No
Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 1

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

**Factor of Safety Convergence Settings** 

Maximum Number of Iterations: 100 Tolerable difference in F of S: 0.001

**Solution Settings** 

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

### **Materials**

### ESU 1B Medium Dense to Very Dense Coarse-Grained Fill

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 41 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### **ESU 2B Medium Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 115 pcf Effective Cohesion: 0 psf Effective Friction Angle: 34 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

## **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **SEW Wall**

Material Model: High Strength

Unit Weight: 130 pcf
Pore Water Pressure
Piezometric Line: 1

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 42 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### Forward Compatible Wall

Material Model: High Strength

Unit Weight: 130 pcf
Pore Water Pressure
Piezometric Line: 1

#### **Lightweight EPS**

Material Model: Mohr-Coulomb

Unit Weight: 5 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 0 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

## Slip Surface Entry and Exit

Left Type: Range

Left-Zone Left Coordinate: (-40.9, 191.85458) ft Left-Zone Right Coordinate: (-0.9, 199.92697) ft

Left-Zone Increment: 20

Right Type: Range

Right-Zone Left Coordinate: (20.000001, 233.5) ft

Right-Zone Right Coordinate: (65, 233.85753) ft

Right-Zone Increment: 25 Radius Increments: 20

# **Slip Surface Limits**

Left Coordinate: (-80, 186.2) ft Right Coordinate: (80, 234.2) ft

## **Piezometric Lines**

### Piezometric Line 1

#### Coordinates

|               | Х         | Υ          |
|---------------|-----------|------------|
| Coordinate 1  | -48.3 ft  | 180 ft     |
| Coordinate 2  | -4.1 ft   | 190.1 ft   |
| Coordinate 3  | 11.7 ft   | 193.8 ft   |
| Coordinate 4  | 17.165 ft | 194.87 ft  |
| Coordinate 5  | 24.11 ft  | 196.755 ft |
| Coordinate 6  | 29.52 ft  | 198.8 ft   |
| Coordinate 7  | 32.23 ft  | 199.83 ft  |
| Coordinate 8  | 60.885 ft | 211.35 ft  |
| Coordinate 9  | 70.775 ft | 215.12 ft  |
| Coordinate 10 | 74.125 ft | 216.15 ft  |
| Coordinate 11 | 80 ft     | 217.365 ft |

# **Surcharge Loads**

## **Surcharge Load 1**

Surcharge (Unit Weight): 250 pcf

**Direction: Vertical** 

#### Coordinates

| Х       | Υ        |
|---------|----------|
| 8.1 ft  | 234.5 ft |
| 45 ft   | 234.5 ft |
| 58.1 ft | 234.7 ft |
| 80 ft   | 235.2 ft |

# Geometry

Name: 2. Global Stability

## Settings

View: 2D

Element Thickness: 1 ft

### **Points**

| LS       |          |          |
|----------|----------|----------|
|          | Х        | Y        |
| Point 1  | 80 ft    | 199.4 ft |
| Point 2  | 58 ft    | 196.6 ft |
| Point 3  | 37.6 ft  | 191.9 ft |
| Point 4  | 42.1 ft  | 180 ft   |
| Point 5  | 80 ft    | 180 ft   |
| Point 6  | 80 ft    | 226 ft   |
| Point 7  | 58 ft    | 225.3 ft |
| Point 8  | 29.8 ft  | 195 ft   |
| Point 9  | 11.7 ft  | 193.8 ft |
| Point 10 | -48.3 ft | 180 ft   |
| Point 11 | 80 ft    | 234.2 ft |
| Point 12 | 58.1 ft  | 233.7 ft |
| Point 13 | 26.5 ft  | 214.1 ft |
| Point 14 | -10.8 ft | 197 ft   |
| Point 15 | -18.3 ft | 195.3 ft |
| Point 16 | -21.1 ft | 194.7 ft |
| Point 17 | -24.4 ft | 193.6 ft |
| Point 18 | -32.1 ft | 193.1 ft |
| Point 19 | -36.6 ft | 192.3 ft |
| Point 20 | -61.7 ft | 189.7 ft |
| Point 21 | -65.4 ft | 189.3 ft |
| Point 22 | -73.2 ft | 188 ft   |
| Point 23 | -80 ft   | 186.2 ft |
| Point 24 | -80 ft   | 180 ft   |
| Point 25 | -4.1 ft  | 190.1 ft |
| Point 26 | 32 ft    | 197.4 ft |
| Point 27 | -0.9 ft  | 219.4 ft |
| Point 28 | -0.9 ft  | 196.3 ft |
| Point 29 | -4.9 ft  | 199.8 ft |
| Point 30 | -0.9 ft  | 199.8 ft |
| Point 31 | -0.9 ft  | 199.4 ft |
| Point 32 | 17.1 ft  | 196.3 ft |
| Point 33 | 15.6 ft  | 219.4 ft |
| Point 34 | 11.1 ft  | 196.3 ft |
| Point 35 | 17.1 ft  | 214.2 ft |
| Point 36 | 45 ft    | 233.5 ft |
| Point 37 | 37.1 ft  | 228.2 ft |
| Point 38 | 29.4 ft  | 222.3 ft |
| Point 39 | 29.5 ft  | 233.5 ft |
| Point 40 | 1.5 ft   | 219.4 ft |
| Point 41 | 31.5 ft  | 233.5 ft |
| Point 42 | 6.1 ft   | 233.5 ft |
| Point 43 | 14.1 ft  | 233.5 ft |
|          |          |          |

| Point 44 | 14.1 ft | 219.4 ft  |  |  |
|----------|---------|-----------|--|--|
| Point 45 | 6.1 ft  | 219.4 ft  |  |  |
| Point 46 | 14.1 ft | 225.9 ft  |  |  |
| Point 47 | 6.1 ft  | 221.74 ft |  |  |
| Point 48 | 15.6 ft | 214.2 ft  |  |  |
| Point 49 | 15.6 ft | 196.3 ft  |  |  |
| Point 50 | 17.1 ft | 208.4 ft  |  |  |
| Point 51 | 17.1 ft | 219.4 ft  |  |  |
| Point 52 | 6.1 ft  | 232 ft    |  |  |
| Point 53 | 14.1 ft | 232 ft    |  |  |
| Point 54 | 39 ft   | 233.5 ft  |  |  |
| Point 55 | 39 ft   | 230.5 ft  |  |  |

# Regions

|              | Material   | Points  | Area                       |
|--------------|--|---|----------------------------|
| Region<br>1  | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 1,2,3,4,5                                       | 659.92<br>ft <sup>2</sup>  |
| Region<br>2  | ESU 4B Dense to Very Dense Sand/Gravel                           | 1,6,7,26,8,9,25,10,4,3,2                        | 1,867.8<br>ft <sup>2</sup> |
| Region<br>3  | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill        | 14,29,30,31                                     | 7.58 ft <sup>2</sup>       |
| Region<br>4  | SEW Wall   | 27,30,31,28,34,49,48,33,44,45,40                | 381.15<br>ft <sup>2</sup>  |
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel                                  | 14,15,16,17,18,19,20,21,22,23,24,10,25,34,28,31 | 748.7<br>ft <sup>2</sup>   |
| Region<br>6  | ESU 2B Medium Dense Sand/Gravel                                  | 7,6,11,12,13,50,32,49,34,25,9,8,26              | 856.44<br>ft <sup>2</sup>  |
| Region<br>7  | Forward Compatible Wall  | 45,44,46,47                                     | 35.36<br>ft <sup>2</sup>   |
| Region<br>8  | Common Borrow  | 36,55,51,35,38,37                               | 75.79<br>ft²               |
| Region<br>9  | Lightweight EPS  | 43,53,46,39                                     | 58.52<br>ft <sup>2</sup>   |
| Region<br>10 | Forward Compatible Wall  | 43,42,52,53                                     | 12 ft²                     |
| Region<br>11 |  | 47,40,45  | 5.382<br>ft²               |
| Region<br>12 | Gravel Borrow  | 32,50,35,48,49                                  | 26.85<br>ft <sup>2</sup>   |
| Region<br>13 | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill        | 35,50,13,12,36,37,38                            | 241.79<br>ft <sup>2</sup>  |
| Region<br>14 | Gravel Borrow  | 33,48,35,51                                     | 7.8 ft <sup>2</sup>        |
| Region<br>15 | Forward Compatible Wall  | 47,46,53,52                                     | 65.44<br>ft <sup>2</sup>   |
| Region<br>16 | Lightweight EPS  | 41,39,46,44,33,51,55,54                         | 171.02<br>ft <sup>2</sup>  |
| Region<br>17 | Common Borrow  | 36,54,55  | 9 ft²                      |

# **Slip Results**

Slip Surfaces Analysed: 1520 of 11466 converged

# **Current Slip Surface**

Slip Surface: 3,101 Factor of Safety: 1.5 Volume: 1,536.2538 ft<sup>3</sup> Weight: 163,163.5 lbf

Resisting Moment: 7,456,039.3 lbf·ft Activating Moment: 4,992,124.5 lbf·ft

Resisting Force: 97,655.951 lbf Activating Force: 65,394.513 lbf Slip Rank: 1 of 11,466 slip surfaces Exit: (-30.671631, 193.19275) ft Entry: (50.601608, 233.58552) ft

Radius: 66.587809 ft

Center: (-11.723356, 257.02769) ft

## **Slip Slices**

|            | Х                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material                         |
|------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|---------------------------------------|
| Slice<br>1 | -29.103723<br>ft | 192.76867<br>ft | -523.04891<br>psf | 118.23679<br>psf         | 79.751725<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>2 | -25.967908<br>ft | 192.00113<br>ft | -430.4414<br>psf  | 307.12896<br>psf         | 207.1611<br>psf        | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>3 | -22.75 ft        | 191.38052<br>ft | -345.83178<br>psf | 522.59411<br>psf         | 352.49418<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>4 | -19.7 ft         | 190.93441<br>ft | -274.50507<br>psf | 714.07291<br>psf         | 481.64826<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>5 | -17.05 ft        | 190.66512<br>ft | -219.91518<br>psf | 815.53796<br>psf         | 550.0873<br>psf        | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>6 | -14.55 ft        | 190.51167<br>ft | -174.69272<br>psf | 888.52104<br>psf         | 599.31501<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>7 | -12.05 ft        | 190.45241<br>ft | -135.3483<br>psf  | 940.66203<br>psf         | 634.48455<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>8 | -9.325 ft        | 190.49946<br>ft | -99.428369<br>psf | 1,034.8536<br>psf        | 698.01759<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>9 | -6.375 ft        | 190.67152<br>ft | -68.10139<br>psf  | 1,161.3319<br>psf        | 783.32829<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |

| Slice<br>10 | -4.5 ft          | 190.83405<br>ft | -51.508337<br>psf | 1,199.8332<br>psf | 809.29773<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
|-------------|------------------|-----------------|-------------------|-------------------|-------------------|-------|-------|---------------------------------------|
| Slice<br>11 | -2.6625312<br>ft | 191.07519<br>ft | -39.846403<br>psf | 1,125.638<br>psf  | 759.25244<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>12 | -1.0625312<br>ft | 191.29903<br>ft | -30.434203<br>psf | 1,062.6248<br>psf | 716.74947<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>13 | 0.3 ft           | 191.54573<br>ft | -25.917929<br>psf | 3,749.3773<br>psf | 2,528.987<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>14 | 2.65 ft          | 192.02034<br>ft | -21.193533<br>psf | 3,556.5692<br>psf | 2,398.9362<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>15 | 4.95 ft          | 192.57209<br>ft | -22.013664<br>psf | 3,368.4004<br>psf | 2,272.0147<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>16 | 7.1 ft           | 193.16431<br>ft | -27.551338<br>psf | 4,933.148<br>psf  | 3,327.4504<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>17 | 9.6 ft           | 193.96626<br>ft | -41.061281<br>psf | 4,889.6345<br>psf | 3,298.1001<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>18 | 11.4 ft          | 194.58456<br>ft | -53.340267<br>psf | 4,692.394<br>psf  | 3,165.0597<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>19 | 12.9 ft          | 195.17336<br>ft | -71.036518<br>psf | 4,525.1291<br>psf | 3,052.2382<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>20 | 14.85 ft         | 195.97751<br>ft | -97.391985<br>psf | 2,828.1284<br>psf | 1,907.5967<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>21 | 16.3825 ft       | 196.66833<br>ft | -121.77589<br>psf | 2,697.3789<br>psf | 2,107.4234<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>22 | 18.3225 ft       | 197.61809<br>ft | -151.8768<br>psf  | 2,394.0129<br>psf | 1,614.7821<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>23 | 20.6375 ft       | 198.8473<br>ft  | -189.3718<br>psf  | 2,295.7307<br>psf | 1,548.4899<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>24 | 22.9525 ft       | 200.19739<br>ft | -234.40916<br>psf | 2,188.8188<br>psf | 1,476.377<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>25 | 25.305 ft        | 201.70347<br>ft | -280.59734<br>psf | 2,071.1978<br>psf | 1,397.0405<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>26 | 28 ft            | 203.61892<br>ft | -336.5534<br>psf  | 1,922.2807<br>psf | 1,296.5947<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>27 | 29.51 ft         | 204.74245<br>ft | -371.0445<br>psf  | 1,840.3438<br>psf | 1,241.3276<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
|             |                  | l               |                   |                   |                   |       |       | ESU 2B Medium                         |

|             | ore wan (spens  | )               |                    |                   |                   |       |       |  |
|-------------|-----------------|-----------------|--------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>28 | 30.51 ft        | 205.56275<br>ft | -398.51615<br>psf  | 1,779.8865<br>psf | 1,200.5486<br>psf | 0 psf | 0 psf | Dense<br>Sand/Gravel                                   |
| Slice<br>29 | 31.865 ft       | 206.69124<br>ft | -436.79766<br>psf  | 1,698.4587<br>psf | 1,145.6248<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                  |
| Slice<br>30 | 33.4475 ft      | 208.13206<br>ft | -487.50578<br>psf  | 1,595.6423<br>psf | 1,076.2743<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                  |
| Slice<br>31 | 35.8825 ft      | 210.50259<br>ft | -574.34203<br>psf  | 1,431.9559<br>psf | 965.86645<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                  |
| Slice<br>32 | 38.05 ft        | 212.81793<br>ft | -664.44438<br>psf  | 1,277.7929<br>psf | 861.88222<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                  |
| Slice<br>33 | 40.5 ft         | 215.78694<br>ft | -788.24917<br>psf  | 1,217.6007<br>psf | 821.28203<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                  |
| Slice<br>34 | 43.5 ft         | 219.9186<br>ft  | -970.80587<br>psf  | 880.17528<br>psf  | 593.68572<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                  |
| Slice<br>35 | 46.447672<br>ft | 224.76067<br>ft | -1,199.0047<br>psf | 545.65025<br>psf  | 368.04574<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                  |
| Slice<br>36 | 49.248476<br>ft | 230.47803<br>ft | -1,485.5061<br>psf | 203.24754<br>psf  | 176.68039<br>psf  | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill |

# 2B.2 Global - Static FC Wall (M-P)

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### **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Bo Zhang Revision Number: 314 Date: 01/12/2022

Time: 10:44:22 AM

Tool Version: 11.1.1.22700

File Name: Wall 05.85L-B Sta 2+60\_FC Wall (lightweight fill).gsz Directory: P:\0\0180366\01\Analysis\Wall 05.85L-B\22-01-13\

Last Solved Date: 01/12/2022 Last Solved Time: 10:49:14 AM

### **Project Settings**

Unit System: U.S. Customary Units

## **Analysis Settings**

### 2B.2 Global - Static FC Wall (M-P)

**Description: With Forward Compatible Wall** 

Kind: SLOPE/W

Analysis Type: Morgenstern-Price

Settings

**Side Function** 

Interslice force function option: Half-Sine

PWP Conditions from: Piezometric Line

Apply Phreatic Correction: No
Use Staged Rapid Drawdown: No
Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 1

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

**Factor of Safety Convergence Settings** 

Maximum Number of Iterations: 100
Tolerable difference in F of S: 0.001

**Solution Settings** 

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

### **Materials**

### **ESU 1B Medium Dense to Very Dense Coarse-Grained Fill**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 41 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### **ESU 2B Medium Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 115 pcf Effective Cohesion: 0 psf Effective Friction Angle: 34 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### ESU 4B Dense to Very Dense Sand/Gravel

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **SEW Wall**

Material Model: High Strength

Unit Weight: 130 pcf
Pore Water Pressure
Piezometric Line: 1

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 42 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### Forward Compatible Wall

Material Model: High Strength

Unit Weight: 130 pcf
Pore Water Pressure
Piezometric Line: 1

### **Lightweight EPS**

Material Model: Mohr-Coulomb

Unit Weight: 5 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 0 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### Slip Surface Entry and Exit

Left Type: Range

Left-Zone Left Coordinate: (-40.9, 191.85458) ft Left-Zone Right Coordinate: (-0.9, 199.92697) ft

Left-Zone Increment: 20

Right Type: Range

Right-Zone Left Coordinate: (20.000001, 233.5) ft Right-Zone Right Coordinate: (65, 233.85753) ft

Right-Zone Increment: 25
Radius Increments: 20

## **Slip Surface Limits**

Left Coordinate: (-80, 186.2) ft Right Coordinate: (80, 234.2) ft

### **Piezometric Lines**

### Piezometric Line 1

#### **Coordinates**

|               | X         | Υ          |
|---------------|-----------|------------|
| Coordinate 1  | -48.3 ft  | 180 ft     |
| Coordinate 2  | -4.1 ft   | 190.1 ft   |
| Coordinate 3  | 11.7 ft   | 193.8 ft   |
| Coordinate 4  | 17.165 ft | 194.87 ft  |
| Coordinate 5  | 24.11 ft  | 196.755 ft |
| Coordinate 6  | 29.52 ft  | 198.8 ft   |
| Coordinate 7  | 32.23 ft  | 199.83 ft  |
| Coordinate 8  | 60.885 ft | 211.35 ft  |
| Coordinate 9  | 70.775 ft | 215.12 ft  |
| Coordinate 10 | 74.125 ft | 216.15 ft  |
| Coordinate 11 | 80 ft     | 217.365 ft |
|               |           |            |

## **Surcharge Loads**

### **Surcharge Load 1**

Surcharge (Unit Weight): 250 pcf

**Direction: Vertical** 

#### **Coordinates**

| Х       | Υ        |
|---------|----------|
| 8.1 ft  | 234.5 ft |
| 45 ft   | 234.5 ft |
| 58.1 ft | 234.7 ft |
| 80 ft   | 235.2 ft |

## **Geometry**

Name: 2. Global Stability

**Settings** 

View: 2D

Element Thickness: 1 ft

### **Points**

|          | Х        | Υ        |
|----------|----------|----------|
| Point 1  | 80 ft    | 199.4 ft |
| Point 2  | 58 ft    | 196.6 ft |
| Point 3  | 37.6 ft  | 191.9 ft |
| Point 4  | 42.1 ft  | 180 ft   |
| Point 5  | 80 ft    | 180 ft   |
| Point 6  | 80 ft    | 226 ft   |
| Point 7  | 58 ft    | 225.3 ft |
| Point 8  | 29.8 ft  | 195 ft   |
| Point 9  | 11.7 ft  | 193.8 ft |
| Point 10 | -48.3 ft | 180 ft   |
| Point 11 | 80 ft    | 234.2 ft |
| Point 12 | 58.1 ft  | 233.7 ft |
| Point 13 | 26.5 ft  | 214.1 ft |
| Point 14 | -10.8 ft | 197 ft   |
| Point 15 | -18.3 ft | 195.3 ft |
| Point 16 | -21.1 ft | 194.7 ft |
| Point 17 | -24.4 ft | 193.6 ft |
| Point 18 | -32.1 ft | 193.1 ft |
| Point 19 | -36.6 ft | 192.3 ft |
| Point 20 | -61.7 ft | 189.7 ft |
| Point 21 | -65.4 ft | 189.3 ft |
| Point 22 | -73.2 ft | 188 ft   |
| Point 23 | -80 ft   | 186.2 ft |
| Point 24 | -80 ft   | 180 ft   |
| Point 25 | -4.1 ft  | 190.1 ft |
| Point 26 | 32 ft    | 197.4 ft |
| Point 27 | -0.9 ft  | 219.4 ft |
| Point 28 | -0.9 ft  | 196.3 ft |
| Point 29 | -4.9 ft  | 199.8 ft |
| Point 30 | -0.9 ft  | 199.8 ft |
| Point 31 | -0.9 ft  | 199.4 ft |
| Point 32 | 17.1 ft  | 196.3 ft |
| Point 33 | 15.6 ft  | 219.4 ft |
| Point 34 | 11.1 ft  | 196.3 ft |
| Point 35 | 17.1 ft  | 214.2 ft |
| Point 36 | 45 ft    | 233.5 ft |
| Point 37 | 37.1 ft  | 228.2 ft |
| Point 38 | 29.4 ft  | 222.3 ft |
| Point 39 | 29.5 ft  | 233.5 ft |
| Point 40 | 1.5 ft   | 219.4 ft |
|          |          |          |

| Point 41 | 31.5 ft | 233.5 ft  |
|----------|---------|-----------|
| Point 42 | 6.1 ft  | 233.5 ft  |
| Point 43 | 14.1 ft | 233.5 ft  |
| Point 44 | 14.1 ft | 219.4 ft  |
| Point 45 | 6.1 ft  | 219.4 ft  |
| Point 46 | 14.1 ft | 225.9 ft  |
| Point 47 | 6.1 ft  | 221.74 ft |
| Point 48 | 15.6 ft | 214.2 ft  |
| Point 49 | 15.6 ft | 196.3 ft  |
| Point 50 | 17.1 ft | 208.4 ft  |
| Point 51 | 17.1 ft | 219.4 ft  |
| Point 52 | 6.1 ft  | 232 ft    |
| Point 53 | 14.1 ft | 232 ft    |
| Point 54 | 39 ft   | 233.5 ft  |
| Point 55 | 39 ft   | 230.5 ft  |

## Regions

|              | Material   | Points  | Area                      |
|--------------|--|---|---------------------------|
| Region<br>1  | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 1,2,3,4,5                                       | 659.92<br>ft <sup>2</sup> |
| Region<br>2  | ESU 4B Dense to Very Dense Sand/Gravel                           | 1,6,7,26,8,9,25,10,4,3,2                        | 1,867.8<br>ft²            |
| Region<br>3  | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill        | 14,29,30,31                                     | 7.58 ft <sup>2</sup>      |
| Region<br>4  | SEW Wall   | 27,30,31,28,34,49,48,33,44,45,40                | 381.15<br>ft <sup>2</sup> |
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel                                  | 14,15,16,17,18,19,20,21,22,23,24,10,25,34,28,31 | 748.7<br>ft <sup>2</sup>  |
| Region<br>6  | ESU 2B Medium Dense Sand/Gravel                                  | 7,6,11,12,13,50,32,49,34,25,9,8,26              | 856.44<br>ft²             |
| Region<br>7  | Forward Compatible Wall  | 45,44,46,47                                     | 35.36<br>ft <sup>2</sup>  |
| Region<br>8  | Common Borrow  | 36,55,51,35,38,37                               | 75.79<br>ft²              |
| Region<br>9  | Lightweight EPS  | 43,53,46,39                                     | 58.52<br>ft <sup>2</sup>  |
| Region<br>10 | Forward Compatible Wall  | 43,42,52,53                                     | 12 ft²                    |
| Region<br>11 |  | 47,40,45  | 5.382<br>ft <sup>2</sup>  |
| Region<br>12 | Gravel Borrow  | 32,50,35,48,49                                  | 26.85<br>ft <sup>2</sup>  |
| Region<br>13 | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill        | 35,50,13,12,36,37,38                            | 241.79<br>ft²             |
| Region<br>14 | Gravel Borrow  | 33,48,35,51                                     | 7.8 ft <sup>2</sup>       |
| Region<br>15 | Forward Compatible Wall  | 47,46,53,52                                     | 65.44<br>ft²              |
| Region<br>16 | Lightweight EPS  | 41,39,46,44,33,51,55,54                         | 171.02<br>ft²             |
| Region       |  |   |                           |

Common Borrow 36,54,55 9 ft<sup>2</sup>

## **Slip Results**

Slip Surfaces Analysed: 1764 of 11466 converged

### **Current Slip Surface**

Slip Surface: 3,101 Factor of Safety: 1.5 Volume: 1,536.2538 ft<sup>3</sup> Weight: 163,163.5 lbf

Resisting Moment: 7,470,604.9 lbf·ft Activating Moment: 4,992,124.5 lbf·ft

Resisting Force: 97,699.546 lbf Activating Force: 65,300.757 lbf Slip Rank: 1 of 11,466 slip surfaces Exit: (-30.671631, 193.19275) ft Entry: (50.601608, 233.58552) ft

Radius: 66.587809 ft

Center: (-11.723356, 257.02769) ft

### **Slip Slices**

|            | x                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material                         |
|------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|---------------------------------------|
| Slice<br>1 | -29.103723<br>ft | 192.76867<br>ft | -523.04891<br>psf | 73.610151<br>psf         | 49.650674<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>2 | -25.967908<br>ft | 192.00113<br>ft | -430.4414<br>psf  | 221.13724<br>psf         | 149.15895<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>3 | -22.75 ft        | 191.38052<br>ft | -345.83178<br>psf | 428.02183<br>psf         | 288.70437<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>4 | -19.7 ft         | 190.93441<br>ft | -274.50507<br>psf | 647.4718<br>psf          | 436.72525<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>5 | -17.05 ft        | 190.66512<br>ft | -219.91518<br>psf | 799.05469<br>psf         | 538.96919<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>6 | -14.55 ft        | 190.51167<br>ft | -174.69272<br>psf | 922.90431<br>psf         | 622.50682<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>7 | -12.05 ft        | 190.45241<br>ft | -135.3483<br>psf  | 1,021.5192<br>psf        | 689.02342<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>8 | -9.325 ft        | 190.49946<br>ft | -99.428369<br>psf | 1,154.2945<br>psf        | 778.58149<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |

| Slice<br>9  | -6.375 ft        | 190.67152<br>ft | -68.10139<br>psf  | 1,308.9014<br>psf | 882.86512<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
|-------------|------------------|-----------------|-------------------|-------------------|-------------------|-------|-------|---------------------------------------|
| Slice<br>10 | -4.5 ft          | 190.83405<br>ft | -51.508337<br>psf | 1,356.7884<br>psf | 915.16531<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>11 | -2.6625312<br>ft | 191.07519<br>ft | -39.846403<br>psf | 1,279.5664<br>psf | 863.07843<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>12 | -1.0625312<br>ft | 191.29903<br>ft | -30.434203<br>psf | 1,208.6673<br>psf | 815.25641<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>13 | 0.3 ft           | 191.54573<br>ft | -25.917929<br>psf | 3,966.9348<br>psf | 2,675.7313<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>14 | 2.65 ft          | 192.02034<br>ft | -21.193533<br>psf | 3,754.6028<br>psf | 2,532.5116<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>15 | 4.95 ft          | 192.57209<br>ft | -22.013664<br>psf | 3,526.871<br>psf  | 2,378.9045<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>16 | 7.1 ft           | 193.16431<br>ft | -27.551338<br>psf | 5,080.1017<br>psf | 3,426.5718<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>17 | 9.6 ft           | 193.96626<br>ft | -41.061281<br>psf | 4,966.5129<br>psf | 3,349.9553<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>18 | 11.4 ft          | 194.58456<br>ft | -53.340267<br>psf | 4,714.7482<br>psf | 3,180.1378<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>19 | 12.9 ft          | 195.17336<br>ft | -71.036518<br>psf | 4,503.2813<br>psf | 3,037.5016<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>20 | 14.85 ft         | 195.97751<br>ft | -97.391985<br>psf | 2,751.5284<br>psf | 1,855.9293<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>21 | 16.3825 ft       | 196.66833<br>ft | -121.77589<br>psf | 2,607.2458<br>psf | 2,037.0037<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>22 | 18.3225 ft       | 197.61809<br>ft | -151.8768<br>psf  | 2,252.8747<br>psf | 1,519.5832<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>23 | 20.6375 ft       | 198.8473<br>ft  | -189.3718<br>psf  | 2,125.2683<br>psf | 1,433.5116<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>24 | 22.9525 ft       | 200.19739<br>ft | -234.40916<br>psf | 2,000.483<br>psf  | 1,349.3428<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>25 | 25.305 ft        | 201.70347<br>ft | -280.59734<br>psf | 1,876.9752<br>psf | 1,266.0358<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>26 | 28 ft            | 203.61892<br>ft | -336.5534<br>psf  | 1,736.7233<br>psf | 1,171.4347<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
|             |                  |                 |                   |                   |                   |       |       | ESU 2B Medium                         |

| Slice<br>27 | 29.51 ft        | 204.74245<br>ft | -371.0445<br>psf   | 1,665.3716<br>psf | 1,123.3073<br>psf | 0 psf | 0 psf | Dense<br>Sand/Gravel                                   |
|-------------|-----------------|-----------------|--------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>28 | 30.51 ft        | 205.56275<br>ft | -398.51615<br>psf  | 1,615.4648<br>psf | 1,089.6448<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                  |
| Slice<br>29 | 31.865 ft       | 206.69124<br>ft | -436.79766<br>psf  | 1,550.5301<br>psf | 1,045.8457<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                  |
| Slice<br>30 | 33.4475 ft      | 208.13206<br>ft | -487.50578<br>psf  | 1,472.0255<br>psf | 992.89372<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                  |
| Slice<br>31 | 35.8825 ft      | 210.50259<br>ft | -574.34203<br>psf  | 1,352.3638<br>psf | 912.18087<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                  |
| Slice<br>32 | 38.05 ft        | 212.81793<br>ft | -664.44438<br>psf  | 1,242.8916<br>psf | 838.34099<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                  |
| Slice<br>33 | 40.5 ft         | 215.78694<br>ft | -788.24917<br>psf  | 1,254.7536<br>psf | 846.34201<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                  |
| Slice<br>34 | 43.5 ft         | 219.9186<br>ft  | -970.80587<br>psf  | 974.57752<br>psf  | 657.36084<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                  |
| Slice<br>35 | 46.447672<br>ft | 224.76067<br>ft | -1,199.0047<br>psf | 666.17182<br>psf  | 449.33857<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                  |
| Slice<br>36 | 49.248476<br>ft | 230.47803<br>ft | -1,485.5061<br>psf | 265.84408<br>psf  | 231.09474<br>psf  | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill |

# 2B.3 Global - Pseudo-Static FC Wall (Spencer)

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### **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Bo Zhang Revision Number: 314 Date: 01/12/2022 Time: 10:44:22 AM

Tool Version: 11.1.1.22700

File Name: Wall 05.85L-B Sta 2+60\_FC Wall (lightweight fill).gsz Directory: P:\0\0180366\01\Analysis\Wall 05.85L-B\22-01-13\

Last Solved Date: 01/12/2022 Last Solved Time: 10:49:24 AM

### **Project Settings**

Unit System: U.S. Customary Units

### **Analysis Settings**

### 2B.3 Global - Pseudo-Static FC Wall (Spencer)

**Description: With Forward Compatible Wall** 

Kind: SLOPE/W

Analysis Type: Spencer

Settings

PWP Conditions from: Piezometric Line

Apply Phreatic Correction: No
Use Staged Rapid Drawdown: No
Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 1

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

**Factor of Safety Convergence Settings** 

Maximum Number of Iterations: 100 Tolerable difference in F of S: 0.001

**Solution Settings** 

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

### **Materials**

### ESU 4B Dense to Very Dense Sand/Gravel

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **SEW Wall**

Material Model: High Strength

Unit Weight: 130 pcf
Pore Water Pressure
Piezometric Line: 1

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 42 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### **ESU 1B Medium Dense to Very Dense Coarse-Grained Fill (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 100 psf Effective Friction Angle: 41 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### **ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 115 pcf Effective Cohesion: 200 psf Effective Friction Angle: 34°

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### **Forward Compatible Wall**

Material Model: High Strength

Unit Weight: 130 pcf
Pore Water Pressure
Piezometric Line: 1

### **Common Borrow (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 50 psf Effective Friction Angle: 32 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### **Lightweight EPS**

Material Model: Mohr-Coulomb

Unit Weight: 5 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 0 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### Slip Surface Entry and Exit

Left Type: Range

Left-Zone Left Coordinate: (-40.9, 191.85458) ft Left-Zone Right Coordinate: (-0.9, 199.92697) ft

Left-Zone Increment: 20

Right Type: Range

Right-Zone Left Coordinate: (20.000001, 233.5) ft

Right-Zone Right Coordinate: (65, 233.85753) ft

Right-Zone Increment: 25 Radius Increments: 20

## **Slip Surface Limits**

Left Coordinate: (-80, 186.2) ft Right Coordinate: (80, 234.2) ft

### **Piezometric Lines**

### Piezometric Line 1

#### Coordinates

|               | Х         | Υ          |
|---------------|-----------|------------|
| Coordinate 1  | -48.3 ft  | 180 ft     |
| Coordinate 2  | -4.1 ft   | 190.1 ft   |
| Coordinate 3  | 11.7 ft   | 193.8 ft   |
| Coordinate 4  | 17.165 ft | 194.87 ft  |
| Coordinate 5  | 24.11 ft  | 196.755 ft |
| Coordinate 6  | 29.52 ft  | 198.8 ft   |
| Coordinate 7  | 32.23 ft  | 199.83 ft  |
| Coordinate 8  | 60.885 ft | 211.35 ft  |
| Coordinate 9  | 70.775 ft | 215.12 ft  |
| Coordinate 10 | 74.125 ft | 216.15 ft  |
| Coordinate 11 | 80 ft     | 217.365 ft |

### **Seismic Coefficients**

Horz Seismic Coef.: 0.197

## **Surcharge Loads**

### Surcharge Load 1

Surcharge (Unit Weight): 125 pcf

**Direction: Vertical** 

#### **Coordinates**

| Х       | Υ        |
|---------|----------|
| 8.1 ft  | 234.5 ft |
| 45 ft   | 234.5 ft |
| 58.1 ft | 234.7 ft |
| 80 ft   | 235.2 ft |

## **Geometry**

Name: 2. Global Stability

## Settings

View: 2D

Element Thickness: 1 ft

### **Points**

| 11.5     |          |          |  |  |  |
|----------|----------|----------|--|--|--|
|          | Х        | Υ        |  |  |  |
| Point 1  | 80 ft    | 199.4 ft |  |  |  |
| Point 2  | 58 ft    | 196.6 ft |  |  |  |
| Point 3  | 37.6 ft  | 191.9 ft |  |  |  |
| Point 4  | 42.1 ft  | 180 ft   |  |  |  |
| Point 5  | 80 ft    | 180 ft   |  |  |  |
| Point 6  | 80 ft    | 226 ft   |  |  |  |
| Point 7  | 58 ft    | 225.3 ft |  |  |  |
| Point 8  | 29.8 ft  | 195 ft   |  |  |  |
| Point 9  | 11.7 ft  | 193.8 ft |  |  |  |
| Point 10 | -48.3 ft | 180 ft   |  |  |  |
| Point 11 | 80 ft    | 234.2 ft |  |  |  |
| Point 12 | 58.1 ft  | 233.7 ft |  |  |  |
| Point 13 | 26.5 ft  | 214.1 ft |  |  |  |
| Point 14 | -10.8 ft | 197 ft   |  |  |  |
| Point 15 | -18.3 ft | 195.3 ft |  |  |  |
| Point 16 | -21.1 ft | 194.7 ft |  |  |  |
| Point 17 | -24.4 ft | 193.6 ft |  |  |  |
| Point 18 | -32.1 ft | 193.1 ft |  |  |  |
| Point 19 | -36.6 ft | 192.3 ft |  |  |  |
| Point 20 | -61.7 ft | 189.7 ft |  |  |  |
| Point 21 | -65.4 ft | 189.3 ft |  |  |  |
| Point 22 | -73.2 ft | 188 ft   |  |  |  |
| Point 23 | -80 ft   | 186.2 ft |  |  |  |
| Point 24 | -80 ft   | 180 ft   |  |  |  |
| Point 25 | -4.1 ft  | 190.1 ft |  |  |  |
| Point 26 | 32 ft    | 197.4 ft |  |  |  |
| Point 27 | -0.9 ft  | 219.4 ft |  |  |  |
| Point 28 | -0.9 ft  | 196.3 ft |  |  |  |
| Point 29 | -4.9 ft  | 199.8 ft |  |  |  |
| Point 30 | -0.9 ft  | 199.8 ft |  |  |  |
| Point 31 | -0.9 ft  | 199.4 ft |  |  |  |
| Point 32 | 17.1 ft  | 196.3 ft |  |  |  |
| Point 33 | 15.6 ft  | 219.4 ft |  |  |  |
| Point 34 | 11.1 ft  | 196.3 ft |  |  |  |
| Point 35 | 17.1 ft  | 214.2 ft |  |  |  |
| Point 36 | 45 ft    | 233.5 ft |  |  |  |
| Point 37 | 37.1 ft  | 228.2 ft |  |  |  |
| Point 38 | 29.4 ft  | 222.3 ft |  |  |  |
| Point 39 | 29.5 ft  | 233.5 ft |  |  |  |
|          |          | . ——     |  |  |  |

| Point 40 | 1.5 ft  | 219.4 ft  |
|----------|---------|-----------|
| Point 41 | 31.5 ft | 233.5 ft  |
| Point 42 | 6.1 ft  | 233.5 ft  |
| Point 43 | 14.1 ft | 233.5 ft  |
| Point 44 | 14.1 ft | 219.4 ft  |
| Point 45 | 6.1 ft  | 219.4 ft  |
| Point 46 | 14.1 ft | 225.9 ft  |
| Point 47 | 6.1 ft  | 221.74 ft |
| Point 48 | 15.6 ft | 214.2 ft  |
| Point 49 | 15.6 ft | 196.3 ft  |
| Point 50 | 17.1 ft | 208.4 ft  |
| Point 51 | 17.1 ft | 219.4 ft  |
| Point 52 | 6.1 ft  | 232 ft    |
| Point 53 | 14.1 ft | 232 ft    |
| Point 54 | 39 ft   | 233.5 ft  |
| Point 55 | 39 ft   | 230.5 ft  |

## Regions

|              | Material  | Points  | Area                       |
|--------------|---|---|----------------------------|
| Region<br>1  | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt              | 1,2,3,4,5                                       | 659.92<br>ft <sup>2</sup>  |
| Region<br>2  | ESU 4B Dense to Very Dense Sand/Gravel  | 1,6,7,26,8,9,25,10,4,3,2                        | 1,867.8<br>ft <sup>2</sup> |
| Region<br>3  | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill (Apparent Cohesion) | 14,29,30,31                                     | 7.58 ft <sup>2</sup>       |
| Region<br>4  | SEW Wall  | 27,30,31,28,34,49,48,33,44,45,40                | 381.15<br>ft <sup>2</sup>  |
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                           | 14,15,16,17,18,19,20,21,22,23,24,10,25,34,28,31 | 748.7<br>ft <sup>2</sup>   |
| Region<br>6  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                           | 7,6,11,12,13,50,32,49,34,25,9,8,26              | 856.44<br>ft <sup>2</sup>  |
| Region<br>7  | Forward Compatible Wall   | 45,44,46,47                                     | 35.36<br>ft <sup>2</sup>   |
| Region<br>8  | Common Borrow (Apparent Cohesion)   | 36,55,51,35,38,37                               | 75.79<br>ft²               |
| Region<br>9  | Lightweight EPS   | 43,53,46,39                                     | 58.52<br>ft <sup>2</sup>   |
| Region<br>10 | Forward Compatible Wall   | 43,42,52,53                                     | 12 ft²                     |
| Region<br>11 |   | 47,40,45  | 5.382<br>ft <sup>2</sup>   |
| Region<br>12 | Gravel Borrow   | 32,50,35,48,49                                  | 26.85<br>ft <sup>2</sup>   |
| Region<br>13 | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill (Apparent Cohesion) | 35,50,13,12,36,37,38                            | 241.79<br>ft <sup>2</sup>  |
| Region<br>14 | Gravel Borrow   | 33,48,35,51                                     | 7.8 ft <sup>2</sup>        |
| Region<br>15 | Forward Compatible Wall   | 47,46,53,52                                     | 65.44<br>ft <sup>2</sup>   |
| Region<br>16 | Lightweight EPS   | 41,39,46,44,33,51,55,54                         | 171.02<br>ft <sup>2</sup>  |

Region 17

Common Borrow (Apparent Cohesion)

36,54,55

9 ft<sup>2</sup>

## **Slip Results**

Slip Surfaces Analysed: 971 of 11466 converged

### **Current Slip Surface**

Slip Surface: 2,070 Factor of Safety: 1.3 Volume: 1,662.3467 ft<sup>3</sup> Weight: 177,985.54 lbf

Resisting Moment: 10,585,397 lbf·ft Activating Moment: 8,057,639 lbf·ft Resisting Force: 118,889.15 lbf Activating Force: 90,479.516 lbf Slip Rank: 1 of 11,466 slip surfaces Exit: (-34.756941, 192.62766) ft Entry: (56.001378, 233.66796) ft

Radius: 79.563783 ft

Center: (-14.943487, 269.68492) ft

### Slip Slices

|            | x                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material   |
|------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|---|
| Slice<br>1 | -33.42847<br>ft  | 192.31028<br>ft | -556.11098<br>psf | 653.50667<br>psf         | 440.79581<br>psf       | 200 psf              | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>2 | -30.816667<br>ft | 191.73159<br>ft | -482.75933<br>psf | 812.05672<br>psf         | 547.73917<br>psf       | 200 psf              | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>3 | -28.25 ft        | 191.25255<br>ft | -416.26943<br>psf | 875.6494<br>psf          | 590.63298<br>psf       | 200 psf              | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>4 | -25.683333<br>ft | 190.85997<br>ft | -355.17489<br>psf | 907.42491<br>psf         | 612.06583<br>psf       | 200 psf              | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>5 | -22.75 ft        | 190.5224<br>ft  | -292.28489<br>psf | 1,004.071<br>psf         | 677.25443<br>psf       | 200 psf              | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent              |

|             |            |                 |                   |                   |                   |         |       | Cohesion)   |
|-------------|------------|-----------------|-------------------|-------------------|-------------------|---------|-------|---|
| Slice<br>6  | -19.7 ft   | 190.27583<br>ft | -233.40945<br>psf | 1,102.4351<br>psf | 743.60186<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>7  | -16.425 ft | 190.15704<br>ft | -179.29946<br>psf | 1,134.0562<br>psf | 764.93059<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>8  | -12.675 ft | 190.17561<br>ft | -126.98744<br>psf | 1,143.319<br>psf  | 771.17839<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>9  | -9.325 ft  | 190.33354<br>ft | -89.075424<br>psf | 1,187.3695<br>psf | 800.89085<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>10 | -6.375 ft  | 190.59779<br>ft | -63.500632<br>psf | 1,263.8719<br>psf | 852.49236<br>psf  | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>11 | -4.5 ft    | 190.81055<br>ft | -50.042038<br>psf | 1,274.4901<br>psf | 859.65442<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>12 | -2.5 ft    | 191.11692<br>ft | -40.07564<br>psf  | 1,173.1915<br>psf | 791.32769<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>13 | 0.3 ft     | 191.6046<br>ft  | -29.591407<br>psf | 3,611.997<br>psf  | 2,436.3227<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>14 | 2.65 ft    | 192.09965<br>ft | -26.142884<br>psf | 3,390.8409<br>psf | 2,287.151<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>15 | 4.95 ft    | 192.65743<br>ft | -27.339381<br>psf | 3,182.294<br>psf  | 2,146.4844<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>16 | 7.1 ft     | 193.24281<br>ft | -32.449431<br>psf | 4,589.33<br>psf   | 3,095.5422<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent              |

|             |                 |                 |                   |                   |                   |         |       | Cohesion)   |
|-------------|-----------------|-----------------|-------------------|-------------------|-------------------|---------|-------|---|
| Slice<br>17 | 9.6 ft          | 194.01772<br>ft | -44.272157<br>psf | 4,426.025<br>psf  | 2,985.3915<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>18 | 11.4 ft         | 194.60953<br>ft | -54.898289<br>psf | 4,225.5963<br>psf | 2,850.2007<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>19 | 12.9 ft         | 195.16315<br>ft | -70.399693<br>psf | 4,059.6177<br>psf | 2,738.2467<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>20 | 14.85 ft        | 195.9144<br>ft  | -93.454108<br>psf | 2,517.8407<br>psf | 1,698.305<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>21 | 15.699077<br>ft | 196.25865<br>ft | -104.56166<br>psf | 2,448.6749<br>psf | 1,651.6521<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>22 | 16.481577<br>ft | 196.59383<br>ft | -115.91684<br>psf | 2,393.5692<br>psf | 1,870.0612<br>psf | 0 psf   | 0 psf | Gravel Borrow   |
| Slice<br>23 | 18.90125 ft     | 197.70404<br>ft | -147.43779<br>psf | 2,094.8932<br>psf | 1,413.0233<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>24 | 22.37375 ft     | 199.44281<br>ft | -197.1256<br>psf  | 1,956.6589<br>psf | 1,319.7831<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>25 | 25.305 ft       | 201.06615<br>ft | -240.82905<br>psf | 1,834.2519<br>psf | 1,237.2185<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>26 | 28 ft           | 202.72914<br>ft | -281.03125<br>psf | 1,712.3055<br>psf | 1,154.9646<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>27 | 29.51 ft        | 203.69793<br>ft | -305.86691<br>psf | 1,646.6629<br>psf | 1,110.6881<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
|             |                 |                 |                   |                   |                   |         |       | ESU 2B Medium<br>Dense  |

| Slice<br>28 | 30.51 ft        | 204.39388<br>ft | -325.5784<br>psf   | 1,599.5285<br>psf | 1,078.8956<br>psf | 200 psf | 0 psf | Sand/Gravel<br>(Apparent<br>Cohesion)                                      |
|-------------|-----------------|-----------------|--------------------|-------------------|-------------------|---------|-------|--|
| Slice<br>29 | 31.865 ft       | 205.34864<br>ft | -353.01972<br>psf  | 1,536.4731<br>psf | 1,036.3642<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                        |
| Slice<br>30 | 33.4475 ft      | 206.54734<br>ft | -388.61925<br>psf  | 1,458.8915<br>psf | 984.03474<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                        |
| Slice<br>31 | 35.8825 ft      | 208.49171<br>ft | -448.86284<br>psf  | 1,337.8477<br>psf | 902.38964<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                        |
| Slice<br>32 | 38.05 ft        | 210.35143<br>ft | -510.53497<br>psf  | 1,226.6021<br>psf | 827.35353<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                        |
| Slice<br>33 | 40.5 ft         | 212.65828<br>ft | -593.02074<br>psf  | 1,212.3738<br>psf | 817.75646<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                        |
| Slice<br>34 | 43.5 ft         | 215.74178<br>ft | -710.17214<br>psf  | 962.79607<br>psf  | 649.41415<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                        |
| Slice<br>35 | 46.669017<br>ft | 219.41241<br>ft | -859.7211<br>psf   | 701.03826<br>psf  | 472.85628<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                        |
| Slice<br>36 | 50.007051<br>ft | 223.82153<br>ft | -1,051.111<br>psf  | 431.563<br>psf    | 291.09292<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                        |
| Slice<br>37 | 53.345085<br>ft | 228.98556<br>ft | -1,289.6072<br>psf | 173.65588<br>psf  | 117.13237<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                        |
| Slice<br>38 | 55.50774 ft     | 232.72696<br>ft | -1,468.8179<br>psf | 44.028516<br>psf  | 38.273405<br>psf  | 100 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill (Apparent Cohesion) |

# 2B.4 Global - Pseudo-Static FC Wall (M-P)

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### **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Bo Zhang Revision Number: 314 Date: 01/12/2022 Time: 10:44:22 AM

Tool Version: 11.1.1.22700

File Name: Wall 05.85L-B Sta 2+60\_FC Wall (lightweight fill).gsz Directory: P:\0\0180366\01\Analysis\Wall 05.85L-B\22-01-13\

Last Solved Date: 01/12/2022 Last Solved Time: 10:49:28 AM

### **Project Settings**

Unit System: U.S. Customary Units

## **Analysis Settings**

### 2B.4 Global - Pseudo-Static FC Wall (M-P)

**Description: With Forward Compatible Wall** 

Kind: SLOPE/W

Analysis Type: Morgenstern-Price

Settings

**Side Function** 

Interslice force function option: Half-Sine

PWP Conditions from: Piezometric Line

Apply Phreatic Correction: No
Use Staged Rapid Drawdown: No
Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 1

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

**Factor of Safety Convergence Settings** 

Maximum Number of Iterations: 100
Tolerable difference in F of S: 0.001

**Solution Settings** 

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

### **Materials**

### **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **SEW Wall**

Material Model: High Strength

Unit Weight: 130 pcf
Pore Water Pressure
Piezometric Line: 1

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 42 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### **ESU 1B Medium Dense to Very Dense Coarse-Grained Fill (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 41°

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### **ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 115 pcf Effective Cohesion: 200 psf Effective Friction Angle: 34 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### **Forward Compatible Wall**

Material Model: High Strength

Unit Weight: 130 pcf
Pore Water Pressure
Piezometric Line: 1

### **Common Borrow (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 50 psf Effective Friction Angle: 32 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### **Lightweight EPS**

Material Model: Mohr-Coulomb

Unit Weight: 5 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 0 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### Slip Surface Entry and Exit

Left Type: Range

Left-Zone Left Coordinate: (-40.9, 191.85458) ft Left-Zone Right Coordinate: (-0.9, 199.92697) ft

Left-Zone Increment: 20

Right Type: Range

Right-Zone Left Coordinate: (20.000001, 233.5) ft Right-Zone Right Coordinate: (65, 233.85753) ft

Right-Zone Increment: 25
Radius Increments: 20

## **Slip Surface Limits**

Left Coordinate: (-80, 186.2) ft Right Coordinate: (80, 234.2) ft

### **Piezometric Lines**

### Piezometric Line 1

#### Coordinates

|               | Х         | Υ          |
|---------------|-----------|------------|
| Coordinate 1  | -48.3 ft  | 180 ft     |
| Coordinate 2  | -4.1 ft   | 190.1 ft   |
| Coordinate 3  | 11.7 ft   | 193.8 ft   |
| Coordinate 4  | 17.165 ft | 194.87 ft  |
| Coordinate 5  | 24.11 ft  | 196.755 ft |
| Coordinate 6  | 29.52 ft  | 198.8 ft   |
| Coordinate 7  | 32.23 ft  | 199.83 ft  |
| Coordinate 8  | 60.885 ft | 211.35 ft  |
| Coordinate 9  | 70.775 ft | 215.12 ft  |
| Coordinate 10 | 74.125 ft | 216.15 ft  |
| Coordinate 11 | 80 ft     | 217.365 ft |

### **Seismic Coefficients**

Horz Seismic Coef.: 0.197

## **Surcharge Loads**

### Surcharge Load 1

Surcharge (Unit Weight): 125 pcf

**Direction: Vertical** 

#### Coordinates

| Х       | Υ        |
|---------|----------|
| 8.1 ft  | 234.5 ft |
| 45 ft   | 234.5 ft |
| 58.1 ft | 234.7 ft |
|         |          |

80 ft 235.2 ft

## **Geometry**

Name: 2. Global Stability

**Settings** 

View: 2D

Element Thickness: 1 ft

### **Points**

| 113      |          |          |
|----------|----------|----------|
|          | Х        | Υ        |
| Point 1  | 80 ft    | 199.4 ft |
| Point 2  | 58 ft    | 196.6 ft |
| Point 3  | 37.6 ft  | 191.9 ft |
| Point 4  | 42.1 ft  | 180 ft   |
| Point 5  | 80 ft    | 180 ft   |
| Point 6  | 80 ft    | 226 ft   |
| Point 7  | 58 ft    | 225.3 ft |
| Point 8  | 29.8 ft  | 195 ft   |
| Point 9  | 11.7 ft  | 193.8 ft |
| Point 10 | -48.3 ft | 180 ft   |
| Point 11 | 80 ft    | 234.2 ft |
| Point 12 | 58.1 ft  | 233.7 ft |
| Point 13 | 26.5 ft  | 214.1 ft |
| Point 14 | -10.8 ft | 197 ft   |
| Point 15 | -18.3 ft | 195.3 ft |
| Point 16 | -21.1 ft | 194.7 ft |
| Point 17 | -24.4 ft | 193.6 ft |
| Point 18 | -32.1 ft | 193.1 ft |
| Point 19 | -36.6 ft | 192.3 ft |
| Point 20 | -61.7 ft | 189.7 ft |
| Point 21 | -65.4 ft | 189.3 ft |
| Point 22 | -73.2 ft | 188 ft   |
| Point 23 | -80 ft   | 186.2 ft |
| Point 24 | -80 ft   | 180 ft   |
| Point 25 | -4.1 ft  | 190.1 ft |
| Point 26 | 32 ft    | 197.4 ft |
| Point 27 | -0.9 ft  | 219.4 ft |
| Point 28 | -0.9 ft  | 196.3 ft |
| Point 29 | -4.9 ft  | 199.8 ft |
| Point 30 | -0.9 ft  | 199.8 ft |
| Point 31 | -0.9 ft  | 199.4 ft |
| Point 32 | 17.1 ft  | 196.3 ft |
| Point 33 | 15.6 ft  | 219.4 ft |
| Point 34 | 11.1 ft  | 196.3 ft |
| Point 35 | 17.1 ft  | 214.2 ft |
| Point 36 | 45 ft    | 233.5 ft |
|          |          |          |

| Point 37 | 37.1 ft | 228.2 ft  |
|----------|---------|-----------|
| Point 38 | 29.4 ft | 222.3 ft  |
| Point 39 | 29.5 ft | 233.5 ft  |
| Point 40 | 1.5 ft  | 219.4 ft  |
| Point 41 | 31.5 ft | 233.5 ft  |
| Point 42 | 6.1 ft  | 233.5 ft  |
| Point 43 | 14.1 ft | 233.5 ft  |
| Point 44 | 14.1 ft | 219.4 ft  |
| Point 45 | 6.1 ft  | 219.4 ft  |
| Point 46 | 14.1 ft | 225.9 ft  |
| Point 47 | 6.1 ft  | 221.74 ft |
| Point 48 | 15.6 ft | 214.2 ft  |
| Point 49 | 15.6 ft | 196.3 ft  |
| Point 50 | 17.1 ft | 208.4 ft  |
| Point 51 | 17.1 ft | 219.4 ft  |
| Point 52 | 6.1 ft  | 232 ft    |
| Point 53 | 14.1 ft | 232 ft    |
| Point 54 | 39 ft   | 233.5 ft  |
| Point 55 | 39 ft   | 230.5 ft  |
|          |         |           |

## Regions

|              | Material  | Points  | Area                       |
|--------------|---|---|----------------------------|
| Region<br>1  | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt              | 1,2,3,4,5                                       | 659.92<br>ft <sup>2</sup>  |
| Region<br>2  | ESU 4B Dense to Very Dense Sand/Gravel  | 1,6,7,26,8,9,25,10,4,3,2                        | 1,867.8<br>ft <sup>2</sup> |
| Region<br>3  | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill (Apparent Cohesion) | 14,29,30,31                                     | 7.58 ft <sup>2</sup>       |
| Region<br>4  | SEW Wall  | 27,30,31,28,34,49,48,33,44,45,40                | 381.15<br>ft <sup>2</sup>  |
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                           | 14,15,16,17,18,19,20,21,22,23,24,10,25,34,28,31 | 748.7<br>ft²               |
| Region<br>6  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                           | 7,6,11,12,13,50,32,49,34,25,9,8,26              | 856.44<br>ft <sup>2</sup>  |
| Region<br>7  | Forward Compatible Wall   | 45,44,46,47                                     | 35.36<br>ft <sup>2</sup>   |
| Region<br>8  | Common Borrow (Apparent Cohesion)   | 36,55,51,35,38,37                               | 75.79<br>ft²               |
| Region<br>9  | Lightweight EPS   | 43,53,46,39                                     | 58.52<br>ft <sup>2</sup>   |
| Region<br>10 | Forward Compatible Wall   | 43,42,52,53                                     | 12 ft²                     |
| Region<br>11 |   | 47,40,45  | 5.382<br>ft²               |
| Region<br>12 | Gravel Borrow   | 32,50,35,48,49                                  | 26.85<br>ft <sup>2</sup>   |
| Region<br>13 | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill (Apparent Cohesion) | 35,50,13,12,36,37,38                            | 241.79<br>ft²              |
| Region<br>14 | Gravel Borrow   | 33,48,35,51                                     | 7.8 ft <sup>2</sup>        |

| Region<br>15 | Forward Compatible Wall           | 47,46,53,52             | 65.44<br>ft <sup>2</sup>  |
|--------------|-----------------------------------|-------------------------|---------------------------|
| Region<br>16 | Lightweight EPS                   | 41,39,46,44,33,51,55,54 | 171.02<br>ft <sup>2</sup> |
| Region<br>17 | Common Borrow (Apparent Cohesion) | 36,54,55                | 9 ft²                     |

## **Slip Results**

Slip Surfaces Analysed: 1712 of 11466 converged

## **Current Slip Surface**

Slip Surface: 2,070 Factor of Safety: 1.3 Volume: 1,662.3467 ft<sup>3</sup> Weight: 177,985.54 lbf

Resisting Moment: 10,563,522 lbf·ft Activating Moment: 8,057,639 lbf·ft Resisting Force: 118,787.18 lbf Activating Force: 90,612.569 lbf Slip Rank: 1 of 11,466 slip surfaces Exit: (-34.756941, 192.62766) ft Entry: (56.001378, 233.66796) ft

Radius: 79.563783 ft

Center: (-14.943487, 269.68492) ft

### Slip Slices

|            | X                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material   |
|------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|---|
| Slice<br>1 | -33.42847<br>ft  | 192.31028<br>ft | -556.11098<br>psf | 139.17015<br>psf         | 93.87145<br>psf        | 200 psf              | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>2 | -30.816667<br>ft | 191.73159<br>ft | -482.75933<br>psf | 313.14298<br>psf         | 211.21761<br>psf       | 200 psf              | 0 psf               | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>3 | -28.25 ft        | 191.25255<br>ft | -416.26943<br>psf | 469.82018<br>psf         | 316.89771<br>psf       | 200 psf              | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>4 | -25.683333<br>ft | 190.85997<br>ft | -355.17489<br>psf | 626.85026<br>psf         | 422.81584<br>psf       | 200 psf              | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |

| Slice<br>5  | -22.75 ft  | 190.5224<br>ft  | -292.28489<br>psf | 865.96343<br>psf  | 584.09971<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
|-------------|------------|-----------------|-------------------|-------------------|-------------------|---------|-------|---|
| Slice<br>6  | -19.7 ft   | 190.27583<br>ft | -233.40945<br>psf | 1,127.3446<br>psf | 760.40357<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>7  | -16.425 ft | 190.15704<br>ft | -179.29946<br>psf | 1,336.6428<br>psf | 901.57694<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>8  | -12.675 ft | 190.17561<br>ft | -126.98744<br>psf | 1,502.1328<br>psf | 1,013.2013<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>9  | -9.325 ft  | 190.33354<br>ft | -89.075424<br>psf | 1,625.5939<br>psf | 1,096.4769<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>10 | -6.375 ft  | 190.59779<br>ft | -63.500632<br>psf | 1,723.3027<br>psf | 1,162.3824<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>11 | -4.5 ft    | 190.81055<br>ft | -50.042038<br>psf | 1,725.9471<br>psf | 1,164.166<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>12 | -2.5 ft    | 191.11692<br>ft | -40.07564<br>psf  | 1,591.1732<br>psf | 1,073.2598<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>13 | 0.3 ft     | 191.6046<br>ft  | -29.591407<br>psf | 4,026.9843<br>psf | 2,716.2352<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>14 | 2.65 ft    | 192.09965<br>ft | -26.142884<br>psf | 3,723.229<br>psf  | 2,511.3497<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>15 | 4.95 ft    | 192.65743<br>ft | -27.339381<br>psf | 3,418.5136<br>psf | 2,305.8166<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |

| Slice<br>16 | 7.1 ft          | 193.24281<br>ft | -32.449431<br>psf | 4,731.9096<br>psf | 3,191.7133<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
|-------------|-----------------|-----------------|-------------------|-------------------|-------------------|---------|-------|---|
| Slice<br>17 | 9.6 ft          | 194.01772<br>ft | -44.272157<br>psf | 4,453.2181<br>psf | 3,003.7336<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>18 | 11.4 ft         | 194.60953<br>ft | -54.898289<br>psf | 4,173.8127<br>psf | 2,815.2722<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>19 | 12.9 ft         | 195.16315<br>ft | -70.399693<br>psf | 3,950.0378<br>psf | 2,664.3342<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>20 | 14.85 ft        | 195.9144<br>ft  | -93.454108<br>psf | 2,381.4239<br>psf | 1,606.2907<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>21 | 15.699077<br>ft | 196.25865<br>ft | -104.56166<br>psf | 2,290.4128<br>psf | 1,544.9029<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>22 | 16.481577<br>ft | 196.59383<br>ft | -115.91684<br>psf | 2,217.9982<br>psf | 1,732.8901<br>psf | 0 psf   | 0 psf | Gravel Borrow   |
| Slice<br>23 | 18.90125 ft     | 197.70404<br>ft | -147.43779<br>psf | 1,877.3546<br>psf | 1,266.2917<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>24 | 22.37375 ft     | 199.44281<br>ft | -197.1256<br>psf  | 1,698.7609<br>psf | 1,145.8287<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>25 | 25.305 ft       | 201.06615<br>ft | -240.82905<br>psf | 1,567.1358<br>psf | 1,057.0464<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>26 | 28 ft           | 202.72914<br>ft | -281.03125<br>psf | 1,456.6708<br>psf | 982.53686<br>psf  | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice       | 29.51 ft        | 203.69793       | -305.86691        | 1,403.5072        | 946.67758         | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                           |

| 27          |                 | ft              | psf                | psf               | psf              |         |       | (Apparent   |
|-------------|-----------------|-----------------|--------------------|-------------------|------------------|---------|-------|---|
| Slice<br>28 | 30.51 ft        | 204.39388<br>ft | -325.5784<br>psf   | 1,368.2791<br>psf | 922.91594<br>psf | 200 psf | 0 psf | Cohesion)  ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)  |
| Slice<br>29 | 31.865 ft       | 205.34864<br>ft | -353.01972<br>psf  | 1,323.5386<br>psf | 892.73809<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>30 | 33.4475 ft      | 206.54734<br>ft | -388.61925<br>psf  | 1,272.2798<br>psf | 858.16355<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>31 | 35.8825 ft      | 208.49171<br>ft | -448.86284<br>psf  | 1,198.1308<br>psf | 808.14944<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>32 | 38.05 ft        | 210.35143<br>ft | -510.53497<br>psf  | 1,134.1127<br>psf | 764.96864<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>33 | 40.5 ft         | 212.65828<br>ft | -593.02074<br>psf  | 1,196.3858<br>psf | 806.9724<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>34 | 43.5 ft         | 215.74178<br>ft | -710.17214<br>psf  | 1,013.506<br>psf  | 683.61842<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>35 | 46.669017<br>ft | 219.41241<br>ft | -859.7211<br>psf   | 800.35723<br>psf  | 539.84777<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>36 | 50.007051<br>ft | 223.82153<br>ft | -1,051.111<br>psf  | 540.14287<br>psf  | 364.33097<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>37 | 53.345085<br>ft | 228.98556<br>ft | -1,289.6072<br>psf | 222.12328<br>psf  | 149.82404<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
|             |                 |                 |                    |                   |                  |         |       | ESU 1B Medium<br>Dense to Very                                  |

|  | Slice<br>38 | 55.50774 ft | 232.72696<br>ft | -1,468.8179<br>psf | 44.552314<br>psf | 38.728735<br>psf | 100 psf | 0 psf | Dense Coarse-<br>Grained Fill<br>(Apparent<br>Cohesion) |  |
|--|-------------|-------------|-----------------|--------------------|------------------|------------------|---------|-------|---|--|
|--|-------------|-------------|-----------------|--------------------|------------------|------------------|---------|-------|---|--|

# 1A. Static (Spencer)

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### **File Information**

File Version: 11.02 Created By: Jon Cracolici Last Edited By: Taylor Booker Revision Number: 291

Date: 01/18/2022 Time: 05:50:42 AM

Tool Version: 11.2.2.23310

File Name: EMB I-405 SB MP 5.88.gsz

Directory: \\geoengineers.com\WAN\Projects\0\0180366\01\Analysis\EMB I-405 SB MP 5.97 to 5.83\01-18-22\

Last Solved Date: 01/18/2022 Last Solved Time: 05:51:25 AM

## **Project Settings**

Unit System: U.S. Customary Units

### **Analysis Settings**

### 1A. Static (Spencer)

Kind: SLOPE/W

Analysis Type: Spencer

Settings

PWP Conditions from: Piezometric Line

Apply Phreatic Correction: No Use Staged Rapid Drawdown: No Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 20

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 4 ft

Number of Slices: 30

**Factor of Safety Convergence Settings** 

Maximum Number of Iterations: 100 Tolerable difference in F of S: 0.001

**Solution Settings** 

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

### **Materials**

### **ESU 2A Very Loose to Loose Sand/Gravel**

Slope Stability Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 15 psf Effective Friction Angle: 32 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### **ESU 2B Medium Dense Sand/Gravel**

Slope Stability Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### **ESU 4B Dense to Very Dense Sand/Gravel**

Slope Stability Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Slope Stability Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **Common Borrow**

Slope Stability Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **Gravel Borrow**

Slope Stability Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38°

Phi-B: 0°

Pore Water Pressure Piezometric Line: 1

### **ESU 1A Loose to Med Dense Granular Fill (Original)**

Slope Stability Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 34°

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### **Quarry Spalls**

Slope Stability Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 42 °

Phi-B: 0°

Pore Water Pressure Piezometric Line: 1

## **Slip Surface Entry and Exit**

Left Type: Range

Left-Zone Left Coordinate: (-86, 193.85013) ft Left-Zone Right Coordinate: (-26, 221.6978) ft

Left-Zone Increment: 30 Right Type: Range

Right-Zone Left Coordinate: (-19.452, 224.97337) ft

Right-Zone Right Coordinate: (60, 227.4) ft

Right-Zone Increment: 38 Radius Increments: 25

### **Slip Surface Limits**

Left Coordinate: (-120, 183.7) ft Right Coordinate: (60, 227.4) ft

### **Piezometric Lines**

#### Piezometric Line 1

#### Coordinates

|              | Х         | Υ        |
|--------------|-----------|----------|
| Coordinate 1 | -120 ft   | 171.9 ft |
| Coordinate 2 | -103.2 ft | 175.5 ft |
| Coordinate 3 | -94.5 ft  | 177 ft   |

| 1             |              |            |
|---------------|--------------|------------|
| Coordinate 4  | -92 ft       | 177.8 ft   |
| Coordinate 5  | -90.25762 ft | 179.711 ft |
| Coordinate 6  | -81.894 ft   | 180.175 ft |
| Coordinate 7  | -65.834 ft   | 181.109 ft |
| Coordinate 8  | -58.616 ft   | 181.817 ft |
| Coordinate 9  | -44.983 ft   | 184.066 ft |
| Coordinate 10 | -32.584 ft   | 185.508 ft |
| Coordinate 11 | -27.777 ft   | 186.156 ft |
| Coordinate 12 | -25.31 ft    | 186.665 ft |
| Coordinate 13 | -21.273 ft   | 187.982 ft |
| Coordinate 14 | -18.881 ft   | 189.313 ft |
| Coordinate 15 | -13.948 ft   | 192.408 ft |
| Coordinate 16 | -9.34 ft     | 198.085 ft |
| Coordinate 17 | -7.036 ft    | 200.627 ft |
| Coordinate 18 | -2.894 ft    | 203.633 ft |
| Coordinate 19 | 8.368 ft     | 210.024 ft |
| Coordinate 20 | 18.083 ft    | 214.581 ft |
| Coordinate 21 | 22.799 ft    | 216.342 ft |
| Coordinate 22 | 25.82 ft     | 217.166 ft |
| Coordinate 23 | 29.666 ft    | 217.984 ft |
| Coordinate 24 | 37.76 ft     | 218.338 ft |
| Coordinate 25 | 60 ft        | 219.309 ft |

# **Surcharge Loads**

### **Surcharge Load 1**

Surcharge (Unit Weight): 250 pcf

Direction: Vertical

### **Coordinates**

| Х       | Υ        |
|---------|----------|
| -3.5 ft | 227.3 ft |
| 0.2 ft  | 227.6 ft |
| 37.7 ft | 228.2 ft |
| 60 ft   | 228.4 ft |

## **Geometry**

Name: Default Geometry

## Settings

View: 2D

Element Thickness: 1 ft

### **Points**

|         | Х       | Υ        |
|---------|---------|----------|
| Point 1 | 60 ft   | 170 ft   |
| Point 2 | -4.3 ft | 196.6 ft |
|         |         |          |

| 1        |            |              |
|----------|------------|--------------|
| Point 3  | 4 ft       | 225.3 ft     |
| Point 4  | -120 ft    | 170 ft       |
| Point 5  | 0.2 ft     | 226.6 ft     |
| Point 6  | 37.7 ft    | 227.2 ft     |
| Point 7  | -92.7 ft   | 193.2 ft     |
| Point 8  | -55.6 ft   | 196.8 ft     |
| Point 9  | -50 ft     | 199.6 ft     |
| Point 10 | -4.3 ft    | 225.7 ft     |
| Point 11 | -11.9 ft   | 219.8 ft     |
| Point 12 | -22.9 ft   | 213 ft       |
| Point 13 | -41.2 ft   | 203.1 ft     |
| Point 14 | -53.8 ft   | 193.9 ft     |
| Point 15 | -24.6 ft   | 205.1 ft     |
| Point 16 | -67.8 ft   | 191.1 ft     |
| Point 17 | -92 ft     | 177.8 ft     |
| Point 18 | -85 ft     | 187.7 ft     |
| Point 19 | -88.9 ft   | 181.2 ft     |
| Point 20 | -100.8 ft  | 190.8 ft     |
| Point 21 | -80.509 ft | 194.38295 ft |
| Point 22 | -16.8 ft   | 226.3 ft     |
| Point 23 | -35.1 ft   | 217.1 ft     |
| Point 24 | -35.1 ft   | 226.3 ft     |
| Point 25 | -53.2 ft   | 198.1 ft     |
| Point 26 | -78.51 ft  | 189.1 ft     |
| Point 27 | -7.6 ft    | 173.4 ft     |
| Point 28 | 60 ft      | 185.2 ft     |
| Point 29 | 60 ft      | 211.2 ft     |
| Point 30 | 60 ft      | 225.3 ft     |
| Point 31 | -24.6 ft   | 195.3 ft     |
| Point 32 | -44.8 ft   | 190.9 ft     |
| Point 33 | -55.8 ft   | 188.8 ft     |
| Point 34 | -64.2 ft   | 187.5 ft     |
| Point 35 | -87.6 ft   | 183.3 ft     |
| Point 36 | -94.5 ft   | 177 ft       |
| Point 37 | -120 ft    | 171.9 ft     |
| Point 38 | 60 ft      | 227.4 ft     |
| Point 39 | -69.1 ft   | 186.6 ft     |
| Point 40 | 3.8 ft     | 225.4 ft     |
| Point 41 | -24.9 ft   | 196.1 ft     |
| Point 42 | -26.3 ft   | 195.8 ft     |
| Point 43 | -41.6 ft   | 192.6 ft     |
| Point 44 | -57 ft     | 189.2 ft     |
| Point 45 | -120 ft    | 183.7 ft     |
| Point 46 | 0.9 ft     | 226.5 ft     |
| Point 47 | -11.6 ft   | 216.6 ft     |
| Point 48 | -19.6 ft   | 210.5 ft     |
| Point 49 | -24.7 ft   | 206.4 ft     |
| Point 50 | -28.6 ft   | 204.5 ft     |
| Point 51 | -41.7 ft   | 199.9 ft     |

| Point 52 | -53.6 ft     | 195.7 ft     |
|----------|--------------|--------------|
| Point 53 | -46.7 ft     | 201 ft       |
| Point 54 | -111.255 ft  | 184.5 ft     |
| Point 55 | -103.2 ft    | 175.5 ft     |
| Point 56 | -105.5313 ft | 188.8 ft     |
| Point 57 | -27.1 ft     | 226.3 ft     |
| Point 58 | -35.1 ft     | 215.1 ft     |
| Point 59 | -27.1 ft     | 221.14754 ft |
| Point 60 | -39.1 ft     | 215.1 ft     |
| Point 61 | -120 ft      | 178.102 ft   |
| Point 62 | -107.308 ft  | 180.256 ft   |
| Point 63 | -35.1 ft     | 213.1 ft     |
| Point 64 | -27.1 ft     | 213.1 ft     |

## Regions

|              | Material   | Points  | Area                       |
|--------------|--|---|----------------------------|
| Region<br>1  | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 27,28,29,2  | 1,600.6<br>ft <sup>2</sup> |
| Region<br>2  | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 1,28,27,2,29,30,3,31,32,33,34,39,35,19,17,36,55,37,4  | 4,026.8<br>ft <sup>2</sup> |
| Region<br>3  | Gravel Borrow  | 5,46,40,3,30,38,6                                     | 101.83<br>ft²              |
| Region<br>4  | ESU 2B Medium Dense<br>Sand/Gravel                               | 39,34,33,32,31,3,40,41,42,43,44                       | 52.08<br>ft²               |
| Region<br>5  | Quarry Spalls  | 36,17,19,35,18,54,62,55                               | 182.94<br>ft²              |
| Region<br>6  | Gravel Borrow  | 20,7,21,8,25,52,14,16,26,18,54,56                     | 272.45<br>ft²              |
| Region<br>7  | ESU 1A Loose to Med Dense<br>Granular Fill (Original)            | 5,46,47,48,49,50,51,52,25,9,53,13,12,11,10            | 199.45<br>ft²              |
| Region<br>8  | Common Borrow  | 5,22,59,64,63,58,60,21,8,25,9,53,13,12,11,10          | 544.6<br>ft <sup>2</sup>   |
| Region<br>9  | ESU 2A Very Loose to Loose<br>Sand/Gravel                        | 40,41,42,43,44,39,35,18,26,16,14,52,51,50,49,48,47,46 | 545.83<br>ft²              |
| Region<br>10 | Common Borrow  | 58,63,64,59,23  | 48.19<br>ft²               |
| Region<br>11 |  | 22,57,59  | 26.535<br>ft²              |
| Region<br>12 | ESU 2A Very Loose to Loose<br>Sand/Gravel                        | 45,61,62,54   | 55.661<br>ft²              |
| Region<br>13 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 61,37,55,62   | 86.703<br>ft²              |
| Region<br>14 |  | 24,23,59,57   | 57.41<br>ft²               |
| Region<br>15 | Common Borrow  | 23,60,58  | 4 ft²                      |

# **Slip Results**

Slip Surfaces Analysed: 29900 of 31434 converged

## **Current Slip Surface**

Slip Surface: 2,084 Factor of Safety: 1.28 Volume: 182.3259 ft<sup>3</sup> Weight: 21,879.108 lbf

Resisting Moment: 2,308,143.7 lbf·ft Activating Moment: 1,809,627.1 lbf·ft

Resisting Force: 11,025.512 lbf Activating Force: 8,644.0212 lbf Slip Rank: 1 of 31,434 slip surfaces Exit: (-79.732674, 194.77135) ft Entry: (-15.566887, 226.32176) ft

Radius: 187.2457 ft

Center: (-128.75123, 375.48697) ft

## **Slip Slices**

|             | X                | Y               | PWP                | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base<br>Materia  |
|-------------|------------------|-----------------|--------------------|--------------------------|------------------------|----------------------|---------------------|------------------|
| Slice<br>1  | -78.574451<br>ft | 195.09351<br>ft | -918.86842<br>psf  | 29.983556<br>psf         | 18.735805<br>psf       | 0 psf                | 0 psf               | Commor<br>Borrow |
| Slice<br>2  | -76.258006<br>ft | 195.75395<br>ft | -951.67319<br>psf  | 86.910048<br>psf         | 54.307425<br>psf       | 0 psf                | 0 psf               | Commor<br>Borrow |
| Slice<br>3  | -73.94156<br>ft  | 196.44679<br>ft | -986.50008<br>psf  | 138.65353<br>psf         | 86.640344<br>psf       | 0 psf                | 0 psf               | Commor<br>Borrow |
| Slice<br>4  | -71.625114<br>ft | 197.17241<br>ft | -1,023.3726<br>psf | 185.34899<br>psf         | 115.81891<br>psf       | 0 psf                | 0 psf               | Commor<br>Borrow |
| Slice<br>5  | -69.308669<br>ft | 197.93122<br>ft | -1,062.316<br>psf  | 227.12468<br>psf         | 141.92325<br>psf       | 0 psf                | 0 psf               | Common<br>Borrow |
| Slice<br>6  | -66.992223<br>ft | 198.72364<br>ft | -1,103.3567<br>psf | 264.10251<br>psf         | 165.02956<br>psf       | 0 psf                | 0 psf               | Common<br>Borrow |
| Slice<br>7  | -64.631 ft       | 199.56678<br>ft | -1,144.4026<br>psf | 296.94061<br>psf         | 185.54909<br>psf       | 0 psf                | 0 psf               | Commor<br>Borrow |
| Slice<br>8  | -62.225 ft       | 200.46252<br>ft | -1,185.5698<br>psf | 325.55604<br>psf         | 203.42999<br>psf       | 0 psf                | 0 psf               | Commor<br>Borrow |
| Slice<br>9  | -59.819 ft       | 201.39611<br>ft | -1,229.0995<br>psf | 349.35977<br>psf         | 218.30422<br>psf       | 0 psf                | 0 psf               | Commor<br>Borrow |
| Slice<br>10 | -57.479917<br>ft | 202.34008<br>ft | -1,268.9454<br>psf | 368.05015<br>psf         | 229.98326<br>psf       | 0 psf                | 0 psf               | Commor<br>Borrow |
| Slice<br>11 | -55.20775<br>ft  | 203.29294<br>ft | -1,305.014<br>psf  | 381.99289<br>psf         | 238.69565<br>psf       | 0 psf                | 0 psf               | Commor<br>Borrow |
| Slice<br>12 | -52.935583<br>ft | 204.28125<br>ft | -1,343.2951<br>psf | 391.92331<br>psf         | 244.90086<br>psf       | 0 psf                | 0 psf               | Commor<br>Borrow |
| Slice<br>13 | -50.663417<br>ft | 205.30564<br>ft | -1,383.8274<br>psf | 397.92392<br>psf         | 248.65046<br>psf       | 0 psf                | 0 psf               | Commor<br>Borrow |
| Slice<br>14 | -48.39125<br>ft  | 206.36676<br>ft | -1,426.6516<br>psf | 400.07393<br>psf         | 249.99394<br>psf       | 0 psf                | 0 psf               | Commor<br>Borrow |
| Slice<br>15 | -46.119083<br>ft | 207.4653<br>ft  | -1,471.8113<br>psf | 398.44941<br>psf         | 248.97883<br>psf       | 0 psf                | 0 psf               | Commor<br>Borrow |
| Slice<br>16 | -44.0025 ft      | 208.52171<br>ft | -1,518.9206<br>psf | 393.7244<br>psf          | 246.02631<br>psf       | 0 psf                | 0 psf               | Commor<br>Borrow |
| Slice       | -42.0415 ft      | 209.53169       | -1,567.7125        | 386.42025                | 241.46217              | 0 psf                | 0 psf               | Commor           |

| 17          |                  | ft              | psf                | psf              | psf              |       |       | Borrow           |
|-------------|------------------|-----------------|--------------------|------------------|------------------|-------|-------|------------------|
| Slice<br>18 | -40.0805 ft      | 210.57118<br>ft | -1,618.3454<br>psf | 376.45239<br>psf | 235.23356<br>psf | 0 psf | 0 psf | Common<br>Borrow |
| Slice<br>19 | -38.1 ft         | 211.65168<br>ft | -1,671.3956<br>psf | 363.68324<br>psf | 227.25451<br>psf | 0 psf | 0 psf | Common<br>Borrow |
| Slice<br>20 | -36.1 ft         | 212.7744<br>ft  | -1,726.9393<br>psf | 348.10704<br>psf | 217.52142<br>psf | 0 psf | 0 psf | Common<br>Borrow |
| Slice<br>21 | -33.842 ft       | 214.08355<br>ft | -1,792.2439<br>psf | 327.80444<br>psf | 204.83494<br>psf | 0 psf | 0 psf | Common<br>Borrow |
| Slice<br>22 | -31.38225<br>ft  | 215.55493<br>ft | -1,864.8196<br>psf | 302.77371<br>psf | 189.19401<br>psf | 0 psf | 0 psf | Common<br>Borrow |
| Slice<br>23 | -28.97875<br>ft  | 217.04332<br>ft | -1,937.4775<br>psf | 274.51518<br>psf | 171.53612<br>psf | 0 psf | 0 psf | Common<br>Borrow |
| Slice<br>24 | -27.4385 ft      | 218.01785<br>ft | -1,983.8214<br>psf | 255.00972<br>psf | 159.34776<br>psf | 0 psf | 0 psf | Common<br>Borrow |
| Slice<br>25 | -26.205 ft       | 218.82146<br>ft | -2,018.0859<br>psf | 237.20652<br>psf | 148.22308<br>psf | 0 psf | 0 psf | Common<br>Borrow |
| Slice<br>26 | -24.30075<br>ft  | 220.08564<br>ft | -2,064.9027<br>psf | 207.9765<br>psf  | 129.95814<br>psf | 0 psf | 0 psf | Common<br>Borrow |
| Slice<br>27 | -22.28225<br>ft  | 221.46163<br>ft | -2,109.6739<br>psf | 174.71037<br>psf | 109.17116<br>psf | 0 psf | 0 psf | Common<br>Borrow |
| Slice<br>28 | -20.077 ft       | 223.01169<br>ft | -2,144.3257<br>psf | 135.45375<br>psf | 84.640896<br>psf | 0 psf | 0 psf | Common<br>Borrow |
| Slice<br>29 | -17.8405 ft      | 224.6291<br>ft  | -2,162.9888<br>psf | 93.078686<br>psf | 58.162018<br>psf | 0 psf | 0 psf | Common<br>Borrow |
| Slice<br>30 | -16.183443<br>ft | 225.85792<br>ft | -2,174.7929<br>psf | 36.235281<br>psf | 22.642317<br>psf | 0 psf | 0 psf | Common<br>Borrow |

# 1B. Static (M-P)

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## **File Information**

File Version: 11.02 Created By: Jon Cracolici Last Edited By: Taylor Booker Revision Number: 291

Date: 01/18/2022 Time: 05:50:42 AM

Tool Version: 11.2.2.23310

File Name: EMB I-405 SB MP 5.88.gsz

Directory: \\geoengineers.com\WAN\Projects\0\0180366\01\Analysis\EMB I-405 SB MP 5.97 to 5.83\01-18-22\

Last Solved Date: 01/18/2022 Last Solved Time: 05:52:00 AM

## **Project Settings**

Unit System: U.S. Customary Units

## **Analysis Settings**

### 1B. Static (M-P)

Description: Project Num: 00180-366-01 Embankment: EMB I-405 SB MP 5.97 to 5.83 Station: MP 5.88

Kind: SLOPE/W

Analysis Type: Morgenstern-Price

Settings

Side Function

Interslice force function option: Half-Sine

PWP Conditions from: Piezometric Line

Apply Phreatic Correction: No Use Staged Rapid Drawdown: No Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 20

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 4 ft

Number of Slices: 30

**Factor of Safety Convergence Settings** 

Maximum Number of Iterations: 100 Tolerable difference in F of S: 0.001

**Solution Settings** 

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3 Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

### **Materials**

#### **ESU 2A Very Loose to Loose Sand/Gravel**

Slope Stability Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 15 psf Effective Friction Angle: 32 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **ESU 2B Medium Dense Sand/Gravel**

Slope Stability Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

Pore Water Pressure Piezometric Line: 1

### **ESU 4B Dense to Very Dense Sand/Gravel**

Slope Stability Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

Pore Water Pressure Piezometric Line: 1

### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Slope Stability Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **Common Borrow**

Slope Stability Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

Pore Water Pressure Piezometric Line: 1

#### **Gravel Borrow**

Slope Stability Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

Pore Water Pressure Piezometric Line: 1

### **ESU 1A Loose to Med Dense Granular Fill (Original)**

Slope Stability Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 34 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### **Quarry Spalls**

Slope Stability Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 42 °

Phi-B: 0°

Pore Water Pressure Piezometric Line: 1

## **Slip Surface Entry and Exit**

Left Type: Range

Left-Zone Left Coordinate: (-86, 193.85013) ft Left-Zone Right Coordinate: (-26, 221.6978) ft

Left-Zone Increment: 30 Right Type: Range

Right-Zone Left Coordinate: (-19.583, 224.90784) ft

Right-Zone Right Coordinate: (60, 227.4) ft

Right-Zone Increment: 38 Radius Increments: 25

## **Slip Surface Limits**

Left Coordinate: (-120, 183.7) ft Right Coordinate: (60, 227.4) ft

## **Piezometric Lines**

#### Piezometric Line 1

#### **Coordinates**

|              | Х       | Υ        |
|--------------|---------|----------|
| Coordinate 1 | -120 ft | 171.9 ft |

| Coordinate 2  | -103.2 ft    | 175.5 ft   |
|---------------|--------------|------------|
| Coordinate 3  | -94.5 ft     | 177 ft     |
| Coordinate 4  | -92 ft       | 177.8 ft   |
| Coordinate 5  | -90.25762 ft | 179.711 ft |
| Coordinate 6  | -81.894 ft   | 180.175 ft |
| Coordinate 7  | -65.834 ft   | 181.109 ft |
| Coordinate 8  | -58.616 ft   | 181.817 ft |
| Coordinate 9  | -44.983 ft   | 184.066 ft |
| Coordinate 10 | -32.584 ft   | 185.508 ft |
| Coordinate 11 | -27.777 ft   | 186.156 ft |
| Coordinate 12 | -25.31 ft    | 186.665 ft |
| Coordinate 13 | -21.273 ft   | 187.982 ft |
| Coordinate 14 | -18.881 ft   | 189.313 ft |
| Coordinate 15 | -13.948 ft   | 192.408 ft |
| Coordinate 16 | -9.34 ft     | 198.085 ft |
| Coordinate 17 | -7.036 ft    | 200.627 ft |
| Coordinate 18 | -2.894 ft    | 203.633 ft |
| Coordinate 19 | 8.368 ft     | 210.024 ft |
| Coordinate 20 | 18.083 ft    | 214.581 ft |
| Coordinate 21 | 22.799 ft    | 216.342 ft |
| Coordinate 22 | 25.82 ft     | 217.166 ft |
| Coordinate 23 | 29.666 ft    | 217.984 ft |
| Coordinate 24 | 37.76 ft     | 218.338 ft |
| Coordinate 25 | 60 ft        | 219.309 ft |

# **Surcharge Loads**

## **Surcharge Load 1**

Surcharge (Unit Weight): 250 pcf

Direction: Vertical

### Coordinates

| Х       | Υ        |
|---------|----------|
| -3.5 ft | 227.3 ft |
| 0.2 ft  | 227.6 ft |
| 37.7 ft | 228.2 ft |
| 60 ft   | 228.4 ft |

## **Geometry**

Name: Default Geometry

## **Settings**

View: 2D

Element Thickness: 1 ft

#### **Points**

| X | Υ |
|---|---|
|   |   |

| Point 1  | 60 ft      | 170 ft       |
|----------|------------|--------------|
| Point 2  | -4.3 ft    | 196.6 ft     |
| Point 3  | 4 ft       | 225.3 ft     |
| Point 4  | -120 ft    | 170 ft       |
| Point 5  | 0.2 ft     | 226.6 ft     |
| Point 6  | 37.7 ft    | 227.2 ft     |
| Point 7  | -92.7 ft   | 193.2 ft     |
| Point 8  | -55.6 ft   | 196.8 ft     |
| Point 9  | -50 ft     | 199.6 ft     |
| Point 10 | -4.3 ft    | 225.7 ft     |
| Point 10 | -4.5 ft    | 219.8 ft     |
| Point 12 | -22.9 ft   | 213.8 ft     |
| Point 12 | -41.2 ft   | 203.1 ft     |
|          | -41.2 it   |              |
| Point 14 | -          | 193.9 ft     |
| Point 15 | -24.6 ft   | 205.1 ft     |
| Point 16 | -67.8 ft   | 191.1 ft     |
| Point 17 | -92 ft     | 177.8 ft     |
| Point 18 | -85 ft     | 187.7 ft     |
| Point 19 | -88.9 ft   | 181.2 ft     |
| Point 20 | -100.8 ft  | 190.8 ft     |
| Point 21 | -80.509 ft | 194.38295 ft |
| Point 22 | -16.8 ft   | 226.3 ft     |
| Point 23 | -35.1 ft   | 217.1 ft     |
| Point 24 | -35.1 ft   | 226.3 ft     |
| Point 25 | -53.2 ft   | 198.1 ft     |
| Point 26 | -78.51 ft  | 189.1 ft     |
| Point 27 | -7.6 ft    | 173.4 ft     |
| Point 28 | 60 ft      | 185.2 ft     |
| Point 29 | 60 ft      | 211.2 ft     |
| Point 30 | 60 ft      | 225.3 ft     |
| Point 31 | -24.6 ft   | 195.3 ft     |
| Point 32 | -44.8 ft   | 190.9 ft     |
| Point 33 | -55.8 ft   | 188.8 ft     |
| Point 34 | -64.2 ft   | 187.5 ft     |
| Point 35 | -87.6 ft   | 183.3 ft     |
| Point 36 | -94.5 ft   | 177 ft       |
| Point 37 | -120 ft    | 171.9 ft     |
| Point 38 | 60 ft      | 227.4 ft     |
| Point 39 | -69.1 ft   | 186.6 ft     |
| Point 40 | 3.8 ft     | 225.4 ft     |
| Point 41 | -24.9 ft   | 196.1 ft     |
| Point 42 | -26.3 ft   | 195.8 ft     |
| Point 43 | -41.6 ft   | 192.6 ft     |
| Point 44 | -57 ft     | 189.2 ft     |
| Point 45 | -120 ft    | 183.7 ft     |
| Point 46 | 0.9 ft     | 226.5 ft     |
| Point 47 | -11.6 ft   | 216.6 ft     |
| Point 48 | -19.6 ft   | 210.5 ft     |
| Point 49 | -24.7 ft   | 206.4 ft     |
| L 3      |            | +            |

| Point 50 | -28.6 ft     | 204.5 ft     |
|----------|--------------|--------------|
| Point 51 | -41.7 ft     | 199.9 ft     |
| Point 52 | -53.6 ft     | 195.7 ft     |
| Point 53 | -46.7 ft     | 201 ft       |
| Point 54 | -111.255 ft  | 184.5 ft     |
| Point 55 | -103.2 ft    | 175.5 ft     |
| Point 56 | -105.5313 ft | 188.8 ft     |
| Point 57 | -27.1 ft     | 226.3 ft     |
| Point 58 | -35.1 ft     | 215.1 ft     |
| Point 59 | -27.1 ft     | 221.14754 ft |
| Point 60 | -39.1 ft     | 215.1 ft     |
| Point 61 | -120 ft      | 178.102 ft   |
| Point 62 | -107.308 ft  | 180.256 ft   |
| Point 63 | -35.1 ft     | 213.1 ft     |
| Point 64 | -27.1 ft     | 213.1 ft     |

## Regions

|              | Material   | Points  | Area                       |
|--------------|--|---|----------------------------|
| Region<br>1  | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 27,28,29,2  | 1,600.6<br>ft²             |
| Region<br>2  | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 1,28,27,2,29,30,3,31,32,33,34,39,35,19,17,36,55,37,4  | 4,026.8<br>ft <sup>2</sup> |
| Region<br>3  | Gravel Borrow  | 5,46,40,3,30,38,6                                     | 101.83<br>ft²              |
| Region<br>4  | ESU 2B Medium Dense<br>Sand/Gravel                               | 39,34,33,32,31,3,40,41,42,43,44                       | 52.08<br>ft²               |
| Region<br>5  | Quarry Spalls  | 36,17,19,35,18,54,62,55                               | 182.94<br>ft²              |
| Region<br>6  | Gravel Borrow  | 20,7,21,8,25,52,14,16,26,18,54,56                     | 272.45<br>ft <sup>2</sup>  |
| Region<br>7  | ESU 1A Loose to Med Dense<br>Granular Fill (Original)            | 5,46,47,48,49,50,51,52,25,9,53,13,12,11,10            | 199.45<br>ft²              |
| Region<br>8  | Common Borrow  | 5,22,59,64,63,58,60,21,8,25,9,53,13,12,11,10          | 544.6<br>ft <sup>2</sup>   |
| Region<br>9  | ESU 2A Very Loose to Loose<br>Sand/Gravel                        | 40,41,42,43,44,39,35,18,26,16,14,52,51,50,49,48,47,46 | 545.83<br>ft <sup>2</sup>  |
| Region<br>10 | Common Borrow  | 58,63,64,59,23  | 48.19<br>ft²               |
| Region<br>11 |  | 22,57,59  | 26.535<br>ft²              |
| Region<br>12 | ESU 2A Very Loose to Loose<br>Sand/Gravel                        | 45,61,62,54   | 55.661<br>ft²              |
| Region<br>13 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 61,37,55,62   | 86.703<br>ft²              |
| Region<br>14 |  | 24,23,59,57   | 57.41<br>ft²               |
| Region<br>15 | Common Borrow  | 23,60,58  | 4 ft²                      |

# **Slip Results**

## **Current Slip Surface**

Slip Surface: 2,084 Factor of Safety: 1.27 Volume: 179.42814 ft<sup>3</sup> Weight: 21,531.376 lbf

Resisting Moment: 2,269,199.4 lbf·ft Activating Moment: 1,780,309.6 lbf·ft Resisting Force: 10,845.204 lbf

Activating Force: 8,514.8169 lbf Slip Rank: 1 of 31,434 slip surfaces Exit: (-79.724166, 194.7756) ft Entry: (-15.705632, 226.31931) ft

Radius: 187.08702 ft

Center: (-128.88693, 375.28759) ft

## **Slip Slices**

|             | X                | Y               | PWP                | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base<br>Material |
|-------------|------------------|-----------------|--------------------|--------------------------|------------------------|----------------------|---------------------|------------------|
| Slice<br>1  | -78.732011<br>ft | 195.0517<br>ft  | -916.83097<br>psf  | 23.505992<br>psf         | 14.688174<br>psf       | 0 psf                | 0 psf               | Common<br>Borrow |
| Slice<br>2  | -76.747702<br>ft | 195.6157<br>ft  | -944.82386<br>psf  | 69.776053<br>psf         | 43.600917<br>psf       | 0 psf                | 0 psf               | Common<br>Borrow |
| Slice<br>3  | -74.763392<br>ft | 196.20347<br>ft | -974.29953<br>psf  | 114.1201<br>psf          | 71.310155<br>psf       | 0 psf                | 0 psf               | Common<br>Borrow |
| Slice<br>4  | -72.779083<br>ft | 196.81523<br>ft | -1,005.2726<br>psf | 156.18341<br>psf         | 97.594225<br>psf       | 0 psf                | 0 psf               | Common<br>Borrow |
| Slice<br>5  | -70.794774<br>ft | 197.45124<br>ft | -1,037.7586<br>psf | 195.60858<br>psf         | 122.22981<br>psf       | 0 psf                | 0 psf               | Common<br>Borrow |
| Slice<br>6  | -68.810464<br>ft | 198.11176<br>ft | -1,071.7738<br>psf | 232.05617<br>psf         | 145.00479<br>psf       | 0 psf                | 0 psf               | Common<br>Borrow |
| Slice<br>7  | -66.826155<br>ft | 198.79706<br>ft | -1,107.3353<br>psf | 265.22358<br>psf         | 165.73008<br>psf       | 0 psf                | 0 psf               | Common<br>Borrow |
| Slice<br>8  | -64.631 ft       | 199.58589<br>ft | -1,145.5945<br>psf | 297.62607<br>psf         | 185.97741<br>psf       | 0 psf                | 0 psf               | Common<br>Borrow |
| Slice<br>9  | -62.225 ft       | 200.48461<br>ft | -1,186.9482<br>psf | 328.0714<br>psf          | 205.00176<br>psf       | 0 psf                | 0 psf               | Common<br>Borrow |
| Slice<br>10 | -59.819 ft       | 201.42126<br>ft | -1,230.6692<br>psf | 352.86066<br>psf         | 220.49181<br>psf       | 0 psf                | 0 psf               | Common<br>Borrow |
| Slice<br>11 | -57.479917<br>ft | 202.3683<br>ft  | -1,270.7062<br>psf | 371.57666<br>psf         | 232.18687<br>psf       | 0 psf                | 0 psf               | Common<br>Borrow |
| Slice<br>12 | -55.20775<br>ft  | 203.32421<br>ft | -1,306.9654<br>psf | 384.66443<br>psf         | 240.36501<br>psf       | 0 psf                | 0 psf               | Common<br>Borrow |
| Slice<br>13 | -52.935583<br>ft | 204.31566<br>ft | -1,345.4422<br>psf | 392.9888<br>psf          | 245.56666<br>psf       | 0 psf                | 0 psf               | Common<br>Borrow |
| Slice<br>14 | -50.663417<br>ft | 205.34327<br>ft | -1,386.1756<br>psf | 396.81864<br>psf         | 247.95981<br>psf       | 0 psf                | 0 psf               | Common<br>Borrow |
| Slice<br>15 | -48.39125<br>ft  | 206.4077<br>ft  | -1,429.2068<br>psf | 396.46787<br>psf         | 247.74062<br>psf       | 0 psf                | 0 psf               | Common<br>Borrow |
| Slice       | -46.119083       | 207.50966       | -1,474.5794        | 392.26915                | 245.11697              | 0 psf                | 0 psf               | Common           |

| 16          | ft               | ft              | psf                | psf              | psf              |       |       | Borrow           |
|-------------|------------------|-----------------|--------------------|------------------|------------------|-------|-------|------------------|
| Slice<br>17 | -44.0025 ft      | 208.56933<br>ft | -1,521.8924<br>psf | 385.29989<br>psf | 240.76209<br>psf | 0 psf | 0 psf | Common<br>Borrow |
| Slice<br>18 | -42.0415 ft      | 209.58243<br>ft | -1,570.8785<br>psf | 376.21968<br>psf | 235.08815<br>psf | 0 psf | 0 psf | Common<br>Borrow |
| Slice<br>19 | -40.0805 ft      | 210.62511<br>ft | -1,621.7108<br>psf | 364.89436<br>psf | 228.0113<br>psf  | 0 psf | 0 psf | Common<br>Borrow |
| Slice<br>20 | -38.1 ft         | 211.70893<br>ft | -1,674.9679<br>psf | 351.27516<br>psf | 219.50108<br>psf | 0 psf | 0 psf | Common<br>Borrow |
| Slice<br>21 | -36.1 ft         | 212.83509<br>ft | -1,730.7266<br>psf | 335.42917<br>psf | 209.59941<br>psf | 0 psf | 0 psf | Common<br>Borrow |
| Slice<br>22 | -33.842 ft       | 214.14826<br>ft | -1,796.2819<br>psf | 315.5699<br>psf  | 197.18996<br>psf | 0 psf | 0 psf | Common<br>Borrow |
| Slice<br>23 | -31.38225<br>ft  | 215.62417<br>ft | -1,869.14<br>psf   | 291.83876<br>psf | 182.3611<br>psf  | 0 psf | 0 psf | Common<br>Borrow |
| Slice<br>24 | -28.97875<br>ft  | 217.11715<br>ft | -1,942.0843<br>psf | 265.54104<br>psf | 165.92846<br>psf | 0 psf | 0 psf | Common<br>Borrow |
| Slice<br>25 | -27.4385 ft      | 218.09469<br>ft | -1,988.6162<br>psf | 247.52339<br>psf | 154.66978<br>psf | 0 psf | 0 psf | Common<br>Borrow |
| Slice<br>26 | -26.205 ft       | 218.9008<br>ft  | -2,023.0365<br>psf | 230.97751<br>psf | 144.33077<br>psf | 0 psf | 0 psf | Common<br>Borrow |
| Slice<br>27 | -24.30075<br>ft  | 220.16891<br>ft | -2,070.0991<br>psf | 203.62606<br>psf | 127.23969<br>psf | 0 psf | 0 psf | Common<br>Borrow |
| Slice<br>28 | -22.28225<br>ft  | 221.54922<br>ft | -2,115.1394<br>psf | 172.03635<br>psf | 107.50024<br>psf | 0 psf | 0 psf | Common<br>Borrow |
| Slice<br>29 | -20.077 ft       | 223.10418<br>ft | -2,150.0966<br>psf | 133.81111<br>psf | 83.614463<br>psf | 0 psf | 0 psf | Common<br>Borrow |
| Slice<br>30 | -17.8405 ft      | 224.72673<br>ft | -2,169.0809<br>psf | 91.150274<br>psf | 56.957012<br>psf | 0 psf | 0 psf | Common<br>Borrow |
| Slice<br>31 | -16.252816<br>ft | 225.90673<br>ft | -2,180.5549<br>psf | 35.104117<br>psf | 21.935487<br>psf | 0 psf | 0 psf | Common<br>Borrow |







In Association with

## Appendix K Slope/W Reports - Compound Stability

# 1A.1 Compound - Static (Spencer)

Report generated using GeoStudio 2021 R2. Copyright © 1991-2021 GEOSLOPE International Ltd.

## **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 650 Date: 01/17/2022 Time: 01:45:50 PM

Tool Version: 11.1.1.22085

Last Solved Date: 01/17/2022 Last Solved Time: 01:49:05 PM

## **Project Settings**

Unit System: U.S. Customary Units

## **Analysis Settings**

#### 1A.1 Compound - Static (Spencer)

Kind: SLOPE/W

Parent: 1. Steady State (Compound)

Analysis Type: Spencer

Settings

PWP Conditions from Parent Analysis: 1. Steady State (Compound) [(last)]

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 20

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

Factor of Safety Convergence Settings

Maximum Number of Iterations: 100 Tolerable difference in F of S: 0.001

**Solution Settings** 

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

### **Materials**

#### ESU 2A Very Loose to Loose Sand/Gravel

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **ESU 2B Medium Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

### **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

## ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

#### 1A.1 Compound - Static (Spencer)

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

## Reinforcements

#### Row 1

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 6.6 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 2

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 6.1 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 3

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 5.6 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 4

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 5.1 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 5

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 4.6 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 6

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 4.1 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

### Row 7 (4 straps)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 7.2 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 7,860 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 7,860 lbf/ft

### Row 8 (4 straps)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 6.2 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 7,860 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 7,860 lbf/ft

## Slip Surface Entry and Exit

Left Type: Range

Left-Zone Left Coordinate: (-45, 181.43065) ft

Left-Zone Right Coordinate: (0, 200) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15, 218.535) ft Right-Zone Right Coordinate: (55, 223.299) ft

Right-Zone Increment: 20 Radius Increments: 20

## **Slip Surface Limits**

Left Coordinate: (-100, 170.1) ft Right Coordinate: (100, 223.6) ft

## **Reinforcement Lines**

#### Reinforcement Line 1

Reinforcement: Row 1 Lock to Ground Surface: Yes Outside Point: (0, 210.5) ft Inside Point: (15.5, 210.5) ft

Length: 15.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft

Governing Component: (none)

#### **Reinforcement Line 2**

Reinforcement: Row 8 (4 straps) Lock to Ground Surface: No Outside Point: (0, 193.7) ft Inside Point: (20, 193.7) ft

Length: 20 ft
Orientation: 0 °

Slip Surface Intersection: (14.983919, 193.7) ft

Max. Pullout Force: 7,860 lbf Available Length: 5.0160809 ft Required Length: 5.0160809 ft Pullout Force: 3,478.3709 lbf

Pullout Force per Length: 693.44394 lbf/ft Governing Component: Pullout Resistance

#### **Reinforcement Line 3**

Reinforcement: Row 6 Lock to Ground Surface: Yes Outside Point: (0, 198.5) ft Inside Point: (15.5, 198.5) ft

Length: 15.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 4**

Reinforcement: Row 2 Lock to Ground Surface: Yes Outside Point: (0, 208.1) ft Inside Point: (15.5, 208.1) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 5**

Reinforcement: Row 5 Lock to Ground Surface: Yes Outside Point: (0, 200.9) ft Inside Point: (15.5, 200.9) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### Reinforcement Line 6

Reinforcement: Row 4 Lock to Ground Surface: Yes Outside Point: (0, 203.3) ft Inside Point: (15.5, 203.3) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 7**

Reinforcement: Row 3 Lock to Ground Surface: Yes Outside Point: (0, 205.7) ft Inside Point: (15.5, 205.7) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 8**

Reinforcement: Row 7 (4 straps) Lock to Ground Surface: Yes Outside Point: (0, 196.1) ft Inside Point: (20, 196.1) ft

Length: 20 ft
Orientation: 0 °

Slip Surface Intersection: (17.588678, 196.1) ft

Max. Pullout Force: 7,860 lbf

Available Length: 2.4113217 ft Required Length: 2.4113217 ft Pullout Force: 1,832.5947 lbf

Pullout Force per Length: 759.99596 lbf/ft Governing Component: Pullout Resistance

## **Surcharge Loads**

## **Surcharge Load 1**

Surcharge (Unit Weight): 250 pcf

Direction: Vertical

#### Coordinates

| X       | Υ         |
|---------|-----------|
| 35.9 ft | 224.15 ft |
| 40.2 ft | 224.2 ft  |
| 100 ft  | 224.6 ft  |

## **Geometry**

Name: Default Geometry

## **Settings**

View: 2D

Element Thickness: 1 ft

#### **Points**

| 163      |             |             |
|----------|-------------|-------------|
|          | X           | Υ           |
| Point 1  | 100 ft      | 160 ft      |
| Point 2  | 100 ft      | 185.5 ft    |
| Point 3  | 0.9 ft      | 160 ft      |
| Point 4  | 100 ft      | 211.1475 ft |
| Point 5  | 3.8 ft      | 183 ft      |
| Point 6  | -20.1275 ft | 160 ft      |
| Point 7  | 100 ft      | 219.64 ft   |
| Point 8  | 42.5825 ft  | 219.8525 ft |
| Point 9  | 40.2 ft     | 223.2 ft    |
| Point 10 | 100 ft      | 223.6 ft    |
| Point 11 | 0 ft        | 211.7 ft    |
| Point 12 | 0 ft        | 192 ft      |
| Point 13 | 13 ft       | 192 ft      |
| Point 14 | 24.5 ft     | 213.8 ft    |
| Point 15 | 24.5 ft     | 192 ft      |
| Point 16 | 24.5 ft     | 203 ft      |
| Point 17 | 24.5 ft     | 205 ft      |
| Point 18 | 41.8 ft     | 220.7 ft    |
|          |             |             |

| Point 19         26.6 ft         215.4 ft           Point 20         37.9 ft         223.2 ft           Point 21         6.13959 ft         185.3 ft           Point 22         8.9 ft         192 ft           Point 23         -100 ft         170.1 ft           Point 24         -100 ft         170.1 ft           Point 25         -91.8 ft         174.4 ft           Point 26         -88.3 ft         176.5 ft           Point 27         -85.7 ft         177.8 ft           Point 28         -83.4 ft         178.4 ft           Point 29         -76 ft         178.9 ft           Point 30         -74 ft         179.7 ft           Point 31         -55.9 ft         180.2 ft           Point 32         -37.3 ft         182.3 ft           Point 33         -30.3 ft         182.9 ft           Point 34         -13.6 ft         190.2 ft           Point 35         7 ft         223 ft           Point 36         15 ft         223 ft           Point 37         15 ft         211.7 ft           Point 38         7 ft         211.7 ft           Point 39         -6 ft         195 ft           Point 40  | •        | . •         |              |
|---|----------|-------------|--------------|
| Point 21         6.13959 ft         185.3 ft           Point 22         8.9 ft         192 ft           Point 23         -100 ft         160 ft           Point 24         -100 ft         170.1 ft           Point 25         -91.8 ft         174.4 ft           Point 26         -88.3 ft         176.5 ft           Point 27         -85.7 ft         177.8 ft           Point 28         -83.4 ft         178.4 ft           Point 29         -76 ft         178.9 ft           Point 30         -74 ft         179.7 ft           Point 30         -74 ft         179.7 ft           Point 31         -55.9 ft         180.2 ft           Point 32         -37.3 ft         182.3 ft           Point 31         -55.9 ft         180.2 ft           Point 32         -37.3 ft         182.9 ft           Point 33         -30.3 ft         182.9 ft           Point 34         -13.6 ft         190.2 ft           Point 35         7 ft         223 ft           Point 36         15 ft         211.7 ft           Point 37         15 ft         211.7 ft           Point 40         -37.3275 ft         162.2725 ft           Poin   | Point 19 | 26.6 ft     | 215.4 ft     |
| Point 22         8.9 ft         192 ft           Point 23         -100 ft         160 ft           Point 24         -100 ft         170.1 ft           Point 25         -91.8 ft         174.4 ft           Point 26         -88.3 ft         176.5 ft           Point 27         -85.7 ft         177.8 ft           Point 28         -83.4 ft         178.4 ft           Point 29         -76 ft         178.9 ft           Point 30         -74 ft         179.7 ft           Point 30         -74 ft         179.7 ft           Point 31         -55.9 ft         180.2 ft           Point 32         -37.3 ft         182.9 ft           Point 33         -30.3 ft         182.9 ft           Point 34         -13.6 ft         190.2 ft           Point 35         7 ft         223 ft           Point 36         15 ft         221.7 ft           Point 37         15 ft         211.7 ft           Point 38         7 ft         211.7 ft           Point 39         -6 ft         195 ft           Point 40         -37.3275 ft         162.2725 ft           Point 41         -47.26 ft         160 ft           Point 42   | Point 20 | 37.9 ft     | 223.2 ft     |
| Point 23         -100 ft         170.1 ft           Point 24         -100 ft         170.1 ft           Point 25         -91.8 ft         174.4 ft           Point 26         -88.3 ft         176.5 ft           Point 27         -85.7 ft         177.8 ft           Point 28         -83.4 ft         178.4 ft           Point 29         -76 ft         178.9 ft           Point 30         -74 ft         179.7 ft           Point 30         -74 ft         179.7 ft           Point 31         -55.9 ft         180.2 ft           Point 32         -37.3 ft         182.3 ft           Point 32         -37.3 ft         182.9 ft           Point 33         -30.3 ft         182.9 ft           Point 34         -13.6 ft         190.2 ft           Point 35         7 ft         223 ft           Point 36         15 ft         223 ft           Point 37         15 ft         211.7 ft           Point 38         7 ft         211.7 ft           Point 39         -6 ft         195 ft           Point 40         -37.3275 ft         162.2725 ft           Point 41         -47.26 ft         160 ft           Point 42 <td>Point 21</td> <td>6.13959 ft</td> <td>185.3 ft</td>                         | Point 21 | 6.13959 ft  | 185.3 ft     |
| Point 24         -100 ft         170.1 ft           Point 25         -91.8 ft         174.4 ft           Point 26         -88.3 ft         176.5 ft           Point 27         -85.7 ft         177.8 ft           Point 28         -83.4 ft         178.4 ft           Point 29         -76 ft         178.9 ft           Point 30         -74 ft         179.7 ft           Point 31         -55.9 ft         180.2 ft           Point 31         -55.9 ft         182.3 ft           Point 32         -37.3 ft         182.3 ft           Point 33         -30.3 ft         182.9 ft           Point 34         -13.6 ft         190.2 ft           Point 35         7 ft         223 ft           Point 36         15 ft         223 ft           Point 37         15 ft         211.7 ft           Point 38         7 ft         211.7 ft           Point 39         -6 ft         195 ft           Point 40         -37.3275 ft         162.2725 ft           Point 41         -47.26 ft         160 ft           Point 42         -5.125 ft         182.98095 ft           Point 43         80.7025 ft         160 ft           Poin   | Point 22 | 8.9 ft      | 192 ft       |
| Point 25         -91.8 ft         174.4 ft           Point 26         -88.3 ft         176.5 ft           Point 27         -85.7 ft         177.8 ft           Point 28         -83.4 ft         178.4 ft           Point 29         -76 ft         178.9 ft           Point 30         -74 ft         179.7 ft           Point 31         -55.9 ft         180.2 ft           Point 32         -37.3 ft         182.3 ft           Point 33         -30.3 ft         182.9 ft           Point 34         -13.6 ft         190.2 ft           Point 35         7 ft         223 ft           Point 36         15 ft         211.7 ft           Point 37         15 ft         211.7 ft           Point 38         7 ft         211.7 ft           Point 39         -6 ft         195 ft           Point 40         -37.3275 ft         162.2725 ft           Point 41         -47.26 ft         160 ft           Point 42         -5.125 ft         182.98095 ft           Point 43         80.7025 ft         160 ft           Point 44         -100 ft         129.8675 ft           Point 45         100 ft         129.8675 ft <t< td=""><td>Point 23</td><td>-100 ft</td><td>160 ft</td></t<>                      | Point 23 | -100 ft     | 160 ft       |
| Point 26         -88.3 ft         176.5 ft           Point 27         -85.7 ft         177.8 ft           Point 28         -83.4 ft         178.4 ft           Point 29         -76 ft         178.9 ft           Point 30         -74 ft         179.7 ft           Point 31         -55.9 ft         180.2 ft           Point 32         -37.3 ft         182.9 ft           Point 33         -30.3 ft         182.9 ft           Point 34         -13.6 ft         190.2 ft           Point 35         7 ft         223 ft           Point 36         15 ft         223 ft           Point 37         15 ft         211.7 ft           Point 38         7 ft         211.7 ft           Point 39         -6 ft         195 ft           Point 40         -37.3275 ft         162.2725 ft           Point 41         -47.26 ft         160 ft           Point 42         -5.125 ft         182.98095 ft           Point 43         80.7025 ft         160 ft           Point 44         -100 ft         129.8675 ft           Point 45         100 ft         129.8675 ft           Point 47         -27.95 ft         152.3875 ft  | Point 24 | -100 ft     | 170.1 ft     |
| Point 27         -85.7 ft         177.8 ft           Point 28         -83.4 ft         178.4 ft           Point 29         -76 ft         178.9 ft           Point 30         -74 ft         179.7 ft           Point 31         -55.9 ft         180.2 ft           Point 32         -37.3 ft         182.9 ft           Point 34         -13.6 ft         190.2 ft           Point 34         -13.6 ft         190.2 ft           Point 35         7 ft         223 ft           Point 36         15 ft         211.7 ft           Point 37         15 ft         211.7 ft           Point 38         7 ft         211.7 ft           Point 39         -6 ft         195 ft           Point 40         -37.3275 ft         162.2725 ft           Point 41         -47.26 ft         160 ft           Point 42         -5.125 ft         182.98095 ft           Point 43         80.7025 ft         160 ft           Point 44         -100 ft         129.8675 ft           Point 45         100 ft         129.8675 ft           Point 46         -100 ft         147.8625 ft           Point 47         -27.95 ft         152.3875 ft  | Point 25 | -91.8 ft    | 174.4 ft     |
| Point 28         -83.4 ft         178.9 ft           Point 29         -76 ft         178.9 ft           Point 30         -74 ft         179.7 ft           Point 31         -55.9 ft         180.2 ft           Point 32         -37.3 ft         182.9 ft           Point 34         -13.6 ft         190.2 ft           Point 35         7 ft         223 ft           Point 36         15 ft         223 ft           Point 37         15 ft         211.7 ft           Point 38         7 ft         211.7 ft           Point 39         -6 ft         195 ft           Point 40         -37.3275 ft         162.2725 ft           Point 41         -47.26 ft         160 ft           Point 42         -5.125 ft         182.98095 ft           Point 43         80.7025 ft         160 ft           Point 44         -100 ft         129.8675 ft           Point 45         100 ft         129.8675 ft           Point 46         -100 ft         147.8625 ft           Point 47         -27.95 ft         152.3875 ft           Point 48         -100 ft         198.75 ft           Point 50         100 ft         209.9025 ft   | Point 26 | -88.3 ft    | 176.5 ft     |
| Point 29         -76 ft         178.9 ft           Point 30         -74 ft         179.7 ft           Point 31         -55.9 ft         180.2 ft           Point 32         -37.3 ft         182.3 ft           Point 33         -30.3 ft         182.9 ft           Point 34         -13.6 ft         190.2 ft           Point 35         7 ft         223 ft           Point 36         15 ft         211.7 ft           Point 37         15 ft         211.7 ft           Point 38         7 ft         211.7 ft           Point 39         -6 ft         195 ft           Point 40         -37.3275 ft         162.2725 ft           Point 41         -47.26 ft         160 ft           Point 42         -5.125 ft         182.98095 ft           Point 43         80.7025 ft         160 ft           Point 44         -100 ft         129.8675 ft           Point 45         100 ft         129.8675 ft           Point 47         -27.95 ft         152.3875 ft           Point 48         -100 ft         147.8625 ft           Point 49         16.5 ft         197.3 ft           Point 50         100 ft         209.9025 ft  | Point 27 | -85.7 ft    | 177.8 ft     |
| Point 30         -74 ft         179.7 ft           Point 31         -55.9 ft         180.2 ft           Point 32         -37.3 ft         182.3 ft           Point 33         -30.3 ft         182.9 ft           Point 34         -13.6 ft         190.2 ft           Point 35         7 ft         223 ft           Point 36         15 ft         211.7 ft           Point 37         15 ft         211.7 ft           Point 38         7 ft         211.7 ft           Point 39         -6 ft         195 ft           Point 40         -37.3275 ft         162.2725 ft           Point 40         -37.3275 ft         162.2725 ft           Point 41         -47.26 ft         160 ft           Point 42         -5.125 ft         182.98095 ft           Point 43         80.7025 ft         160 ft           Point 44         -100 ft         129.8675 ft           Point 45         100 ft         129.8675 ft           Point 46         -100 ft         147.8625 ft           Point 47         -27.95 ft         152.3875 ft           Point 48         -100 ft         193.97 ft           Point 50         100 ft         209.9025 ft   | Point 28 | -83.4 ft    | 178.4 ft     |
| Point 31         -55.9 ft         180.2 ft           Point 32         -37.3 ft         182.3 ft           Point 33         -30.3 ft         182.9 ft           Point 34         -13.6 ft         190.2 ft           Point 35         7 ft         223 ft           Point 36         15 ft         211.7 ft           Point 37         15 ft         211.7 ft           Point 38         7 ft         211.7 ft           Point 39         -6 ft         195 ft           Point 40         -37.3275 ft         162.2725 ft           Point 41         -47.26 ft         160 ft           Point 42         -5.125 ft         182.98095 ft           Point 43         80.7025 ft         160 ft           Point 44         -100 ft         129.8675 ft           Point 45         100 ft         129.8675 ft           Point 46         -100 ft         147.8625 ft           Point 47         -27.95 ft         152.3875 ft           Point 48         -100 ft         147.8625 ft           Point 49         16.5 ft         197.3 ft           Point 50         100 ft         209.80965 ft           Point 51         95.42762 ft         209.80965 ft  | Point 29 | -76 ft      | 178.9 ft     |
| Point 32         -37.3 ft         182.9 ft           Point 34         -13.6 ft         190.2 ft           Point 35         7 ft         223 ft           Point 36         15 ft         223 ft           Point 37         15 ft         211.7 ft           Point 38         7 ft         211.7 ft           Point 39         -6 ft         195 ft           Point 40         -37.3275 ft         162.2725 ft           Point 41         -47.26 ft         160 ft           Point 42         -5.125 ft         182.98095 ft           Point 43         80.7025 ft         160 ft           Point 44         -100 ft         129.8675 ft           Point 45         100 ft         129.8675 ft           Point 45         100 ft         147.8625 ft           Point 46         -100 ft         147.8625 ft           Point 47         -27.95 ft         152.3875 ft           Point 48         -100 ft         147.8625 ft           Point 49         16.5 ft         197.3 ft           Point 50         100 ft         209.9025 ft           Point 51         95.42762 ft         209.80965 ft           Point 52         3.915 ft         160.77581 ft <td>Point 30</td> <td>-74 ft</td> <td>179.7 ft</td>            | Point 30 | -74 ft      | 179.7 ft     |
| Point 33         -30.3 ft         190.2 ft           Point 34         -13.6 ft         190.2 ft           Point 35         7 ft         223 ft           Point 36         15 ft         211.7 ft           Point 37         15 ft         211.7 ft           Point 38         7 ft         211.7 ft           Point 39         -6 ft         195 ft           Point 40         -37.3275 ft         162.2725 ft           Point 41         -47.26 ft         160 ft           Point 41         -47.26 ft         160 ft           Point 42         -5.125 ft         182.98095 ft           Point 43         80.7025 ft         160 ft           Point 44         -100 ft         129.8675 ft           Point 45         100 ft         129.8675 ft           Point 46         -100 ft         147.8625 ft           Point 47         -27.95 ft         152.3875 ft           Point 48         -100 ft         147.8625 ft           Point 49         16.5 ft         197.3 ft           Point 50         100 ft         209.9025 ft           Point 51         95.42762 ft         209.80965 ft           Point 52         3.915 ft         160.77581 ft <td>Point 31</td> <td>-55.9 ft</td> <td>180.2 ft</td>          | Point 31 | -55.9 ft    | 180.2 ft     |
| Point 34         -13.6 ft         190.2 ft           Point 35         7 ft         223 ft           Point 36         15 ft         223 ft           Point 37         15 ft         211.7 ft           Point 38         7 ft         211.7 ft           Point 39         -6 ft         195 ft           Point 40         -37.3275 ft         162.2725 ft           Point 41         -47.26 ft         160 ft           Point 42         -5.125 ft         182.98095 ft           Point 43         80.7025 ft         160 ft           Point 44         -100 ft         129.8675 ft           Point 45         100 ft         129.8675 ft           Point 45         100 ft         147.8625 ft           Point 47         -27.95 ft         152.3875 ft           Point 48         -100 ft         147.8625 ft           Point 49         16.5 ft         197.3 ft           Point 50         100 ft         209.9025 ft           Point 51         95.42762 ft         209.80965 ft           Point 52         3.915 ft         160.77581 ft           Point 53         17.7925 ft         187.09412 ft           Point 54         28.7 ft         129.8675 ft  | Point 32 | -37.3 ft    | 182.3 ft     |
| Point 35         7 ft         223 ft           Point 36         15 ft         211.7 ft           Point 38         7 ft         211.7 ft           Point 39         -6 ft         195 ft           Point 40         -37.3275 ft         162.2725 ft           Point 41         -47.26 ft         160 ft           Point 42         -5.125 ft         182.98095 ft           Point 43         80.7025 ft         160 ft           Point 44         -100 ft         129.8675 ft           Point 45         100 ft         129.8675 ft           Point 45         100 ft         129.8675 ft           Point 46         -100 ft         147.8625 ft           Point 47         -27.95 ft         152.3875 ft           Point 48         -100 ft         147.8625 ft           Point 49         16.5 ft         197.3 ft           Point 50         100 ft         209.9025 ft           Point 51         95.42762 ft         209.80965 ft           Point 52         3.915 ft         160.77581 ft           Point 53         17.7925 ft         187.09412 ft           Point 54         28.7 ft         129.8675 ft           Point 55         0 ft         198.7 ft <td>Point 33</td> <td>-30.3 ft</td> <td>182.9 ft</td> | Point 33 | -30.3 ft    | 182.9 ft     |
| Point 36         15 ft         223 ft           Point 37         15 ft         211.7 ft           Point 38         7 ft         211.7 ft           Point 39         -6 ft         195 ft           Point 40         -37.3275 ft         162.2725 ft           Point 41         -47.26 ft         160 ft           Point 42         -5.125 ft         182.98095 ft           Point 43         80.7025 ft         160 ft           Point 44         -100 ft         129.8675 ft           Point 45         100 ft         129.8675 ft           Point 45         100 ft         147.8625 ft           Point 46         -100 ft         147.8625 ft           Point 47         -27.95 ft         152.3875 ft           Point 48         -100 ft         133.97 ft           Point 49         16.5 ft         197.3 ft           Point 50         100 ft         209.9025 ft           Point 51         95.42762 ft         209.80965 ft           Point 52         3.915 ft         160.77581 ft           Point 53         17.7925 ft         187.09412 ft           Point 54         28.7 ft         129.8675 ft           Point 55         0 ft         198.7 ft  | Point 34 | -13.6 ft    | 190.2 ft     |
| Point 37         15 ft         211.7 ft           Point 38         7 ft         211.7 ft           Point 39         -6 ft         195 ft           Point 40         -37.3275 ft         162.2725 ft           Point 41         -47.26 ft         160 ft           Point 42         -5.125 ft         182.98095 ft           Point 43         80.7025 ft         160 ft           Point 44         -100 ft         129.8675 ft           Point 45         100 ft         129.8675 ft           Point 46         -100 ft         147.8625 ft           Point 47         -27.95 ft         152.3875 ft           Point 48         -100 ft         133.97 ft           Point 49         16.5 ft         197.3 ft           Point 50         100 ft         209.9025 ft           Point 51         95.42762 ft         209.80965 ft           Point 52         3.915 ft         160.77581 ft           Point 53         17.7925 ft         187.09412 ft           Point 54         28.7 ft         129.8675 ft           Point 55         0 ft         198.7 ft           Point 56         47.15 ft         195.68393 ft           Point 57         42.67 ft         194.3   | Point 35 | 7 ft        | 223 ft       |
| Point 38         7 ft         211.7 ft           Point 39         -6 ft         195 ft           Point 40         -37.3275 ft         162.2725 ft           Point 41         -47.26 ft         160 ft           Point 42         -5.125 ft         182.98095 ft           Point 43         80.7025 ft         160 ft           Point 44         -100 ft         129.8675 ft           Point 45         100 ft         147.8625 ft           Point 46         -100 ft         147.8625 ft           Point 47         -27.95 ft         152.3875 ft           Point 48         -100 ft         133.97 ft           Point 49         16.5 ft         197.3 ft           Point 50         100 ft         209.9025 ft           Point 51         95.42762 ft         209.80965 ft           Point 52         3.915 ft         160.77581 ft           Point 53         17.7925 ft         187.09412 ft           Point 54         28.7 ft         129.8675 ft           Point 55         0 ft         198.7 ft           Point 56         47.15 ft         195.68393 ft           Point 57         42.67 ft         194.37311 ft           Point 58         0 ft         19   | Point 36 | 15 ft       | 223 ft       |
| Point 39         -6 ft         195 ft           Point 40         -37.3275 ft         162.2725 ft           Point 41         -47.26 ft         160 ft           Point 42         -5.125 ft         182.98095 ft           Point 43         80.7025 ft         160 ft           Point 44         -100 ft         129.8675 ft           Point 45         100 ft         129.8675 ft           Point 46         -100 ft         147.8625 ft           Point 47         -27.95 ft         152.3875 ft           Point 48         -100 ft         133.97 ft           Point 49         16.5 ft         197.3 ft           Point 50         100 ft         209.9025 ft           Point 51         95.42762 ft         209.80965 ft           Point 52         3.915 ft         160.77581 ft           Point 53         17.7925 ft         187.09412 ft           Point 54         28.7 ft         129.8675 ft           Point 55         0 ft         198.7 ft           Point 56         47.15 ft         195.68393 ft           Point 57         42.67 ft         194.37311 ft           Point 58         0 ft         195 ft           Point 59         -32.3 ft  | Point 37 | 15 ft       | 211.7 ft     |
| Point 40         -37.3275 ft         162.2725 ft           Point 41         -47.26 ft         160 ft           Point 42         -5.125 ft         182.98095 ft           Point 43         80.7025 ft         160 ft           Point 44         -100 ft         129.8675 ft           Point 45         100 ft         129.8675 ft           Point 46         -100 ft         147.8625 ft           Point 47         -27.95 ft         152.3875 ft           Point 48         -100 ft         133.97 ft           Point 49         16.5 ft         197.3 ft           Point 50         100 ft         209.9025 ft           Point 51         95.42762 ft         209.80965 ft           Point 52         3.915 ft         160.77581 ft           Point 53         17.7925 ft         187.09412 ft           Point 53         17.7925 ft         129.8675 ft           Point 54         28.7 ft         129.8675 ft           Point 55         0 ft         198.7 ft           Point 56         47.15 ft         195.68393 ft           Point 57         42.67 ft         194.37311 ft           Point 58         0 ft         195 ft           Point 60         -16 ft  | Point 38 | 7 ft        | 211.7 ft     |
| Point 41         -47.26 ft         160 ft           Point 42         -5.125 ft         182.98095 ft           Point 43         80.7025 ft         160 ft           Point 44         -100 ft         129.8675 ft           Point 45         100 ft         147.8625 ft           Point 46         -100 ft         147.8625 ft           Point 47         -27.95 ft         152.3875 ft           Point 48         -100 ft         133.97 ft           Point 49         16.5 ft         197.3 ft           Point 50         100 ft         209.9025 ft           Point 51         95.42762 ft         209.80965 ft           Point 52         3.915 ft         160.77581 ft           Point 53         17.7925 ft         187.09412 ft           Point 53         17.7925 ft         187.09412 ft           Point 54         28.7 ft         129.8675 ft           Point 55         0 ft         198.7 ft           Point 55         0 ft         198.7 ft           Point 56         47.15 ft         195.68393 ft           Point 57         42.67 ft         194.37311 ft           Point 59         -32.3 ft         165.4 ft           Point 60         -16 ft   | Point 39 | -6 ft       | 195 ft       |
| Point 42         -5.125 ft         182.98095 ft           Point 43         80.7025 ft         160 ft           Point 44         -100 ft         129.8675 ft           Point 45         100 ft         147.8625 ft           Point 46         -100 ft         147.8625 ft           Point 47         -27.95 ft         152.3875 ft           Point 48         -100 ft         133.97 ft           Point 49         16.5 ft         197.3 ft           Point 50         100 ft         209.9025 ft           Point 51         95.42762 ft         209.80965 ft           Point 52         3.915 ft         160.77581 ft           Point 53         17.7925 ft         187.09412 ft           Point 54         28.7 ft         129.8675 ft           Point 55         0 ft         198.7 ft           Point 55         0 ft         198.7 ft           Point 56         47.15 ft         195.68393 ft           Point 57         42.67 ft         194.37311 ft           Point 58         0 ft         195 ft           Point 59         -32.3 ft         165.4 ft           Point 60         -16 ft         164.1 ft           Point 61         -100 ft         150.052   | Point 40 | -37.3275 ft | 162.2725 ft  |
| Point 43         80.7025 ft         160 ft           Point 44         -100 ft         129.8675 ft           Point 45         100 ft         129.8675 ft           Point 46         -100 ft         147.8625 ft           Point 47         -27.95 ft         152.3875 ft           Point 48         -100 ft         133.97 ft           Point 49         16.5 ft         197.3 ft           Point 50         100 ft         209.9025 ft           Point 51         95.42762 ft         209.80965 ft           Point 52         3.915 ft         160.77581 ft           Point 53         17.7925 ft         187.09412 ft           Point 53         17.7925 ft         187.09412 ft           Point 54         28.7 ft         129.8675 ft           Point 55         0 ft         198.7 ft           Point 55         0 ft         198.7 ft           Point 57         42.67 ft         194.37311 ft           Point 58         0 ft         195 ft           Point 59         -32.3 ft         165.4 ft           Point 60         -16 ft         164.1 ft           Point 61         -100 ft         150.0525 ft           Point 62         15 ft         218.535 ft   | Point 41 | -47.26 ft   | 160 ft       |
| Point 44         -100 ft         129.8675 ft           Point 45         100 ft         129.8675 ft           Point 46         -100 ft         147.8625 ft           Point 47         -27.95 ft         152.3875 ft           Point 48         -100 ft         133.97 ft           Point 49         16.5 ft         197.3 ft           Point 50         100 ft         209.9025 ft           Point 51         95.42762 ft         209.80965 ft           Point 52         3.915 ft         160.77581 ft           Point 53         17.7925 ft         187.09412 ft           Point 54         28.7 ft         129.8675 ft           Point 55         0 ft         198.7 ft           Point 56         47.15 ft         195.68393 ft           Point 57         42.67 ft         194.37311 ft           Point 58         0 ft         195 ft           Point 59         -32.3 ft         165.4 ft           Point 60         -16 ft         164.1 ft           Point 61         -100 ft         150.0525 ft           Point 62         15 ft         218.535 ft           Point 64         7 ft         214.495 ft           Point 65         1.355 ft         211.7 ft   | Point 42 | -5.125 ft   | 182.98095 ft |
| Point 45         100 ft         129.8675 ft           Point 46         -100 ft         147.8625 ft           Point 47         -27.95 ft         152.3875 ft           Point 48         -100 ft         133.97 ft           Point 49         16.5 ft         197.3 ft           Point 50         100 ft         209.9025 ft           Point 51         95.42762 ft         209.80965 ft           Point 52         3.915 ft         160.77581 ft           Point 53         17.7925 ft         187.09412 ft           Point 54         28.7 ft         129.8675 ft           Point 55         0 ft         198.7 ft           Point 55         0 ft         195.68393 ft           Point 57         42.67 ft         194.37311 ft           Point 58         0 ft         195 ft           Point 59         -32.3 ft         165.4 ft           Point 60         -16 ft         164.1 ft           Point 61         -100 ft         150.0525 ft           Point 62         15 ft         218.535 ft           Point 64         7 ft         214.495 ft           Point 65         1.355 ft         211.7 ft  | Point 43 | 80.7025 ft  | 160 ft       |
| Point 46         -100 ft         147.8625 ft           Point 47         -27.95 ft         152.3875 ft           Point 48         -100 ft         133.97 ft           Point 49         16.5 ft         197.3 ft           Point 50         100 ft         209.9025 ft           Point 51         95.42762 ft         209.80965 ft           Point 52         3.915 ft         160.77581 ft           Point 53         17.7925 ft         187.09412 ft           Point 54         28.7 ft         129.8675 ft           Point 55         0 ft         198.7 ft           Point 56         47.15 ft         195.68393 ft           Point 57         42.67 ft         194.37311 ft           Point 58         0 ft         195 ft           Point 59         -32.3 ft         165.4 ft           Point 60         -16 ft         164.1 ft           Point 61         -100 ft         150.0525 ft           Point 62         15 ft         218.535 ft           Point 64         7 ft         214.495 ft           Point 65         1.355 ft         211.7 ft  | Point 44 | -100 ft     | 129.8675 ft  |
| Point 47         -27.95 ft         152.3875 ft           Point 48         -100 ft         133.97 ft           Point 49         16.5 ft         197.3 ft           Point 50         100 ft         209.9025 ft           Point 51         95.42762 ft         209.80965 ft           Point 52         3.915 ft         160.77581 ft           Point 53         17.7925 ft         187.09412 ft           Point 54         28.7 ft         129.8675 ft           Point 55         0 ft         198.7 ft           Point 56         47.15 ft         195.68393 ft           Point 57         42.67 ft         194.37311 ft           Point 58         0 ft         195 ft           Point 59         -32.3 ft         165.4 ft           Point 60         -16 ft         164.1 ft           Point 61         -100 ft         150.0525 ft           Point 62         15 ft         218.535 ft           Point 64         7 ft         214.495 ft           Point 65         1.355 ft         211.7 ft   | Point 45 | 100 ft      | 129.8675 ft  |
| Point 48         -100 ft         133.97 ft           Point 49         16.5 ft         197.3 ft           Point 50         100 ft         209.9025 ft           Point 51         95.42762 ft         209.80965 ft           Point 52         3.915 ft         160.77581 ft           Point 53         17.7925 ft         187.09412 ft           Point 54         28.7 ft         129.8675 ft           Point 55         0 ft         198.7 ft           Point 56         47.15 ft         195.68393 ft           Point 57         42.67 ft         194.37311 ft           Point 58         0 ft         195 ft           Point 59         -32.3 ft         165.4 ft           Point 60         -16 ft         164.1 ft           Point 61         -100 ft         150.0525 ft           Point 62         15 ft         218.535 ft           Point 64         7 ft         214.495 ft           Point 65         1.355 ft         211.7 ft  | Point 46 | -100 ft     | 147.8625 ft  |
| Point 49         16.5 ft         197.3 ft           Point 50         100 ft         209.9025 ft           Point 51         95.42762 ft         209.80965 ft           Point 52         3.915 ft         160.77581 ft           Point 53         17.7925 ft         187.09412 ft           Point 54         28.7 ft         129.8675 ft           Point 55         0 ft         198.7 ft           Point 56         47.15 ft         195.68393 ft           Point 57         42.67 ft         194.37311 ft           Point 58         0 ft         195 ft           Point 59         -32.3 ft         165.4 ft           Point 60         -16 ft         164.1 ft           Point 61         -100 ft         150.0525 ft           Point 62         15 ft         218.535 ft           Point 64         7 ft         214.495 ft           Point 65         1.355 ft         211.7 ft   | Point 47 | -27.95 ft   | 152.3875 ft  |
| Point 50         100 ft         209.9025 ft           Point 51         95.42762 ft         209.80965 ft           Point 52         3.915 ft         160.77581 ft           Point 53         17.7925 ft         187.09412 ft           Point 54         28.7 ft         129.8675 ft           Point 55         0 ft         198.7 ft           Point 56         47.15 ft         195.68393 ft           Point 57         42.67 ft         194.37311 ft           Point 58         0 ft         195 ft           Point 59         -32.3 ft         165.4 ft           Point 60         -16 ft         164.1 ft           Point 61         -100 ft         150.0525 ft           Point 62         15 ft         218.535 ft           Point 63         24 ft         223 ft           Point 64         7 ft         214.495 ft           Point 65         1.355 ft         211.7 ft   | Point 48 | -100 ft     | 133.97 ft    |
| Point 51         95.42762 ft         209.80965 ft           Point 52         3.915 ft         160.77581 ft           Point 53         17.7925 ft         187.09412 ft           Point 54         28.7 ft         129.8675 ft           Point 55         0 ft         198.7 ft           Point 56         47.15 ft         195.68393 ft           Point 57         42.67 ft         194.37311 ft           Point 58         0 ft         195 ft           Point 59         -32.3 ft         165.4 ft           Point 60         -16 ft         164.1 ft           Point 61         -100 ft         150.0525 ft           Point 62         15 ft         218.535 ft           Point 63         24 ft         223 ft           Point 64         7 ft         214.495 ft           Point 65         1.355 ft         211.7 ft   | Point 49 | 16.5 ft     | 197.3 ft     |
| Point 52       3.915 ft       160.77581 ft         Point 53       17.7925 ft       187.09412 ft         Point 54       28.7 ft       129.8675 ft         Point 55       0 ft       198.7 ft         Point 56       47.15 ft       195.68393 ft         Point 57       42.67 ft       194.37311 ft         Point 58       0 ft       195 ft         Point 59       -32.3 ft       165.4 ft         Point 60       -16 ft       164.1 ft         Point 61       -100 ft       150.0525 ft         Point 62       15 ft       218.535 ft         Point 63       24 ft       223 ft         Point 64       7 ft       214.495 ft         Point 65       1.355 ft       211.7 ft   | Point 50 | 100 ft      | 209.9025 ft  |
| Point 53       17.7925 ft       187.09412 ft         Point 54       28.7 ft       129.8675 ft         Point 55       0 ft       198.7 ft         Point 56       47.15 ft       195.68393 ft         Point 57       42.67 ft       194.37311 ft         Point 58       0 ft       195 ft         Point 59       -32.3 ft       165.4 ft         Point 60       -16 ft       164.1 ft         Point 61       -100 ft       150.0525 ft         Point 62       15 ft       218.535 ft         Point 63       24 ft       223 ft         Point 64       7 ft       214.495 ft         Point 65       1.355 ft       211.7 ft  | Point 51 | 95.42762 ft | 209.80965 ft |
| Point 54       28.7 ft       129.8675 ft         Point 55       0 ft       198.7 ft         Point 56       47.15 ft       195.68393 ft         Point 57       42.67 ft       194.37311 ft         Point 58       0 ft       195 ft         Point 59       -32.3 ft       165.4 ft         Point 60       -16 ft       164.1 ft         Point 61       -100 ft       150.0525 ft         Point 62       15 ft       218.535 ft         Point 63       24 ft       223 ft         Point 64       7 ft       214.495 ft         Point 65       1.355 ft       211.7 ft   | Point 52 | 3.915 ft    | 160.77581 ft |
| Point 55         0 ft         198.7 ft           Point 56         47.15 ft         195.68393 ft           Point 57         42.67 ft         194.37311 ft           Point 58         0 ft         195 ft           Point 59         -32.3 ft         165.4 ft           Point 60         -16 ft         164.1 ft           Point 61         -100 ft         150.0525 ft           Point 62         15 ft         218.535 ft           Point 63         24 ft         223 ft           Point 64         7 ft         214.495 ft           Point 65         1.355 ft         211.7 ft  | Point 53 | 17.7925 ft  | 187.09412 ft |
| Point 56       47.15 ft       195.68393 ft         Point 57       42.67 ft       194.37311 ft         Point 58       0 ft       195 ft         Point 59       -32.3 ft       165.4 ft         Point 60       -16 ft       164.1 ft         Point 61       -100 ft       150.0525 ft         Point 62       15 ft       218.535 ft         Point 63       24 ft       223 ft         Point 64       7 ft       214.495 ft         Point 65       1.355 ft       211.7 ft   | Point 54 | 28.7 ft     | 129.8675 ft  |
| Point 5742.67 ft194.37311 ftPoint 580 ft195 ftPoint 59-32.3 ft165.4 ftPoint 60-16 ft164.1 ftPoint 61-100 ft150.0525 ftPoint 6215 ft218.535 ftPoint 6324 ft223 ftPoint 647 ft214.495 ftPoint 651.355 ft211.7 ft  | Point 55 | 0 ft        | 198.7 ft     |
| Point 58       0 ft       195 ft         Point 59       -32.3 ft       165.4 ft         Point 60       -16 ft       164.1 ft         Point 61       -100 ft       150.0525 ft         Point 62       15 ft       218.535 ft         Point 63       24 ft       223 ft         Point 64       7 ft       214.495 ft         Point 65       1.355 ft       211.7 ft   | Point 56 | 47.15 ft    | 195.68393 ft |
| Point 59       -32.3 ft       165.4 ft         Point 60       -16 ft       164.1 ft         Point 61       -100 ft       150.0525 ft         Point 62       15 ft       218.535 ft         Point 63       24 ft       223 ft         Point 64       7 ft       214.495 ft         Point 65       1.355 ft       211.7 ft  | Point 57 | 42.67 ft    | 194.37311 ft |
| Point 60       -16 ft       164.1 ft         Point 61       -100 ft       150.0525 ft         Point 62       15 ft       218.535 ft         Point 63       24 ft       223 ft         Point 64       7 ft       214.495 ft         Point 65       1.355 ft       211.7 ft   | Point 58 | 0 ft        | 195 ft       |
| Point 61       -100 ft       150.0525 ft         Point 62       15 ft       218.535 ft         Point 63       24 ft       223 ft         Point 64       7 ft       214.495 ft         Point 65       1.355 ft       211.7 ft  | Point 59 | -32.3 ft    | 165.4 ft     |
| Point 62       15 ft       218.535 ft         Point 63       24 ft       223 ft         Point 64       7 ft       214.495 ft         Point 65       1.355 ft       211.7 ft   | Point 60 | -16 ft      | 164.1 ft     |
| Point 63       24 ft       223 ft         Point 64       7 ft       214.495 ft         Point 65       1.355 ft       211.7 ft   | Point 61 | -100 ft     | 150.0525 ft  |
| Point 64         7 ft         214.495 ft           Point 65         1.355 ft         211.7 ft   | Point 62 | 15 ft       | 218.535 ft   |
| Point 65 1.355 ft 211.7 ft  | Point 63 | 24 ft       | 223 ft       |
|   | Point 64 | 7 ft        | 214.495 ft   |
| Point 66 25.9 ft 223 ft   | Point 65 | 1.355 ft    | 211.7 ft     |
|   | Point 66 | 25.9 ft     | 223 ft       |
|   |          |             |              |

### 1A.1 Compound - Static (Spencer)

| Point 67 | 22 ft       | 192 ft       |
|----------|-------------|--------------|
| Point 68 | 15.0117 ft  | 208.01106 ft |
| Point 69 | 21.5 ft     | 192 ft       |
| Point 70 | 15.5 ft     | 192 ft       |
| Point 71 | 15.5 ft     | 211.7 ft     |
| Point 72 | 15.5 ft     | 194.35 ft    |
| Point 73 | 15.5 ft     | 197.3 ft     |
| Point 74 | 15.5 ft     | 208.29 ft    |
| Point 75 | 18.50702 ft | 197.3 ft     |
| Point 76 | 15.5 ft     | 196.43333 ft |
| Point 77 | 21.5 ft     | 211.7 ft     |
| Point 78 | 20 ft       | 197.3 ft     |
| Point 79 | 20 ft       | 192 ft       |
| Point 80 | 21.5 ft     | 202 ft       |
| Point 81 | 21.5 ft     | 200 ft       |
| Point 82 | 21.5 ft     | 208.29 ft    |
| Point 83 | 31.9 ft     | 223.1 ft     |
| Point 84 | 31.9 ft     | 219.08 ft    |

## Regions

|              | Material   | Points   | Area                       |
|--------------|--|--|----------------------------|
| Region<br>1  | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 1,2,52,3,43  | 1,263.5<br>ft <sup>2</sup> |
| Region<br>2  | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 52,2,50,51,56,57,53,5,60,6,47,3                          | 2,656.9<br>ft <sup>2</sup> |
| Region<br>3  | Gravel Borrow  | 9,18,8,7,10  | 214.55<br>ft <sup>2</sup>  |
| Region<br>4  | Gravel Borrow  | 38,65,11,55,68,74,71,37                                  | 127 ft²                    |
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel                                  | 8,16,17,18   | 31.556<br>ft <sup>2</sup>  |
| Region<br>6  | ESU 2A Very Loose to Loose<br>Sand/Gravel                        | 18,17,14,19,84,20,9                                      | 115.05<br>ft <sup>2</sup>  |
| Region<br>7  | Common Borrow  | 38,37,62,64  | 38.52<br>ft <sup>2</sup>   |
| Region<br>8  | Common Borrow  | 14,19,84,83,66,63,62,37,71,77                            | 132.58<br>ft <sup>2</sup>  |
| Region<br>9  | ESU 2B Medium Dense Sand/Gravel                                  | 22,42,59,40,60,5,21,13                                   | 332.37<br>ft <sup>2</sup>  |
| Region<br>10 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 44,54,45,1,43,3,47,48                                    | 4,704.7<br>ft <sup>2</sup> |
| Region<br>11 | ESU 2B Medium Dense Sand/Gravel                                  | 41,46,48,47,6,60,40                                      | 992.46<br>ft <sup>2</sup>  |
| Region<br>12 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 56,51,50,4,7,8,16,15,67,69,79,70,13,21,5,53,57           | 1,417.8<br>ft <sup>2</sup> |
| Region<br>13 | ESU 2A Very Loose to Loose<br>Sand/Gravel                        | 34,33,32,31,30,29,28,27,26,25,24,23,40,59,42,22,12,58,39 | 1,656.2<br>ft <sup>2</sup> |
| Region<br>14 | ESU 2A Very Loose to Loose<br>Sand/Gravel                        | 40,23,61,46,41   | 379.99<br>ft <sup>2</sup>  |
| Region<br>15 |  | 63,36,62   | 20.093<br>ft <sup>2</sup>  |

| Region<br>16 |   | 36,35,64,62             | 51.88<br>ft <sup>2</sup>   |
|--------------|---|-------------------------|----------------------------|
| Region<br>17 | Common Borrow                             | 64,65,38                | 7.8889<br>ft <sup>2</sup>  |
| Region<br>18 | ESU 4B Dense to Very Dense<br>Sand/Gravel | 15,16,81,69,67          | 28.5 ft <sup>2</sup>       |
| Region<br>19 | Gravel Borrow                             | 72,76,22,13             | 11.692<br>ft <sup>2</sup>  |
| Region<br>20 | Gravel Borrow                             | 70,72,13                | 2.9375<br>ft <sup>2</sup>  |
| Region<br>21 | Gravel Borrow                             | 70,79,78,75,72          | 19.415<br>ft <sup>2</sup>  |
| Region<br>22 | Gravel Borrow                             | 81,75,78,79,69          | 11.991<br>ft <sup>2</sup>  |
| Region<br>23 | Gravel Borrow                             | 49,75,81,80             | 7.7095<br>ft <sup>2</sup>  |
| Region<br>24 | Gravel Borrow                             | 49,76,72,75             | 4.002<br>ft <sup>2</sup>   |
| Region<br>25 | Gravel Borrow                             | 73,76,49                | 0.43333<br>ft <sup>2</sup> |
| Region<br>26 | Gravel Borrow                             | 76,73,74,68,55,58,12,22 | 163.72<br>ft <sup>2</sup>  |
| Region<br>27 | ESU 2B Medium Dense Sand/Gravel           | 80,81,16,17             | 6 ft²                      |
| Region<br>28 | Gravel Borrow                             | 74,82,77                | 10.23<br>ft <sup>2</sup>   |
| Region<br>29 | Gravel Borrow                             | 77,71,74                | 10.23<br>ft <sup>2</sup>   |
| Region<br>30 | ESU 2A Very Loose to Loose<br>Sand/Gravel | 77,82,80,17,14          | 27.75<br>ft <sup>2</sup>   |
| Region<br>31 | Gravel Borrow                             | 73,49,80,82,74          | 54.19<br>ft <sup>2</sup>   |
| Region<br>32 | Common Borrow                             | 20,83,84                | 12.06<br>ft <sup>2</sup>   |
| Region<br>33 |   | 55,39,58                | 11.1 ft²                   |

## **Slip Results**

Slip Surfaces Analysed: 9745 of 11466 converged

## **Current Slip Surface**

Slip Surface: 2,852 Factor of Safety: 1.3 Volume: 926.15021 ft<sup>3</sup> Weight: 111,473.27 lbf

Resisting Moment: 3,612,669.1 lbf·ft Activating Moment: 2,792,227.2 lbf·ft

Resisting Force: 56,229.62 lbf

#### 1A.1 Compound - Static (Spencer)

Activating Force: 43,471.782 lbf Slip Rank: 1 of 11,466 slip surfaces Exit: (-32.349646, 182.72432) ft Entry: (32.424307, 223.10874) ft

Radius: 52.811397 ft

Center: (-19.274577, 233.89155) ft

## **Slip Slices**

| Slices      | I                |                 | I                 |                          | ı                      | 1                    | I                   | I  |
|-------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|--|
|             | X                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material                                |
| Slice<br>1  | -31.324823<br>ft | 182.48409<br>ft | -181.68176<br>psf | 69.591423<br>psf         | 43.485547<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>2  | -29.25625<br>ft  | 182.04293<br>ft | -180.15416<br>psf | 257.8555<br>psf          | 161.126<br>psf         | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>3  | -27.16875<br>ft  | 181.68417<br>ft | -178.93878<br>psf | 472.73904<br>psf         | 295.40014<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>4  | -25.08125<br>ft  | 181.41086<br>ft | -178.88779<br>psf | 646.2097<br>psf          | 403.79663<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>5  | -22.99375<br>ft  | 181.22167<br>ft | -179.14535<br>psf | 786.17185<br>psf         | 491.25469<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>6  | -20.90625<br>ft  | 181.1157<br>ft  | -177.96849<br>psf | 898.38896<br>psf         | 561.37573<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>7  | -18.81875<br>ft  | 181.09244<br>ft | -176.75492<br>psf | 987.16635<br>psf         | 616.85 psf             | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>8  | -16.73125<br>ft  | 181.15179<br>ft | -177.75218<br>psf | 1,055.7875<br>psf        | 659.72925<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>9  | -14.64375<br>ft  | 181.29401<br>ft | -179.44633<br>psf | 1,106.8015<br>psf        | 691.60636<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>10 | -12.65 ft        | 181.50604<br>ft | -184.2186<br>psf  | 1,164.3132<br>psf        | 727.54366<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>11 | -10.75 ft        | 181.78159<br>ft | -200.14219<br>psf | 1,228.3695<br>psf        | 767.57043<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>12 | -8.85 ft         | 182.12832<br>ft | -294.87555<br>psf | 1,278.325<br>psf         | 798.7861<br>psf        | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>13 | -6.95 ft         | 182.54767<br>ft | -362.48685<br>psf | 1,388.2344<br>psf        | 867.46514<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>14 | -5.521266<br>ft  | 182.90485<br>ft | -396.27515<br>psf | 1,443.877<br>psf         | 902.23446<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |

| Slice<br>15 | -3.781899<br>ft | 183.42095<br>ft | -389.40397<br>psf | 1,255.4769<br>psf | 784.50904<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
|-------------|-----------------|-----------------|-------------------|-------------------|-------------------|-------|-------|---------------------------------------|
| Slice<br>16 | -1.260633<br>ft | 184.26552<br>ft | -355.49357<br>psf | 1,109.1323<br>psf | 693.06278<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>17 | 0.6775 ft       | 184.9996<br>ft  | -331.74593<br>psf | 3,012.3532<br>psf | 1,882.3272<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>18 | 2.2958333<br>ft | 185.69717<br>ft | -312.89226<br>psf | 2,858.8371<br>psf | 1,786.3997<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>19 | 4.1775 ft       | 186.58467<br>ft | -292.03965<br>psf | 2,760.0952<br>psf | 1,724.6989<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>20 | 6.0591667<br>ft | 187.56559<br>ft | -272.64084<br>psf | 2,654.7246<br>psf | 1,658.856<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>21 | 7.95 ft         | 188.65178<br>ft | -254.49171<br>psf | 2,541.9838<br>psf | 1,588.4078<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>22 | 9.8958729<br>ft | 189.88359<br>ft | -237.26176<br>psf | 2,416.3601<br>psf | 1,509.9094<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>23 | 11.887619<br>ft | 191.27185<br>ft | -220.50564<br>psf | 2,283.6536<br>psf | 1,426.9851<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>24 | 13.227615<br>ft | 192.26872<br>ft | -209.5233<br>psf  | 2,273.7015<br>psf | 1,776.4103<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>25 | 14.285869<br>ft | 193.12534<br>ft | -200.2752<br>psf  | 2,076.5959<br>psf | 1,622.4145<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>26 | 15.25 ft        | 193.92922<br>ft | -190.94009<br>psf | 1,995.0411<br>psf | 1,558.6969<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>27 | 16 ft           | 194.59402<br>ft | -185.40797<br>psf | 1,879.6808<br>psf | 1,468.5676<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>28 | 17.50351 ft     | 196.0173<br>ft  | -176.11263<br>psf | 1,716.8318<br>psf | 1,341.336<br>psf  | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>29 | 18.656323<br>ft | 197.14588<br>ft | -172.10212<br>psf | 1,589.6038<br>psf | 1,241.9346<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>30 | 19.543751<br>ft | 198.10056<br>ft | -176.31912<br>psf | 1,503.2657<br>psf | 1,174.4799<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>31 | 20.890939<br>ft | 199.61482<br>ft | -189.41042<br>psf | 1,371.6608<br>psf | 1,071.6588<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>32 | 22.75 ft        | 201.97436<br>ft | -214.35342<br>psf | 1,135.1803<br>psf | 709.33937<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>33 | 24.25 ft        | 203.98403<br>ft | -237.06792<br>psf | 992.64495<br>psf  | 620.27341<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>34 | 25.01513 ft     | 205.14142<br>ft | -254.02098<br>psf | 897.66765<br>psf  | 560.925<br>psf    | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice       |                 | 206.23572       | -263.26581        | 812.19653         | 507.51672         |       |       | ESU 2A Very                           |

| _           |                 |                 |                   |                  | _                |       |       |  |
|-------------|-----------------|-----------------|-------------------|------------------|------------------|-------|-------|--|
| 35          | 25.71513 ft     | ft              | psf               | psf              | psf              | 0 psf | 0 psf | Loose to Loose<br>Sand/Gravel                |
| Slice<br>36 | 26.25 ft        | 207.13189<br>ft | -251.73198<br>psf | 745.92615<br>psf | 466.10639<br>psf | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>37 | 27.772997<br>ft | 210.0412<br>ft  | -214.97451<br>psf | 551.16542<br>psf | 344.40638<br>psf | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>38 | 30.11899 ft     | 215.50645<br>ft | -181.88356<br>psf | 258.40327<br>psf | 161.46829<br>psf | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>39 | 31.595994<br>ft | 219.75154<br>ft | 0 psf             | 93.238487<br>psf | 58.261873<br>psf | 0 psf | 0 psf | Common Borrow                                |
| Slice       | 32.162153       | 221.97699<br>ft | 0 psf             | 27.224015        | 17.011452        | 0 psf | 0 psf | Common Borrow                                |

# 1A.2 Compound - Static (M-P)

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## **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 650 Date: 01/17/2022 Time: 01:45:50 PM

Tool Version: 11.1.1.22085

Last Solved Date: 01/17/2022 Last Solved Time: 01:59:30 PM

## **Project Settings**

Unit System: U.S. Customary Units

## **Analysis Settings**

### 1A.2 Compound - Static (M-P)

Kind: SLOPE/W

Parent: 1. Steady State (Compound) Analysis Type: Morgenstern-Price

Settings

Side Function

Interslice force function option: Half-Sine

PWP Conditions from Parent Analysis: 1. Steady State (Compound) [(last)]

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 20

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

Factor of Safety Convergence Settings

Maximum Number of Iterations: 100 Tolerable difference in F of S: 0.001

Solution Settings

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

### **Materials**

### ESU 2A Very Loose to Loose Sand/Gravel

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **ESU 2B Medium Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

## **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

## ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

### Reinforcements

#### Row 1

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 6.6 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 2

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 6.1 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 3

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 5.6 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 4

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 5.1 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 5

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 4.6 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 6

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 4.1 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

### Row 7 (4 straps)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 7.2 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 7,860 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 7,860 lbf/ft

### Row 8 (4 straps)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 6.2 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 7,860 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 7,860 lbf/ft

## Slip Surface Entry and Exit

Left Type: Range

Left-Zone Left Coordinate: (-45, 181.43065) ft

Left-Zone Right Coordinate: (0, 200) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15, 218.535) ft Right-Zone Right Coordinate: (55, 223.299) ft

Right-Zone Increment: 20 Radius Increments: 20

## **Slip Surface Limits**

Left Coordinate: (-100, 170.1) ft Right Coordinate: (100, 223.6) ft

## **Reinforcement Lines**

#### Reinforcement Line 1

Reinforcement: Row 1 Lock to Ground Surface: Yes Outside Point: (0, 210.5) ft Inside Point: (15.5, 210.5) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf
Available Length: 0 ft
Required Length: 0 ft
Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 2**

Reinforcement: Row 8 (4 straps) Lock to Ground Surface: No Outside Point: (0, 193.7) ft Inside Point: (20, 193.7) ft

Length: 20 ft
Orientation: 0 °

Slip Surface Intersection: (14.983919, 193.7) ft

Max. Pullout Force: 7,860 lbf Available Length: 5.0160809 ft Required Length: 5.0160809 ft Pullout Force: 3,478.3709 lbf

Pullout Force per Length: 693.44394 lbf/ft Governing Component: Pullout Resistance

#### **Reinforcement Line 3**

Reinforcement: Row 6 Lock to Ground Surface: Yes Outside Point: (0, 198.5) ft Inside Point: (15.5, 198.5) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 4**

Reinforcement: Row 2 Lock to Ground Surface: Yes Outside Point: (0, 208.1) ft Inside Point: (15.5, 208.1) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 5**

Reinforcement: Row 5

Lock to Ground Surface: Yes Outside Point: (0, 200.9) ft Inside Point: (15.5, 200.9) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 6**

Reinforcement: Row 4 Lock to Ground Surface: Yes Outside Point: (0, 203.3) ft Inside Point: (15.5, 203.3) ft

Length: 15.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 7**

Reinforcement: Row 3 Lock to Ground Surface: Yes Outside Point: (0, 205.7) ft Inside Point: (15.5, 205.7) ft

Length: 15.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 8**

Reinforcement: Row 7 (4 straps) Lock to Ground Surface: Yes Outside Point: (0, 196.1) ft Inside Point: (20, 196.1) ft

Length: 20 ft
Orientation: 0 °

Slip Surface Intersection: (17.588678, 196.1) ft

Max. Pullout Force: 7,860 lbf Available Length: 2.4113217 ft Required Length: 2.4113217 ft Pullout Force: 1,832.5947 lbf

Pullout Force per Length: 759.99596 lbf/ft Governing Component: Pullout Resistance

## **Surcharge Loads**

## **Surcharge Load 1**

Surcharge (Unit Weight): 250 pcf

Direction: Vertical

#### **Coordinates**

| X       | Υ         |
|---------|-----------|
| 35.9 ft | 224.15 ft |
| 40.2 ft | 224.2 ft  |
| 100 ft  | 224.6 ft  |

## Geometry

Name: Default Geometry

## **Settings**

View: 2D

Element Thickness: 1 ft

#### **Points**

|          | Х           | Y           |
|----------|-------------|-------------|
| Point 1  | 100 ft      | 160 ft      |
| Point 2  | 100 ft      | 185.5 ft    |
| Point 3  | 0.9 ft      | 160 ft      |
| Point 4  | 100 ft      | 211.1475 ft |
| Point 5  | 3.8 ft      | 183 ft      |
| Point 6  | -20.1275 ft | 160 ft      |
| Point 7  | 100 ft      | 219.64 ft   |
| Point 8  | 42.5825 ft  | 219.8525 ft |
| Point 9  | 40.2 ft     | 223.2 ft    |
| Point 10 | 100 ft      | 223.6 ft    |
| Point 11 | 0 ft        | 211.7 ft    |
| Point 12 | 0 ft        | 192 ft      |
| Point 13 | 13 ft       | 192 ft      |
| Point 14 | 24.5 ft     | 213.8 ft    |
| Point 15 | 24.5 ft     | 192 ft      |
| Point 16 | 24.5 ft     | 203 ft      |
| Point 17 | 24.5 ft     | 205 ft      |
|          |             |             |

| Point 18 | 41.8 ft            | 220.7 ft             |
|----------|--------------------|----------------------|
| Point 19 | 26.6 ft            | 215.4 ft             |
| Point 20 | 37.9 ft            | 223.2 ft             |
| Point 21 | 6.13959 ft         | 185.3 ft             |
| Point 22 | 8.9 ft             | 192 ft               |
| Point 23 | -100 ft            | 160 ft               |
| Point 24 | -100 ft            | 170.1 ft             |
| Point 25 | -91.8 ft           | 174.4 ft             |
| Point 26 | -88.3 ft           | 174.4 ft             |
| Point 27 | -85.7 ft           | 177.8 ft             |
| Point 28 | -83.4 ft           | 177.8 ft             |
| Point 29 | -76 ft             | 178.4 ft             |
| Point 30 | -74 ft             |                      |
| Point 30 | -74 It<br>-55.9 ft | 179.7 ft<br>180.2 ft |
|          |                    |                      |
| Point 32 | -37.3 ft           | 182.3 ft             |
| Point 33 | -30.3 ft           | 182.9 ft             |
| Point 34 | -13.6 ft           | 190.2 ft             |
| Point 35 | 7 ft               | 223 ft               |
| Point 36 | 15 ft              | 223 ft               |
| Point 37 | 15 ft              | 211.7 ft             |
| Point 38 | 7 ft               | 211.7 ft             |
| Point 39 | -6 ft              | 195 ft               |
| Point 40 | -37.3275 ft        | 162.2725 ft          |
| Point 41 | -47.26 ft          | 160 ft               |
| Point 42 | -5.125 ft          | 182.98095 ft         |
| Point 43 | 80.7025 ft         | 160 ft               |
| Point 44 | -100 ft            | 129.8675 ft          |
| Point 45 | 100 ft             | 129.8675 ft          |
| Point 46 | -100 ft            | 147.8625 ft          |
| Point 47 | -27.95 ft          | 152.3875 ft          |
| Point 48 | -100 ft            | 133.97 ft            |
| Point 49 | 16.5 ft            | 197.3 ft             |
| Point 50 | 100 ft             | 209.9025 ft          |
| Point 51 | 95.42762 ft        | 209.80965 ft         |
| Point 52 | 3.915 ft           | 160.77581 ft         |
| Point 53 | 17.7925 ft         | 187.09412 ft         |
| Point 54 | 28.7 ft            | 129.8675 ft          |
| Point 55 | 0 ft               | 198.7 ft             |
| Point 56 | 47.15 ft           | 195.68393 ft         |
| Point 57 | 42.67 ft           | 194.37311 ft         |
| Point 58 | O ft               | 195 ft               |
| Point 59 | -32.3 ft           | 165.4 ft             |
| Point 60 | -16 ft             | 164.1 ft             |
| Point 61 | -100 ft            | 150.0525 ft          |
| Point 62 | 15 ft              | 218.535 ft           |
| Point 63 | 24 ft              | 223 ft               |
| Point 64 | 7 ft               | 214.495 ft           |
| Point 65 | 1.355 ft           | 211.7 ft             |
|          |                    |                      |

| Point 66 | 25.9 ft     | 223 ft       |
|----------|-------------|--------------|
| Point 67 | 22 ft       | 192 ft       |
| Point 68 | 15.0117 ft  | 208.01106 ft |
| Point 69 | 21.5 ft     | 192 ft       |
| Point 70 | 15.5 ft     | 192 ft       |
| Point 71 | 15.5 ft     | 211.7 ft     |
| Point 72 | 15.5 ft     | 194.35 ft    |
| Point 73 | 15.5 ft     | 197.3 ft     |
| Point 74 | 15.5 ft     | 208.29 ft    |
| Point 75 | 18.50702 ft | 197.3 ft     |
| Point 76 | 15.5 ft     | 196.43333 ft |
| Point 77 | 21.5 ft     | 211.7 ft     |
| Point 78 | 20 ft       | 197.3 ft     |
| Point 79 | 20 ft       | 192 ft       |
| Point 80 | 21.5 ft     | 202 ft       |
| Point 81 | 21.5 ft     | 200 ft       |
| Point 82 | 21.5 ft     | 208.29 ft    |
| Point 83 | 31.9 ft     | 223.1 ft     |
| Point 84 | 31.9 ft     | 219.08 ft    |

## Regions

|              | Material   | Points   | Area                       |
|--------------|--|--|----------------------------|
| Region<br>1  | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 1,2,52,3,43  | 1,263.5<br>ft <sup>2</sup> |
| Region<br>2  | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 52,2,50,51,56,57,53,5,60,6,47,3                          | 2,656.9<br>ft <sup>2</sup> |
| Region<br>3  | Gravel Borrow  | 9,18,8,7,10  | 214.55<br>ft <sup>2</sup>  |
| Region<br>4  | Gravel Borrow  | 38,65,11,55,68,74,71,37                                  | 127 ft <sup>2</sup>        |
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel                                  | 8,16,17,18   | 31.556<br>ft <sup>2</sup>  |
| Region<br>6  | ESU 2A Very Loose to Loose<br>Sand/Gravel                        | 18,17,14,19,84,20,9                                      | 115.05<br>ft <sup>2</sup>  |
| Region<br>7  | Common Borrow  | 38,37,62,64  | 38.52<br>ft <sup>2</sup>   |
| Region<br>8  | Common Borrow  | 14,19,84,83,66,63,62,37,71,77                            | 132.58<br>ft <sup>2</sup>  |
| Region<br>9  | ESU 2B Medium Dense Sand/Gravel                                  | 22,42,59,40,60,5,21,13                                   | 332.37<br>ft <sup>2</sup>  |
| Region<br>10 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 44,54,45,1,43,3,47,48                                    | 4,704.7<br>ft <sup>2</sup> |
| Region<br>11 | ESU 2B Medium Dense Sand/Gravel                                  | 41,46,48,47,6,60,40                                      | 992.46<br>ft <sup>2</sup>  |
| Region<br>12 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 56,51,50,4,7,8,16,15,67,69,79,70,13,21,5,53,57           | 1,417.8<br>ft <sup>2</sup> |
| Region<br>13 | ESU 2A Very Loose to Loose<br>Sand/Gravel                        | 34,33,32,31,30,29,28,27,26,25,24,23,40,59,42,22,12,58,39 | 1,656.2<br>ft <sup>2</sup> |
| Region<br>14 | ESU 2A Very Loose to Loose<br>Sand/Gravel                        | 40,23,61,46,41   | 379.99<br>ft <sup>2</sup>  |

| Region<br>15 |   | 63,36,62                | 20.093<br>ft <sup>2</sup>  |
|--------------|---|-------------------------|----------------------------|
| Region<br>16 |   | 36,35,64,62             | 51.88<br>ft <sup>2</sup>   |
| Region<br>17 | Common Borrow                             | 64,65,38                | 7.8889<br>ft <sup>2</sup>  |
| Region<br>18 | ESU 4B Dense to Very Dense<br>Sand/Gravel | 15,16,81,69,67          | 28.5 ft <sup>2</sup>       |
| Region<br>19 | Gravel Borrow                             | 72,76,22,13             | 11.692<br>ft <sup>2</sup>  |
| Region<br>20 | Gravel Borrow                             | 70,72,13                | 2.9375<br>ft <sup>2</sup>  |
| Region<br>21 | Gravel Borrow                             | 70,79,78,75,72          | 19.415<br>ft <sup>2</sup>  |
| Region<br>22 | Gravel Borrow                             | 81,75,78,79,69          | 11.991<br>ft <sup>2</sup>  |
| Region<br>23 | Gravel Borrow                             | 49,75,81,80             | 7.7095<br>ft <sup>2</sup>  |
| Region<br>24 | Gravel Borrow                             | 49,76,72,75             | 4.002<br>ft <sup>2</sup>   |
| Region<br>25 | Gravel Borrow                             | 73,76,49                | 0.43333<br>ft <sup>2</sup> |
| Region<br>26 | Gravel Borrow                             | 76,73,74,68,55,58,12,22 | 163.72<br>ft <sup>2</sup>  |
| Region<br>27 | ESU 2B Medium Dense Sand/Gravel           | 80,81,16,17             | 6 ft²                      |
| Region<br>28 | Gravel Borrow                             | 74,82,77                | 10.23<br>ft <sup>2</sup>   |
| Region<br>29 | Gravel Borrow                             | 77,71,74                | 10.23<br>ft <sup>2</sup>   |
| Region<br>30 | ESU 2A Very Loose to Loose<br>Sand/Gravel | 77,82,80,17,14          | 27.75<br>ft <sup>2</sup>   |
| Region<br>31 | Gravel Borrow                             | 73,49,80,82,74          | 54.19<br>ft <sup>2</sup>   |
| Region<br>32 | Common Borrow                             | 20,83,84                | 12.06<br>ft <sup>2</sup>   |
| Region<br>33 |   | 55,39,58                | 11.1 ft <sup>2</sup>       |

## **Slip Results**

Slip Surfaces Analysed: 10925 of 11466 converged

## **Current Slip Surface**

Slip Surface: 2,852 Factor of Safety: 1.3 Volume: 926.15021 ft<sup>3</sup> Weight: 111,473.27 lbf

Resisting Moment: 3,610,085.7 lbf·ft Activating Moment: 2,792,227.2 lbf·ft Resisting Force: 56,114.321 lbf Activating Force: 43,416.061 lbf Slip Rank: 1 of 11,466 slip surfaces Exit: (-32.349646, 182.72432) ft Entry: (32.424307, 223.10874) ft

Radius: 52.811397 ft

Center: (-19.274577, 233.89155) ft

### **Slip Slices**

|             | X                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material                                |
|-------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|--|
| Slice<br>1  | -31.324823<br>ft | 182.48409<br>ft | -181.68176<br>psf | 43.030043<br>psf         | 26.888155<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>2  | -29.25625<br>ft  | 182.04293<br>ft | -180.15416<br>psf | 179.53902<br>psf         | 112.18843<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>3  | -27.16875<br>ft  | 181.68417<br>ft | -178.93878<br>psf | 368.11373<br>psf         | 230.02299<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>4  | -25.08125<br>ft  | 181.41086<br>ft | -178.88779<br>psf | 556.78167<br>psf         | 347.9158<br>psf        | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>5  | -22.99375<br>ft  | 181.22167<br>ft | -179.14535<br>psf | 738.53006<br>psf         | 461.4848<br>psf        | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>6  | -20.90625<br>ft  | 181.1157<br>ft  | -177.96849<br>psf | 905.78236<br>psf         | 565.99563<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>7  | -18.81875<br>ft  | 181.09244<br>ft | -176.75492<br>psf | 1,051.3784<br>psf        | 656.97412<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>8  | -16.73125<br>ft  | 181.15179<br>ft | -177.75218<br>psf | 1,169.5394<br>psf        | 730.80932<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>9  | -14.64375<br>ft  | 181.29401<br>ft | -179.44633<br>psf | 1,256.5893<br>psf        | 785.20417<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>10 | -12.65 ft        | 181.50604<br>ft | -184.2186<br>psf  | 1,333.5412<br>psf        | 833.28903<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>11 | -10.75 ft        | 181.78159<br>ft | -200.14219<br>psf | 1,402.6138<br>psf        | 876.4504<br>psf        | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>12 | -8.85 ft         | 182.12832<br>ft | -294.87555<br>psf | 1,444.6412<br>psf        | 902.712<br>psf         | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>13 | -6.95 ft         | 182.54767<br>ft | -362.48685<br>psf | 1,556.9847<br>psf        | 972.91202<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice       | -5.521266        | 182.90485       | -396.27515        | 1,615.8917               | 1,009.7212             | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose                |

| 14          | ft              | ft              | psf               | psf               | psf               |       |       | <br>  Sand/Gravel                     |
|-------------|-----------------|-----------------|-------------------|-------------------|-------------------|-------|-------|---------------------------------------|
| Slice<br>15 | -3.781899<br>ft | 183.42095<br>ft | -389.40397<br>psf | 1,367.4624<br>psf | 854.48535<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>16 | -1.260633<br>ft | 184.26552<br>ft | -355.49357<br>psf | 1,166.4006<br>psf | 728.84796<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>17 | 0.6775 ft       | 184.9996<br>ft  | -331.74593<br>psf | 3,077.5638<br>psf | 1,923.0753<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>18 | 2.2958333<br>ft | 185.69717<br>ft | -312.89226<br>psf | 2,863.1613<br>psf | 1,789.1018<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>19 | 4.1775 ft       | 186.58467<br>ft | -292.03965<br>psf | 2,712.0422<br>psf | 1,694.6721<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>20 | 6.0591667<br>ft | 187.56559<br>ft | -272.64084<br>psf | 2,561.0481<br>psf | 1,600.3205<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>21 | 7.95 ft         | 188.65178<br>ft | -254.49171<br>psf | 2,411.7877<br>psf | 1,507.0522<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>22 | 9.8958729<br>ft | 189.88359<br>ft | -237.26176<br>psf | 2,260.2536<br>psf | 1,412.3632<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>23 | 11.887619<br>ft | 191.27185<br>ft | -220.50564<br>psf | 2,115.6829<br>psf | 1,322.0254<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>24 | 13.227615<br>ft | 192.26872<br>ft | -209.5233<br>psf  | 2,117.4277<br>psf | 1,654.3158<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>25 | 14.285869<br>ft | 193.12534<br>ft | -200.2752<br>psf  | 1,909.8169<br>psf | 1,492.1125<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>26 | 15.25 ft        | 193.92922<br>ft | -190.94009<br>psf | 1,827.4012<br>psf | 1,427.7223<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>27 | 16 ft           | 194.59402<br>ft | -185.40797<br>psf | 1,717.191<br>psf  | 1,341.6166<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>28 | 17.50351 ft     | 196.0173<br>ft  | -176.11263<br>psf | 1,572.3485<br>psf | 1,228.4533<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>29 | 18.656323<br>ft | 197.14588<br>ft | -172.10212<br>psf | 1,465.402<br>psf  | 1,144.8975<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>30 | 19.543751<br>ft | 198.10056<br>ft | -176.31912<br>psf | 1,396.5119<br>psf | 1,091.0747<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>31 | 20.890939<br>ft | 199.61482<br>ft | -189.41042<br>psf | 1,293.9254<br>psf | 1,010.9253<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>32 | 22.75 ft        | 201.97436<br>ft | -214.35342<br>psf | 1,114.3532<br>psf | 696.32516<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>33 | 24.25 ft        | 203.98403<br>ft | -237.06792<br>psf | 1,013.7378<br>psf | 633.45369<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>34 | 25.01513 ft     | 205.14142<br>ft | -254.02098<br>psf | 937.56793<br>psf  | 585.85747<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |

| Slice<br>35 | 25.71513 ft     | 206.23572<br>ft | -263.26581<br>psf | 867.92207<br>psf | 542.3379<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
|-------------|-----------------|-----------------|-------------------|------------------|------------------|-------|-------|--|
| Slice<br>36 | 26.25 ft        | 207.13189<br>ft | -251.73198<br>psf | 812.57863<br>psf | 507.75548<br>psf | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>37 | 27.772997<br>ft | 210.0412<br>ft  | -214.97451<br>psf | 639.9921<br>psf  | 399.91145<br>psf | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>38 | 30.11899 ft     | 215.50645<br>ft | -181.88356<br>psf | 342.59516<br>psf | 214.07722<br>psf | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>39 | 31.595994<br>ft | 219.75154<br>ft | 0 psf             | 139.60161<br>psf | 87.23277<br>psf  | 0 psf | 0 psf | Common Borrow                                |
| Slice<br>40 | 32.162153<br>ft | 221.97699<br>ft | 0 psf             | 42.923206<br>psf | 26.821396<br>psf | 0 psf | 0 psf | Common Borrow                                |

# 1A.3 Compound - Pseudo-Static (Spencer)

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### **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 650 Date: 01/17/2022 Time: 01:45:50 PM

Tool Version: 11.1.1.22085

Last Solved Date: 01/17/2022 Last Solved Time: 01:55:57 PM

### **Project Settings**

Unit System: U.S. Customary Units

## **Analysis Settings**

### 1A.3 Compound - Pseudo-Static (Spencer)

Description: Project Num: 00180-366-01 Wall: 05.85L-A Station: 1+90

Kind: SLOPE/W

Parent: 1. Steady State (Compound)

Analysis Type: Spencer

Settings

PWP Conditions from Parent Analysis: 1. Steady State (Compound) [(last)]

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 20

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

Factor of Safety Convergence Settings
Maximum Number of Iterations: 100
Tolerable difference in F of S: 0.001

Solution Settings

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3 Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

#### **Materials**

### **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

### **ESU 2A Very Loose to Loose Sand/Gravel (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 100 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

### **ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf

Effective Cohesion: 200 psf Effective Friction Angle: 32°

Phi-B: 0°

### Reinforcements

### Row 1 (EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 8.8 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

#### Row 2 (EQ)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 8.1 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

### Row 3 (EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 7.4 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

#### Row 4 (EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 6.8 ° Surface Area Factor: 2

Surface Area ractor. 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

#### Row 5 (EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 6.1 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

#### Row 6 (EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 5.5 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

### Row 7 (4 straps)(EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 9.5 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 10,480 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 10,480 lbf/ft

#### Row 8 (4 straps)(EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 8.2 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 10,480 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 10,480 lbf/ft

### **Slip Surface Entry and Exit**

Left Type: Range

Left-Zone Left Coordinate: (-45, 181.43065) ft

Left-Zone Right Coordinate: (0, 200) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15, 218.535) ft Right-Zone Right Coordinate: (55, 223.299) ft

Right-Zone Increment: 20 Radius Increments: 20

### **Slip Surface Limits**

Left Coordinate: (-100, 170.1) ft Right Coordinate: (100, 223.6) ft

### **Seismic Coefficients**

Horz Seismic Coef.: 0.193

### **Reinforcement Lines**

#### **Reinforcement Line 1**

Reinforcement: Row 1 (EQ) Lock to Ground Surface: Yes Outside Point: (0, 210.5) ft Inside Point: (15.5, 210.5) ft

Length: 15.5 ft

Orientation: 0°

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 2**

Reinforcement: Row 8 (4 straps)(EQ)

Lock to Ground Surface: No Outside Point: (0, 193.7) ft Inside Point: (19.6, 193.7) ft

Length: 19.6 ft Orientation: 0 °

Slip Surface Intersection: (16.500257, 193.7) ft

Max. Pullout Force: 10,480 lbf Available Length: 3.0997429 ft Required Length: 3.0997429 ft Pullout Force: 2,883.2886 lbf

Pullout Force per Length: 930.17024 lbf/ft Governing Component: Pullout Resistance

#### **Reinforcement Line 3**

Reinforcement: Row 6 (EQ) Lock to Ground Surface: Yes Outside Point: (0, 198.5) ft Inside Point: (15.5, 198.5) ft

Length: 15.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 4**

Reinforcement: Row 2 (EQ) Lock to Ground Surface: Yes Outside Point: (0, 208.1) ft Inside Point: (15.5, 208.1) ft

Length: 15.5 ft
Orientation: 0°

Max. Pullout Force: 0 lbf
Available Length: 0 ft
Required Length: 0 ft
Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 5**

Reinforcement: Row 5 (EQ) Lock to Ground Surface: Yes Outside Point: (0, 200.9) ft Inside Point: (15.5, 200.9) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 6**

Reinforcement: Row 4 (EQ) Lock to Ground Surface: Yes Outside Point: (0, 203.3) ft Inside Point: (15.5, 203.3) ft

Length: 15.5 ft
Orientation: 0°

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 7**

Reinforcement: Row 3 (EQ) Lock to Ground Surface: Yes Outside Point: (0, 205.7) ft Inside Point: (15.5, 205.7) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 8**

Reinforcement: Row 7 (4 straps)(EQ)

Lock to Ground Surface: Yes

#### 1A.3 Compound - Pseudo-Static (Spencer)

Outside Point: (0, 196.1) ft Inside Point: (19.6, 196.1) ft

Length: 19.6 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

### **Surcharge Loads**

### **Surcharge Load 1**

Surcharge (Unit Weight): 125 pcf

Direction: Vertical

#### **Coordinates**

| X       | Υ         |
|---------|-----------|
| 35.9 ft | 224.15 ft |
| 39.4 ft | 224.2 ft  |
| 40.2 ft | 224.2 ft  |
| 100 ft  | 224.6 ft  |

### Geometry

Name: Default Geometry

### **Settings**

View: 2D

Element Thickness: 1 ft

#### **Points**

|          | X           | Υ           |
|----------|-------------|-------------|
| Point 1  | 100 ft      | 160 ft      |
| Point 2  | 100 ft      | 185.5 ft    |
| Point 3  | 0.9 ft      | 160 ft      |
| Point 4  | 100 ft      | 211.1475 ft |
| Point 5  | 3.8 ft      | 183 ft      |
| Point 6  | -20.1275 ft | 160 ft      |
| Point 7  | 100 ft      | 219.64 ft   |
| Point 8  | 42.5825 ft  | 219.8525 ft |
| Point 9  | 40.2 ft     | 223.2 ft    |
| Point 10 | 100 ft      | 223.6 ft    |
| Point 11 | 0 ft        | 211.7 ft    |
| Point 12 | 0 ft        | 192 ft      |
|          |             |             |

| Point 13   | 13 ft       | 192 ft       |
|------------|-------------|--------------|
| Point 14   | 24.5 ft     | 213.8 ft     |
| Point 15   | 24.5 ft     | 192 ft       |
| Point 16   | 24.5 ft     | 203 ft       |
|            |             |              |
| Point 17   | 24.5 ft     | 205 ft       |
| Point 18   | 41.8 ft     | 220.7 ft     |
| Point 19   | 26.6 ft     | 215.4 ft     |
| Point 20   | 37.9 ft     | 223.2 ft     |
| Point 21   | 6.13959 ft  | 185.3 ft     |
| Point 22   | 8.9 ft      | 192 ft       |
| Point 23   | -100 ft     | 160 ft       |
| Point 24   | -100 ft     | 170.1 ft     |
| Point 25   | -91.8 ft    | 174.4 ft     |
| Point 26   | -88.3 ft    | 176.5 ft     |
| Point 27   | -85.7 ft    | 177.8 ft     |
| Point 28   | -83.4 ft    | 178.4 ft     |
| Point 29   | -76 ft      | 178.9 ft     |
| Point 30   | -74 ft      | 179.7 ft     |
| Point 31   | -55.9 ft    | 180.2 ft     |
| Point 32   | -37.3 ft    | 182.3 ft     |
| Point 33   | -30.3 ft    | 182.9 ft     |
| Point 34   | -13.6 ft    | 190.2 ft     |
| Point 35   | 7 ft        | 223 ft       |
| Point 36   | 15 ft       | 223 ft       |
| Point 37   | 15 ft       | 211.7 ft     |
| Point 38   | 7 ft        | 211.7 ft     |
| Point 39   | -6 ft       | 195 ft       |
| Point 40   | -37.3275 ft | 162.2725 ft  |
| Point 41   | -47.26 ft   | 160 ft       |
| Point 42   | -5.125 ft   | 182.98095 ft |
| Point 43   | 80.7025 ft  | 160 ft       |
| Point 44   | -100 ft     | 129.8675 ft  |
| Point 45   | 100 ft      | 129.8675 ft  |
| Point 46   | -100 ft     | 147.8625 ft  |
| Point 47   | -27.95 ft   | 152.3875 ft  |
| Point 48   | -100 ft     | 133.97 ft    |
| Point 49   | 16.5 ft     | 197.3 ft     |
| Point 50   | 100 ft      | 209.9025 ft  |
| Point 51   | 95.42762 ft | 209.80965 ft |
| Point 52   | 3.915 ft    | 160.77581 ft |
| Point 53   | 17.7925 ft  | 187.09412 ft |
| Point 54   | 28.7 ft     | 129.8675 ft  |
| Point 55   | 0 ft        | 198.7 ft     |
| Point 56   | 47.15 ft    | 195.68393 ft |
| Point 57   | 42.67 ft    | 194.37311 ft |
| Point 58   | 0 ft        | 195 ft       |
| Point 59   | -32.3 ft    | 165.4 ft     |
| Point 60   | -32.3 ft    | 164.1 ft     |
| 1 01111 00 | -1010       | 104.110      |

| Point 61 | -100 ft     | 150.0525 ft  |
|----------|-------------|--------------|
| Point 62 | 15 ft       | 218.535 ft   |
| Point 63 | 24 ft       | 223 ft       |
| Point 64 | 7 ft        | 214.495 ft   |
| Point 65 | 1.355 ft    | 211.7 ft     |
| Point 66 | 25.9 ft     | 223 ft       |
| Point 67 | 22 ft       | 192 ft       |
| Point 68 | 15.0117 ft  | 208.01106 ft |
| Point 69 | 21.5 ft     | 192 ft       |
| Point 70 | 15.5 ft     | 192 ft       |
| Point 71 | 15.5 ft     | 211.7 ft     |
| Point 72 | 15.5 ft     | 194.35 ft    |
| Point 73 | 15.5 ft     | 197.3 ft     |
| Point 74 | 15.5 ft     | 208.29 ft    |
| Point 75 | 18.50702 ft | 197.3 ft     |
| Point 76 | 15.5 ft     | 196.43333 ft |
| Point 77 | 21.5 ft     | 211.7 ft     |
| Point 78 | 20 ft       | 197.3 ft     |
| Point 79 | 20 ft       | 192 ft       |
| Point 80 | 21.5 ft     | 202 ft       |
| Point 81 | 21.5 ft     | 200 ft       |
| Point 82 | 21.5 ft     | 208.29 ft    |
| Point 83 | 31.9 ft     | 223.1 ft     |
| Point 84 | 31.9 ft     | 219.08 ft    |

## Regions

|              | Material   | Points   | Area                       |
|--------------|--|--|----------------------------|
| Region<br>1  | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 1,2,52,3,43                                    | 1,263.5<br>ft <sup>2</sup> |
| Region<br>2  | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 52,2,50,51,56,57,53,5,60,6,47,3                | 2,656.9<br>ft <sup>2</sup> |
| Region<br>3  | Gravel Borrow  | 9,18,8,7,10                                    | 214.55<br>ft <sup>2</sup>  |
| Region<br>4  | Gravel Borrow  | 38,65,11,55,68,74,71,37                        | 127 ft²                    |
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)              | 8,16,17,18                                     | 31.556<br>ft <sup>2</sup>  |
| Region<br>6  | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion)    | 18,17,14,19,84,20,9                            | 115.05<br>ft <sup>2</sup>  |
| Region<br>7  | Common Borrow  | 38,37,62,64                                    | 38.52<br>ft <sup>2</sup>   |
| Region<br>8  | Common Borrow  | 14,19,84,83,66,63,62,37,71,77                  | 132.58<br>ft <sup>2</sup>  |
| Region<br>9  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)              | 22,42,59,40,60,5,21,13                         | 332.37<br>ft <sup>2</sup>  |
| Region<br>10 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 44,54,45,1,43,3,47,48                          | 4,704.7<br>ft <sup>2</sup> |
| Region<br>11 | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)              | 41,46,48,47,6,60,40                            | 992.46<br>ft <sup>2</sup>  |
| Region       | ESU 4B Dense to Very Dense                                       | 56,51,50,4,7,8,16,15,67,69,79,70,13,21,5,53,57 | 1,417.8                    |

| 12           | Sand/Gravel   |  | ft <sup>2</sup>            |
|--------------|---|--|----------------------------|
| Region<br>13 | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion) | 34,33,32,31,30,29,28,27,26,25,24,23,40,59,42,22,12,58,39 | 1,656.2<br>ft <sup>2</sup> |
| Region<br>14 | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion) | 40,23,61,46,41   | 379.99<br>ft <sup>2</sup>  |
| Region<br>15 |   | 63,36,62   | 20.093<br>ft <sup>2</sup>  |
| Region<br>16 |   | 36,35,64,62  | 51.88<br>ft <sup>2</sup>   |
| Region<br>17 | Common Borrow   | 64,65,38   | 7.8889<br>ft <sup>2</sup>  |
| Region<br>18 | ESU 4B Dense to Very Dense<br>Sand/Gravel                     | 15,16,81,69,67   | 28.5 ft <sup>2</sup>       |
| Region<br>19 | Gravel Borrow   | 72,76,22,13  | 11.692<br>ft²              |
| Region<br>20 | Gravel Borrow   | 70,72,13   | 2.9375<br>ft <sup>2</sup>  |
| Region<br>21 | Gravel Borrow   | 70,79,78,75,72   | 19.415<br>ft <sup>2</sup>  |
| Region<br>22 | Gravel Borrow   | 81,75,78,79,69   | 11.991<br>ft²              |
| Region<br>23 | Gravel Borrow   | 49,75,81,80  | 7.7095<br>ft <sup>2</sup>  |
| Region<br>24 | Gravel Borrow   | 49,76,72,75  | 4.002<br>ft <sup>2</sup>   |
| Region<br>25 | Gravel Borrow   | 73,76,49   | 0.43333<br>ft <sup>2</sup> |
| Region<br>26 | Gravel Borrow   | 76,73,74,68,55,58,12,22                                  | 163.72<br>ft²              |
| Region<br>27 | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)           | 80,81,16,17  | 6 ft²                      |
| Region<br>28 | Gravel Borrow   | 74,82,77   | 10.23<br>ft <sup>2</sup>   |
| Region<br>29 | Gravel Borrow   | 77,71,74   | 10.23<br>ft <sup>2</sup>   |
| Region<br>30 | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion) | 77,82,80,17,14   | 27.75<br>ft²               |
| Region<br>31 | Gravel Borrow   | 73,49,80,82,74   | 54.19<br>ft <sup>2</sup>   |
| Region<br>32 | Common Borrow   | 20,83,84   | 12.06<br>ft²               |
| Region<br>33 |   | 55,39,58   | 11.1 ft²                   |

## **Slip Results**

Slip Surfaces Analysed: 7583 of 11466 converged

## **Current Slip Surface**

Slip Surface: 2,972

#### 1A.3 Compound - Pseudo-Static (Spencer)

Factor of Safety: 1.1 Volume: 1,089.4547 ft<sup>3</sup> Weight: 131,373.28 lbf

Resisting Moment: 6,899,088.9 lbf·ft Activating Moment: 6,225,832.8 lbf·ft

Resisting Force: 76,257.173 lbf Activating Force: 68,809.653 lbf Slip Rank: 1 of 11,466 slip surfaces Exit: (-32.349646, 182.72432) ft Entry: (44.738055, 223.23035) ft

Radius: 78.641419 ft

Center: (-24.267402, 260.94931) ft

#### **Slip Slices**

| -31.324823<br>ft<br>-28.908333<br>ft | 182.63197<br>ft<br>182.45733<br>ft                 | -181.69787<br>psf<br>-179.8031   | 281.36586<br>psf   | 175.8169<br>psf                                       | 100 psf   | 0 psf      | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent                             |
|--------------------------------------|--|--|--------------------|---|---|------------|---|
|                                      |  |  |                    |   |   |            | Cohesion)   |
|                                      |  | psf  | 440.21654<br>psf   | 275.07783<br>psf                                      | 100 psf   | 0 psf      | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion)                |
| -26.125 ft                           | 182.34216<br>ft                                    | -178.31292<br>psf  | 650.61498<br>psf   | 406.54936<br>psf                                      | 100 psf   | 0 psf      | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion)                |
| -23.341667<br>ft                     | 182.32566<br>ft                                    | -178.32011<br>psf  | 800.99872<br>psf   | 500.51955<br>psf                                      | 100 psf   | 0 psf      | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion)                |
| -20.558333<br>ft                     | 182.40777<br>ft                                    | -177.3301<br>psf   | 906.92936<br>psf   | 566.71236<br>psf                                      | 100 psf   | 0 psf      | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion)                |
| -17.775 ft                           | 182.58879<br>ft                                    | -176.47058<br>psf  | 979.13463<br>psf   | 611.83122<br>psf                                      | 100 psf   | 0 psf      | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion)                |
| -14.991667<br>ft                     | 182.86942<br>ft                                    | -176.62434<br>psf  | 1,025.1265<br>psf  | 640.57015<br>psf                                      | 100 psf   | 0 psf      | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion)<br>ESU 2A Very |
|                                      | -23.341667<br>ft<br>-20.558333<br>ft<br>-17.775 ft | -23.341667 ft 182.32566 ft ft -20.558333 182.40777 ft 182.58879 ft 182.86942 | ft psf  -23.341667 | region of the psf | region of the psf | -23.341667 | psf   |

| Slice<br>8  | -12.333333<br>ft  | 183.22925<br>ft | -175.23349<br>psf | 1,081.069<br>psf  | 675.5269<br>psf   | 100 psf | 0 psf | Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion)                |
|-------------|-------------------|-----------------|-------------------|-------------------|-------------------|---------|-------|--|
| Slice<br>9  | -9.8 ft           | 183.66085<br>ft | -180.39959<br>psf | 1,146.2015<br>psf | 716.22619<br>psf  | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>10 | -7.2666667<br>ft  | 184.17845<br>ft | -238.51697<br>psf | 1,192.3505<br>psf | 745.06327<br>psf  | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>11 | -4.6017274<br>ft  | 184.82016<br>ft | -303.95054<br>psf | 1,207.3372<br>psf | 754.42801<br>psf  | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>12 | -1.8051822<br>ft  | 185.59818<br>ft | -358.26732<br>psf | 1,051.2828<br>psf | 656.9144<br>psf   | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>13 | -0.20345477<br>ft | 186.0804<br>ft  | -374.77997<br>psf | 1,426.9232<br>psf | 891.64058<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                    |
| Slice<br>14 | 0.6775 ft         | 186.37241<br>ft | -362.92551<br>psf | 2,921.4418<br>psf | 1,825.5194<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                    |
| Slice<br>15 | 2.76625 ft        | 187.11574<br>ft | -334.76816<br>psf | 2,715.9923<br>psf | 1,697.1403<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                    |
| Slice<br>16 | 5.58875 ft        | 188.21173<br>ft | -297.17026<br>psf | 2,582.6305<br>psf | 1,613.8067<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                    |
| Slice<br>17 | 7.95 ft           | 189.21768<br>ft | -266.4414<br>psf  | 2,499.003<br>psf  | 1,561.5504<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                    |
| Slice<br>18 | 10.611532<br>ft   | 190.49163<br>ft | -233.63671<br>psf | 2,332.4574<br>psf | 1,457.4811<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion)        |
|             |                   |                 |                   |                   |                   |         |       | ESU 4B Dense to  |

| Slice<br>19 | 12.661532<br>ft | 191.51892<br>ft | -204.75428<br>psf | 2,566.6254<br>psf | 2,393.4169<br>psf | 0 psf | 0 psf | Very Dense<br>Sand/Gravel                    |
|-------------|-----------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>20 | 13.277044<br>ft | 191.84947<br>ft | -192.3219<br>psf  | 2,575.3929<br>psf | 2,401.5927<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>21 | 14.277044<br>ft | 192.40655<br>ft | -172.11952<br>psf | 2,242.0754<br>psf | 1,751.7013<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>22 | 15.25 ft        | 192.9584<br>ft  | -149.2578<br>psf  | 2,368.913<br>psf  | 1,850.7977<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>23 | 16 ft           | 193.40177<br>ft | -137.38527<br>psf | 2,177.0271<br>psf | 1,700.88<br>psf   | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>24 | 17.50351 ft     | 194.32904<br>ft | -116.39919<br>psf | 2,011.4624<br>psf | 1,571.5267<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>25 | 19.25351 ft     | 195.45428<br>ft | -101.25132<br>psf | 1,837.7176<br>psf | 1,435.7823<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>26 | 20.75 ft        | 196.47397<br>ft | -92.486908<br>psf | 1,746.4961<br>psf | 1,364.5123<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>27 | 22.75 ft        | 197.93023<br>ft | -82.637841<br>psf | 1,529.3482<br>psf | 1,426.1402<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>28 | 24.25 ft        | 199.05882<br>ft | -79.331138<br>psf | 1,439.4105<br>psf | 1,342.272<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>29 | 25.2 ft         | 199.82127<br>ft | -78.129103<br>psf | 1,356.8302<br>psf | 1,265.2646<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>30 | 26.25 ft        | 200.68111<br>ft | -77.908915<br>psf | 1,268.2622<br>psf | 1,182.6736<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>31 | 27.925 ft       | 202.15061<br>ft | -77.837572<br>psf | 1,129.3615<br>psf | 1,053.1467<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>32 | 30.575 ft       | 204.61669<br>ft | -84.964815<br>psf | 920.89922<br>psf  | 858.75241<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>33 | 32.9 ft         | 206.96562<br>ft | -99.671373<br>psf | 746.94451<br>psf  | 696.53702<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>34 | 34.9 ft         | 209.16721<br>ft | -123.43094<br>psf | 602.46768<br>psf  | 561.8102<br>psf   | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>35 | 36.9 ft         | 211.54801<br>ft | -164.66922<br>psf | 514.6925<br>psf   | 479.95852<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>36 | 38.65 ft        | 213.78672<br>ft | -228.53372<br>psf | 396.84403<br>psf  | 370.06304<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>37 | 39.8 ft         | 215.34926<br>ft | -286.83402<br>psf | 323.3106<br>psf   | 301.49201<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>38 | 41 ft           | 217.10207<br>ft | -369.13159<br>psf | 254.33046<br>psf  | 237.16699<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |

#### 1A.3 Compound - Pseudo-Static (Spencer)

| Slice<br>39 | 42.19125 ft     | 218.91142<br>ft | -478.68475<br>psf | 191.45321<br>psf | 178.53301<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
|-------------|-----------------|-----------------|-------------------|------------------|------------------|-------|-------|--|
| Slice<br>40 | 42.681662<br>ft | 219.69086<br>ft | -531.43838<br>psf | 164.00281<br>psf | 152.9351<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>41 | 43.759439<br>ft | 221.54106<br>ft | 0 psf             | 97.227797<br>psf | 75.96268         | 0 psf | 0 psf | Gravel Borrow                                |

# 1A.4 Compound - Pseudo-Static (M-P)

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### **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 650 Date: 01/17/2022 Time: 01:45:50 PM

Tool Version: 11.1.1.22085

Last Solved Date: 01/17/2022 Last Solved Time: 02:01:23 PM

### **Project Settings**

Unit System: U.S. Customary Units

## **Analysis Settings**

#### 1A.4 Compound - Pseudo-Static (M-P)

Description: Project Num: 00180-366-01 Wall: 05.85L-A Station: 1+90

Kind: SLOPE/W

Parent: 1. Steady State (Compound) Analysis Type: Morgenstern-Price

Settings

Side Function

Interslice force function option: Half-Sine

PWP Conditions from Parent Analysis: 1. Steady State (Compound) [(last)]

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 20

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

Factor of Safety Convergence Settings

Maximum Number of Iterations: 100 Tolerable difference in F of S: 0.001

Solution Settings

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

#### **Materials**

#### **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

### **ESU 2A Very Loose to Loose Sand/Gravel (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

### **ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf

Effective Cohesion: 200 psf Effective Friction Angle: 32 °

Phi-B: 0°

### Reinforcements

### Row 1 (EQ)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 8.8 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

#### Row 2 (EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 8.1 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

### Row 3 (EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 7.4 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

#### Row 4 (EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 6.8 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

#### Row 5 (EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 6.1 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

#### Row 6 (EQ)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 5.5 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

### Row 7 (4 straps)(EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 9.5 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 10,480 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 10,480 lbf/ft

#### Row 8 (4 straps)(EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 8.2 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 10,480 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 10,480 lbf/ft

### **Slip Surface Entry and Exit**

Left Type: Range

Left-Zone Left Coordinate: (-45, 181.43065) ft

Left-Zone Right Coordinate: (0, 200) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15, 218.535) ft Right-Zone Right Coordinate: (55, 223.299) ft

Right-Zone Increment: 20 Radius Increments: 20

### **Slip Surface Limits**

Left Coordinate: (-100, 170.1) ft Right Coordinate: (100, 223.6) ft

### **Seismic Coefficients**

Horz Seismic Coef.: 0.193

### **Reinforcement Lines**

#### **Reinforcement Line 1**

Reinforcement: Row 1 (EQ) Lock to Ground Surface: Yes Outside Point: (0, 210.5) ft Inside Point: (15.5, 210.5) ft

Length: 15.5 ft

Orientation: 0°

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 2**

Reinforcement: Row 8 (4 straps)(EQ)

Lock to Ground Surface: No Outside Point: (0, 193.7) ft Inside Point: (19.6, 193.7) ft

Length: 19.6 ft Orientation: 0 °

Slip Surface Intersection: (16.500257, 193.7) ft

Max. Pullout Force: 10,480 lbf Available Length: 3.0997429 ft Required Length: 3.0997429 ft Pullout Force: 2,883.2886 lbf

Pullout Force per Length: 930.17024 lbf/ft Governing Component: Pullout Resistance

#### **Reinforcement Line 3**

Reinforcement: Row 6 (EQ) Lock to Ground Surface: Yes Outside Point: (0, 198.5) ft Inside Point: (15.5, 198.5) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 4**

Reinforcement: Row 2 (EQ) Lock to Ground Surface: Yes Outside Point: (0, 208.1) ft Inside Point: (15.5, 208.1) ft

Length: 15.5 ft
Orientation: 0°

Max. Pullout Force: 0 lbf
Available Length: 0 ft
Required Length: 0 ft
Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 5**

Reinforcement: Row 5 (EQ) Lock to Ground Surface: Yes Outside Point: (0, 200.9) ft Inside Point: (15.5, 200.9) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 6**

Reinforcement: Row 4 (EQ) Lock to Ground Surface: Yes Outside Point: (0, 203.3) ft Inside Point: (15.5, 203.3) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### Reinforcement Line 7

Reinforcement: Row 3 (EQ) Lock to Ground Surface: Yes Outside Point: (0, 205.7) ft Inside Point: (15.5, 205.7) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 8**

Reinforcement: Row 7 (4 straps)(EQ)

Lock to Ground Surface: Yes

#### 1A.4 Compound - Pseudo-Static (M-P)

Outside Point: (0, 196.1) ft Inside Point: (19.6, 196.1) ft

Length: 19.6 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

### **Surcharge Loads**

### **Surcharge Load 1**

Surcharge (Unit Weight): 125 pcf

Direction: Vertical

#### **Coordinates**

| X       | Υ         |
|---------|-----------|
| 35.9 ft | 224.15 ft |
| 39.4 ft | 224.2 ft  |
| 40.2 ft | 224.2 ft  |
| 100 ft  | 224.6 ft  |

### Geometry

Name: Default Geometry

### **Settings**

View: 2D

Element Thickness: 1 ft

#### **Points**

|          | X           | Υ           |
|----------|-------------|-------------|
| Point 1  | 100 ft      | 160 ft      |
| Point 2  | 100 ft      | 185.5 ft    |
| Point 3  | 0.9 ft      | 160 ft      |
| Point 4  | 100 ft      | 211.1475 ft |
| Point 5  | 3.8 ft      | 183 ft      |
| Point 6  | -20.1275 ft | 160 ft      |
| Point 7  | 100 ft      | 219.64 ft   |
| Point 8  | 42.5825 ft  | 219.8525 ft |
| Point 9  | 40.2 ft     | 223.2 ft    |
| Point 10 | 100 ft      | 223.6 ft    |
| Point 11 | 0 ft        | 211.7 ft    |
| Point 12 | 0 ft        | 192 ft      |
|          |             |             |

| ı                    |             | 1 -                      |
|----------------------|-------------|--------------------------|
| Point 13             | 13 ft       | 192 ft                   |
| Point 14             | 24.5 ft     | 213.8 ft                 |
| Point 15             | 24.5 ft     | 192 ft                   |
| Point 16             | 24.5 ft     | 203 ft                   |
| Point 17             | 24.5 ft     | 205 ft                   |
| Point 18             | 41.8 ft     | 220.7 ft                 |
| Point 19             | 26.6 ft     | 215.4 ft                 |
| Point 20             | 37.9 ft     | 223.2 ft                 |
| Point 21             | 6.13959 ft  | 185.3 ft                 |
| Point 22             | 8.9 ft      | 192 ft                   |
| Point 23             | -100 ft     | 160 ft                   |
| Point 24             | -100 ft     | 170.1 ft                 |
| Point 25             | -91.8 ft    | 174.4 ft                 |
| Point 26             | -88.3 ft    | 176.5 ft                 |
| Point 27             | -85.7 ft    | 177.8 ft                 |
| Point 28             | -83.4 ft    | 178.4 ft                 |
| Point 29             | -76 ft      | 178.9 ft                 |
| Point 30             | -74 ft      | 179.7 ft                 |
| Point 31             | -55.9 ft    | 180.2 ft                 |
| Point 32             | -37.3 ft    | 182.3 ft                 |
| Point 33             | -30.3 ft    | 182.9 ft                 |
| Point 34             | -13.6 ft    | 190.2 ft                 |
| Point 35             | 7 ft        | 223 ft                   |
| Point 36             | 15 ft       | 223 ft                   |
| Point 37             | 15 ft       | 211.7 ft                 |
| Point 38             | 7 ft        | 211.7 ft                 |
| Point 39             | -6 ft       | 195 ft                   |
| Point 40             | -37.3275 ft | 162.2725 ft              |
| Point 41             | -47.26 ft   | 160 ft                   |
| Point 42             | -5.125 ft   | 182.98095 ft             |
| Point 43             | 80.7025 ft  | 160 ft                   |
| Point 44             | -100 ft     | 129.8675 ft              |
| Point 45             | 100 ft      | 129.8675 ft              |
| Point 46             | -100 ft     | 147.8625 ft              |
| Point 47             | -27.95 ft   | 152.3875 ft              |
| Point 48             | -100 ft     | 133.97 ft                |
| Point 49             | 16.5 ft     | 197.3 ft                 |
| Point 50             | 10.5 ft     | 209.9025 ft              |
| Point 50             | 95.42762 ft | 209.80965 ft             |
| Point 51 Point 52    | 3.915 ft    | 160.77581 ft             |
| Point 52<br>Point 53 | 17.7925 ft  | 187.09412 ft             |
| Point 54             | 28.7 ft     | 129.8675 ft              |
| Point 54 Point 55    | 0 ft        | 198.7 ft                 |
| Point 55<br>Point 56 | 47.15 ft    | 198.7 It<br>195.68393 ft |
|                      |             |                          |
| Point 57             | 42.67 ft    | 194.37311 ft             |
| Point 58             | 0 ft        | 195 ft                   |
| Point 59             | -32.3 ft    | 165.4 ft                 |
| Point 60             | -16 ft      | 164.1 ft                 |

|          | I           | ı            |
|----------|-------------|--------------|
| Point 61 | -100 ft     | 150.0525 ft  |
| Point 62 | 15 ft       | 218.535 ft   |
| Point 63 | 24 ft       | 223 ft       |
| Point 64 | 7 ft        | 214.495 ft   |
| Point 65 | 1.355 ft    | 211.7 ft     |
| Point 66 | 25.9 ft     | 223 ft       |
| Point 67 | 22 ft       | 192 ft       |
| Point 68 | 15.0117 ft  | 208.01106 ft |
| Point 69 | 21.5 ft     | 192 ft       |
| Point 70 | 15.5 ft     | 192 ft       |
| Point 71 | 15.5 ft     | 211.7 ft     |
| Point 72 | 15.5 ft     | 194.35 ft    |
| Point 73 | 15.5 ft     | 197.3 ft     |
| Point 74 | 15.5 ft     | 208.29 ft    |
| Point 75 | 18.50702 ft | 197.3 ft     |
| Point 76 | 15.5 ft     | 196.43333 ft |
| Point 77 | 21.5 ft     | 211.7 ft     |
| Point 78 | 20 ft       | 197.3 ft     |
| Point 79 | 20 ft       | 192 ft       |
| Point 80 | 21.5 ft     | 202 ft       |
| Point 81 | 21.5 ft     | 200 ft       |
| Point 82 | 21.5 ft     | 208.29 ft    |
| Point 83 | 31.9 ft     | 223.1 ft     |
| Point 84 | 31.9 ft     | 219.08 ft    |
|          |             |              |

## Regions

|              | Material   | Points   | Area                       |
|--------------|--|--|----------------------------|
| Region<br>1  | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 1,2,52,3,43                                    | 1,263.5<br>ft <sup>2</sup> |
| Region<br>2  | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 52,2,50,51,56,57,53,5,60,6,47,3                | 2,656.9<br>ft <sup>2</sup> |
| Region<br>3  | Gravel Borrow  | 9,18,8,7,10                                    | 214.55<br>ft <sup>2</sup>  |
| Region<br>4  | Gravel Borrow  | 38,65,11,55,68,74,71,37                        | 127 ft²                    |
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)              | 8,16,17,18                                     | 31.556<br>ft <sup>2</sup>  |
| Region<br>6  | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion)    | 18,17,14,19,84,20,9                            | 115.05<br>ft <sup>2</sup>  |
| Region<br>7  | Common Borrow  | 38,37,62,64                                    | 38.52<br>ft <sup>2</sup>   |
| Region<br>8  | Common Borrow  | 14,19,84,83,66,63,62,37,71,77                  | 132.58<br>ft²              |
| Region<br>9  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)              | 22,42,59,40,60,5,21,13                         | 332.37<br>ft <sup>2</sup>  |
| Region<br>10 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 44,54,45,1,43,3,47,48                          | 4,704.7<br>ft <sup>2</sup> |
| Region<br>11 | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)              | 41,46,48,47,6,60,40                            | 992.46<br>ft <sup>2</sup>  |
| Region       | ESU 4B Dense to Very Dense                                       | 56,51,50,4,7,8,16,15,67,69,79,70,13,21,5,53,57 | 1,417.8                    |

| 12           | Sand/Gravel   |  | ft <sup>2</sup>            |
|--------------|---|--|----------------------------|
| Region<br>13 | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion) | 34,33,32,31,30,29,28,27,26,25,24,23,40,59,42,22,12,58,39 | 1,656.2<br>ft <sup>2</sup> |
| Region<br>14 | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion) | 40,23,61,46,41   | 379.99<br>ft <sup>2</sup>  |
| Region<br>15 |   | 63,36,62   | 20.093<br>ft <sup>2</sup>  |
| Region<br>16 |   | 36,35,64,62  | 51.88<br>ft²               |
| Region<br>17 | Common Borrow   | 64,65,38   | 7.8889<br>ft <sup>2</sup>  |
| Region<br>18 | ESU 4B Dense to Very Dense<br>Sand/Gravel                     | 15,16,81,69,67   | 28.5 ft <sup>2</sup>       |
| Region<br>19 | Gravel Borrow   | 72,76,22,13  | 11.692<br>ft²              |
| Region<br>20 | Gravel Borrow   | 70,72,13   | 2.9375<br>ft <sup>2</sup>  |
| Region<br>21 | Gravel Borrow   | 70,79,78,75,72   | 19.415<br>ft²              |
| Region<br>22 | Gravel Borrow   | 81,75,78,79,69   | 11.991<br>ft²              |
| Region<br>23 | Gravel Borrow   | 49,75,81,80  | 7.7095<br>ft <sup>2</sup>  |
| Region<br>24 | Gravel Borrow   | 49,76,72,75  | 4.002<br>ft <sup>2</sup>   |
| Region<br>25 | Gravel Borrow   | 73,76,49   | 0.43333<br>ft <sup>2</sup> |
| Region<br>26 | Gravel Borrow   | 76,73,74,68,55,58,12,22                                  | 163.72<br>ft²              |
| Region<br>27 | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)           | 80,81,16,17  | 6 ft²                      |
| Region<br>28 | Gravel Borrow   | 74,82,77   | 10.23<br>ft <sup>2</sup>   |
| Region<br>29 | Gravel Borrow   | 77,71,74   | 10.23<br>ft <sup>2</sup>   |
| Region<br>30 | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion) | 77,82,80,17,14   | 27.75<br>ft <sup>2</sup>   |
| Region<br>31 | Gravel Borrow   | 73,49,80,82,74   | 54.19<br>ft <sup>2</sup>   |
| Region<br>32 | Common Borrow   | 20,83,84   | 12.06<br>ft <sup>2</sup>   |
| Region<br>33 |   | 55,39,58   | 11.1 ft <sup>2</sup>       |

## **Slip Results**

Slip Surfaces Analysed: 10196 of 11466 converged

## **Current Slip Surface**

Slip Surface: 2,972

#### 1A.4 Compound - Pseudo-Static (M-P)

Factor of Safety: 1.1 Volume: 1,089.4547 ft<sup>3</sup> Weight: 131,373.28 lbf

Resisting Moment: 6,860,180.7 lbf·ft Activating Moment: 6,225,832.8 lbf·ft

Resisting Force: 75,821.94 lbf Activating Force: 68,834.441 lbf Slip Rank: 1 of 11,466 slip surfaces Exit: (-32.349646, 182.72432) ft Entry: (44.738055, 223.23035) ft

Radius: 78.641419 ft

Center: (-24.267402, 260.94931) ft

#### **Slip Slices**

|                  |  | PWP                                      | Normal<br>Stress   | Frictional<br>Strength  | Cohesive<br>Strength   | Suction<br>Strength   | Base Material  |
|------------------|--|--|--|---|--|---|--|
| -31.324823<br>ft | 182.63197<br>ft  | -181.69787<br>psf                        | 40.746197<br>psf   | 25.46105<br>psf   | 100 psf  | 0 psf   | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion)   |
| -28.908333<br>ft | 182.45733<br>ft  | -179.8031<br>psf                         | 176.9578<br>psf  | 110.57551<br>psf  | 100 psf  | 0 psf   | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion)   |
| -26.125 ft       | 182.34216<br>ft  | -178.31292<br>psf                        | 396.53087<br>psf   | 247.77999<br>psf  | 100 psf  | 0 psf   | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion)   |
| -23.341667<br>ft | 182.32566<br>ft  | -178.32011<br>psf                        | 624.03133<br>psf   | 389.93805<br>psf  | 100 psf  | 0 psf   | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion)   |
| -20.558333<br>ft | 182.40777<br>ft  | -177.3301<br>psf                         | 846.09089<br>psf   | 528.69627<br>psf  | 100 psf  | 0 psf   | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion)   |
| -17.775 ft       | 182.58879<br>ft  | -176.47058<br>psf                        | 1,045.3991<br>psf  | 653.23783<br>psf  | 100 psf  | 0 psf   | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion)   |
| -14.991667<br>ft | 182.86942<br>ft  | -176.62434<br>psf                        | 1,204.3962<br>psf  | 752.59028<br>psf  | 100 psf  | 0 psf   | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion)<br>ESU 2A Very  |
|                  | -28.908333 ft  -26.125 ft  -23.341667 ft  -17.775 ft  -14.991667 | ft f | ft       psf         -28.908333 ft       182.45733 ft       -179.8031 psf         -26.125 ft       182.34216 ft       -178.31292 psf         -23.341667 ft       182.32566 ft       -178.32011 psf         -20.558333 ft       182.40777 ft       -177.3301 psf         -17.775 ft       182.58879 ft       -176.47058 psf         -14.991667       182.86942       -176.62434 | ft       psf       psf         -28.908333 ft       182.45733 ft       -179.8031 psf       176.9578 psf         -26.125 ft       182.34216 ft       -178.31292 psf       396.53087 psf         -23.341667 ft       182.32566 rt       -178.32011 psf       624.03133 psf         -20.558333 ft       182.40777 psf       -177.3301 psf       846.09089 psf         -17.775 ft       182.58879 psf       -176.47058 psf       1,045.3991 psf         -14.991667       182.86942 rt       -176.62434 rt       1,204.3962 | ft         psf         psf         psf           -28.908333 ft         182.45733 ft         -179.8031 psf         176.9578 psf         110.57551 psf           -26.125 ft         182.34216 ft         -178.31292 psf         396.53087 psf         247.77999 psf           -23.341667 ft         182.32566 psf         -178.32011 psf         624.03133 psf         389.93805 psf           -20.558333 ft         182.40777 psf         -177.3301 psf         846.09089 psf         528.69627 psf           -17.775 ft         182.58879 psf         -176.47058 psf         1,045.3991 psf         653.23783 psf           -14.991667         182.86942 psf         -176.62434 psf         1,204.3962 psf         752.59028 | ft         psf         psf         psf         psf           -28.908333 ft         182.45733 ft         -179.8031 psf         176.9578 psf         110.57551 psf         100 psf           -26.125 ft         182.34216 ft         -178.31292 psf         396.53087 psf         247.77999 psf         100 psf           -23.341667 ft         182.32566 ft         -178.32011 psf         624.03133 psf         389.93805 psf         100 psf           -20.558333 ft         182.40777 psf         -177.3301 psf         846.09089 psf         528.69627 psf         100 psf           -17.775 ft         182.58879 psf         -176.47058 psf         1,045.3991 psf         653.23783 psf         100 psf           -14.991667         182.86942 -176.62434 psf         1,204.3962 psf         752.59028 psf         100 psf | ft ft psf psf psf psf psf 100 psf 0 psf 100 psf 0 psf ft 100 psf 0 psf ft 100 psf psf 100 psf psf ft 100 psf psf psf psf psf 100 psf psf 100 psf psf psf psf 100 psf psf 100 psf psf 100 psf 0 psf psf psf psf 100 psf psf psf 100 psf 100 psf psf 100 psf psf 100 psf 100 psf 100 psf psf 100 psf psf 100 psf 100 psf psf 100 psf 100 psf psf 100 |

| Slice<br>8  | -12.333333<br>ft  | 183.22925<br>ft | -175.23349<br>psf | 1,337.7146<br>psf | 835.89684<br>psf  | 100 psf | 0 psf | Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion)                |
|-------------|-------------------|-----------------|-------------------|-------------------|-------------------|---------|-------|--|
| Slice<br>9  | -9.8 ft           | 183.66085<br>ft | -180.39959<br>psf | 1,442.9374<br>psf | 901.64737<br>psf  | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>10 | -7.2666667<br>ft  | 184.17845<br>ft | -238.51697<br>psf | 1,494.8196<br>psf | 934.06697<br>psf  | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>11 | -4.6017274<br>ft  | 184.82016<br>ft | -303.95054<br>psf | 1,496.0889<br>psf | 934.86011<br>psf  | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>12 | -1.8051822<br>ft  | 185.59818<br>ft | -358.26732<br>psf | 1,287.1517<br>psf | 804.30165<br>psf  | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>13 | -0.20345477<br>ft | 186.0804<br>ft  | -374.77997<br>psf | 1,754.6737<br>psf | 1,096.4418<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                    |
| Slice<br>14 | 0.6775 ft         | 186.37241<br>ft | -362.92551<br>psf | 3,144.6847<br>psf | 1,965.0171<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                    |
| Slice<br>15 | 2.76625 ft        | 187.11574<br>ft | -334.76816<br>psf | 2,844.0203<br>psf | 1,777.1411<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                    |
| Slice<br>16 | 5.58875 ft        | 188.21173<br>ft | -297.17026<br>psf | 2,607.5404<br>psf | 1,629.372<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                    |
| Slice<br>17 | 7.95 ft           | 189.21768<br>ft | -266.4414<br>psf  | 2,453.8152<br>psf | 1,533.3139<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                    |
| Slice<br>18 | 10.611532<br>ft   | 190.49163<br>ft | -233.63671<br>psf | 2,208.5134<br>psf | 1,380.0323<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion)        |
|             |                   |                 |                   |                   |                   |         |       | ESU 4B Dense to  |

| Slice<br>19 | 12.661532<br>ft | 191.51892<br>ft | -204.75428<br>psf | 2,509.9725<br>psf | 2,340.5872<br>psf | 0 psf | 0 psf | Very Dense<br>Sand/Gravel                    |
|-------------|-----------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>20 | 13.277044<br>ft | 191.84947<br>ft | -192.3219<br>psf  | 2,507.2379<br>psf | 2,338.0372<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>21 | 14.277044<br>ft | 192.40655<br>ft | -172.11952<br>psf | 2,067.1419<br>psf | 1,615.0282<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>22 | 15.25 ft        | 192.9584<br>ft  | -149.2578<br>psf  | 2,212.9823<br>psf | 1,728.9713<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>23 | 16 ft           | 193.40177<br>ft | -137.38527<br>psf | 1,985.1173<br>psf | 1,550.9436<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>24 | 17.50351 ft     | 194.32904<br>ft | -116.39919<br>psf | 1,800.587<br>psf  | 1,406.7727<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>25 | 19.25351 ft     | 195.45428<br>ft | -101.25132<br>psf | 1,625.3662<br>psf | 1,269.8753<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>26 | 20.75 ft        | 196.47397<br>ft | -92.486908<br>psf | 1,550.3738<br>psf | 1,211.2848<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>27 | 22.75 ft        | 197.93023<br>ft | -82.637841<br>psf | 1,355.2136<br>psf | 1,263.7571<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>28 | 24.25 ft        | 199.05882<br>ft | -79.331138<br>psf | 1,284.5881<br>psf | 1,197.8978<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>29 | 25.2 ft         | 199.82127<br>ft | -78.129103<br>psf | 1,217.1699<br>psf | 1,135.0293<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>30 | 26.25 ft        | 200.68111<br>ft | -77.908915<br>psf | 1,146.5418<br>psf | 1,069.1675<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>31 | 27.925 ft       | 202.15061<br>ft | -77.837572<br>psf | 1,039.4081<br>psf | 969.26373<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>32 | 30.575 ft       | 204.61669<br>ft | -84.964815<br>psf | 882.32469<br>psf  | 822.78108<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>33 | 32.9 ft         | 206.96562<br>ft | -99.671373<br>psf | 750.83822<br>psf  | 700.16797<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>34 | 34.9 ft         | 209.16721<br>ft | -123.43094<br>psf | 637.21432<br>psf  | 594.21196<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>35 | 36.9 ft         | 211.54801<br>ft | -164.66922<br>psf | 576.92388<br>psf  | 537.99022<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>36 | 38.65 ft        | 213.78672<br>ft | -228.53372<br>psf | 471.23986<br>psf  | 439.43828<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>37 | 39.8 ft         | 215.34926<br>ft | -286.83402<br>psf | 400.0565<br>psf   | 373.05873<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>38 | 41 ft           | 217.10207<br>ft | -369.13159<br>psf | 329.58965<br>psf  | 307.34732<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |

| Slice<br>39 | 42.19125 ft     | 218.91142<br>ft | -478.68475<br>psf | 260.66228<br>psf | 243.07151<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
|-------------|-----------------|-----------------|-------------------|------------------|------------------|-------|-------|--|
| Slice<br>40 | 42.681662<br>ft | 219.69086<br>ft | -531.43838<br>psf | 227.64835<br>psf | 212.28552<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>41 | 43.759439<br>ft | 221.54106<br>ft | 0 psf             | 146.90679        | 114.77617        | 0 psf | 0 psf | Gravel Borrow                                |

# 1A.5 Compound - Post-Seismic (Spencer)

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### **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 650 Date: 01/17/2022 Time: 01:45:50 PM

Tool Version: 11.1.1.22085

Last Solved Date: 01/17/2022 Last Solved Time: 01:58:32 PM

### **Project Settings**

Unit System: U.S. Customary Units

## **Analysis Settings**

### 1A.5 Compound - Post-Seismic (Spencer)

Description: Project Num: 00180-366-01 Wall: 05.85L-A Station: 1+90

Kind: SLOPE/W

Parent: 1. Steady State (Compound)

Analysis Type: Spencer

Settings

PWP Conditions from Parent Analysis: 1. Steady State (Compound) [(last)]

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 20

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

Factor of Safety Convergence Settings
Maximum Number of Iterations: 100
Tolerable difference in F of S: 0.001
Solution Settings

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3 Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

#### **Materials**

### **ESU 2A Very Loose to Loose Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

### **ESU 2B Medium Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

## **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

## ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

## **ESU 2B Medium Dense Sand/Gravel (Residual Strength)**

#### 1A.5 Compound - Post-Seismic (Spencer)

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf

Effective Cohesion: 497 psf Effective Friction Angle: 0 °

Phi-B: 0°

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

## Reinforcements

#### Row 1

Type: Geosynthetic Interface Adhesion: 0 psf

Interface Shear Angle: 6.6 °

Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 2

Type: Geosynthetic

Interface Adhesion: 0 psf Interface Shear Angle: 6.1 °

Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 3

Type: Geosynthetic

Interface Adhesion: 0 psf Interface Shear Angle: 5.6 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 4

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 5.1 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 5

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 4.6 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 6

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 4.1 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

### Row 7 (4 straps)

Type: Geosynthetic

Interface Adhesion: 0 psf Interface Shear Angle: 7.2 °

Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 7,860 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 7,860 lbf/ft

### Row 8 (4 straps)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 6.2 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 7,860 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 7,860 lbf/ft

## Slip Surface Entry and Exit

Left Type: Range

Left-Zone Left Coordinate: (-45, 181.43065) ft

Left-Zone Right Coordinate: (0, 200) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15, 218.535) ft Right-Zone Right Coordinate: (55, 223.299) ft

Right-Zone Increment: 20 Radius Increments: 20

## **Slip Surface Limits**

Left Coordinate: (-100, 170.1) ft Right Coordinate: (100, 223.6) ft

## **Reinforcement Lines**

#### **Reinforcement Line 1**

Reinforcement: Row 1 Lock to Ground Surface: Yes Outside Point: (0, 210.5) ft Inside Point: (15.5, 210.5) ft

Length: 15.5 ft
Orientation: 0°

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 2**

Reinforcement: Row 8 (4 straps) Lock to Ground Surface: No Outside Point: (0, 193.7) ft Inside Point: (20, 193.7) ft

Length: 20 ft Orientation: 0 °

Slip Surface Intersection: (14.983919, 193.7) ft

Max. Pullout Force: 7,860 lbf Available Length: 5.0160809 ft Required Length: 5.0160809 ft Pullout Force: 3,478.3709 lbf

Pullout Force per Length: 693.44394 lbf/ft Governing Component: Pullout Resistance

#### **Reinforcement Line 3**

Reinforcement: Row 6 Lock to Ground Surface: Yes Outside Point: (0, 198.5) ft Inside Point: (15.5, 198.5) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 4**

Reinforcement: Row 2 Lock to Ground Surface: Yes Outside Point: (0, 208.1) ft Inside Point: (15.5, 208.1) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 5**

Reinforcement: Row 5 Lock to Ground Surface: Yes Outside Point: (0, 200.9) ft Inside Point: (15.5, 200.9) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### Reinforcement Line 6

Reinforcement: Row 4 Lock to Ground Surface: Yes Outside Point: (0, 203.3) ft Inside Point: (15.5, 203.3) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### Reinforcement Line 7

Reinforcement: Row 3 Lock to Ground Surface: Yes Outside Point: (0, 205.7) ft Inside Point: (15.5, 205.7) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 8**

#### 1A.5 Compound - Post-Seismic (Spencer)

Reinforcement: Row 7 (4 straps) Lock to Ground Surface: Yes Outside Point: (0, 196.1) ft Inside Point: (20, 196.1) ft

Length: 20 ft
Orientation: 0 °

Slip Surface Intersection: (17.588678, 196.1) ft

Max. Pullout Force: 7,860 lbf Available Length: 2.4113217 ft Required Length: 2.4113217 ft Pullout Force: 1,832.5947 lbf

Pullout Force per Length: 759.99596 lbf/ft Governing Component: Pullout Resistance

## **Surcharge Loads**

## **Surcharge Load 1**

Surcharge (Unit Weight): 125 pcf

Direction: Vertical

#### **Coordinates**

| X       | Υ         |
|---------|-----------|
| 35.9 ft | 224.15 ft |
| 39.4 ft | 224.2 ft  |
| 40.2 ft | 224.2 ft  |
| 100 ft  | 224.6 ft  |

## Geometry

Name: Default Geometry

## Settings

View: 2D

Element Thickness: 1 ft

#### **Points**

|         | X           | Υ           |
|---------|-------------|-------------|
| Point 1 | 100 ft      | 160 ft      |
| Point 2 | 100 ft      | 185.5 ft    |
| Point 3 | 0.9 ft      | 160 ft      |
| Point 4 | 100 ft      | 211.1475 ft |
| Point 5 | 3.8 ft      | 183 ft      |
| Point 6 | -20.1275 ft | 160 ft      |
| Point 7 | 100 ft      | 219.64 ft   |
| Point 8 | 42.5825 ft  | 219.8525 ft |
| Point 9 | 40.2 ft     | 223.2 ft    |
|         |             |             |

| Point 10 | 100 ft      | 223.6 ft             |
|----------|-------------|----------------------|
| Point 11 | 0 ft        | 211.7 ft             |
| Point 12 | 0 ft        | 192 ft               |
| Point 13 | 13 ft       | 192 ft               |
| Point 14 | 24.5 ft     | 213.8 ft             |
| Point 15 | 24.5 ft     | 192 ft               |
| Point 16 | 24.5 ft     | 203 ft               |
| Point 17 | 24.5 ft     | 205 ft               |
| Point 18 | 41.8 ft     | 220.7 ft             |
| Point 19 | 26.6 ft     | 215.4 ft             |
| Point 20 | 37.9 ft     | 223.4 ft             |
| Point 21 | 6.13959 ft  | 185.3 ft             |
| Point 22 | 8.9 ft      | 192 ft               |
| Point 23 | -100 ft     | 160 ft               |
|          |             |                      |
| Point 24 | -100 ft     | 170.1 ft             |
| Point 25 | -91.8 ft    | 174.4 ft             |
| Point 26 | -88.3 ft    | 176.5 ft<br>177.8 ft |
| Point 27 | -85.7 ft    |                      |
| Point 28 | -83.4 ft    | 178.4 ft             |
| Point 29 | -76 ft      | 178.9 ft             |
| Point 30 | -74 ft      | 179.7 ft             |
| Point 31 | -55.9 ft    | 180.2 ft             |
| Point 32 | -37.3 ft    | 182.3 ft             |
| Point 33 | -30.3 ft    | 182.9 ft             |
| Point 34 | -13.6 ft    | 190.2 ft             |
| Point 35 | 7 ft        | 223 ft               |
| Point 36 | 15 ft       | 223 ft               |
| Point 37 | 15 ft       | 211.7 ft             |
| Point 38 | 7 ft        | 211.7 ft             |
| Point 39 | -6 ft       | 195 ft               |
| Point 40 | -37.3275 ft | 162.2725 ft          |
| Point 41 | -47.26 ft   | 160 ft               |
| Point 42 | -5.125 ft   | 182.98095 ft         |
| Point 43 | 80.7025 ft  | 160 ft               |
| Point 44 | -100 ft     | 129.8675 ft          |
| Point 45 | 100 ft      | 129.8675 ft          |
| Point 46 | -100 ft     | 147.8625 ft          |
| Point 47 | -27.95 ft   | 152.3875 ft          |
| Point 48 | -100 ft     | 133.97 ft            |
| Point 49 | 16.5 ft     | 197.3 ft             |
| Point 50 | 100 ft      | 209.9025 ft          |
| Point 51 | 95.42762 ft | 209.80965 ft         |
| Point 52 | 3.915 ft    | 160.77581 ft         |
| Point 53 | 17.7925 ft  | 187.09412 ft         |
| Point 54 | 28.7 ft     | 129.8675 ft          |
| Point 55 | 0 ft        | 198.7 ft             |
| Point 56 | 47.15 ft    | 195.68393 ft         |
| Point 57 | 42.67 ft    | 194.37311 ft         |
|          |             |                      |

| Point 58 | 0 ft        | 195 ft       |
|----------|-------------|--------------|
| Point 59 | -32.3 ft    | 165.4 ft     |
| Point 60 | -16 ft      | 164.1 ft     |
| Point 61 | -100 ft     | 150.0525 ft  |
| Point 62 | 15 ft       | 218.535 ft   |
| Point 63 | 24 ft       | 223 ft       |
| Point 64 | 7 ft        | 214.495 ft   |
| Point 65 | 1.355 ft    | 211.7 ft     |
| Point 66 | 25.9 ft     | 223 ft       |
| Point 67 | 22 ft       | 192 ft       |
| Point 68 | 15.0117 ft  | 208.01106 ft |
| Point 69 | 21.5 ft     | 192 ft       |
| Point 70 | 15.5 ft     | 192 ft       |
| Point 71 | 15.5 ft     | 211.7 ft     |
| Point 72 | 15.5 ft     | 194.35 ft    |
| Point 73 | 15.5 ft     | 197.3 ft     |
| Point 74 | 15.5 ft     | 208.29 ft    |
| Point 75 | 18.50702 ft | 197.3 ft     |
| Point 76 | 15.5 ft     | 196.43333 ft |
| Point 77 | 21.5 ft     | 211.7 ft     |
| Point 78 | 20 ft       | 197.3 ft     |
| Point 79 | 20 ft       | 192 ft       |
| Point 80 | 21.5 ft     | 202 ft       |
| Point 81 | 21.5 ft     | 200 ft       |
| Point 82 | 21.5 ft     | 208.29 ft    |
| Point 83 | 31.9 ft     | 223.1 ft     |
| Point 84 | 31.9 ft     | 219.08 ft    |
|          |             |              |

## Regions

|              | Material   | Points                          | Area                       |
|--------------|--|---------------------------------|----------------------------|
| Region<br>1  | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 1,2,52,3,43                     | 1,263.5<br>ft <sup>2</sup> |
| Region<br>2  | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 52,2,50,51,56,57,53,5,60,6,47,3 | 2,656.9<br>ft <sup>2</sup> |
| Region<br>3  | Gravel Borrow  | 9,18,8,7,10                     | 214.55<br>ft <sup>2</sup>  |
| Region<br>4  | Gravel Borrow  | 38,65,11,55,68,74,71,37         | 127 ft <sup>2</sup>        |
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel                                  | 8,16,17,18                      | 31.556<br>ft <sup>2</sup>  |
| Region<br>6  | ESU 2A Very Loose to Loose<br>Sand/Gravel                        | 18,17,14,19,84,20,9             | 115.05<br>ft <sup>2</sup>  |
| Region<br>7  | Common Borrow  | 38,37,62,64                     | 38.52<br>ft <sup>2</sup>   |
| Region<br>8  | Common Borrow  | 14,19,84,83,66,63,62,37,71,77   | 132.58<br>ft <sup>2</sup>  |
| Region<br>9  | ESU 2B Medium Dense Sand/Gravel                                  | 22,42,59,40,60,5,21,13          | 332.37<br>ft <sup>2</sup>  |
| Region<br>10 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 44,54,45,1,43,3,47,48           | 4,704.7<br>ft <sup>2</sup> |

| Region<br>11 | ESU 2B Medium Dense Sand/Gravel (Residual Strength) | 41,46,48,47,6,60,40                                      | 992.46<br>ft <sup>2</sup>  |
|--------------|---|--|----------------------------|
| Region<br>12 | ESU 4B Dense to Very Dense<br>Sand/Gravel           | 56,51,50,4,7,8,16,15,67,69,79,70,13,21,5,53,57           | 1,417.8<br>ft <sup>2</sup> |
| Region<br>13 | ESU 2A Very Loose to Loose<br>Sand/Gravel           | 34,33,32,31,30,29,28,27,26,25,24,23,40,59,42,22,12,58,39 | 1,656.2<br>ft <sup>2</sup> |
| Region<br>14 | ESU 2A Very Loose to Loose<br>Sand/Gravel           | 40,23,61,46,41   | 379.99<br>ft <sup>2</sup>  |
| Region<br>15 |   | 63,36,62   | 20.093<br>ft <sup>2</sup>  |
| Region<br>16 |   | 36,35,64,62  | 51.88<br>ft <sup>2</sup>   |
| Region<br>17 | Common Borrow                                       | 64,65,38   | 7.8889<br>ft <sup>2</sup>  |
| Region<br>18 | ESU 4B Dense to Very Dense<br>Sand/Gravel           | 15,16,81,69,67   | 28.5 ft <sup>2</sup>       |
| Region<br>19 | Gravel Borrow                                       | 72,76,22,13  | 11.692<br>ft <sup>2</sup>  |
| Region<br>20 | Gravel Borrow                                       | 70,72,13   | 2.9375<br>ft <sup>2</sup>  |
| Region<br>21 | Gravel Borrow                                       | 70,79,78,75,72   | 19.415<br>ft <sup>2</sup>  |
| Region<br>22 | Gravel Borrow                                       | 81,75,78,79,69   | 11.991<br>ft²              |
| Region<br>23 | Gravel Borrow                                       | 49,75,81,80  | 7.7095<br>ft <sup>2</sup>  |
| Region<br>24 | Gravel Borrow                                       | 49,76,72,75  | 4.002<br>ft <sup>2</sup>   |
| Region<br>25 | Gravel Borrow                                       | 73,76,49   | 0.43333<br>ft <sup>2</sup> |
| Region<br>26 | Gravel Borrow                                       | 76,73,74,68,55,58,12,22                                  | 163.72<br>ft <sup>2</sup>  |
| Region<br>27 | ESU 2B Medium Dense Sand/Gravel                     | 80,81,16,17  | 6 ft²                      |
| Region<br>28 | Gravel Borrow                                       | 74,82,77   | 10.23<br>ft <sup>2</sup>   |
| Region<br>29 | Gravel Borrow                                       | 77,71,74   | 10.23<br>ft <sup>2</sup>   |
| Region<br>30 | ESU 2A Very Loose to Loose<br>Sand/Gravel           | 77,82,80,17,14   | 27.75<br>ft <sup>2</sup>   |
| Region<br>31 | Gravel Borrow                                       | 73,49,80,82,74   | 54.19<br>ft <sup>2</sup>   |
| Region<br>32 | Common Borrow                                       | 20,83,84   | 12.06<br>ft <sup>2</sup>   |
| Region<br>33 |   | 55,39,58   | 11.1 ft²                   |

## **Slip Results**

Slip Surfaces Analysed: 9780 of 11466 converged

## **Current Slip Surface**

Slip Surface: 2,852 Factor of Safety: 1.3 Volume: 926.15021 ft<sup>3</sup> Weight: 111,473.27 lbf

Resisting Moment: 3,612,669.1 lbf·ft Activating Moment: 2,792,227.2 lbf·ft

Resisting Force: 56,229.62 lbf Activating Force: 43,471.782 lbf Slip Rank: 1 of 11,466 slip surfaces Exit: (-32.349646, 182.72432) ft Entry: (32.424307, 223.10874) ft

Radius: 52.811397 ft

Center: (-19.274577, 233.89155) ft

### **Slip Slices**

|             | Х                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material                                |
|-------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|--|
| Slice<br>1  | -31.324823<br>ft | 182.48409<br>ft | -181.68176<br>psf | 69.591423<br>psf         | 43.485547<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>2  | -29.25625<br>ft  | 182.04293<br>ft | -180.15416<br>psf | 257.8555<br>psf          | 161.126<br>psf         | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>3  | -27.16875<br>ft  | 181.68417<br>ft | -178.93878<br>psf | 472.73904<br>psf         | 295.40014<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>4  | -25.08125<br>ft  | 181.41086<br>ft | -178.88779<br>psf | 646.2097<br>psf          | 403.79663<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>5  | -22.99375<br>ft  | 181.22167<br>ft | -179.14535<br>psf | 786.17185<br>psf         | 491.25469<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>6  | -20.90625<br>ft  | 181.1157<br>ft  | -177.96849<br>psf | 898.38896<br>psf         | 561.37573<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>7  | -18.81875<br>ft  | 181.09244<br>ft | -176.75492<br>psf | 987.16635<br>psf         | 616.85 psf             | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>8  | -16.73125<br>ft  | 181.15179<br>ft | -177.75218<br>psf | 1,055.7875<br>psf        | 659.72925<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>9  | -14.64375<br>ft  | 181.29401<br>ft | -179.44633<br>psf | 1,106.8015<br>psf        | 691.60636<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>10 | -12.65 ft        | 181.50604<br>ft | -184.2186<br>psf  | 1,164.3132<br>psf        | 727.54366<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>11 | -10.75 ft        | 181.78159<br>ft | -200.14219<br>psf | 1,228.3695<br>psf        | 767.57043<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose                |

|             |                 |                 |                   |                   |                   |       |       | Sand/Gravel                                  |
|-------------|-----------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>12 | -8.85 ft        | 182.12832<br>ft | -294.87555<br>psf | 1,278.325<br>psf  | 798.7861<br>psf   | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>13 | -6.95 ft        | 182.54767<br>ft | -362.48685<br>psf | 1,388.2344<br>psf | 867.46514<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>14 | -5.521266<br>ft | 182.90485<br>ft | -396.27515<br>psf | 1,443.877<br>psf  | 902.23446<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>15 | -3.781899<br>ft | 183.42095<br>ft | -389.40397<br>psf | 1,255.4769<br>psf | 784.50904<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>16 | -1.260633<br>ft | 184.26552<br>ft | -355.49357<br>psf | 1,109.1323<br>psf | 693.06278<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>17 | 0.6775 ft       | 184.9996<br>ft  | -331.74593<br>psf | 3,012.3532<br>psf | 1,882.3272<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>18 | 2.2958333<br>ft | 185.69717<br>ft | -312.89226<br>psf | 2,858.8371<br>psf | 1,786.3997<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>19 | 4.1775 ft       | 186.58467<br>ft | -292.03965<br>psf | 2,760.0952<br>psf | 1,724.6989<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>20 | 6.0591667<br>ft | 187.56559<br>ft | -272.64084<br>psf | 2,654.7246<br>psf | 1,658.856<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>21 | 7.95 ft         | 188.65178<br>ft | -254.49171<br>psf | 2,541.9838<br>psf | 1,588.4078<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>22 | 9.8958729<br>ft | 189.88359<br>ft | -237.26176<br>psf | 2,416.3601<br>psf | 1,509.9094<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>23 | 11.887619<br>ft | 191.27185<br>ft | -220.50564<br>psf | 2,283.6536<br>psf | 1,426.9851<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>24 | 13.227615<br>ft | 192.26872<br>ft | -209.5233<br>psf  | 2,273.7015<br>psf | 1,776.4103<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>25 | 14.285869<br>ft | 193.12534<br>ft | -200.2752<br>psf  | 2,076.5959<br>psf | 1,622.4145<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>26 | 15.25 ft        | 193.92922<br>ft | -190.94009<br>psf | 1,995.0411<br>psf | 1,558.6969<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>27 | 16 ft           | 194.59402<br>ft | -185.40797<br>psf | 1,879.6808<br>psf | 1,468.5676<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>28 | 17.50351 ft     | 196.0173<br>ft  | -176.11263        | 1,716.8318<br>psf | 1,341.336<br>psf  | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>29 | 18.656323<br>ft | 197.14588<br>ft | -172.10212<br>psf | 1,589.6038<br>psf | 1,241.9346<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>30 | 19.543751<br>ft | 198.10056<br>ft | -176.31912<br>psf | 1,503.2657<br>psf | 1,174.4799<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>31 | 20.890939<br>ft | 199.61482<br>ft | -189.41042<br>psf | 1,371.6608<br>psf | 1,071.6588<br>psf | 0 psf | 0 psf | Gravel Borrow                                |

| pound       | rost seisime (spe | neer)           |                   |                   |                  |       |       |  |
|-------------|-------------------|-----------------|-------------------|-------------------|------------------|-------|-------|--|
| Slice<br>32 | 22.75 ft          | 201.97436<br>ft | -214.35342<br>psf | 1,135.1803<br>psf | 709.33937<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>33 | 24.25 ft          | 203.98403<br>ft | -237.06792<br>psf | 992.64495<br>psf  | 620.27341<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>34 | 25.01513 ft       | 205.14142<br>ft | -254.02098<br>psf | 897.66765<br>psf  | 560.925<br>psf   | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>35 | 25.71513 ft       | 206.23572<br>ft | -263.26581<br>psf | 812.19653<br>psf  | 507.51672<br>psf | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>36 | 26.25 ft          | 207.13189<br>ft | -251.73198<br>psf | 745.92615<br>psf  | 466.10639<br>psf | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>37 | 27.772997<br>ft   | 210.0412<br>ft  | -214.97451<br>psf | 551.16542<br>psf  | 344.40638<br>psf | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>38 | 30.11899 ft       | 215.50645<br>ft | -181.88356<br>psf | 258.40327<br>psf  | 161.46829<br>psf | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>39 | 31.595994<br>ft   | 219.75154<br>ft | 0 psf             | 93.238487<br>psf  | 58.261873<br>psf | 0 psf | 0 psf | Common Borrow                                |
| Slice<br>40 | 32.162153<br>ft   | 221.97699<br>ft | 0 psf             | 27.224015<br>psf  | 17.011452<br>psf | 0 psf | 0 psf | Common Borrow                                |

# 1A.6 Compound - Post-Seismic (M-P)

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## **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 650 Date: 01/17/2022 Time: 01:45:50 PM

Tool Version: 11.1.1.22085

Last Solved Date: 01/17/2022 Last Solved Time: 02:00:26 PM

## **Project Settings**

Unit System: U.S. Customary Units

## **Analysis Settings**

### 1A.6 Compound - Post-Seismic (M-P)

Description: Project Num: 00180-366-01 Wall: 05.85L-A Station: 1+90

Kind: SLOPE/W

Parent: 1. Steady State (Compound) Analysis Type: Morgenstern-Price

Settings

Side Function

Interslice force function option: Half-Sine

PWP Conditions from Parent Analysis: 1. Steady State (Compound) [(last)]

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 20

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

Factor of Safety Convergence Settings

Maximum Number of Iterations: 100 Tolerable difference in F of S: 0.001

Solution Settings

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

#### **Materials**

### **ESU 2A Very Loose to Loose Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **ESU 2B Medium Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

## **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

## ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

## **ESU 2B Medium Dense Sand/Gravel (Residual Strength)**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf

Effective Cohesion: 497 psf Effective Friction Angle: 0 °

Phi-B: 0°

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

### Reinforcements

#### Row 1

Type: Geosynthetic

Interface Adhesion: 0 psf Interface Shear Angle: 6.6 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 2

Type: Geosynthetic

Interface Adhesion: 0 psf Interface Shear Angle: 6.1 °

Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 3

Type: Geosynthetic

Interface Adhesion: 0 psf Interface Shear Angle: 5.6 ° Surface Area Factor: 2 Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 4

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 5.1 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 5

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 4.6 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 6

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 4.1 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

## Row 7 (4 straps)

#### 1A.6 Compound - Post-Seismic (M-P)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 7.2 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 7,860 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 7,860 lbf/ft

#### Row 8 (4 straps)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 6.2 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 7,860 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 7,860 lbf/ft

## Slip Surface Entry and Exit

Left Type: Range

Left-Zone Left Coordinate: (-45, 181.43065) ft

Left-Zone Right Coordinate: (0, 200) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15, 218.535) ft Right-Zone Right Coordinate: (55, 223.299) ft

Right-Zone Increment: 20 Radius Increments: 20

## **Slip Surface Limits**

Left Coordinate: (-100, 170.1) ft Right Coordinate: (100, 223.6) ft

## **Reinforcement Lines**

#### **Reinforcement Line 1**

Reinforcement: Row 1 Lock to Ground Surface: Yes Outside Point: (0, 210.5) ft Inside Point: (15.5, 210.5) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### Reinforcement Line 2

Reinforcement: Row 8 (4 straps) Lock to Ground Surface: No Outside Point: (0, 193.7) ft Inside Point: (20, 193.7) ft

Length: 20 ft Orientation: 0 °

Slip Surface Intersection: (14.983919, 193.7) ft

Max. Pullout Force: 7,860 lbf Available Length: 5.0160809 ft Required Length: 5.0160809 ft Pullout Force: 3,478.3709 lbf

Pullout Force per Length: 693.44394 lbf/ft Governing Component: Pullout Resistance

#### **Reinforcement Line 3**

Reinforcement: Row 6 Lock to Ground Surface: Yes Outside Point: (0, 198.5) ft Inside Point: (15.5, 198.5) ft

Length: 15.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### Reinforcement Line 4

Reinforcement: Row 2 Lock to Ground Surface: Yes Outside Point: (0, 208.1) ft Inside Point: (15.5, 208.1) ft

Length: 15.5 ft
Orientation: 0°

Max. Pullout Force: 0 lbf

Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 5**

Reinforcement: Row 5 Lock to Ground Surface: Yes Outside Point: (0, 200.9) ft Inside Point: (15.5, 200.9) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 6**

Reinforcement: Row 4 Lock to Ground Surface: Yes Outside Point: (0, 203.3) ft Inside Point: (15.5, 203.3) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 7**

Reinforcement: Row 3 Lock to Ground Surface: Yes Outside Point: (0, 205.7) ft Inside Point: (15.5, 205.7) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 8**

Reinforcement: Row 7 (4 straps) Lock to Ground Surface: Yes Outside Point: (0, 196.1) ft Inside Point: (20, 196.1) ft

Length: 20 ft
Orientation: 0 °

Slip Surface Intersection: (17.588678, 196.1) ft

Max. Pullout Force: 7,860 lbf Available Length: 2.4113217 ft Required Length: 2.4113217 ft Pullout Force: 1,832.5947 lbf

Pullout Force per Length: 759.99596 lbf/ft Governing Component: Pullout Resistance

## **Surcharge Loads**

### **Surcharge Load 1**

Surcharge (Unit Weight): 125 pcf

Direction: Vertical

#### **Coordinates**

| X       | Υ         |
|---------|-----------|
| 35.9 ft | 224.15 ft |
| 39.4 ft | 224.2 ft  |
| 40.2 ft | 224.2 ft  |
| 100 ft  | 224.6 ft  |

## **Geometry**

Name: Default Geometry

## Settings

View: 2D

Element Thickness: 1 ft

#### **Points**

|         | X           | Υ           |
|---------|-------------|-------------|
| Point 1 | 100 ft      | 160 ft      |
| Point 2 | 100 ft      | 185.5 ft    |
| Point 3 | 0.9 ft      | 160 ft      |
| Point 4 | 100 ft      | 211.1475 ft |
| Point 5 | 3.8 ft      | 183 ft      |
| Point 6 | -20.1275 ft | 160 ft      |
| Point 7 | 100 ft      | 219.64 ft   |
| Point 8 | 42.5825 ft  | 219.8525 ft |
|         |             |             |

| Point 9  | 40.2 ft     | 223.2 ft     |
|----------|-------------|--------------|
| Point 10 | 100 ft      | 223.6 ft     |
| Point 11 | 0 ft        | 211.7 ft     |
| Point 12 | 0 ft        | 192 ft       |
| Point 13 | 13 ft       | 192 ft       |
| Point 14 | 24.5 ft     | 213.8 ft     |
| Point 15 | 24.5 ft     | 192 ft       |
| Point 16 | 24.5 ft     | 203 ft       |
| Point 17 | 24.5 ft     | 205 ft       |
| Point 18 | 41.8 ft     | 220.7 ft     |
| Point 19 | 26.6 ft     | 215.4 ft     |
| Point 20 | 37.9 ft     | 223.2 ft     |
| Point 21 | 6.13959 ft  | 185.3 ft     |
| Point 22 | 8.9 ft      | 192 ft       |
| Point 23 | -100 ft     | 160 ft       |
| Point 24 | -100 ft     | 170.1 ft     |
| Point 25 | -91.8 ft    | 174.4 ft     |
| Point 26 | -88.3 ft    | 176.5 ft     |
| Point 27 | -85.7 ft    | 177.8 ft     |
| Point 28 | -83.4 ft    | 178.4 ft     |
| Point 29 | -76 ft      | 178.9 ft     |
| Point 30 | -74 ft      | 179.7 ft     |
| Point 31 | -55.9 ft    | 180.2 ft     |
| Point 32 | -37.3 ft    | 182.3 ft     |
| Point 33 | -30.3 ft    | 182.9 ft     |
| Point 34 | -13.6 ft    | 190.2 ft     |
| Point 35 | 7 ft        | 223 ft       |
| Point 36 | 15 ft       | 223 ft       |
| Point 37 | 15 ft       | 211.7 ft     |
| Point 38 | 7 ft        | 211.7 ft     |
| Point 39 | -6 ft       | 195 ft       |
| Point 40 | -37.3275 ft | 162.2725 ft  |
| Point 41 | -47.26 ft   | 160 ft       |
| Point 42 | -5.125 ft   | 182.98095 ft |
| Point 43 | 80.7025 ft  | 160 ft       |
| Point 44 | -100 ft     | 129.8675 ft  |
| Point 45 | 100 ft      | 129.8675 ft  |
| Point 46 | -100 ft     | 147.8625 ft  |
| Point 47 | -27.95 ft   | 152.3875 ft  |
| Point 48 | -100 ft     | 133.97 ft    |
| Point 49 | 16.5 ft     | 197.3 ft     |
| Point 50 | 100 ft      | 209.9025 ft  |
| Point 51 | 95.42762 ft | 209.80965 ft |
| Point 52 | 3.915 ft    | 160.77581 ft |
| Point 53 | 17.7925 ft  | 187.09412 ft |
| Point 54 | 28.7 ft     | 129.8675 ft  |
| Point 55 | 0 ft        | 198.7 ft     |
| Point 56 | 47.15 ft    | 195.68393 ft |
|          |             |              |

| Point 57 | 42.67 ft    | 194.37311 ft |
|----------|-------------|--------------|
| Point 58 | 0 ft        | 195 ft       |
| Point 59 | -32.3 ft    | 165.4 ft     |
| Point 60 | -16 ft      | 164.1 ft     |
| Point 61 | -100 ft     | 150.0525 ft  |
| Point 62 | 15 ft       | 218.535 ft   |
| Point 63 | 24 ft       | 223 ft       |
| Point 64 | 7 ft        | 214.495 ft   |
| Point 65 | 1.355 ft    | 211.7 ft     |
| Point 66 | 25.9 ft     | 223 ft       |
| Point 67 | 22 ft       | 192 ft       |
| Point 68 | 15.0117 ft  | 208.01106 ft |
| Point 69 | 21.5 ft     | 192 ft       |
| Point 70 | 15.5 ft     | 192 ft       |
| Point 71 | 15.5 ft     | 211.7 ft     |
| Point 72 | 15.5 ft     | 194.35 ft    |
| Point 73 | 15.5 ft     | 197.3 ft     |
| Point 74 | 15.5 ft     | 208.29 ft    |
| Point 75 | 18.50702 ft | 197.3 ft     |
| Point 76 | 15.5 ft     | 196.43333 ft |
| Point 77 | 21.5 ft     | 211.7 ft     |
| Point 78 | 20 ft       | 197.3 ft     |
| Point 79 | 20 ft       | 192 ft       |
| Point 80 | 21.5 ft     | 202 ft       |
| Point 81 | 21.5 ft     | 200 ft       |
| Point 82 | 21.5 ft     | 208.29 ft    |
| Point 83 | 31.9 ft     | 223.1 ft     |
| Point 84 | 31.9 ft     | 219.08 ft    |
|          |             |              |

## Regions

|             | Material  | Points                          | Area                       |
|-------------|---|---------------------------------|----------------------------|
| Region<br>1 | ESU 4B Dense to Very Dense<br>Sand/Gravel                           | 1,2,52,3,43                     | 1,263.5<br>ft <sup>2</sup> |
| Region<br>2 | ESU 5B Very Stiff to Hard Silt and<br>Clay/Dense to Very Dense Silt | 52,2,50,51,56,57,53,5,60,6,47,3 | 2,656.9<br>ft <sup>2</sup> |
| Region<br>3 | Gravel Borrow   | 9,18,8,7,10                     | 214.55<br>ft <sup>2</sup>  |
| Region<br>4 | Gravel Borrow   | 38,65,11,55,68,74,71,37         | 127 ft²                    |
| Region<br>5 | ESU 2B Medium Dense Sand/Gravel                                     | 8,16,17,18                      | 31.556<br>ft <sup>2</sup>  |
| Region<br>6 | ESU 2A Very Loose to Loose<br>Sand/Gravel                           | 18,17,14,19,84,20,9             | 115.05<br>ft <sup>2</sup>  |
| Region<br>7 | Common Borrow   | 38,37,62,64                     | 38.52<br>ft <sup>2</sup>   |
| Region<br>8 | Common Borrow   | 14,19,84,83,66,63,62,37,71,77   | 132.58<br>ft <sup>2</sup>  |
| Region<br>9 | ESU 2B Medium Dense Sand/Gravel                                     | 22,42,59,40,60,5,21,13          | 332.37<br>ft <sup>2</sup>  |
| Region      | ESU 4B Dense to Very Dense  |                                 | 4,704.7                    |

| 10           | Sand/Gravel   | 44,54,45,1,43,3,47,48                                    | ft²                        |
|--------------|---|--|----------------------------|
| Region<br>11 | ESU 2B Medium Dense Sand/Gravel (Residual Strength) | 41,46,48,47,6,60,40                                      | 992.46<br>ft <sup>2</sup>  |
| Region<br>12 | ESU 4B Dense to Very Dense<br>Sand/Gravel           | 56,51,50,4,7,8,16,15,67,69,79,70,13,21,5,53,57           | 1,417.8<br>ft <sup>2</sup> |
| Region<br>13 | ESU 2A Very Loose to Loose<br>Sand/Gravel           | 34,33,32,31,30,29,28,27,26,25,24,23,40,59,42,22,12,58,39 | 1,656.2<br>ft <sup>2</sup> |
| Region<br>14 | ESU 2A Very Loose to Loose<br>Sand/Gravel           | 40,23,61,46,41   | 379.99<br>ft <sup>2</sup>  |
| Region<br>15 |   | 63,36,62   | 20.093<br>ft <sup>2</sup>  |
| Region<br>16 |   | 36,35,64,62  | 51.88<br>ft²               |
| Region<br>17 | Common Borrow                                       | 64,65,38   | 7.8889<br>ft <sup>2</sup>  |
| Region<br>18 | ESU 4B Dense to Very Dense<br>Sand/Gravel           | 15,16,81,69,67   | 28.5 ft <sup>2</sup>       |
| Region<br>19 | Gravel Borrow                                       | 72,76,22,13  | 11.692<br>ft <sup>2</sup>  |
| Region<br>20 | Gravel Borrow                                       | 70,72,13   | 2.9375<br>ft <sup>2</sup>  |
| Region<br>21 | Gravel Borrow                                       | 70,79,78,75,72   | 19.415<br>ft <sup>2</sup>  |
| Region<br>22 | Gravel Borrow                                       | 81,75,78,79,69   | 11.991<br>ft²              |
| Region<br>23 | Gravel Borrow                                       | 49,75,81,80  | 7.7095<br>ft <sup>2</sup>  |
| Region<br>24 | Gravel Borrow                                       | 49,76,72,75  | 4.002<br>ft <sup>2</sup>   |
| Region<br>25 | Gravel Borrow                                       | 73,76,49   | 0.43333<br>ft <sup>2</sup> |
| Region<br>26 | Gravel Borrow                                       | 76,73,74,68,55,58,12,22                                  | 163.72<br>ft <sup>2</sup>  |
| Region<br>27 | ESU 2B Medium Dense Sand/Gravel                     | 80,81,16,17  | 6 ft²                      |
| Region<br>28 | Gravel Borrow                                       | 74,82,77   | 10.23<br>ft <sup>2</sup>   |
| Region<br>29 | Gravel Borrow                                       | 77,71,74   | 10.23<br>ft <sup>2</sup>   |
| Region<br>30 | ESU 2A Very Loose to Loose<br>Sand/Gravel           | 77,82,80,17,14   | 27.75<br>ft <sup>2</sup>   |
| Region<br>31 | Gravel Borrow                                       | 73,49,80,82,74   | 54.19<br>ft <sup>2</sup>   |
| Region<br>32 | Common Borrow                                       | 20,83,84   | 12.06<br>ft <sup>2</sup>   |
| Region<br>33 |   | 55,39,58   | 11.1 ft²                   |

## **Slip Results**

Slip Surfaces Analysed: 10931 of 11466 converged

## **Current Slip Surface**

Slip Surface: 2,852 Factor of Safety: 1.3 Volume: 926.15021 ft<sup>3</sup> Weight: 111,473.27 lbf

Resisting Moment: 3,610,085.7 lbf·ft Activating Moment: 2,792,227.2 lbf·ft

Resisting Force: 56,114.321 lbf Activating Force: 43,416.061 lbf Slip Rank: 1 of 11,466 slip surfaces Exit: (-32.349646, 182.72432) ft Entry: (32.424307, 223.10874) ft

Radius: 52.811397 ft

Center: (-19.274577, 233.89155) ft

## **Slip Slices**

|             | X                | Υ               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material                                |
|-------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|--|
| Slice<br>1  | -31.324823<br>ft | 182.48409<br>ft | -181.68176<br>psf | 43.030043<br>psf         | 26.888155<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>2  | -29.25625<br>ft  | 182.04293<br>ft | -180.15416<br>psf | 179.53902<br>psf         | 112.18843<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>3  | -27.16875<br>ft  | 181.68417<br>ft | -178.93878<br>psf | 368.11373<br>psf         | 230.02299<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>4  | -25.08125<br>ft  | 181.41086<br>ft | -178.88779<br>psf | 556.78167<br>psf         | 347.9158<br>psf        | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>5  | -22.99375<br>ft  | 181.22167<br>ft | -179.14535<br>psf | 738.53006<br>psf         | 461.4848<br>psf        | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>6  | -20.90625<br>ft  | 181.1157<br>ft  | -177.96849<br>psf | 905.78236<br>psf         | 565.99563<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>7  | -18.81875<br>ft  | 181.09244<br>ft | -176.75492<br>psf | 1,051.3784<br>psf        | 656.97412<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>8  | -16.73125<br>ft  | 181.15179<br>ft | -177.75218<br>psf | 1,169.5394<br>psf        | 730.80932<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>9  | -14.64375<br>ft  | 181.29401<br>ft | -179.44633<br>psf | 1,256.5893<br>psf        | 785.20417<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>10 | -12.65 ft        | 181.50604<br>ft | -184.2186<br>psf  | 1,333.5412<br>psf        | 833.28903<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
|             |                  |                 |                   |                          |                        |                      |                     | ESU 2A Very                                  |

| Slice<br>11 | -10.75 ft       | 181.78159<br>ft | -200.14219<br>psf | 1,402.6138<br>psf | 876.4504<br>psf   | 0 psf | 0 psf | Loose to Loose<br>Sand/Gravel                |
|-------------|-----------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>12 | -8.85 ft        | 182.12832<br>ft | -294.87555<br>psf | 1,444.6412<br>psf | 902.712<br>psf    | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>13 | -6.95 ft        | 182.54767<br>ft | -362.48685<br>psf | 1,556.9847<br>psf | 972.91202<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>14 | -5.521266<br>ft | 182.90485<br>ft | -396.27515<br>psf | 1,615.8917<br>psf | 1,009.7212<br>psf | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>15 | -3.781899<br>ft | 183.42095<br>ft | -389.40397<br>psf | 1,367.4624<br>psf | 854.48535<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>16 | -1.260633<br>ft | 184.26552<br>ft | -355.49357<br>psf | 1,166.4006<br>psf | 728.84796<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>17 | 0.6775 ft       | 184.9996<br>ft  | -331.74593<br>psf | 3,077.5638<br>psf | 1,923.0753<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>18 | 2.2958333<br>ft | 185.69717<br>ft | -312.89226<br>psf | 2,863.1613<br>psf | 1,789.1018<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>19 | 4.1775 ft       | 186.58467<br>ft | -292.03965<br>psf | 2,712.0422<br>psf | 1,694.6721<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>20 | 6.0591667<br>ft | 187.56559<br>ft | -272.64084<br>psf | 2,561.0481<br>psf | 1,600.3205<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>21 | 7.95 ft         | 188.65178<br>ft | -254.49171<br>psf | 2,411.7877<br>psf | 1,507.0522<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>22 | 9.8958729<br>ft | 189.88359<br>ft | -237.26176<br>psf | 2,260.2536<br>psf | 1,412.3632<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>23 | 11.887619<br>ft | 191.27185<br>ft | -220.50564<br>psf | 2,115.6829<br>psf | 1,322.0254<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>24 | 13.227615<br>ft | 192.26872<br>ft | -209.5233<br>psf  | 2,117.4277<br>psf | 1,654.3158<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>25 | 14.285869<br>ft | 193.12534<br>ft | -200.2752<br>psf  | 1,909.8169<br>psf | 1,492.1125<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>26 | 15.25 ft        | 193.92922<br>ft | -190.94009<br>psf | 1,827.4012<br>psf | 1,427.7223<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>27 | 16 ft           | 194.59402<br>ft | -185.40797<br>psf | 1,717.191<br>psf  | 1,341.6166<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>28 | 17.50351 ft     | 196.0173<br>ft  | -176.11263<br>psf | 1,572.3485<br>psf | 1,228.4533<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>29 | 18.656323<br>ft | 197.14588<br>ft | -172.10212<br>psf | 1,465.402<br>psf  | 1,144.8975<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>30 | 19.543751<br>ft | 198.10056<br>ft | -176.31912<br>psf | 1,396.5119<br>psf | 1,091.0747<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice       | 20.890939       | 199.61482       | -189.41042        | 1,293.9254        | 1,010.9253        |       |       |  |

| •           | `               |                 |                   |                   |                  |       |       |  |
|-------------|-----------------|-----------------|-------------------|-------------------|------------------|-------|-------|--|
| 31          | ft              | ft              | psf               | psf               | psf              | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>32 | 22.75 ft        | 201.97436<br>ft | -214.35342<br>psf | 1,114.3532<br>psf | 696.32516<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>33 | 24.25 ft        | 203.98403<br>ft | -237.06792<br>psf | 1,013.7378<br>psf | 633.45369<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>34 | 25.01513 ft     | 205.14142<br>ft | -254.02098<br>psf | 937.56793<br>psf  | 585.85747<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>35 | 25.71513 ft     | 206.23572<br>ft | -263.26581<br>psf | 867.92207<br>psf  | 542.3379<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>36 | 26.25 ft        | 207.13189<br>ft | -251.73198<br>psf | 812.57863<br>psf  | 507.75548<br>psf | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>37 | 27.772997<br>ft | 210.0412<br>ft  | -214.97451<br>psf | 639.9921<br>psf   | 399.91145<br>psf | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>38 | 30.11899 ft     | 215.50645<br>ft | -181.88356<br>psf | 342.59516<br>psf  | 214.07722<br>psf | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>39 | 31.595994<br>ft | 219.75154<br>ft | 0 psf             | 139.60161<br>psf  | 87.23277<br>psf  | 0 psf | 0 psf | Common Borrow                                |
| Slice<br>40 | 32.162153<br>ft | 221.97699<br>ft | 0 psf             | 42.923206<br>psf  | 26.821396<br>psf | 0 psf | 0 psf | Common Borrow                                |

# 1B.1 Compound - Static FC Wall (Spencer)

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## **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 652 Date: 01/17/2022 Time: 02:07:09 PM

Tool Version: 11.1.1.22085

Last Solved Date: 01/17/2022 Last Solved Time: 02:37:20 PM

## **Project Settings**

Unit System: U.S. Customary Units

## **Analysis Settings**

### 1B.1 Compound - Static FC Wall (Spencer)

Description: With Forward Compatible Wall

Kind: SLOPE/W

Parent: 1. Steady State (Compound)

Analysis Type: Spencer

Settings

PWP Conditions from Parent Analysis: 1. Steady State (Compound) [(last)]

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 20

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

Factor of Safety Convergence Settings
Maximum Number of Iterations: 100
Tolerable difference in F of S: 0.001

Solution Settings

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3 Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

### **Materials**

## **ESU 2A Very Loose to Loose Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **ESU 2B Medium Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

## **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

## ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

#### Common Borrow

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **Gravel Borrow**

#### 1B.1 Compound - Static FC Wall (Spencer)

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

### **Forward Compatible Wall**

Material Model: High Strength

Unit Weight: 130 pcf

#### **Lightweight EPS**

Material Model: Mohr-Coulomb

Unit Weight: 5 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 0 °

Phi-B: 0°

## Reinforcements

#### Row 1

Type: Geosynthetic Interface Adhesion: 0 psf

Interface Shear Angle: 6.6 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 2

Type: Geosynthetic

Interface Adhesion: 0 psf Interface Shear Angle: 6.1 °

Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 3

Type: Geosynthetic

Interface Adhesion: 0 psf Interface Shear Angle: 5.6 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 4

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 5.1 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 5

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 4.6 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 6

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 4.1 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

### Row 7 (4 straps)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 7.2 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 7,860 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 7,860 lbf/ft

#### Row 8 (4 straps)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 6.2 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 7,860 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 7,860 lbf/ft

## Slip Surface Entry and Exit

Left Type: Range

Left-Zone Left Coordinate: (-45, 181.43065) ft

Left-Zone Right Coordinate: (0, 200) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15, 223) ft Right-Zone Right Coordinate: (55, 223.299) ft

Right-Zone Increment: 20 Radius Increments: 20

## **Slip Surface Limits**

Left Coordinate: (-100, 170.1) ft Right Coordinate: (100, 223.6) ft

## **Reinforcement Lines**

#### **Reinforcement Line 1**

Reinforcement: Row 1 Lock to Ground Surface: Yes Outside Point: (0, 210.5) ft Inside Point: (15.5, 210.5) ft

Length: 15.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf
Available Length: 0 ft
Required Length: 0 ft
Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 2**

Reinforcement: Row 8 (4 straps) Lock to Ground Surface: No Outside Point: (0, 193.7) ft Inside Point: (20, 193.7) ft

Length: 20 ft
Orientation: 0 °

Slip Surface Intersection: (15.079752, 193.7) ft

Max. Pullout Force: 7,860 lbf Available Length: 4.9202484 ft Required Length: 4.9202484 ft Pullout Force: 3,010.1026 lbf

Pullout Force per Length: 611.77858 lbf/ft Governing Component: Pullout Resistance

#### **Reinforcement Line 3**

Reinforcement: Row 6 Lock to Ground Surface: Yes Outside Point: (0, 198.5) ft Inside Point: (15.5, 198.5) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 4**

Reinforcement: Row 2 Lock to Ground Surface: Yes Outside Point: (0, 208.1) ft Inside Point: (15.5, 208.1) ft Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 5**

Reinforcement: Row 5 Lock to Ground Surface: Yes Outside Point: (0, 200.9) ft Inside Point: (15.5, 200.9) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### Reinforcement Line 6

Reinforcement: Row 4 Lock to Ground Surface: Yes Outside Point: (0, 203.3) ft Inside Point: (15.5, 203.3) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 7**

Reinforcement: Row 3 Lock to Ground Surface: Yes Outside Point: (0, 205.7) ft Inside Point: (15.5, 205.7) ft

Length: 15.5 ft
Orientation: 0°

Max. Pullout Force: 0 lbf
Available Length: 0 ft
Required Length: 0 ft
Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 8**

Reinforcement: Row 7 (4 straps) Lock to Ground Surface: Yes Outside Point: (0, 196.1) ft Inside Point: (20, 196.1) ft

Length: 20 ft
Orientation: 0 °

Slip Surface Intersection: (17.823618, 196.1) ft

Max. Pullout Force: 7,860 lbf Available Length: 2.1763818 ft Required Length: 2.1763818 ft Pullout Force: 1,407.5924 lbf

Pullout Force per Length: 646.75803 lbf/ft Governing Component: Pullout Resistance

## **Surcharge Loads**

## **Surcharge Load 1**

Surcharge (Unit Weight): 250 pcf

Direction: Vertical

#### **Coordinates**

| Χ         | Υ         |
|-----------|-----------|
| 9 ft      | 224.75 ft |
| 19.995 ft | 224.75 ft |
| 20 ft     | 224 ft    |
| 26 ft     | 224 ft    |
| 40.2 ft   | 224.2 ft  |
| 100 ft    | 224.6 ft  |

## **Geometry**

Name: Default Geometry

## Settings

View: 2D

Element Thickness: 1 ft

#### **Points**

|         | X      | Υ        |
|---------|--------|----------|
| Point 1 | 100 ft | 160 ft   |
| Point 2 | 100 ft | 185.5 ft |
| Point 3 | 0.9 ft | 160 ft   |
|         |        |          |

| Point 4  | 100 ft               | 211.1475 ft           |
|----------|----------------------|-----------------------|
| Point 5  | 3.8 ft               | 183 ft                |
| Point 6  | -20.1275 ft          | 160 ft                |
| Point 7  | 100 ft               | 219.64 ft             |
| Point 8  | 42.5825 ft           | 219.8525 ft           |
| Point 9  | 40.2 ft              | 223.2 ft              |
| Point 10 | 100 ft               | 223.6 ft              |
| Point 11 | 0 ft                 | 211.7 ft              |
| Point 12 | 0 ft                 | 192 ft                |
| Point 13 | 13 ft                | 192 ft                |
| Point 14 | 24.5 ft              | 213.8 ft              |
| Point 15 | 24.5 ft              | 192 ft                |
| Point 16 | 24.5 ft              | 203 ft                |
| Point 17 | 24.5 ft              | 205 ft                |
| Point 18 | 41.8 ft              | 220.7 ft              |
| Point 19 | 26.6 ft              | 215.4 ft              |
| Point 20 | 37.9 ft              | 223.2 ft              |
| Point 21 | 6.13959 ft           | 185.3 ft              |
| Point 22 | 8.9 ft               | 192 ft                |
| Point 23 | -100 ft              | 160 ft                |
| Point 24 | -100 ft              | 170.1 ft              |
| Point 25 | -91.8 ft             | 174.4 ft              |
| Point 26 | -88.3 ft             | 176.5 ft              |
| Point 27 | -85.7 ft             | 177.8 ft              |
| Point 28 | -83.4 ft             | 178.4 ft              |
| Point 29 | -76 ft               | 178.9 ft              |
| Point 30 | -74 ft               | 179.7 ft              |
| Point 31 | -55.9 ft             | 180.2 ft              |
| Point 32 | -37.3 ft             | 182.3 ft              |
| Point 33 | -30.3 ft             | 182.9 ft              |
| Point 34 | -13.6 ft             | 190.2 ft              |
| Point 35 | 7 ft                 | 223 ft                |
| Point 36 | 15 ft                | 223 ft                |
| Point 37 | 15 ft                | 211.7 ft              |
| Point 38 | 7 ft                 | 211.7 ft              |
| Point 39 | -6 ft                | 195 ft                |
| Point 40 | -37.3275 ft          | 162.2725 ft           |
| Point 41 | -47.26 ft            | 160 ft                |
| Point 42 | -5.125 ft            | 182.98095 ft          |
| Point 43 | 80.7025 ft           | 160 ft                |
| Point 44 | -100 ft              | 129.8675 ft           |
| Point 45 | 100 ft               | 129.8675 ft           |
| Point 46 | -100 ft              | 147.8625 ft           |
| Point 47 | -100 ft<br>-27.95 ft | 152.3875 ft           |
|          |                      |                       |
| Point 48 | -100 ft<br>16.5 ft   | 133.97 ft<br>197.3 ft |
| Point 49 |                      |                       |
| Point 50 | 100 ft               | 209.9025 ft           |
| Point 51 | 95.42762 ft          | 209.80965 ft          |

|   | •        | <b>\ 1</b>  | ,            |
|---|----------|-------------|--------------|
|   | Point 52 | 3.915 ft    | 160.77581 ft |
|   | Point 53 | 17.7925 ft  | 187.09412 ft |
|   | Point 54 | 28.7 ft     | 129.8675 ft  |
|   | Point 55 | 0 ft        | 198.7 ft     |
|   | Point 56 | 47.15 ft    | 195.68393 ft |
|   | Point 57 | 42.67 ft    | 194.37311 ft |
|   | Point 58 | 0 ft        | 195 ft       |
|   | Point 59 | -32.3 ft    | 165.4 ft     |
|   | Point 60 | -16 ft      | 164.1 ft     |
|   | Point 61 | -100 ft     | 150.0525 ft  |
|   | Point 62 | 15 ft       | 218.535 ft   |
|   | Point 63 | 24 ft       | 223 ft       |
| ĺ | Point 64 | 7 ft        | 214.495 ft   |
|   | Point 65 | 1.355 ft    | 211.7 ft     |
|   | Point 66 | 25.9 ft     | 223 ft       |
|   | Point 67 | 22 ft       | 192 ft       |
|   | Point 68 | 15.0117 ft  | 208.01106 ft |
|   | Point 69 | 21.5 ft     | 192 ft       |
|   | Point 70 | 15.5 ft     | 192 ft       |
|   | Point 71 | 15.5 ft     | 211.7 ft     |
|   | Point 72 | 15.5 ft     | 194.35 ft    |
|   | Point 73 | 15.5 ft     | 197.3 ft     |
|   | Point 74 | 15.5 ft     | 208.29 ft    |
|   | Point 75 | 18.50702 ft | 197.3 ft     |
|   | Point 76 | 15.5 ft     | 196.43333 ft |
|   | Point 77 | 21.5 ft     | 211.7 ft     |
|   | Point 78 | 20 ft       | 197.3 ft     |
|   | Point 79 | 20 ft       | 192 ft       |
| ĺ | Point 80 | 21.5 ft     | 202 ft       |
| ĺ | Point 81 | 21.5 ft     | 200 ft       |
| ĺ | Point 82 | 21.5 ft     | 208.29 ft    |
| ĵ | Point 83 | 31.9 ft     | 223.1 ft     |
|   | Point 84 | 31.9 ft     | 219.08 ft    |
|   |          |             |              |

# Regions

|             | Material   | Points                          | Area                       |
|-------------|--|---------------------------------|----------------------------|
| Region<br>1 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 1,2,52,3,43                     | 1,263.5<br>ft <sup>2</sup> |
| Region<br>2 | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 52,2,50,51,56,57,53,5,60,6,47,3 | 2,656.9<br>ft <sup>2</sup> |
| Region<br>3 | Gravel Borrow  | 9,18,8,7,10                     | 214.55<br>ft <sup>2</sup>  |
| Region<br>4 | Gravel Borrow  | 38,65,11,55,68,74,71,37         | 127 ft²                    |
| Region<br>5 | ESU 2B Medium Dense Sand/Gravel                                  | 8,16,17,18                      | 31.556<br>ft <sup>2</sup>  |
| Region<br>6 | ESU 2A Very Loose to Loose<br>Sand/Gravel                        | 18,17,14,19,84,20,9             | 115.05<br>ft <sup>2</sup>  |
| Region      | Forward Compatible Wall  | 38,37,62,64                     | 38.52                      |

| 7            |   |  | ft²                        |
|--------------|---|--|----------------------------|
| Region<br>8  | Lightweight EPS                           | 14,19,84,83,66,63,62,37,71,77                            | 132.58<br>ft <sup>2</sup>  |
| Region<br>9  | ESU 2B Medium Dense Sand/Gravel           | 22,42,59,40,60,5,21,13                                   | 332.37<br>ft <sup>2</sup>  |
| Region<br>10 | ESU 4B Dense to Very Dense<br>Sand/Gravel | 44,54,45,1,43,3,47,48                                    | 4,704.7<br>ft <sup>2</sup> |
| Region<br>11 | ESU 2B Medium Dense Sand/Gravel           | 41,46,48,47,6,60,40                                      | 992.46<br>ft <sup>2</sup>  |
| Region<br>12 | ESU 4B Dense to Very Dense<br>Sand/Gravel | 56,51,50,4,7,8,16,15,67,69,79,70,13,21,5,53,57           | 1,417.8<br>ft <sup>2</sup> |
| Region<br>13 | ESU 2A Very Loose to Loose<br>Sand/Gravel | 34,33,32,31,30,29,28,27,26,25,24,23,40,59,42,22,12,58,39 | 1,656.2<br>ft <sup>2</sup> |
| Region<br>14 | ESU 2A Very Loose to Loose<br>Sand/Gravel | 40,23,61,46,41   | 379.99<br>ft <sup>2</sup>  |
| Region<br>15 | Lightweight EPS                           | 63,36,62   | 20.093<br>ft <sup>2</sup>  |
| Region<br>16 | Forward Compatible Wall                   | 36,35,64,62  | 51.88<br>ft <sup>2</sup>   |
| Region<br>17 |   | 64,65,38   | 7.8889<br>ft <sup>2</sup>  |
| Region<br>18 | ESU 4B Dense to Very Dense<br>Sand/Gravel | 15,16,81,69,67   | 28.5 ft <sup>2</sup>       |
| Region<br>19 | Gravel Borrow                             | 72,76,22,13  | 11.692<br>ft <sup>2</sup>  |
| Region<br>20 | Gravel Borrow                             | 70,72,13   | 2.9375<br>ft <sup>2</sup>  |
| Region<br>21 | Gravel Borrow                             | 70,79,78,75,72   | 19.415<br>ft <sup>2</sup>  |
| Region<br>22 | Gravel Borrow                             | 81,75,78,79,69   | 11.991<br>ft <sup>2</sup>  |
| Region<br>23 | Gravel Borrow                             | 49,75,81,80  | 7.7095<br>ft <sup>2</sup>  |
| Region<br>24 | Gravel Borrow                             | 49,76,72,75  | 4.002<br>ft <sup>2</sup>   |
| Region<br>25 | Gravel Borrow                             | 73,76,49   | 0.43333<br>ft <sup>2</sup> |
| Region<br>26 | Gravel Borrow                             | 76,73,74,68,55,58,12,22                                  | 163.72<br>ft <sup>2</sup>  |
| Region<br>27 | ESU 2B Medium Dense Sand/Gravel           | 80,81,16,17  | 6 ft²                      |
| Region<br>28 | Gravel Borrow                             | 74,82,77   | 10.23<br>ft <sup>2</sup>   |
| Region<br>29 | Gravel Borrow                             | 77,71,74   | 10.23<br>ft <sup>2</sup>   |
| Region 30    | ESU 2A Very Loose to Loose<br>Sand/Gravel | 77,82,80,17,14   | 27.75<br>ft <sup>2</sup>   |
| Region<br>31 | Gravel Borrow                             | 73,49,80,82,74   | 54.19<br>ft <sup>2</sup>   |
| Region 32    | Common Borrow                             | 20,83,84   | 12.06<br>ft <sup>2</sup>   |
| Region       |   | 55,39,58   | 11.1 ft <sup>2</sup>       |

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# **Slip Results**

Slip Surfaces Analysed: 6769 of 11466 converged

# **Current Slip Surface**

Slip Surface: 1,107 Factor of Safety: 1.3 Volume: 1,073.6112 ft<sup>3</sup> Weight: 111,807.65 lbf

Resisting Moment: 4,586,543.7 lbf·ft Activating Moment: 3,447,161.1 lbf·ft

Resisting Force: 61,881.24 lbf Activating Force: 46,517.32 lbf Slip Rank: 1 of 11,466 slip surfaces Exit: (-40.78762, 181.90624) ft Entry: (34.999735, 223.15166) ft

Radius: 62.096408 ft

Center: (-24.243501, 241.75819) ft

### **Slip Slices**

|            | X                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material                                |
|------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|--|
| Slice<br>1 | -39.04381<br>ft  | 181.47809<br>ft | -184.62609<br>psf | 126.77147<br>psf         | 79.215604<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>2 | -36.133333<br>ft | 180.8223<br>ft  | -184.06914<br>psf | 294.14797<br>psf         | 183.80405<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>3 | -33.8 ft         | 180.41291<br>ft | -182.77569<br>psf | 383.5427<br>psf          | 239.66408<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>4 | -31.466667<br>ft | 180.0945<br>ft  | -181.51734<br>psf | 448.27608<br>psf         | 280.11398<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>5 | -29.107143<br>ft | 179.86411<br>ft | -179.81086<br>psf | 558.64631<br>psf         | 349.08096<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>6 | -26.721429<br>ft | 179.72272<br>ft | -178.81296<br>psf | 707.59718<br>psf         | 442.15579<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>7 | -24.335714<br>ft | 179.67331<br>ft | -179.75536<br>psf | 829.5393<br>psf          | 518.35368<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>8 | -21.95 ft        | 179.71563<br>ft | -179.27882<br>psf | 928.04363<br>psf         | 579.90602<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |

| Slice<br>9  | -19.564286<br>ft | 179.84989<br>ft | -177.12713<br>psf | 1,005.926<br>psf  | 628.57233<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
|-------------|------------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>10 | -17.178571<br>ft | 180.07667<br>ft | -181.32295<br>psf | 1,065.4365<br>psf | 665.75862<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>11 | -14.792857<br>ft | 180.39702<br>ft | -186.651<br>psf   | 1,108.3939<br>psf | 692.60138<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>12 | -12.339565<br>ft | 180.82699<br>ft | -200.67145<br>psf | 1,164.7726<br>psf | 727.8307<br>psf   | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>13 | -9.8186957<br>ft | 181.37434<br>ft | -296.88615<br>psf | 1,231.4977<br>psf | 769.52515<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>14 | -7.2791304<br>ft | 182.0388<br>ft  | -383.76897<br>psf | 1,279.8958<br>psf | 799.76769<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>15 | -5.5625 ft       | 182.54017<br>ft | -404.88014<br>psf | 1,393.8296<br>psf | 870.96139<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>16 | -3.84375 ft      | 183.12395<br>ft | -383.82621<br>psf | 1,221.322<br>psf  | 763.16669<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>17 | -1.28125 ft      | 184.07979<br>ft | -351.82381<br>psf | 1,079.6558<br>psf | 674.64383<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>18 | 0.6775 ft        | 184.88675<br>ft | -329.17673<br>psf | 2,911.4998<br>psf | 1,819.307<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>19 | 2.76625 ft       | 185.86561<br>ft | -306.5904<br>psf  | 2,671.3396<br>psf | 1,669.2382<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>20 | 5.58875 ft       | 187.32097<br>ft | -277.57173<br>psf | 2,420.9606<br>psf | 1,512.7841<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>21 | 7.95 ft          | 188.67045<br>ft | -254.88611<br>psf | 3,320.8837<br>psf | 2,075.1184<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>22 | 8.95 ft          | 189.27817<br>ft | -245.58458<br>psf | 4,364.2179<br>psf | 2,727.066<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>23 | 9.9765041<br>ft  | 189.95485<br>ft | -236.93585<br>psf | 3,408.8056<br>psf | 2,130.0581<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>24 | 11.929512<br>ft  | 191.29995<br>ft | -220.10199<br>psf | 3,181.9857<br>psf | 1,988.3254<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>25 | 13.143619<br>ft  | 192.17917<br>ft | -209.68292<br>psf | 3,149.6607<br>psf | 2,460.7846<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>26 | 14.190611<br>ft  | 192.99631<br>ft | -199.12368<br>psf | 2,848.6766<br>psf | 2,225.6301<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>27 | 15.25 ft         | 193.84032<br>ft | -186.82298<br>psf | 1,971.9784<br>psf | 1,540.6784<br>psf | 0 psf | 0 psf | Gravel Borrow                                |

| Slice<br>28 | 16 ft           | 194.4719<br>ft  | -180.08144<br>psf | 1,715.7156<br>psf | 1,340.4639<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
|-------------|-----------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>29 | 17.50351 ft     | 195.80917<br>ft | -167.99769<br>psf | 1,533.662<br>psf  | 1,198.2281<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>30 | 18.807976<br>ft | 197.01045<br>ft | -161.36396<br>psf | 1,377.9082<br>psf | 1,076.5399<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>31 | 19.551966<br>ft | 197.7408<br>ft  | -160.21572<br>psf | 1,297.4264<br>psf | 1,013.6606<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>32 | 19.9975 ft      | 198.18414<br>ft | -162.27411<br>psf | 1,197.7547<br>psf | 935.78856<br>psf  | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>33 | 20.75 ft        | 198.97543<br>ft | -167.4718<br>psf  | 1,065.6579<br>psf | 832.58322<br>psf  | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>34 | 22.364152<br>ft | 200.74625<br>ft | -188.63507<br>psf | 786.70251<br>psf  | 733.61196<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>35 | 23.614152<br>ft | 202.19505<br>ft | -203.72234<br>psf | 784.16151<br>psf  | 489.9985<br>psf   | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>36 | 24.25 ft        | 202.97438<br>ft | -211.31843<br>psf | 748.85109<br>psf  | 467.93409<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>37 | 25.2 ft         | 204.20869<br>ft | -225.83795<br>psf | 695.23097<br>psf  | 434.42853<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>38 | 25.95 ft        | 205.19907<br>ft | -239.25229<br>psf | 653.75372<br>psf  | 408.51066<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>39 | 26.3 ft         | 205.68809<br>ft | -246.35413<br>psf | 632.98265<br>psf  | 395.53146<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>40 | 27.286631<br>ft | 207.13025<br>ft | -268.80823<br>psf | 570.22897<br>psf  | 356.31861<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>41 | 28.954947<br>ft | 209.78543<br>ft | -262.03638<br>psf | 457.07376<br>psf  | 285.61139<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>42 | 30.918316<br>ft | 213.32322<br>ft | -217.03131<br>psf | 316.93103<br>psf  | 198.04049<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>43 | 33.022443<br>ft | 217.92455<br>ft | -189.37484<br>psf | 278.7332<br>psf   | 174.17183<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>44 | 34.572311<br>ft | 221.88658<br>ft | 0 psf             | 111.00891<br>psf  | 69.366063<br>psf  | 0 psf | 0 psf | Common Borrov                                |

# 1B.2 Compound - Static FC Wall (M-P)

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### **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 652 Date: 01/17/2022 Time: 02:07:09 PM

Tool Version: 11.1.1.22085

Last Solved Date: 01/17/2022 Last Solved Time: 02:30:57 PM

### **Project Settings**

Unit System: U.S. Customary Units

# **Analysis Settings**

### 1B.2 Compound - Static FC Wall (M-P)

Description: With Forward Compatible Wall

Kind: SLOPE/W

Parent: 1. Steady State (Compound) Analysis Type: Morgenstern-Price

Settings

Side Function

Interslice force function option: Half-Sine

PWP Conditions from Parent Analysis: 1. Steady State (Compound) [(last)]

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 20

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

Factor of Safety Convergence Settings

Maximum Number of Iterations: 100 Tolerable difference in F of S: 0.001

Solution Settings

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

#### **Materials**

### **ESU 2A Very Loose to Loose Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **ESU 2B Medium Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

### **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

#### **Forward Compatible Wall**

Material Model: High Strength

Unit Weight: 130 pcf

### **Lightweight EPS**

Material Model: Mohr-Coulomb

Unit Weight: 5 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 0 °

Phi-B: 0°

### Reinforcements

#### Row 1

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 6.6 °

Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 2

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 6.1 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 3

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 5.6 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 4

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 5.1 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 5

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 4.6 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 6

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 4.1 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

### Row 7 (4 straps)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 7.2 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 7,860 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 7,860 lbf/ft

### Row 8 (4 straps)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 6.2 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 7,860 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 7,860 lbf/ft

# Slip Surface Entry and Exit

Left Type: Range

Left-Zone Left Coordinate: (-45, 181.43065) ft

Left-Zone Right Coordinate: (0, 200) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15, 223) ft Right-Zone Right Coordinate: (55, 223.299) ft

Right-Zone Increment: 20 Radius Increments: 20

# **Slip Surface Limits**

Left Coordinate: (-100, 170.1) ft Right Coordinate: (100, 223.6) ft

### **Reinforcement Lines**

#### **Reinforcement Line 1**

Reinforcement: Row 1 Lock to Ground Surface: Yes Outside Point: (0, 210.5) ft Inside Point: (15.5, 210.5) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 2**

Reinforcement: Row 8 (4 straps) Lock to Ground Surface: No Outside Point: (0, 193.7) ft Inside Point: (20, 193.7) ft

Length: 20 ft
Orientation: 0 °

Slip Surface Intersection: (15.079752, 193.7) ft

Max. Pullout Force: 7,860 lbf Available Length: 4.9202484 ft Required Length: 4.9202484 ft Pullout Force: 3,010.1026 lbf

Pullout Force per Length: 611.77858 lbf/ft Governing Component: Pullout Resistance

#### **Reinforcement Line 3**

Reinforcement: Row 6 Lock to Ground Surface: Yes Outside Point: (0, 198.5) ft Inside Point: (15.5, 198.5) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 4**

Reinforcement: Row 2 Lock to Ground Surface: Yes Outside Point: (0, 208.1) ft Inside Point: (15.5, 208.1) ft

Length: 15.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 5**

Reinforcement: Row 5 Lock to Ground Surface: Yes Outside Point: (0, 200.9) ft Inside Point: (15.5, 200.9) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 6**

Reinforcement: Row 4 Lock to Ground Surface: Yes Outside Point: (0, 203.3) ft Inside Point: (15.5, 203.3) ft

Length: 15.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 7**

Reinforcement: Row 3 Lock to Ground Surface: Yes Outside Point: (0, 205.7) ft Inside Point: (15.5, 205.7) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 8**

Reinforcement: Row 7 (4 straps) Lock to Ground Surface: Yes Outside Point: (0, 196.1) ft Inside Point: (20, 196.1) ft

Length: 20 ft
Orientation: 0 °

Slip Surface Intersection: (17.823618, 196.1) ft

Max. Pullout Force: 7,860 lbf Available Length: 2.1763818 ft Required Length: 2.1763818 ft Pullout Force: 1,407.5924 lbf

Pullout Force per Length: 646.75803 lbf/ft Governing Component: Pullout Resistance

# **Surcharge Loads**

### **Surcharge Load 1**

Surcharge (Unit Weight): 250 pcf

Direction: Vertical

#### Coordinates

| X         | Υ         |
|-----------|-----------|
| 9 ft      | 224.75 ft |
| 19.995 ft | 224.75 ft |
| 20 ft     | 224 ft    |
| 26 ft     | 224 ft    |
| 40.2 ft   | 224.2 ft  |
| 100 ft    | 224.6 ft  |

### Geometry

Name: Default Geometry

# Settings

View: 2D

Element Thickness: 1 ft

### **Points**

|         | X      | Y        |
|---------|--------|----------|
| Point 1 | 100 ft | 160 ft   |
| Point 2 | 100 ft | 185.5 ft |
|         |        |          |

| Point 3    | 0.9 ft      | 160 ft       |
|------------|-------------|--------------|
| Point 4    | 100 ft      | 211.1475 ft  |
| Point 5    | 3.8 ft      | 183 ft       |
| Point 6    | -20.1275 ft | 160 ft       |
| Point 7    | 100 ft      | 219.64 ft    |
| Point 8    | 42.5825 ft  | 219.8525 ft  |
| Point 9    | 40.2 ft     | 223.2 ft     |
| Point 10   | 100 ft      | 223.6 ft     |
| Point 11   | 0 ft        | 211.7 ft     |
| Point 12   | 0 ft        | 192 ft       |
| Point 13   | 13 ft       | 192 ft       |
| Point 14   | 24.5 ft     | 213.8 ft     |
| Point 15   | 24.5 ft     | 192 ft       |
| Point 16   | 24.5 ft     | 203 ft       |
| Point 17   | 24.5 ft     | 205 ft       |
| Point 18   | 41.8 ft     | 220.7 ft     |
| Point 19   | 26.6 ft     | 215.4 ft     |
| Point 20   | 37.9 ft     | 223.2 ft     |
| Point 21   | 6.13959 ft  | 185.3 ft     |
| Point 22   | 8.9 ft      | 192 ft       |
| Point 23   | -100 ft     | 160 ft       |
| Point 24   | -100 ft     | 170.1 ft     |
| Point 25   | -91.8 ft    | 174.4 ft     |
| Point 26   | -88.3 ft    | 176.5 ft     |
| Point 27   | -85.7 ft    | 177.8 ft     |
| Point 28   | -83.4 ft    | 178.4 ft     |
| Point 29   | -76 ft      | 178.9 ft     |
| Point 30   | -74 ft      | 179.7 ft     |
| Point 31   | -55.9 ft    | 180.2 ft     |
| Point 32   | -37.3 ft    | 182.3 ft     |
| Point 33   | -30.3 ft    | 182.9 ft     |
| Point 34   | -13.6 ft    | 190.2 ft     |
| Point 35   | 7 ft        | 223 ft       |
| Point 36   | 15 ft       | 223 ft       |
| Point 37   | 15 ft       | 211.7 ft     |
| Point 38   | 7 ft        | 211.7 ft     |
| Point 39   | -6 ft       | 195 ft       |
| Point 40   | -37.3275 ft | 162.2725 ft  |
| Point 41   | -47.26 ft   | 160 ft       |
| Point 42   | -5.125 ft   | 182.98095 ft |
| Point 43   | 80.7025 ft  | 160 ft       |
| Point 44   | -100 ft     | 129.8675 ft  |
| Point 45   | 100 ft      | 129.8675 ft  |
| Point 46   | -100 ft     | 147.8625 ft  |
| Point 47   | -27.95 ft   | 152.3875 ft  |
| Point 48   | -100 ft     | 133.97 ft    |
| Point 49   | 16.5 ft     | 197.3 ft     |
| Point 50   | 10.5 ft     | 209.9025 ft  |
| 1 01110 00 | 10010       | 203.302310   |

| 1        | ,           |              |
|----------|-------------|--------------|
| Point 51 | 95.42762 ft | 209.80965 ft |
| Point 52 | 3.915 ft    | 160.77581 ft |
| Point 53 | 17.7925 ft  | 187.09412 ft |
| Point 54 | 28.7 ft     | 129.8675 ft  |
| Point 55 | 0 ft        | 198.7 ft     |
| Point 56 | 47.15 ft    | 195.68393 ft |
| Point 57 | 42.67 ft    | 194.37311 ft |
| Point 58 | 0 ft        | 195 ft       |
| Point 59 | -32.3 ft    | 165.4 ft     |
| Point 60 | -16 ft      | 164.1 ft     |
| Point 61 | -100 ft     | 150.0525 ft  |
| Point 62 | 15 ft       | 218.535 ft   |
| Point 63 | 24 ft       | 223 ft       |
| Point 64 | 7 ft        | 214.495 ft   |
| Point 65 | 1.355 ft    | 211.7 ft     |
| Point 66 | 25.9 ft     | 223 ft       |
| Point 67 | 22 ft       | 192 ft       |
| Point 68 | 15.0117 ft  | 208.01106 ft |
| Point 69 | 21.5 ft     | 192 ft       |
| Point 70 | 15.5 ft     | 192 ft       |
| Point 71 | 15.5 ft     | 211.7 ft     |
| Point 72 | 15.5 ft     | 194.35 ft    |
| Point 73 | 15.5 ft     | 197.3 ft     |
| Point 74 | 15.5 ft     | 208.29 ft    |
| Point 75 | 18.50702 ft | 197.3 ft     |
| Point 76 | 15.5 ft     | 196.43333 ft |
| Point 77 | 21.5 ft     | 211.7 ft     |
| Point 78 | 20 ft       | 197.3 ft     |
| Point 79 | 20 ft       | 192 ft       |
| Point 80 | 21.5 ft     | 202 ft       |
| Point 81 | 21.5 ft     | 200 ft       |
| Point 82 | 21.5 ft     | 208.29 ft    |
| Point 83 | 31.9 ft     | 223.1 ft     |
| Point 84 | 31.9 ft     | 219.08 ft    |
|          |             |              |

# Regions

|             | Material   | Points                          | Area                       |
|-------------|--|---------------------------------|----------------------------|
| Region<br>1 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 1,2,52,3,43                     | 1,263.5<br>ft <sup>2</sup> |
| Region<br>2 | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 52,2,50,51,56,57,53,5,60,6,47,3 | 2,656.9<br>ft <sup>2</sup> |
| Region<br>3 | Gravel Borrow  | 9,18,8,7,10                     | 214.55<br>ft <sup>2</sup>  |
| Region<br>4 | Gravel Borrow  | 38,65,11,55,68,74,71,37         | 127 ft²                    |
| Region<br>5 | ESU 2B Medium Dense Sand/Gravel                                  | 8,16,17,18                      | 31.556<br>ft <sup>2</sup>  |
| Region<br>6 | ESU 2A Very Loose to Loose<br>Sand/Gravel                        | 18,17,14,19,84,20,9             | 115.05<br>ft <sup>2</sup>  |
|             |  |                                 |                            |

| Region<br>7  | Forward Compatible Wall                   | 38,37,62,64  | 38.52<br>ft <sup>2</sup>   |
|--------------|---|--|----------------------------|
| Region<br>8  | Lightweight EPS                           | 14,19,84,83,66,63,62,37,71,77                            | 132.58<br>ft <sup>2</sup>  |
| Region<br>9  | ESU 2B Medium Dense Sand/Gravel           | 22,42,59,40,60,5,21,13                                   | 332.37<br>ft <sup>2</sup>  |
| Region<br>10 | ESU 4B Dense to Very Dense<br>Sand/Gravel | 44,54,45,1,43,3,47,48                                    | 4,704.7<br>ft <sup>2</sup> |
| Region<br>11 | ESU 2B Medium Dense Sand/Gravel           | 41,46,48,47,6,60,40                                      | 992.46<br>ft <sup>2</sup>  |
| Region<br>12 | ESU 4B Dense to Very Dense<br>Sand/Gravel | 56,51,50,4,7,8,16,15,67,69,79,70,13,21,5,53,57           | 1,417.8<br>ft <sup>2</sup> |
| Region<br>13 | ESU 2A Very Loose to Loose<br>Sand/Gravel | 34,33,32,31,30,29,28,27,26,25,24,23,40,59,42,22,12,58,39 | 1,656.2<br>ft <sup>2</sup> |
| Region<br>14 | ESU 2A Very Loose to Loose<br>Sand/Gravel | 40,23,61,46,41   | 379.99<br>ft <sup>2</sup>  |
| Region<br>15 | Lightweight EPS                           | 63,36,62   | 20.093<br>ft <sup>2</sup>  |
| Region<br>16 | Forward Compatible Wall                   | 36,35,64,62  | 51.88<br>ft²               |
| Region<br>17 |   | 64,65,38   | 7.8889<br>ft <sup>2</sup>  |
| Region<br>18 | ESU 4B Dense to Very Dense<br>Sand/Gravel | 15,16,81,69,67   | 28.5 ft <sup>2</sup>       |
| Region<br>19 | Gravel Borrow                             | 72,76,22,13  | 11.692<br>ft <sup>2</sup>  |
| Region<br>20 | Gravel Borrow                             | 70,72,13   | 2.9375<br>ft <sup>2</sup>  |
| Region<br>21 | Gravel Borrow                             | 70,79,78,75,72   | 19.415<br>ft <sup>2</sup>  |
| Region<br>22 | Gravel Borrow                             | 81,75,78,79,69   | 11.991<br>ft²              |
| Region<br>23 | Gravel Borrow                             | 49,75,81,80  | 7.7095<br>ft <sup>2</sup>  |
| Region<br>24 | Gravel Borrow                             | 49,76,72,75  | 4.002<br>ft <sup>2</sup>   |
| Region<br>25 | Gravel Borrow                             | 73,76,49   | 0.43333<br>ft <sup>2</sup> |
| Region<br>26 | Gravel Borrow                             | 76,73,74,68,55,58,12,22                                  | 163.72<br>ft²              |
| Region<br>27 | ESU 2B Medium Dense Sand/Gravel           | 80,81,16,17  | 6 ft²                      |
| Region<br>28 | Gravel Borrow                             | 74,82,77   | 10.23<br>ft²               |
| Region<br>29 | Gravel Borrow                             | 77,71,74   | 10.23<br>ft²               |
| Region<br>30 | ESU 2A Very Loose to Loose<br>Sand/Gravel | 77,82,80,17,14   | 27.75<br>ft <sup>2</sup>   |
| Region<br>31 | Gravel Borrow                             | 73,49,80,82,74   | 54.19<br>ft <sup>2</sup>   |
| Region<br>32 | Common Borrow                             | 20,83,84   | 12.06<br>ft <sup>2</sup>   |

Region 33 55,39,58 11.1 ft<sup>2</sup>

# **Slip Results**

Slip Surfaces Analysed: 8873 of 11466 converged

# **Current Slip Surface**

Slip Surface: 1,107 Factor of Safety: 1.3 Volume: 1,073.6112 ft<sup>3</sup> Weight: 111,807.65 lbf

Resisting Moment: 4,583,873.8 lbf·ft Activating Moment: 3,447,161.1 lbf·ft

Resisting Force: 61,795.166 lbf Activating Force: 46,487.672 lbf Slip Rank: 1 of 11,466 slip surfaces Exit: (-40.78762, 181.90624) ft Entry: (34.999735, 223.15166) ft

Radius: 62.096408 ft

Center: (-24.243501, 241.75819) ft

### **Slip Slices**

|            | Х                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material                                |
|------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|--|
| Slice<br>1 | -39.04381<br>ft  | 181.47809<br>ft | -184.62609<br>psf | 83.846124<br>psf         | 52.392873<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>2 | -36.133333<br>ft | 180.8223<br>ft  | -184.06914<br>psf | 221.22597<br>psf         | 138.23733<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>3 | -33.8 ft         | 180.41291<br>ft | -182.77569<br>psf | 319.29972<br>psf         | 199.52061<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>4 | -31.466667<br>ft | 180.0945<br>ft  | -181.51734<br>psf | 407.89652<br>psf         | 254.88204<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>5 | -29.107143<br>ft | 179.86411<br>ft | -179.81086<br>psf | 542.67243<br>psf         | 339.09937<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>6 | -26.721429<br>ft | 179.72272<br>ft | -178.81296<br>psf | 721.15928<br>psf         | 450.63033<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>7 | -24.335714<br>ft | 179.67331<br>ft | -179.75536<br>psf | 880.05631<br>psf         | 549.92022<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>8 | -21.95 ft        | 179.71563<br>ft | -179.27882<br>psf | 1,014.1903<br>psf        | 633.73644<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |

| Slice<br>9  | -19.564286<br>ft | 179.84989<br>ft | -177.12713<br>psf | 1,120.0786<br>psf | 699.90278<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
|-------------|------------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>10 | -17.178571<br>ft | 180.07667<br>ft | -181.32295<br>psf | 1,196.1905<br>psf | 747.46279<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>11 | -14.792857<br>ft | 180.39702<br>ft | -186.651<br>psf   | 1,242.8981<br>psf | 776.64891<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>12 | -12.339565<br>ft | 180.82699<br>ft | -200.67145<br>psf | 1,291.1263<br>psf | 806.78526<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>13 | -9.8186957<br>ft | 181.37434<br>ft | -296.88615<br>psf | 1,338.8829<br>psf | 836.62688<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>14 | -7.2791304<br>ft | 182.0388<br>ft  | -383.76897<br>psf | 1,358.9767<br>psf | 849.18291<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>15 | -5.5625 ft       | 182.54017<br>ft | -404.88014<br>psf | 1,488.9709<br>psf | 930.41231<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>16 | -3.84375 ft      | 183.12395<br>ft | -383.82621<br>psf | 1,264.2751<br>psf | 790.00675<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>17 | -1.28125 ft      | 184.07979<br>ft | -351.82381<br>psf | 1,083.1659<br>psf | 676.8372<br>psf   | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>18 | 0.6775 ft        | 184.88675<br>ft | -329.17673<br>psf | 2,913.4691<br>psf | 1,820.5375<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>19 | 2.76625 ft       | 185.86561<br>ft | -306.5904<br>psf  | 2,618.8727<br>psf | 1,636.4533<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>20 | 5.58875 ft       | 187.32097<br>ft | -277.57173<br>psf | 2,328.5567<br>psf | 1,455.0437<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>21 | 7.95 ft          | 188.67045<br>ft | -254.88611<br>psf | 3,201.6566<br>psf | 2,000.6171<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>22 | 8.95 ft          | 189.27817<br>ft | -245.58458<br>psf | 4,404.3023<br>psf | 2,752.1135<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>23 | 9.9765041<br>ft  | 189.95485<br>ft | -236.93585<br>psf | 3,276.9863<br>psf | 2,047.6883<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>24 | 11.929512<br>ft  | 191.29995<br>ft | -220.10199<br>psf | 3,056.3477<br>psf | 1,909.818<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>25 | 13.143619<br>ft  | 192.17917<br>ft | -209.68292<br>psf | 3,041.9259<br>psf | 2,376.613<br>psf  | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>26 | 14.190611<br>ft  | 192.99631<br>ft | -199.12368<br>psf | 2,738.5435<br>psf | 2,139.5846<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>27 | 15.25 ft         | 193.84032<br>ft | -186.82298<br>psf | 1,857.3307<br>psf | 1,451.1058<br>psf | 0 psf | 0 psf | Gravel Borrow                                |

| Slice<br>28 | 16 ft           | 194.4719<br>ft  | -180.08144<br>psf | 1,610.4596<br>psf | 1,258.2289<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
|-------------|-----------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>29 | 17.50351 ft     | 195.80917<br>ft | -167.99769<br>psf | 1,441.0569<br>psf | 1,125.877<br>psf  | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>30 | 18.807976<br>ft | 197.01045<br>ft | -161.36396<br>psf | 1,300.0862<br>psf | 1,015.7386<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>31 | 19.551966<br>ft | 197.7408<br>ft  | -160.21572<br>psf | 1,228.0258<br>psf | 959.43888<br>psf  | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>32 | 19.9975 ft      | 198.18414<br>ft | -162.27411<br>psf | 1,132.0399<br>psf | 884.44648<br>psf  | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>33 | 20.75 ft        | 198.97543<br>ft | -167.4718<br>psf  | 1,006.4714<br>psf | 786.34161<br>psf  | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>34 | 22.364152<br>ft | 200.74625<br>ft | -188.63507<br>psf | 731.76451<br>psf  | 682.38145<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>35 | 23.614152<br>ft | 202.19505<br>ft | -203.72234<br>psf | 759.75519<br>psf  | 474.74773<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>36 | 24.25 ft        | 202.97438<br>ft | -211.31843<br>psf | 733.50194<br>psf  | 458.34288<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>37 | 25.2 ft         | 204.20869<br>ft | -225.83795<br>psf | 693.60486<br>psf  | 433.41242<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>38 | 25.95 ft        | 205.19907<br>ft | -239.25229<br>psf | 662.78482<br>psf  | 414.15392<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>39 | 26.3 ft         | 205.68809<br>ft | -246.35413<br>psf | 646.86418<br>psf  | 404.2056<br>psf   | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>40 | 27.286631<br>ft | 207.13025<br>ft | -268.80823<br>psf | 596.77214<br>psf  | 372.90462<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>41 | 28.954947<br>ft | 209.78543<br>ft | -262.03638<br>psf | 500.78421<br>psf  | 312.92471<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>42 | 30.918316<br>ft | 213.32322<br>ft | -217.03131<br>psf | 370.18618<br>psf  | 231.318<br>psf    | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>43 | 33.022443<br>ft | 217.92455<br>ft | -189.37484<br>psf | 367.90396<br>psf  | 229.89191<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>44 | 34.572311<br>ft | 221.88658<br>ft | 0 psf             | 161.5197<br>psf   | 100.92871<br>psf  | 0 psf | 0 psf | Common Borrow                                |

# 1B.3 Compound - Pseudo-Static FC Wall (Spencer)

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### **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 652 Date: 01/17/2022 Time: 02:07:09 PM

Tool Version: 11.1.1.22085

File Name: Wall 05.85L-A - Sta 1+90 - (lightweight fill).gsz Directory: P:\0\0180366\01\Analysis\Wall 05.85L-A\22-01-17\

Last Solved Date: 01/17/2022 Last Solved Time: 02:34:36 PM

### **Project Settings**

Unit System: U.S. Customary Units

# **Analysis Settings**

### 1B.3 Compound - Pseudo-Static FC Wall (Spencer)

Description: With Forward Compatible Wall

Kind: SLOPE/W

Parent: 1. Steady State (Compound)

Analysis Type: Spencer

Settings

PWP Conditions from Parent Analysis: 1. Steady State (Compound) [(last)]

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 20

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

Factor of Safety Convergence Settings

Maximum Number of Iterations: 100

Tolerable difference in F of S: 0.001

Solution Settings

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3 Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

#### **Materials**

### **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

### **ESU 2A Very Loose to Loose Sand/Gravel (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 100 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

## **ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf

Effective Cohesion: 200 psf Effective Friction Angle: 32°

Phi-B: 0°

#### **Forward Compatible Wall**

Material Model: High Strength

Unit Weight: 130 pcf

### **Lightweight EPS**

Material Model: Mohr-Coulomb

Unit Weight: 5 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 0 °

Phi-B: 0°

### Reinforcements

### Row 1 (EQ)

Type: Geosynthetic

Interface Adhesion: 0 psf Interface Shear Angle: 8.8 °

Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

### Row 2 (EQ)

Type: Geosynthetic

Interface Adhesion: 0 psf

Interface Shear Angle: 8.1 °

Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

### Row 3 (EQ)

Type: Geosynthetic

Interface Adhesion: 0 psf Interface Shear Angle: 7.4 °

Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

### Row 4 (EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 6.8 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

### Row 5 (EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 6.1 °

Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

### Row 6 (EQ)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 5.5 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

### Row 7 (4 straps)(EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 9.5 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 10,480 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 10,480 lbf/ft

### Row 8 (4 straps)(EQ)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 8.2 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 10,480 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 10,480 lbf/ft

## Slip Surface Entry and Exit

Left Type: Range

Left-Zone Left Coordinate: (-45, 181.43065) ft

Left-Zone Right Coordinate: (0, 200) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15, 223) ft Right-Zone Right Coordinate: (55, 223.299) ft

Right-Zone Increment: 20 Radius Increments: 20

### **Slip Surface Limits**

Left Coordinate: (-100, 170.1) ft Right Coordinate: (100, 223.6) ft

### **Seismic Coefficients**

Horz Seismic Coef.: 0.193

### **Reinforcement Lines**

#### **Reinforcement Line 1**

Reinforcement: Row 1 (EQ) Lock to Ground Surface: Yes Outside Point: (0, 210.5) ft Inside Point: (15.5, 210.5) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 2**

Reinforcement: Row 8 (4 straps)(EQ)

Lock to Ground Surface: No Outside Point: (0, 193.7) ft Inside Point: (19.6, 193.7) ft

Length: 19.6 ft Orientation: 0 °

Slip Surface Intersection: (16.246848, 193.7) ft

Max. Pullout Force: 10,480 lbf Available Length: 3.3531516 ft Required Length: 3.3531516 ft Pullout Force: 2,454.1915 lbf

Pullout Force per Length: 731.90591 lbf/ft Governing Component: Pullout Resistance

#### **Reinforcement Line 3**

Reinforcement: Row 6 (EQ) Lock to Ground Surface: Yes Outside Point: (0, 198.5) ft Inside Point: (15.5, 198.5) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 4**

Reinforcement: Row 2 (EQ) Lock to Ground Surface: Yes Outside Point: (0, 208.1) ft Inside Point: (15.5, 208.1) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 5**

Reinforcement: Row 5 (EQ) Lock to Ground Surface: Yes Outside Point: (0, 200.9) ft Inside Point: (15.5, 200.9) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 6**

Reinforcement: Row 4 (EQ) Lock to Ground Surface: Yes Outside Point: (0, 203.3) ft Inside Point: (15.5, 203.3) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 7**

Reinforcement: Row 3 (EQ) Lock to Ground Surface: Yes Outside Point: (0, 205.7) ft Inside Point: (15.5, 205.7) ft

Length: 15.5 ft
Orientation: 0°

#### 1B.3 Compound - Pseudo-Static FC Wall (Spencer)

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 8**

Reinforcement: Row 7 (4 straps)(EQ)

Lock to Ground Surface: Yes Outside Point: (0, 196.1) ft Inside Point: (19.6, 196.1) ft

Length: 19.6 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

# **Surcharge Loads**

### **Surcharge Load 1**

Surcharge (Unit Weight): 125 pcf

Direction: Vertical

#### **Coordinates**

| X       | Υ        |
|---------|----------|
| 9 ft    | 224 ft   |
| 26 ft   | 224 ft   |
| 39.4 ft | 224.2 ft |
| 40.2 ft | 224.2 ft |
| 100 ft  | 224.6 ft |

### Geometry

Name: Default Geometry

### **Settings**

View: 2D

Element Thickness: 1 ft

#### **Points**

|         | X      | Y      |
|---------|--------|--------|
| Point 1 | 100 ft | 160 ft |
|         |        |        |

| •                    |                    | . •                  |
|----------------------|--------------------|----------------------|
| Point 2              | 100 ft             | 185.5 ft             |
| Point 3              | 0.9 ft             | 160 ft               |
| Point 4              | 100 ft             | 211.1475 ft          |
| Point 5              | 3.8 ft             | 183 ft               |
| Point 6              | -20.1275 ft        | 160 ft               |
| Point 7              | 100 ft             | 219.64 ft            |
| Point 8              | 42.5825 ft         | 219.8525 ft          |
| Point 9              | 40.2 ft            | 223.2 ft             |
| Point 10             | 100 ft             | 223.6 ft             |
| Point 11             | 0 ft               | 211.7 ft             |
| Point 12             | O ft               | 192 ft               |
| Point 13             | 13 ft              | 192 ft               |
| Point 14             | 24.5 ft            | 213.8 ft             |
| Point 15             | 24.5 ft            | 192 ft               |
| Point 16             | 24.5 ft            | 203 ft               |
| Point 17             | 24.5 ft            | 205 ft               |
| Point 18             | 41.8 ft            | 220.7 ft             |
| Point 19             | 26.6 ft            | 215.4 ft             |
| Point 20             | 37.9 ft            | 223.2 ft             |
| Point 21             | 6.13959 ft         | 185.3 ft             |
| Point 22             | 8.9 ft             | 192 ft               |
| Point 23             | -100 ft            | 160 ft               |
| Point 24             | -100 ft            | 170.1 ft             |
| Point 25             | -91.8 ft           | 170.1 ft<br>174.4 ft |
|                      |                    | 174.4 ft<br>176.5 ft |
| Point 26             | -88.3 ft           |                      |
| Point 27             | -85.7 ft           | 177.8 ft             |
| Point 28<br>Point 29 | -83.4 ft<br>-76 ft | 178.4 ft<br>178.9 ft |
| Point 29 Point 30    |                    |                      |
|                      | -74 ft             | 179.7 ft             |
| Point 31             | -55.9 ft           | 180.2 ft             |
| Point 32             | -37.3 ft           | 182.3 ft             |
| Point 33             | -30.3 ft           | 182.9 ft             |
| Point 34             | -13.6 ft           | 190.2 ft             |
| Point 35             | 7 ft               | 223 ft               |
| Point 36             | 15 ft              | 223 ft               |
| Point 37             | 15 ft              | 211.7 ft             |
| Point 38             | 7 ft               | 211.7 ft             |
| Point 39             | -6 ft              | 195 ft               |
| Point 40             | -37.3275 ft        | 162.2725 ft          |
| Point 41             | -47.26 ft          | 160 ft               |
| Point 42             | -5.125 ft          | 182.98095 ft         |
| Point 43             | 80.7025 ft         | 160 ft               |
| Point 44             | -100 ft            | 129.8675 ft          |
| Point 45             | 100 ft             | 129.8675 ft          |
| Point 46             | -100 ft            | 147.8625 ft          |
| Point 47             | -27.95 ft          | 152.3875 ft          |
| Point 48             | -100 ft            | 133.97 ft            |
| 1 01110 10           | 10010              | 200107.10            |

| Point 50 | 100 ft      | 209.9025 ft  |  |
|----------|-------------|--------------|--|
| Point 51 | 95.42762 ft | 209.80965 ft |  |
| Point 52 | 3.915 ft    | 160.77581 ft |  |
| Point 53 | 17.7925 ft  | 187.09412 ft |  |
| Point 54 | 28.7 ft     | 129.8675 ft  |  |
| Point 55 | 0 ft        | 198.7 ft     |  |
| Point 56 | 47.15 ft    | 195.68393 ft |  |
| Point 57 | 42.67 ft    | 194.37311 ft |  |
| Point 58 | 0 ft        | 195 ft       |  |
| Point 59 | -32.3 ft    | 165.4 ft     |  |
| Point 60 | -16 ft      | 164.1 ft     |  |
| Point 61 | -100 ft     | 150.0525 ft  |  |
| Point 62 | 15 ft       | 218.535 ft   |  |
| Point 63 | 24 ft       | 223 ft       |  |
| Point 64 | 7 ft        | 214.495 ft   |  |
| Point 65 | 1.355 ft    | 211.7 ft     |  |
| Point 66 | 25.9 ft     | 223 ft       |  |
| Point 67 | 22 ft       | 192 ft       |  |
| Point 68 | 15.0117 ft  | 208.01106 ft |  |
| Point 69 | 21.5 ft     | 192 ft       |  |
| Point 70 | 15.5 ft     | 192 ft       |  |
| Point 71 | 15.5 ft     | 211.7 ft     |  |
| Point 72 | 15.5 ft     | 194.35 ft    |  |
| Point 73 | 15.5 ft     | 197.3 ft     |  |
| Point 74 | 15.5 ft     | 208.29 ft    |  |
| Point 75 | 18.50702 ft | 197.3 ft     |  |
| Point 76 | 15.5 ft     | 196.43333 ft |  |
| Point 77 | 21.5 ft     | 211.7 ft     |  |
| Point 78 | 20 ft       | 197.3 ft     |  |
| Point 79 | 20 ft       | 192 ft       |  |
| Point 80 | 21.5 ft     | 202 ft       |  |
| Point 81 | 21.5 ft     | 200 ft       |  |
| Point 82 | 21.5 ft     | 208.29 ft    |  |
| Point 83 | 31.9 ft     | 223.1 ft     |  |
| Point 84 | 31.9 ft     | 219.08 ft    |  |

# Regions

|             | Material  | Points                          | Area                       |
|-------------|---|---------------------------------|----------------------------|
| Region<br>1 | ESU 4B Dense to Very Dense<br>Sand/Gravel                           | 1,2,52,3,43                     | 1,263.5<br>ft <sup>2</sup> |
| Region 2    | ESU 5B Very Stiff to Hard Silt and<br>Clay/Dense to Very Dense Silt | 52,2,50,51,56,57,53,5,60,6,47,3 | 2,656.9<br>ft <sup>2</sup> |
| Region 3    | Gravel Borrow   | 9,18,8,7,10                     | 214.55<br>ft <sup>2</sup>  |
| Region<br>4 | Gravel Borrow   | 38,65,11,55,68,74,71,37         | 127 ft²                    |
| Region<br>5 | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                 | 8,16,17,18                      | 31.556<br>ft <sup>2</sup>  |
| Region      | ESU 2A Very Loose to Loose  | 18,17,14,19,84,20,9             | 115.05                     |

| 6            | Sand/Gravel (Apparent Cohesion)                               |  | ft²                        |
|--------------|---|--|----------------------------|
| Region<br>7  | Forward Compatible Wall                                       | 38,37,62,64  | 38.52<br>ft <sup>2</sup>   |
| Region<br>8  | Lightweight EPS   | 14,19,84,83,66,63,62,37,71,77                            | 132.58<br>ft <sup>2</sup>  |
| Region<br>9  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)           | 22,42,59,40,60,5,21,13                                   | 332.37<br>ft <sup>2</sup>  |
| Region<br>10 | ESU 4B Dense to Very Dense<br>Sand/Gravel                     | 44,54,45,1,43,3,47,48                                    | 4,704.7<br>ft <sup>2</sup> |
| Region<br>11 | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)           | 41,46,48,47,6,60,40                                      | 992.46<br>ft <sup>2</sup>  |
| Region<br>12 | ESU 4B Dense to Very Dense<br>Sand/Gravel                     | 56,51,50,4,7,8,16,15,67,69,79,70,13,21,5,53,57           | 1,417.8<br>ft <sup>2</sup> |
| Region<br>13 | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion) | 34,33,32,31,30,29,28,27,26,25,24,23,40,59,42,22,12,58,39 | 1,656.2<br>ft <sup>2</sup> |
| Region<br>14 | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion) | 40,23,61,46,41   | 379.99<br>ft <sup>2</sup>  |
| Region<br>15 | Lightweight EPS   | 63,36,62   | 20.093<br>ft <sup>2</sup>  |
| Region<br>16 | Forward Compatible Wall                                       | 36,35,64,62  | 51.88<br>ft <sup>2</sup>   |
| Region<br>17 |   | 64,65,38   | 7.8889<br>ft <sup>2</sup>  |
| Region<br>18 | ESU 4B Dense to Very Dense<br>Sand/Gravel                     | 15,16,81,69,67   | 28.5 ft <sup>2</sup>       |
| Region<br>19 | Gravel Borrow   | 72,76,22,13  | 11.692<br>ft <sup>2</sup>  |
| Region<br>20 | Gravel Borrow   | 70,72,13   | 2.9375<br>ft <sup>2</sup>  |
| Region<br>21 | Gravel Borrow   | 70,79,78,75,72   | 19.415<br>ft <sup>2</sup>  |
| Region<br>22 | Gravel Borrow   | 81,75,78,79,69   | 11.991<br>ft <sup>2</sup>  |
| Region<br>23 | Gravel Borrow   | 49,75,81,80  | 7.7095<br>ft <sup>2</sup>  |
| Region<br>24 | Gravel Borrow   | 49,76,72,75  | 4.002<br>ft <sup>2</sup>   |
| Region<br>25 | Gravel Borrow   | 73,76,49   | 0.43333<br>ft <sup>2</sup> |
| Region<br>26 | Gravel Borrow   | 76,73,74,68,55,58,12,22                                  | 163.72<br>ft <sup>2</sup>  |
| Region<br>27 | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)           | 80,81,16,17  | 6 ft <sup>2</sup>          |
| Region<br>28 | Gravel Borrow   | 74,82,77   | 10.23<br>ft <sup>2</sup>   |
| Region<br>29 | Gravel Borrow   | 77,71,74   | 10.23<br>ft <sup>2</sup>   |
| Region 30    | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion) | 77,82,80,17,14   | 27.75<br>ft <sup>2</sup>   |
| Region<br>31 | Gravel Borrow   | 73,49,80,82,74   | 54.19<br>ft <sup>2</sup>   |
| Region       | Common Borrow   | 20,83,84   | 12.06                      |

| 32           |          | ft²      |
|--------------|----------|----------|
| Region<br>33 | 55,39,58 | 11.1 ft² |

# **Slip Results**

Slip Surfaces Analysed: 4977 of 11466 converged

# **Current Slip Surface**

Slip Surface: 2,992 Factor of Safety: 1.1 Volume: 1,169.6531 ft<sup>3</sup> Weight: 124,808.04 lbf

Resisting Moment: 7,325,352 lbf·ft Activating Moment: 6,497,179.6 lbf·ft

Resisting Force: 74,728.49 lbf Activating Force: 66,278.191 lbf Slip Rank: 1 of 11,466 slip surfaces Exit: (-32.349646, 182.72432) ft Entry: (46.999779, 223.24548) ft

Radius: 86.172023 ft

Center: (-26.222374, 268.67822) ft

### **Slip Slices**

| JJCJ       | Sinces           |                 |                   |                          |                        |                      |                     |  |  |
|------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|--|--|
|            | X                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material  |  |
| Slice<br>1 | -31.324823<br>ft | 182.66352<br>ft | -181.70135<br>psf | 259.35935<br>psf         | 162.06571<br>psf       | 100 psf              | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |  |
| Slice<br>2 | -28.908333<br>ft | 182.55933<br>ft | -179.7784<br>psf  | 398.30901<br>psf         | 248.89109<br>psf       | 100 psf              | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |  |
| Slice<br>3 | -26.125 ft       | 182.51749<br>ft | -178.18695<br>psf | 591.91922<br>psf         | 369.87218<br>psf       | 100 psf              | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |  |
| Slice<br>4 | -23.341667<br>ft | 182.56562<br>ft | -178.15181<br>psf | 734.27525<br>psf         | 458.8261<br>psf        | 100 psf              | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |  |
| Slice<br>5 | -20.558333<br>ft | 182.70386<br>ft | -177.22764<br>psf | 837.55954<br>psf         | 523.36529<br>psf       | 100 psf              | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel                           |  |

|             |                  |                 |                   |                   |                   |         |       | (Apparent Cohesion)  |
|-------------|------------------|-----------------|-------------------|-------------------|-------------------|---------|-------|--|
| Slice<br>6  | -17.775 ft       | 182.93265<br>ft | -176.31723<br>psf | 910.47006<br>psf  | 568.92483<br>psf  | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>7  | -14.991667<br>ft | 183.25271<br>ft | -176.12728<br>psf | 959.29551<br>psf  | 599.43437<br>psf  | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>8  | -12.333333<br>ft | 183.64255<br>ft | -174.34767<br>psf | 1,018.7807<br>psf | 636.60487<br>psf  | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>9  | -9.8 ft          | 184.09537<br>ft | -176.51643<br>psf | 1,088.0924<br>psf | 679.91562<br>psf  | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>10 | -7.2666667<br>ft | 184.62697<br>ft | -208.7245<br>psf  | 1,139.4288<br>psf | 711.99411<br>psf  | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>11 | -4.5 ft          | 185.30345<br>ft | -277.93069<br>psf | 1,154.2898<br>psf | 721.2803<br>psf   | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>12 | -1.5 ft          | 186.14356<br>ft | -334.83655<br>psf | 995.15809<br>psf  | 621.84379<br>psf  | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>13 | 0.49889422<br>ft | 186.7556<br>ft  | -361.11436<br>psf | 2,920.3769<br>psf | 1,824.8541<br>psf | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>14 | 1.1763942<br>ft  | 186.97823<br>ft | -365.92602<br>psf | 3,273.2131<br>psf | 2,045.3305<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                    |
| Slice<br>15 | 2.76625 ft       | 187.54234<br>ft | -344.39989<br>psf | 2,639.1842<br>psf | 1,649.1453<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion)        |
| Slice       | 5.58875 ft       | 188.60723       | -306.00015        | 2,394.3581        | 1,496.161         | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                                  |

| 16          |                 | ft              | psf               | psf               | psf               |         |       | (Apparent<br>Cohesion)                              |
|-------------|-----------------|-----------------|-------------------|-------------------|-------------------|---------|-------|---|
| Slice<br>17 | 7.95 ft         | 189.57831<br>ft | -274.42646<br>psf | 3,297.135<br>psf  | 2,060.2786<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion) |
| Slice<br>18 | 8.95 ft         | 190.01108<br>ft | -260.82303<br>psf | 4,810.2884<br>psf | 3,005.8018<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion) |
| Slice<br>19 | 11.048847<br>ft | 191.01672<br>ft | -234.47322<br>psf | 3,041.044<br>psf  | 1,900.2552<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion) |
| Slice<br>20 | 14.048847<br>ft | 192.50284<br>ft | -185.52003<br>psf | 2,863.6166<br>psf | 2,237.3025<br>psf | 0 psf   | 0 psf | Gravel Borrow                                       |
| Slice<br>21 | 15.25 ft        | 193.14294<br>ft | -155.93155<br>psf | 2,035.8237<br>psf | 1,590.5598<br>psf | 0 psf   | 0 psf | Gravel Borrow                                       |
| Slice<br>22 | 16 ft           | 193.56125<br>ft | -143.41807<br>psf | 1,811.6956<br>psf | 1,415.4517<br>psf | 0 psf   | 0 psf | Gravel Borrow                                       |
| Slice<br>23 | 17.50351 ft     | 194.4333<br>ft  | -118.8729<br>psf  | 1,530.5419<br>psf | 1,195.7904<br>psf | 0 psf   | 0 psf | Gravel Borrow                                       |
| Slice<br>24 | 19.25351 ft     | 195.48813<br>ft | -101.97239<br>psf | 1,388.4035<br>psf | 1,084.7397<br>psf | 0 psf   | 0 psf | Gravel Borrow                                       |
| Slice<br>25 | 20.75 ft        | 196.43964<br>ft | -91.862423<br>psf | 1,269.903<br>psf  | 992.15698<br>psf  | 0 psf   | 0 psf | Gravel Borrow                                       |
| Slice<br>26 | 22.75 ft        | 197.79088<br>ft | -80.219783<br>psf | 1,076.4082<br>psf | 1,003.7669<br>psf | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel        |
| Slice<br>27 | 24.25 ft        | 198.8351<br>ft  | -75.466578<br>psf | 1,038.14<br>psf   | 968.08125<br>psf  | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel        |
| Slice<br>28 | 25.2 ft         | 199.53637<br>ft | -73.462837<br>psf | 1,013.4297<br>psf | 945.0385<br>psf   | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel        |
| Slice<br>29 | 25.95 ft        | 200.09501<br>ft | -71.943607<br>psf | 994.47707<br>psf  | 927.36487<br>psf  | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel        |
| Slice<br>30 | 26.3 ft         | 200.3637<br>ft  | -71.688883<br>psf | 985.07699<br>psf  | 918.59915<br>psf  | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel        |
| Slice<br>31 | 27.925 ft       | 201.66496<br>ft | -70.027784<br>psf | 934.22181<br>psf  | 871.17593<br>psf  | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel        |
| Slice<br>32 | 30.575 ft       | 203.89728<br>ft | -71.817883<br>psf | 847.52618<br>psf  | 790.33095<br>psf  | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel        |
| Slice<br>33 | 33.4 ft         | 206.49727<br>ft | -81.425728<br>psf | 895.9252<br>psf   | 835.46376<br>psf  | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel        |

|             |                 | (1)             |                   |                  |                  |       |       |  |
|-------------|-----------------|-----------------|-------------------|------------------|------------------|-------|-------|--|
| Slice<br>34 | 36.4 ft         | 209.52347<br>ft | -107.55454<br>psf | 682.59375<br>psf | 636.52897<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>35 | 38.65 ft        | 211.96937<br>ft | -147.20056<br>psf | 534.07725<br>psf | 498.03509<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>36 | 39.8 ft         | 213.30426<br>ft | -180.8029<br>psf  | 461.80001<br>psf | 430.63547<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>37 | 41 ft           | 214.77892<br>ft | -225.42876<br>psf | 395.03585<br>psf | 368.37689<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>38 | 42.19125 ft     | 216.28758<br>ft | -286.19481<br>psf | 333.90943<br>psf | 311.37558<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>39 | 43.679617<br>ft | 218.32143<br>ft | -384.87387<br>psf | 240.42843<br>psf | 224.20314<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>40 | 45.888257<br>ft | 221.54493<br>ft | 0 psf             | 106.48785<br>psf | 83.197425<br>psf | 0 psf | 0 psf | Gravel Borrow                                |

# 1B.4 Compound - Pseudo-Static FC Wall (M-P)

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### **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 652 Date: 01/17/2022 Time: 02:07:09 PM

Tool Version: 11.1.1.22085

Last Solved Date: 01/17/2022 Last Solved Time: 02:35:22 PM

### **Project Settings**

Unit System: U.S. Customary Units

# **Analysis Settings**

### 1B.4 Compound - Pseudo-Static FC Wall (M-P)

Description: With Forward Compatible Wall

Kind: SLOPE/W

Parent: 1. Steady State (Compound) Analysis Type: Morgenstern-Price

Settings

Side Function

Interslice force function option: Half-Sine

PWP Conditions from Parent Analysis: 1. Steady State (Compound) [(last)]

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 20

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

Factor of Safety Convergence Settings

Maximum Number of Iterations: 100 Tolerable difference in F of S: 0.001

Tolerable difference in Ford. 0.00

Solution Settings

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

#### **Materials**

### **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

### **ESU 2A Very Loose to Loose Sand/Gravel (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

### **ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf

Effective Cohesion: 200 psf Effective Friction Angle: 32 °

Phi-B: 0°

### **Forward Compatible Wall**

Material Model: High Strength

Unit Weight: 130 pcf

### **Lightweight EPS**

Material Model: Mohr-Coulomb

Unit Weight: 5 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 0 °

Phi-B: 0°

### Reinforcements

### Row 1 (EQ)

Type: Geosynthetic Interface Adhesion: 0 psf

Interface Shear Angle: 8.8 °

Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

### Row 2 (EQ)

Type: Geosynthetic

Interface Adhesion: 0 psf Interface Shear Angle: 8.1 °

Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

### Row 3 (EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 7.4 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

### Row 4 (EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 6.8 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

### Row 5 (EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 6.1 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

### Row 6 (EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 5.5 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

### Row 7 (4 straps)(EQ)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 9.5 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 10,480 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 10,480 lbf/ft

### Row 8 (4 straps)(EQ)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 8.2 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 10,480 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 10,480 lbf/ft

# Slip Surface Entry and Exit

Left Type: Range

Left-Zone Left Coordinate: (-45, 181.43065) ft

Left-Zone Right Coordinate: (0, 200) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15, 223) ft Right-Zone Right Coordinate: (55, 223.299) ft

Right-Zone Increment: 20 Radius Increments: 20

# **Slip Surface Limits**

Left Coordinate: (-100, 170.1) ft Right Coordinate: (100, 223.6) ft

### **Seismic Coefficients**

Horz Seismic Coef.: 0.193

### **Reinforcement Lines**

#### **Reinforcement Line 1**

Reinforcement: Row 1 (EQ) Lock to Ground Surface: Yes Outside Point: (0, 210.5) ft Inside Point: (15.5, 210.5) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 2**

Reinforcement: Row 8 (4 straps)(EQ)

Lock to Ground Surface: No Outside Point: (0, 193.7) ft Inside Point: (19.6, 193.7) ft

Length: 19.6 ft Orientation: 0 °

Slip Surface Intersection: (16.246848, 193.7) ft

Max. Pullout Force: 10,480 lbf Available Length: 3.3531516 ft Required Length: 3.3531516 ft Pullout Force: 2,454.1915 lbf

Pullout Force per Length: 731.90591 lbf/ft Governing Component: Pullout Resistance

#### **Reinforcement Line 3**

Reinforcement: Row 6 (EQ) Lock to Ground Surface: Yes Outside Point: (0, 198.5) ft Inside Point: (15.5, 198.5) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 4**

Reinforcement: Row 2 (EQ) Lock to Ground Surface: Yes Outside Point: (0, 208.1) ft Inside Point: (15.5, 208.1) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf
Available Length: 0 ft
Required Length: 0 ft
Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 5**

Reinforcement: Row 5 (EQ) Lock to Ground Surface: Yes Outside Point: (0, 200.9) ft Inside Point: (15.5, 200.9) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 6**

Reinforcement: Row 4 (EQ) Lock to Ground Surface: Yes Outside Point: (0, 203.3) ft Inside Point: (15.5, 203.3) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### Reinforcement Line 7

Reinforcement: Row 3 (EQ) Lock to Ground Surface: Yes Outside Point: (0, 205.7) ft Inside Point: (15.5, 205.7) ft

Length: 15.5 ft

#### 1B.4 Compound - Pseudo-Static FC Wall (M-P)

Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 8**

Reinforcement: Row 7 (4 straps)(EQ)

Lock to Ground Surface: Yes Outside Point: (0, 196.1) ft Inside Point: (19.6, 196.1) ft

Length: 19.6 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

# **Surcharge Loads**

### **Surcharge Load 1**

Surcharge (Unit Weight): 125 pcf

Direction: Vertical

#### **Coordinates**

| X       | Υ        |
|---------|----------|
| 9 ft    | 224 ft   |
| 26 ft   | 224 ft   |
| 39.4 ft | 224.2 ft |
| 40.2 ft | 224.2 ft |
| 100 ft  | 224.6 ft |

# **Geometry**

Name: Default Geometry

# **Settings**

View: 2D

Element Thickness: 1 ft

#### **Points**

|  | Χ | Υ |
|--|---|---|
|  |   |   |

| Point 1          | 100 ft      | 160 ft                  |
|------------------|-------------|-------------------------|
| Point 2          | 100 ft      | 185.5 ft                |
| Point 3          | 0.9 ft      | 160 ft                  |
| Point 4          | 100 ft      | 211.1475 ft             |
| Point 5          | 3.8 ft      | 183 ft                  |
| Point 6          | -20.1275 ft | 160 ft                  |
| Point 7          | 100 ft      | 219.64 ft               |
| Point 8          | 42.5825 ft  | 219.8525 ft             |
|                  | 40.2 ft     | 213.8323 ft<br>223.2 ft |
| Point 9 Point 10 | 100 ft      | 223.2 ft<br>223.6 ft    |
|                  | 0 ft        | -                       |
| Point 11         |             | 211.7 ft                |
| Point 12         | 0 ft        | 192 ft                  |
| Point 13         | 13 ft       | 192 ft                  |
| Point 14         | 24.5 ft     | 213.8 ft                |
| Point 15         | 24.5 ft     | 192 ft                  |
| Point 16         | 24.5 ft     | 203 ft                  |
| Point 17         | 24.5 ft     | 205 ft                  |
| Point 18         | 41.8 ft     | 220.7 ft                |
| Point 19         | 26.6 ft     | 215.4 ft                |
| Point 20         | 37.9 ft     | 223.2 ft                |
| Point 21         | 6.13959 ft  | 185.3 ft                |
| Point 22         | 8.9 ft      | 192 ft                  |
| Point 23         | -100 ft     | 160 ft                  |
| Point 24         | -100 ft     | 170.1 ft                |
| Point 25         | -91.8 ft    | 174.4 ft                |
| Point 26         | -88.3 ft    | 176.5 ft                |
| Point 27         | -85.7 ft    | 177.8 ft                |
| Point 28         | -83.4 ft    | 178.4 ft                |
| Point 29         | -76 ft      | 178.9 ft                |
| Point 30         | -74 ft      | 179.7 ft                |
| Point 31         | -55.9 ft    | 180.2 ft                |
| Point 32         | -37.3 ft    | 182.3 ft                |
| Point 33         | -30.3 ft    | 182.9 ft                |
| Point 34         | -13.6 ft    | 190.2 ft                |
| Point 35         | 7 ft        | 223 ft                  |
| Point 36         | 15 ft       | 223 ft                  |
| Point 37         | 15 ft       | 211.7 ft                |
| Point 38         | 7 ft        | 211.7 ft                |
| Point 39         | -6 ft       | 195 ft                  |
| Point 40         | -37.3275 ft | 162.2725 ft             |
| Point 41         | -47.26 ft   | 160 ft                  |
| Point 42         | -5.125 ft   | 182.98095 ft            |
| Point 43         | 80.7025 ft  | 160 ft                  |
| Point 44         | -100 ft     | 129.8675 ft             |
| Point 45         | 100 ft      | 129.8675 ft             |
| Point 46         | -100 ft     | 147.8625 ft             |
| Point 47         | -27.95 ft   | 152.3875 ft             |
| Point 48         | -100 ft     | 133.97 ft               |
| . 5.116 10       |             | 200,07,10               |

| Point 49 | 16.5 ft     | 197.3 ft     |
|----------|-------------|--------------|
| Point 50 | 100 ft      | 209.9025 ft  |
| Point 51 | 95.42762 ft | 209.80965 ft |
| Point 52 | 3.915 ft    | 160.77581 ft |
| Point 53 | 17.7925 ft  | 187.09412 ft |
| Point 54 | 28.7 ft     | 129.8675 ft  |
| Point 55 | 0 ft        | 198.7 ft     |
| Point 56 | 47.15 ft    | 195.68393 ft |
| Point 57 | 42.67 ft    | 194.37311 ft |
| Point 58 | 0 ft        | 195 ft       |
| Point 59 | -32.3 ft    | 165.4 ft     |
| Point 60 | -16 ft      | 164.1 ft     |
| Point 61 | -100 ft     | 150.0525 ft  |
| Point 62 | 15 ft       | 218.535 ft   |
| Point 63 | 24 ft       | 223 ft       |
| Point 64 | 7 ft        | 214.495 ft   |
| Point 65 | 1.355 ft    | 211.7 ft     |
| Point 66 | 25.9 ft     | 223 ft       |
| Point 67 | 22 ft       | 192 ft       |
| Point 68 | 15.0117 ft  | 208.01106 ft |
| Point 69 | 21.5 ft     | 192 ft       |
| Point 70 | 15.5 ft     | 192 ft       |
| Point 71 | 15.5 ft     | 211.7 ft     |
| Point 72 | 15.5 ft     | 194.35 ft    |
| Point 73 | 15.5 ft     | 197.3 ft     |
| Point 74 | 15.5 ft     | 208.29 ft    |
| Point 75 | 18.50702 ft | 197.3 ft     |
| Point 76 | 15.5 ft     | 196.43333 ft |
| Point 77 | 21.5 ft     | 211.7 ft     |
| Point 78 | 20 ft       | 197.3 ft     |
| Point 79 | 20 ft       | 192 ft       |
| Point 80 | 21.5 ft     | 202 ft       |
| Point 81 | 21.5 ft     | 200 ft       |
| Point 82 | 21.5 ft     | 208.29 ft    |
| Point 83 | 31.9 ft     | 223.1 ft     |
| Point 84 | 31.9 ft     | 219.08 ft    |
|          |             |              |

# Regions

|             | Material   | Points                          | Area                       |
|-------------|--|---------------------------------|----------------------------|
| Region<br>1 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 1,2,52,3,43                     | 1,263.5<br>ft <sup>2</sup> |
| Region<br>2 | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 52,2,50,51,56,57,53,5,60,6,47,3 | 2,656.9<br>ft <sup>2</sup> |
| Region<br>3 | Gravel Borrow  | 9,18,8,7,10                     | 214.55<br>ft <sup>2</sup>  |
| Region<br>4 | Gravel Borrow  | 38,65,11,55,68,74,71,37         | 127 ft <sup>2</sup>        |
| Region<br>5 | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)              | 8,16,17,18                      | 31.556<br>ft <sup>2</sup>  |
|             |  |                                 |                            |

| Region 6     | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion) | 18,17,14,19,84,20,9                                      | 115.05<br>ft <sup>2</sup>  |
|--------------|---|--|----------------------------|
| Region<br>7  | Forward Compatible Wall                                       | 38,37,62,64  | 38.52<br>ft <sup>2</sup>   |
| Region<br>8  | Lightweight EPS   | 14,19,84,83,66,63,62,37,71,77                            | 132.58<br>ft <sup>2</sup>  |
| Region<br>9  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)           | 22,42,59,40,60,5,21,13                                   | 332.37<br>ft <sup>2</sup>  |
| Region<br>10 | ESU 4B Dense to Very Dense<br>Sand/Gravel                     | 44,54,45,1,43,3,47,48                                    | 4,704.7<br>ft <sup>2</sup> |
| Region<br>11 | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)           | 41,46,48,47,6,60,40                                      | 992.46<br>ft <sup>2</sup>  |
| Region<br>12 | ESU 4B Dense to Very Dense<br>Sand/Gravel                     | 56,51,50,4,7,8,16,15,67,69,79,70,13,21,5,53,57           | 1,417.8<br>ft <sup>2</sup> |
| Region<br>13 | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion) | 34,33,32,31,30,29,28,27,26,25,24,23,40,59,42,22,12,58,39 | 1,656.2<br>ft <sup>2</sup> |
| Region<br>14 | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion) | 40,23,61,46,41   | 379.99<br>ft <sup>2</sup>  |
| Region<br>15 | Lightweight EPS   | 63,36,62   | 20.093<br>ft <sup>2</sup>  |
| Region<br>16 | Forward Compatible Wall                                       | 36,35,64,62  | 51.88<br>ft <sup>2</sup>   |
| Region<br>17 |   | 64,65,38   | 7.8889<br>ft <sup>2</sup>  |
| Region<br>18 | ESU 4B Dense to Very Dense<br>Sand/Gravel                     | 15,16,81,69,67   | 28.5 ft <sup>2</sup>       |
| Region<br>19 | Gravel Borrow   | 72,76,22,13  | 11.692<br>ft <sup>2</sup>  |
| Region<br>20 | Gravel Borrow   | 70,72,13   | 2.9375<br>ft <sup>2</sup>  |
| Region<br>21 | Gravel Borrow   | 70,79,78,75,72   | 19.415<br>ft <sup>2</sup>  |
| Region<br>22 | Gravel Borrow   | 81,75,78,79,69   | 11.991<br>ft²              |
| Region<br>23 | Gravel Borrow   | 49,75,81,80  | 7.7095<br>ft <sup>2</sup>  |
| Region<br>24 | Gravel Borrow   | 49,76,72,75  | 4.002<br>ft <sup>2</sup>   |
| Region<br>25 | Gravel Borrow   | 73,76,49   | 0.43333<br>ft <sup>2</sup> |
| Region<br>26 | Gravel Borrow   | 76,73,74,68,55,58,12,22                                  | 163.72<br>ft <sup>2</sup>  |
| Region<br>27 | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)           | 80,81,16,17  | 6 ft²                      |
| Region<br>28 | Gravel Borrow   | 74,82,77   | 10.23<br>ft <sup>2</sup>   |
| Region<br>29 | Gravel Borrow   | 77,71,74   | 10.23<br>ft <sup>2</sup>   |
| Region<br>30 | ESU 2A Very Loose to Loose<br>Sand/Gravel (Apparent Cohesion) | 77,82,80,17,14   | 27.75<br>ft <sup>2</sup>   |
| Region       | Gravel Borrow   | 73,49,80,82,74   | 54.19<br>ft <sup>2</sup>   |

| Regio | Common Borrow | 20,83,84 | 12.06<br>ft <sup>2</sup> |
|-------|---------------|----------|--------------------------|
| Regio | n             | 55,39,58 | 11.1 ft²                 |

# **Slip Results**

Slip Surfaces Analysed: 7284 of 11466 converged

# **Current Slip Surface**

Slip Surface: 2,992 Factor of Safety: 1.1 Volume: 1,169.6531 ft<sup>3</sup> Weight: 124,808.04 lbf

Resisting Moment: 7,283,416.6 lbf·ft Activating Moment: 6,497,179.6 lbf·ft

Resisting Force: 74,282.981 lbf Activating Force: 66,318.601 lbf Slip Rank: 1 of 11,466 slip surfaces Exit: (-32.349646, 182.72432) ft Entry: (46.999779, 223.24548) ft

Radius: 86.172023 ft

Center: (-26.222374, 268.67822) ft

### **Slip Slices**

|            | X                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material  |
|------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|--|
| Slice<br>1 | -31.324823<br>ft | 182.66352<br>ft | -181.70135<br>psf | 32.947971<br>psf         | 20.588177<br>psf       | 100 psf              | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>2 | -28.908333<br>ft | 182.55933<br>ft | -179.7784<br>psf  | 156.3564<br>psf          | 97.702324<br>psf       | 100 psf              | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>3 | -26.125 ft       | 182.51749<br>ft | -178.18695<br>psf | 358.02565<br>psf         | 223.71926<br>psf       | 100 psf              | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>4 | -23.341667<br>ft | 182.56562<br>ft | -178.15181<br>psf | 566.44517<br>psf         | 353.95423<br>psf       | 100 psf              | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice      | -20.558333       | 182.70386       | -177.22764        | 770.61924                | 481.53635              |                      |                     | ESU 2A Very<br>Loose to Loose  |

| 5           | ft               | ft              | psf               | psf               | psf               | 100 psf | 0 psf | Sand/Gravel<br>(Apparent<br>Cohesion)                                  |
|-------------|------------------|-----------------|-------------------|-------------------|-------------------|---------|-------|--|
| Slice<br>6  | -17.775 ft       | 182.93265<br>ft | -176.31723<br>psf | 956.22078<br>psf  | 597.51306<br>psf  | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>7  | -14.991667<br>ft | 183.25271<br>ft | -176.12728<br>psf | 1,108.3344<br>psf | 692.56421<br>psf  | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>8  | -12.333333<br>ft | 183.64255<br>ft | -174.34767<br>psf | 1,242.0237<br>psf | 776.10255<br>psf  | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>9  | -9.8 ft          | 184.09537<br>ft | -176.51643<br>psf | 1,354.0937<br>psf | 846.13163<br>psf  | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>10 | -7.2666667<br>ft | 184.62697<br>ft | -208.7245<br>psf  | 1,418.5131<br>psf | 886.38534<br>psf  | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>11 | -4.5 ft          | 185.30345<br>ft | -277.93069<br>psf | 1,427.3134<br>psf | 891.88439<br>psf  | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>12 | -1.5 ft          | 186.14356<br>ft | -334.83655<br>psf | 1,223.7458<br>psf | 764.68127<br>psf  | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>13 | 0.49889422<br>ft | 186.7556<br>ft  | -361.11436<br>psf | 3,148.0959<br>psf | 1,967.1486<br>psf | 100 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>14 | 1.1763942<br>ft  | 186.97823<br>ft | -365.92602<br>psf | 3,599.8728<br>psf | 2,249.4502<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                    |
| Slice<br>15 | 2.76625 ft       | 187.54234<br>ft | -344.39989<br>psf | 2,787.2829<br>psf | 1,741.6877<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion)        |
|             |                  |                 |                   |                   |                   |         |       | ESU 2B Medium<br>Dense   |

| Slice<br>16 | 5.58875 ft      | 188.60723<br>ft | -306.00015<br>psf | 2,451.2367<br>psf | 1,531.7027<br>psf | 200 psf | 0 psf | Sand/Gravel<br>(Apparent<br>Cohesion)               |
|-------------|-----------------|-----------------|-------------------|-------------------|-------------------|---------|-------|---|
| Slice<br>17 | 7.95 ft         | 189.57831<br>ft | -274.42646<br>psf | 3,262.2581<br>psf | 2,038.4851<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion) |
| Slice<br>18 | 8.95 ft         | 190.01108<br>ft | -260.82303<br>psf | 5,179.559<br>psf  | 3,236.5477<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion) |
| Slice<br>19 | 11.048847<br>ft | 191.01672<br>ft | -234.47322<br>psf | 2,917.5116<br>psf | 1,823.0636<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion) |
| Slice<br>20 | 14.048847<br>ft | 192.50284<br>ft | -185.52003<br>psf | 2,728.6241<br>psf | 2,131.8348<br>psf | 0 psf   | 0 psf | Gravel Borrow                                       |
| Slice<br>21 | 15.25 ft        | 193.14294<br>ft | -155.93155<br>psf | 1,947.5448<br>psf | 1,521.5888<br>psf | 0 psf   | 0 psf | Gravel Borrow                                       |
| Slice<br>22 | 16 ft           | 193.56125<br>ft | -143.41807<br>psf | 1,678.6124<br>psf | 1,311.4758<br>psf | 0 psf   | 0 psf | Gravel Borrow                                       |
| Slice<br>23 | 17.50351 ft     | 194.4333<br>ft  | -118.8729<br>psf  | 1,358.911<br>psf  | 1,061.6976<br>psf | 0 psf   | 0 psf | Gravel Borrow                                       |
| Slice<br>24 | 19.25351 ft     | 195.48813<br>ft | -101.97239        | 1,215.2532<br>psf | 949.45986<br>psf  | 0 psf   | 0 psf | Gravel Borrow                                       |
| Slice<br>25 | 20.75 ft        | 196.43964<br>ft | -91.862423<br>psf | 1,101.3 psf       | 860.4299<br>psf   | 0 psf   | 0 psf | Gravel Borrow                                       |
| Slice<br>26 | 22.75 ft        | 197.79088<br>ft | -80.219783<br>psf | 914.9263<br>psf   | 853.18258<br>psf  | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel        |
| Slice<br>27 | 24.25 ft        | 198.8351<br>ft  | -75.466578<br>psf | 882.32657<br>psf  | 822.78284<br>psf  | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel        |
| Slice<br>28 | 25.2 ft         | 199.53637<br>ft | -73.462837<br>psf | 864.13968<br>psf  | 805.82329<br>psf  | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel        |
| Slice<br>29 | 25.95 ft        | 200.09501<br>ft | -71.943607<br>psf | 851.26163<br>psf  | 793.81431<br>psf  | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel        |
| Slice<br>30 | 26.3 ft         | 200.3637<br>ft  | -71.688883<br>psf | 845.17767<br>psf  | 788.14093<br>psf  | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel        |
| Slice<br>31 | 27.925 ft       | 201.66496<br>ft | -70.027784<br>psf | 812.76208<br>psf  | 757.9129<br>psf   | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel        |
| Slice<br>32 | 30.575 ft       | 203.89728<br>ft | -71.817883<br>psf | 763.07048<br>psf  | 711.57474<br>psf  | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel        |
| Slice<br>33 | 33.4 ft         | 206.49727<br>ft | -81.425728<br>psf | 877.41276<br>psf  | 818.20063<br>psf  | 0 psf   | 0 psf | ESU 4B Dense to<br>Very Dense                       |

| 1           |                 | ,               |                   |                  |                  |       |       |  |
|-------------|-----------------|-----------------|-------------------|------------------|------------------|-------|-------|--|
|             |                 |                 |                   |                  |                  |       |       | Sand/Gravel                                  |
| Slice<br>34 | 36.4 ft         | 209.52347<br>ft | -107.55454<br>psf | 713.75052<br>psf | 665.58313<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>35 | 38.65 ft        | 211.96937<br>ft | -147.20056<br>psf | 593.47702<br>psf | 553.42627<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>36 | 39.8 ft         | 213.30426<br>ft | -180.8029<br>psf  | 531.35474<br>psf | 495.49631<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>37 | 41 ft           | 214.77892<br>ft | -225.42876<br>psf | 473.35616<br>psf | 441.41176<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>38 | 42.19125 ft     | 216.28758<br>ft | -286.19481<br>psf | 418.22608<br>psf | 390.00213<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>39 | 43.679617<br>ft | 218.32143<br>ft | -384.87387<br>psf | 316.90475<br>psf | 295.51846<br>psf | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>40 | 45.888257<br>ft | 221.54493<br>ft | 0 psf             | 158.2982<br>psf  | 123.67611<br>psf | 0 psf | 0 psf | Gravel Borrow                                |

# 1B.5 Compound - Post-Seismic FC Wall (Spencer)

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### **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 652 Date: 01/17/2022 Time: 02:07:09 PM

Tool Version: 11.1.1.22085

File Name: Wall 05.85L-A - Sta 1+90 - (lightweight fill).gsz Directory: P:\0\0180366\01\Analysis\Wall 05.85L-A\22-01-17\

Last Solved Date: 01/17/2022 Last Solved Time: 02:36:48 PM

### **Project Settings**

Unit System: U.S. Customary Units

# **Analysis Settings**

### 1B.5 Compound - Post-Seismic FC Wall (Spencer)

Description: With Forward Compatible Wall

Kind: SLOPE/W

Parent: 1. Steady State (Compound)

Analysis Type: Spencer

Settings

PWP Conditions from Parent Analysis: 1. Steady State (Compound) [(last)]

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 20

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

Factor of Safety Convergence Settings
Maximum Number of Iterations: 100
Tolerable difference in F of S: 0.001
Solution Settings

Solution Settings

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3 Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

### **Materials**

### **ESU 2A Very Loose to Loose Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **ESU 2B Medium Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

### **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

# ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

### **ESU 2B Medium Dense Sand/Gravel (Residual Strength)**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf

Effective Cohesion: 497 psf Effective Friction Angle: 0 °

Phi-B: 0°

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

### **Forward Compatible Wall**

Material Model: High Strength

Unit Weight: 130 pcf

### **Lightweight EPS**

Material Model: Mohr-Coulomb

Unit Weight: 5 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 0 °

Phi-B: 0°

# Reinforcements

#### Row 1

Type: Geosynthetic
Interface Adhesion: 0 psf

Interface Shear Angle: 6.6 °

Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 2

Type: Geosynthetic

Interface Adhesion: 0 psf Interface Shear Angle:  $6.1\,^{\circ}$ 

Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 3

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 5.6 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 4

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 5.1 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 5

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 4.6 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 6

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 4.1 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

### Row 7 (4 straps)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 7.2 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 7,860 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 7,860 lbf/ft

### Row 8 (4 straps)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 6.2 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 7,860 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 7,860 lbf/ft

# **Slip Surface Entry and Exit**

Left Type: Range

Left-Zone Left Coordinate: (-45, 181.43065) ft

Left-Zone Right Coordinate: (0, 200) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15, 223) ft Right-Zone Right Coordinate: (55, 223.299) ft

Right-Zone Increment: 20 Radius Increments: 20

# **Slip Surface Limits**

Left Coordinate: (-100, 170.1) ft Right Coordinate: (100, 223.6) ft

### **Reinforcement Lines**

#### **Reinforcement Line 1**

Reinforcement: Row 1 Lock to Ground Surface: Yes Outside Point: (0, 210.5) ft Inside Point: (15.5, 210.5) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 2**

Reinforcement: Row 8 (4 straps) Lock to Ground Surface: No Outside Point: (0, 193.7) ft Inside Point: (20, 193.7) ft

Length: 20 ft
Orientation: 0 °

Slip Surface Intersection: (15.079752, 193.7) ft

Max. Pullout Force: 7,860 lbf Available Length: 4.9202484 ft Required Length: 4.9202484 ft Pullout Force: 2,676.0338 lbf

Pullout Force per Length: 543.88185 lbf/ft Governing Component: Pullout Resistance

#### **Reinforcement Line 3**

Reinforcement: Row 6 Lock to Ground Surface: Yes Outside Point: (0, 198.5) ft Inside Point: (15.5, 198.5) ft

Length: 15.5 ft
Orientation: 0°

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft

Governing Component: (none)

#### **Reinforcement Line 4**

Reinforcement: Row 2 Lock to Ground Surface: Yes Outside Point: (0, 208.1) ft Inside Point: (15.5, 208.1) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 5**

Reinforcement: Row 5 Lock to Ground Surface: Yes Outside Point: (0, 200.9) ft Inside Point: (15.5, 200.9) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### Reinforcement Line 6

Reinforcement: Row 4 Lock to Ground Surface: Yes Outside Point: (0, 203.3) ft Inside Point: (15.5, 203.3) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 7**

Reinforcement: Row 3 Lock to Ground Surface: Yes Outside Point: (0, 205.7) ft

#### 1B.5 Compound - Post-Seismic FC Wall (Spencer)

Inside Point: (15.5, 205.7) ft

Length: 15.5 ft
Orientation: 0°

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 8**

Reinforcement: Row 7 (4 straps) Lock to Ground Surface: Yes Outside Point: (0, 196.1) ft Inside Point: (20, 196.1) ft

Length: 20 ft
Orientation: 0 °

Slip Surface Intersection: (17.823618, 196.1) ft

Max. Pullout Force: 7,860 lbf Available Length: 2.1763818 ft Required Length: 2.1763818 ft Pullout Force: 1,235.7543 lbf

Pullout Force per Length: 567.80217 lbf/ft Governing Component: Pullout Resistance

# **Surcharge Loads**

### Surcharge Load 1

Surcharge (Unit Weight): 125 pcf

Direction: Vertical

#### **Coordinates**

| X       | Υ        |
|---------|----------|
| 9 ft    | 224 ft   |
| 26 ft   | 224 ft   |
| 39.4 ft | 224.2 ft |
| 40.2 ft | 224.2 ft |
| 100 ft  | 224.6 ft |

# Geometry

Name: Default Geometry

## Settings

View: 2D

Element Thickness: 1 ft

### **Points**

| TS       |             |              |
|----------|-------------|--------------|
|          | X           | Y            |
| Point 1  | 100 ft      | 160 ft       |
| Point 2  | 100 ft      | 185.5 ft     |
| Point 3  | 0.9 ft      | 160 ft       |
| Point 4  | 100 ft      | 211.1475 ft  |
| Point 5  | 3.8 ft      | 183 ft       |
| Point 6  | -20.1275 ft | 160 ft       |
| Point 7  | 100 ft      | 219.64 ft    |
| Point 8  | 42.5825 ft  | 219.8525 ft  |
| Point 9  | 40.2 ft     | 223.2 ft     |
| Point 10 | 100 ft      | 223.6 ft     |
| Point 11 | 0 ft        | 211.7 ft     |
| Point 12 | 0 ft        | 192 ft       |
| Point 13 | 13 ft       | 192 ft       |
| Point 14 | 24.5 ft     | 213.8 ft     |
| Point 15 | 24.5 ft     | 192 ft       |
| Point 16 | 24.5 ft     | 203 ft       |
| Point 17 | 24.5 ft     | 205 ft       |
| Point 18 | 41.8 ft     | 220.7 ft     |
| Point 19 | 26.6 ft     | 215.4 ft     |
| Point 20 | 37.9 ft     | 223.2 ft     |
| Point 21 | 6.13959 ft  | 185.3 ft     |
| Point 22 | 8.9 ft      | 192 ft       |
| Point 23 | -100 ft     | 160 ft       |
| Point 24 | -100 ft     | 170.1 ft     |
| Point 25 | -91.8 ft    | 174.4 ft     |
| Point 26 | -88.3 ft    | 176.5 ft     |
| Point 27 | -85.7 ft    | 177.8 ft     |
| Point 28 | -83.4 ft    | 178.4 ft     |
| Point 29 | -76 ft      | 178.9 ft     |
| Point 30 | -74 ft      | 179.7 ft     |
| Point 31 | -55.9 ft    | 180.2 ft     |
| Point 32 | -37.3 ft    | 182.3 ft     |
| Point 33 | -30.3 ft    | 182.9 ft     |
| Point 34 | -13.6 ft    | 190.2 ft     |
| Point 35 | 7 ft        | 223 ft       |
| Point 36 | 15 ft       | 223 ft       |
| Point 37 | 15 ft       | 211.7 ft     |
| Point 38 | 7 ft        | 211.7 ft     |
| Point 39 | -6 ft       | 195 ft       |
| Point 40 | -37.3275 ft | 162.2725 ft  |
| Point 41 | -47.26 ft   | 160 ft       |
| Point 42 | -5.125 ft   | 182.98095 ft |
| Point 43 | 80.7025 ft  | 160 ft       |
| Point 44 | -100 ft     | 129.8675 ft  |
| Point 45 | 100 ft      | 129.8675 ft  |
| Point 46 | -100 ft     | 147.8625 ft  |
|          |             | 1            |

|          | J -         |              |
|----------|-------------|--------------|
| Point 47 | -27.95 ft   | 152.3875 ft  |
| Point 48 | -100 ft     | 133.97 ft    |
| Point 49 | 16.5 ft     | 197.3 ft     |
| Point 50 | 100 ft      | 209.9025 ft  |
| Point 51 | 95.42762 ft | 209.80965 ft |
| Point 52 | 3.915 ft    | 160.77581 ft |
| Point 53 | 17.7925 ft  | 187.09412 ft |
| Point 54 | 28.7 ft     | 129.8675 ft  |
| Point 55 | 0 ft        | 198.7 ft     |
| Point 56 | 47.15 ft    | 195.68393 ft |
| Point 57 | 42.67 ft    | 194.37311 ft |
| Point 58 | 0 ft        | 195 ft       |
| Point 59 | -32.3 ft    | 165.4 ft     |
| Point 60 | -16 ft      | 164.1 ft     |
| Point 61 | -100 ft     | 150.0525 ft  |
| Point 62 | 15 ft       | 218.535 ft   |
| Point 63 | 24 ft       | 223 ft       |
| Point 64 | 7 ft        | 214.495 ft   |
| Point 65 | 1.355 ft    | 211.7 ft     |
| Point 66 | 25.9 ft     | 223 ft       |
| Point 67 | 22 ft       | 192 ft       |
| Point 68 | 15.0117 ft  | 208.01106 ft |
| Point 69 | 21.5 ft     | 192 ft       |
| Point 70 | 15.5 ft     | 192 ft       |
| Point 71 | 15.5 ft     | 211.7 ft     |
| Point 72 | 15.5 ft     | 194.35 ft    |
| Point 73 | 15.5 ft     | 197.3 ft     |
| Point 74 | 15.5 ft     | 208.29 ft    |
| Point 75 | 18.50702 ft | 197.3 ft     |
| Point 76 | 15.5 ft     | 196.43333 ft |
| Point 77 | 21.5 ft     | 211.7 ft     |
| Point 78 | 20 ft       | 197.3 ft     |
| Point 79 | 20 ft       | 192 ft       |
| Point 80 | 21.5 ft     | 202 ft       |
| Point 81 | 21.5 ft     | 200 ft       |
| Point 82 | 21.5 ft     | 208.29 ft    |
| Point 83 | 31.9 ft     | 223.1 ft     |
| Point 84 | 31.9 ft     | 219.08 ft    |

# Regions

|             | Material  | Points                          | Area                       |
|-------------|---|---------------------------------|----------------------------|
| Region<br>1 | ESU 4B Dense to Very Dense<br>Sand/Gravel                           | 1,2,52,3,43                     | 1,263.5<br>ft <sup>2</sup> |
| Region<br>2 | ESU 5B Very Stiff to Hard Silt and<br>Clay/Dense to Very Dense Silt | 52,2,50,51,56,57,53,5,60,6,47,3 | 2,656.9<br>ft <sup>2</sup> |
| Region<br>3 | Gravel Borrow   | 9,18,8,7,10                     | 214.55<br>ft <sup>2</sup>  |
| Region<br>4 | Gravel Borrow   | 38,65,11,55,68,74,71,37         | 127 ft²                    |

| Region<br>5  | ESU 2B Medium Dense Sand/Gravel                     | 8,16,17,18   | 31.556<br>ft <sup>2</sup>  |
|--------------|---|--|----------------------------|
| Region<br>6  | ESU 2A Very Loose to Loose<br>Sand/Gravel           | 18,17,14,19,84,20,9                                      | 115.05<br>ft <sup>2</sup>  |
| Region<br>7  | Forward Compatible Wall                             | 38,37,62,64  | 38.52<br>ft <sup>2</sup>   |
| Region<br>8  | Lightweight EPS                                     | 14,19,84,83,66,63,62,37,71,77                            | 132.58<br>ft <sup>2</sup>  |
| Region<br>9  | ESU 2B Medium Dense Sand/Gravel                     | 22,42,59,40,60,5,21,13                                   | 332.37<br>ft <sup>2</sup>  |
| Region<br>10 | ESU 4B Dense to Very Dense<br>Sand/Gravel           | 44,54,45,1,43,3,47,48                                    | 4,704.7<br>ft <sup>2</sup> |
| Region<br>11 | ESU 2B Medium Dense Sand/Gravel (Residual Strength) | 41,46,48,47,6,60,40                                      | 992.46<br>ft <sup>2</sup>  |
| Region<br>12 | ESU 4B Dense to Very Dense<br>Sand/Gravel           | 56,51,50,4,7,8,16,15,67,69,79,70,13,21,5,53,57           | 1,417.8<br>ft <sup>2</sup> |
| Region<br>13 | ESU 2A Very Loose to Loose<br>Sand/Gravel           | 34,33,32,31,30,29,28,27,26,25,24,23,40,59,42,22,12,58,39 | 1,656.2<br>ft <sup>2</sup> |
| Region<br>14 | ESU 2A Very Loose to Loose<br>Sand/Gravel           | 40,23,61,46,41   | 379.99<br>ft <sup>2</sup>  |
| Region<br>15 | Lightweight EPS                                     | 63,36,62   | 20.093<br>ft <sup>2</sup>  |
| Region<br>16 | Forward Compatible Wall                             | 36,35,64,62  | 51.88<br>ft <sup>2</sup>   |
| Region<br>17 |   | 64,65,38   | 7.8889<br>ft <sup>2</sup>  |
| Region<br>18 | ESU 4B Dense to Very Dense<br>Sand/Gravel           | 15,16,81,69,67   | 28.5 ft                    |
| Region<br>19 | Gravel Borrow                                       | 72,76,22,13  | 11.692<br>ft²              |
| Region<br>20 | Gravel Borrow                                       | 70,72,13   | 2.9375<br>ft <sup>2</sup>  |
| Region<br>21 | Gravel Borrow                                       | 70,79,78,75,72   | 19.415<br>ft <sup>2</sup>  |
| Region<br>22 | Gravel Borrow                                       | 81,75,78,79,69   | 11.991<br>ft²              |
| Region<br>23 | Gravel Borrow                                       | 49,75,81,80  | 7.7095<br>ft <sup>2</sup>  |
| Region<br>24 | Gravel Borrow                                       | 49,76,72,75  | 4.002<br>ft <sup>2</sup>   |
| Region<br>25 | Gravel Borrow                                       | 73,76,49   | 0.4333<br>ft <sup>2</sup>  |
| Region<br>26 | Gravel Borrow                                       | 76,73,74,68,55,58,12,22                                  | 163.72<br>ft <sup>2</sup>  |
| Region<br>27 | ESU 2B Medium Dense Sand/Gravel                     | 80,81,16,17  | 6 ft <sup>2</sup>          |
| Region<br>28 | Gravel Borrow                                       | 74,82,77   | 10.23<br>ft <sup>2</sup>   |
| Region<br>29 | Gravel Borrow                                       | 77,71,74   | 10.23<br>ft <sup>2</sup>   |
| Region<br>30 | ESU 2A Very Loose to Loose<br>Sand/Gravel           | 77,82,80,17,14   | 27.75<br>ft <sup>2</sup>   |
|              | 1-9 -1-1-1  |  | 1                          |

| Region<br>31 | Gravel Borrow | 73,49,80,82,74 | 54.19<br>ft <sup>2</sup> |
|--------------|---------------|----------------|--------------------------|
| Region<br>32 | Common Borrow | 20,83,84       | 12.06<br>ft²             |
| Region<br>33 |               | 55,39,58       | 11.1 ft²                 |

# **Slip Results**

Slip Surfaces Analysed: 7204 of 11466 converged

# **Current Slip Surface**

Slip Surface: 1,107 Factor of Safety: 1.4 Volume: 1,073.5733 ft³ Weight: 111,802.73 lbf

Resisting Moment: 4,386,087.4 lbf·ft
Activating Moment: 3,241,849 lbf·ft
Resisting Force: 59,552.604 lbf
Activating Force: 44,024.581 lbf
Slip Rank: 1 of 11,466 slip surfaces
Exit: (-40.78762, 181.90624) ft
Entry: (34.999735, 223.15166) ft

Radius: 62.096408 ft

Center: (-24.243501, 241.75819) ft

### Slip Slices

| Silices    |                  |                 |                   |                          |                        |                      |                     |  |
|------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|--|
|            | Х                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material                                |
| Slice<br>1 | -39.04381<br>ft  | 181.47809<br>ft | -184.62609<br>psf | 123.81635<br>psf         | 77.36904<br>psf        | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>2 | -36.133333<br>ft | 180.8223<br>ft  | -184.06914<br>psf | 288.25531<br>psf         | 180.12191<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>3 | -33.8 ft         | 180.41291<br>ft | -182.77569<br>psf | 376.72065<br>psf         | 235.40119<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>4 | -31.466667<br>ft | 180.0945<br>ft  | -181.51734<br>psf | 441.19006<br>psf         | 275.68615<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>5 | -29.107143<br>ft | 179.86411<br>ft | -179.81086<br>psf | 550.81081<br>psf         | 344.1848<br>psf        | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>6 | -26.721429<br>ft | 179.72272<br>ft | -178.81296<br>psf | 698.81627<br>psf         | 436.66887<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice      | -24.335714       | 179.67331       | -179.75536        | 820.45877                | 512.67954              |                      |                     | ESU 2A Very                                  |

| 7           | ft               | ft              | psf               | psf               | psf               | 0 psf | 0 psf | Loose to Loose<br>Sand/Gravel                |
|-------------|------------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>8  | -21.95 ft        | 179.71563<br>ft | -179.27882<br>psf | 919.12427<br>psf  | 574.33259<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>9  | -19.564286<br>ft | 179.84989<br>ft | -177.12713<br>psf | 997.49436<br>psf  | 623.30365<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>10 | -17.178571<br>ft | 180.07667<br>ft | -181.32295<br>psf | 1,057.7199<br>psf | 660.93676<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>11 | -14.792857<br>ft | 180.39702<br>ft | -186.651<br>psf   | 1,101.5452<br>psf | 688.32181<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>12 | -12.339565<br>ft | 180.82699<br>ft | -200.67145<br>psf | 1,158.772<br>psf  | 724.08113<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>13 | -9.8186957<br>ft | 181.37434<br>ft | -296.88615<br>psf | 1,226.3801<br>psf | 766.32737<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>14 | -7.2791304<br>ft | 182.0388<br>ft  | -383.76897<br>psf | 1,275.7966<br>psf | 797.20619<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>15 | -5.5625 ft       | 182.54017<br>ft | -404.88014<br>psf | 1,374.8823<br>psf | 859.12182<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>16 | -3.84375 ft      | 183.12395<br>ft | -383.82621<br>psf | 1,213.807<br>psf  | 758.47081<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>17 | -1.28125 ft      | 184.07979<br>ft | -351.82381<br>psf | 1,073.5699<br>psf | 670.84093<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>18 | 0.6775 ft        | 184.88675<br>ft | -329.17673<br>psf | 2,896.2868<br>psf | 1,809.8009<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>19 | 2.76625 ft       | 185.86561<br>ft | -306.5904<br>psf  | 2,665.497<br>psf  | 1,665.5874<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>20 | 5.58875 ft       | 187.32097<br>ft | -277.57173<br>psf | 2,417.5455<br>psf | 1,510.6501<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>21 | 7.95 ft          | 188.67045<br>ft | -254.88611<br>psf | 3,318.3387<br>psf | 2,073.5281<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>22 | 8.95 ft          | 189.27817<br>ft | -245.58458<br>psf | 4,210.4917<br>psf | 2,631.0072<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>23 | 9.9765041<br>ft  | 189.95485<br>ft | -236.93585<br>psf | 3,185.638<br>psf  | 1,990.6076<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>24 | 11.929512<br>ft  | 191.29995<br>ft | -220.10199<br>psf | 2,968.5792<br>psf | 1,854.9742<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice       | 13.143619        | 192.17917       | -209.68292        | 2,922.1893        | 2,283.0645        |       |       |  |

| 25          | ft              | ft              | psf               | psf               | psf               | 0 psf | 0 psf | Gravel Borrow                                |
|-------------|-----------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>26 | 14.190611<br>ft | 192.99631<br>ft | -199.12368<br>psf | 2,648.2369<br>psf | 2,069.0294<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>27 | 15.25 ft        | 193.84032<br>ft | -186.82298<br>psf | 1,754.8457<br>psf | 1,371.0358<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>28 | 16 ft           | 194.4719<br>ft  | -180.08144<br>psf | 1,524.7405<br>psf | 1,191.2579<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>29 | 17.50351 ft     | 195.80917<br>ft | -167.99769<br>psf | 1,352.2467<br>psf | 1,056.4909<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>30 | 18.807976<br>ft | 197.01045<br>ft | -161.36396<br>psf | 1,204.7926<br>psf | 941.28717<br>psf  | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>31 | 20.304466<br>ft | 198.53209<br>ft | -165.59074<br>psf | 1,047.5981<br>psf | 818.47332<br>psf  | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>32 | 22.364152<br>ft | 200.74625<br>ft | -188.63507<br>psf | 728.83243<br>psf  | 679.64724<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>33 | 23.614152<br>ft | 202.19505<br>ft | -203.72234<br>psf | 724.21532<br>psf  | 452.53996<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>34 | 24.25 ft        | 202.97438<br>ft | -211.31843<br>psf | 690.10922<br>psf  | 431.2281<br>psf   | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>35 | 25.2 ft         | 204.20869<br>ft | -225.83795<br>psf | 638.33078<br>psf  | 398.87334<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>36 | 25.95 ft        | 205.19907<br>ft | -239.25229<br>psf | 598.35775<br>psf  | 373.89542<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>37 | 26.3 ft         | 205.68809<br>ft | -246.35413<br>psf | 578.38805<br>psf  | 361.41697<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>38 | 27.286631<br>ft | 207.13025<br>ft | -268.80823<br>psf | 517.78251<br>psf  | 323.54642<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>39 | 28.954947<br>ft | 209.78543<br>ft | -262.03638<br>psf | 408.32431<br>psf  | 255.14934<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>40 | 30.918316<br>ft | 213.32322<br>ft | -217.03131<br>psf | 272.75071<br>psf  | 170.43356<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>41 | 33.022443<br>ft | 217.92455<br>ft | -189.37484<br>psf | 241.49349<br>psf  | 150.90188<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>42 | 34.572311<br>ft | 221.88658<br>ft | 0 psf             | 77.921513<br>psf  | 48.690766<br>psf  | 0 psf | 0 psf | Common Borrov                                |

# 1B.6 Compound - Post-Seismic FC Wall (M-P)

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# **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 652 Date: 01/17/2022 Time: 02:07:09 PM

Tool Version: 11.1.1.22085

Last Solved Date: 01/17/2022 Last Solved Time: 02:37:10 PM

# **Project Settings**

Unit System: U.S. Customary Units

# **Analysis Settings**

### 1B.6 Compound - Post-Seismic FC Wall (M-P)

Description: With Forward Compatible Wall

Kind: SLOPE/W

Parent: 1. Steady State (Compound) Analysis Type: Morgenstern-Price

Settings

Side Function

Interslice force function option: Half-Sine

PWP Conditions from Parent Analysis: 1. Steady State (Compound) [(last)]

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 20

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

Factor of Safety Convergence Settings

Maximum Number of Iterations: 100 Tolerable difference in F of S: 0.001

Solution Settings

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

### **Materials**

### **ESU 2A Very Loose to Loose Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

#### **ESU 2B Medium Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

# **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

### **ESU 2B Medium Dense Sand/Gravel (Residual Strength)**

Material Model: Mohr-Coulomb

Unit Weight: 110 pcf

Effective Cohesion: 497 psf Effective Friction Angle: 0 °

Phi-B: 0°

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

#### **Forward Compatible Wall**

Material Model: High Strength

Unit Weight: 130 pcf

### **Lightweight EPS**

Material Model: Mohr-Coulomb

Unit Weight: 5 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 0 °

Phi-B: 0°

### Reinforcements

#### Row 1

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 6.6 °

Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 2

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 6.1 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 3

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 5.6 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 4

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 5.1 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 5

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 4.6 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 6

Type: Geosynthetic Interface Adhesion: 0 psf

Interface Shear Angle: 4.1 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

### Row 7 (4 straps)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 7.2 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 7,860 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 7,860 lbf/ft

### Row 8 (4 straps)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 6.2 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 7,860 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 7,860 lbf/ft

# **Slip Surface Entry and Exit**

Left Type: Range

Left-Zone Left Coordinate: (-45, 181.43065) ft

Left-Zone Right Coordinate: (0, 200) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15, 223) ft Right-Zone Right Coordinate: (55, 223.299) ft

Right-Zone Increment: 20 Radius Increments: 20

# **Slip Surface Limits**

Left Coordinate: (-100, 170.1) ft Right Coordinate: (100, 223.6) ft

### **Reinforcement Lines**

#### **Reinforcement Line 1**

Reinforcement: Row 1 Lock to Ground Surface: Yes Outside Point: (0, 210.5) ft Inside Point: (15.5, 210.5) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 2**

Reinforcement: Row 8 (4 straps) Lock to Ground Surface: No Outside Point: (0, 193.7) ft Inside Point: (20, 193.7) ft Length: 20 ft

Length: 20 ft
Orientation: 0 °

Slip Surface Intersection: (15.079752, 193.7) ft

Max. Pullout Force: 7,860 lbf Available Length: 4.9202484 ft Required Length: 4.9202484 ft Pullout Force: 2,676.0338 lbf

Pullout Force per Length: 543.88185 lbf/ft Governing Component: Pullout Resistance

#### **Reinforcement Line 3**

Reinforcement: Row 6 Lock to Ground Surface: Yes Outside Point: (0, 198.5) ft Inside Point: (15.5, 198.5) ft

Length: 15.5 ft
Orientation: 0°

Max. Pullout Force: 0 lbf
Available Length: 0 ft
Required Length: 0 ft
Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 4**

Reinforcement: Row 2 Lock to Ground Surface: Yes Outside Point: (0, 208.1) ft Inside Point: (15.5, 208.1) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 5**

Reinforcement: Row 5 Lock to Ground Surface: Yes Outside Point: (0, 200.9) ft Inside Point: (15.5, 200.9) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 6**

Reinforcement: Row 4 Lock to Ground Surface: Yes Outside Point: (0, 203.3) ft Inside Point: (15.5, 203.3) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### Reinforcement Line 7

Reinforcement: Row 3 Lock to Ground Surface: Yes

#### 1B.6 Compound - Post-Seismic FC Wall (M-P)

Outside Point: (0, 205.7) ft Inside Point: (15.5, 205.7) ft

Length: 15.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 8**

Reinforcement: Row 7 (4 straps) Lock to Ground Surface: Yes Outside Point: (0, 196.1) ft Inside Point: (20, 196.1) ft

Length: 20 ft
Orientation: 0 °

Slip Surface Intersection: (17.823618, 196.1) ft

Max. Pullout Force: 7,860 lbf Available Length: 2.1763818 ft Required Length: 2.1763818 ft Pullout Force: 1,235.7543 lbf

Pullout Force per Length: 567.80217 lbf/ft Governing Component: Pullout Resistance

# **Surcharge Loads**

### Surcharge Load 1

Surcharge (Unit Weight): 125 pcf

Direction: Vertical

#### **Coordinates**

| X       | Υ        |
|---------|----------|
| 9 ft    | 224 ft   |
| 26 ft   | 224 ft   |
| 39.4 ft | 224.2 ft |
| 40.2 ft | 224.2 ft |
| 100 ft  | 224.6 ft |

# Geometry

Name: Default Geometry

# Settings

View: 2D

Element Thickness: 1 ft

### **Points**

| its      | I           |              |
|----------|-------------|--------------|
|          | X           | Y            |
| Point 1  | 100 ft      | 160 ft       |
| Point 2  | 100 ft      | 185.5 ft     |
| Point 3  | 0.9 ft      | 160 ft       |
| Point 4  | 100 ft      | 211.1475 ft  |
| Point 5  | 3.8 ft      | 183 ft       |
| Point 6  | -20.1275 ft | 160 ft       |
| Point 7  | 100 ft      | 219.64 ft    |
| Point 8  | 42.5825 ft  | 219.8525 ft  |
| Point 9  | 40.2 ft     | 223.2 ft     |
| Point 10 | 100 ft      | 223.6 ft     |
| Point 11 | 0 ft        | 211.7 ft     |
| Point 12 | 0 ft        | 192 ft       |
| Point 13 | 13 ft       | 192 ft       |
| Point 14 | 24.5 ft     | 213.8 ft     |
| Point 15 | 24.5 ft     | 192 ft       |
| Point 16 | 24.5 ft     | 203 ft       |
| Point 17 | 24.5 ft     | 205 ft       |
| Point 18 | 41.8 ft     | 220.7 ft     |
| Point 19 | 26.6 ft     | 215.4 ft     |
| Point 20 | 37.9 ft     | 223.2 ft     |
| Point 21 | 6.13959 ft  | 185.3 ft     |
| Point 22 | 8.9 ft      | 192 ft       |
| Point 23 | -100 ft     | 160 ft       |
| Point 24 | -100 ft     | 170.1 ft     |
| Point 25 | -91.8 ft    | 174.4 ft     |
| Point 26 | -88.3 ft    | 176.5 ft     |
| Point 27 | -85.7 ft    | 177.8 ft     |
| Point 28 | -83.4 ft    | 178.4 ft     |
| Point 29 | -76 ft      | 178.9 ft     |
| Point 30 | -74 ft      | 179.7 ft     |
| Point 31 | -55.9 ft    | 180.2 ft     |
| Point 32 | -37.3 ft    | 182.3 ft     |
| Point 33 | -30.3 ft    | 182.9 ft     |
| Point 34 | -13.6 ft    | 190.2 ft     |
| Point 35 | 7 ft        | 223 ft       |
| Point 36 | 15 ft       | 223 ft       |
| Point 37 | 15 ft       | 211.7 ft     |
| Point 38 | 7 ft        | 211.7 ft     |
| Point 39 | -6 ft       | 195 ft       |
| Point 40 | -37.3275 ft | 162.2725 ft  |
| Point 41 | -47.26 ft   | 160 ft       |
| Point 42 | -5.125 ft   | 182.98095 ft |
| Point 43 | 80.7025 ft  | 160 ft       |
| Point 44 | -100 ft     | 129.8675 ft  |
|          |             |              |

| Point 45 | 100 ft      | 129.8675 ft  |
|----------|-------------|--------------|
| Point 46 | -100 ft     | 147.8625 ft  |
| Point 47 | -27.95 ft   | 152.3875 ft  |
| Point 48 | -100 ft     | 133.97 ft    |
| Point 49 | 16.5 ft     | 197.3 ft     |
| Point 50 | 100 ft      | 209.9025 ft  |
| Point 51 | 95.42762 ft | 209.80965 ft |
| Point 52 | 3.915 ft    | 160.77581 ft |
| Point 53 | 17.7925 ft  | 187.09412 ft |
| Point 54 | 28.7 ft     | 129.8675 ft  |
| Point 55 | 0 ft        | 198.7 ft     |
| Point 56 | 47.15 ft    | 195.68393 ft |
| Point 57 | 42.67 ft    | 194.37311 ft |
| Point 58 | 0 ft        | 195 ft       |
| Point 59 | -32.3 ft    | 165.4 ft     |
| Point 60 | -16 ft      | 164.1 ft     |
| Point 61 | -100 ft     | 150.0525 ft  |
| Point 62 | 15 ft       | 218.535 ft   |
| Point 63 | 24 ft       | 223 ft       |
| Point 64 | 7 ft        | 214.495 ft   |
| Point 65 | 1.355 ft    | 211.7 ft     |
| Point 66 | 25.9 ft     | 223 ft       |
| Point 67 | 22 ft       | 192 ft       |
| Point 68 | 15.0117 ft  | 208.01106 ft |
| Point 69 | 21.5 ft     | 192 ft       |
| Point 70 | 15.5 ft     | 192 ft       |
| Point 71 | 15.5 ft     | 211.7 ft     |
| Point 72 | 15.5 ft     | 194.35 ft    |
| Point 73 | 15.5 ft     | 197.3 ft     |
| Point 74 | 15.5 ft     | 208.29 ft    |
| Point 75 | 18.50702 ft | 197.3 ft     |
| Point 76 | 15.5 ft     | 196.43333 ft |
| Point 77 | 21.5 ft     | 211.7 ft     |
| Point 78 | 20 ft       | 197.3 ft     |
| Point 79 | 20 ft       | 192 ft       |
| Point 80 | 21.5 ft     | 202 ft       |
| Point 81 | 21.5 ft     | 200 ft       |
| Point 82 | 21.5 ft     | 208.29 ft    |
| Point 83 | 31.9 ft     | 223.1 ft     |
| Point 84 | 31.9 ft     | 219.08 ft    |

# Regions

|             | Material   | Points                          | Area                       |
|-------------|--|---------------------------------|----------------------------|
| Region<br>1 | ESU 4B Dense to Very Dense<br>Sand/Gravel                        | 1,2,52,3,43                     | 1,263.5<br>ft <sup>2</sup> |
| Region<br>2 | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 52,2,50,51,56,57,53,5,60,6,47,3 | 2,656.9<br>ft <sup>2</sup> |
| Region<br>3 | Gravel Borrow  | 9,18,8,7,10                     | 214.55<br>ft <sup>2</sup>  |

| Region 4     | Gravel Borrow                                       | 38,65,11,55,68,74,71,37                                  | 127 ft²                    |
|--------------|---|--|----------------------------|
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel                     | 8,16,17,18   | 31.556<br>ft <sup>2</sup>  |
| Region<br>6  | ESU 2A Very Loose to Loose<br>Sand/Gravel           | 18,17,14,19,84,20,9                                      | 115.05<br>ft <sup>2</sup>  |
| Region<br>7  | Forward Compatible Wall                             | 38,37,62,64  | 38.52<br>ft <sup>2</sup>   |
| Region<br>8  | Lightweight EPS                                     | 14,19,84,83,66,63,62,37,71,77                            | 132.58<br>ft <sup>2</sup>  |
| Region<br>9  | ESU 2B Medium Dense Sand/Gravel                     | 22,42,59,40,60,5,21,13                                   | 332.37<br>ft <sup>2</sup>  |
| Region<br>10 | ESU 4B Dense to Very Dense<br>Sand/Gravel           | 44,54,45,1,43,3,47,48                                    | 4,704.7<br>ft <sup>2</sup> |
| Region<br>11 | ESU 2B Medium Dense Sand/Gravel (Residual Strength) | 41,46,48,47,6,60,40                                      | 992.46<br>ft <sup>2</sup>  |
| Region<br>12 | ESU 4B Dense to Very Dense<br>Sand/Gravel           | 56,51,50,4,7,8,16,15,67,69,79,70,13,21,5,53,57           | 1,417.8<br>ft <sup>2</sup> |
| Region<br>13 | ESU 2A Very Loose to Loose<br>Sand/Gravel           | 34,33,32,31,30,29,28,27,26,25,24,23,40,59,42,22,12,58,39 | 1,656.2<br>ft <sup>2</sup> |
| Region<br>14 | ESU 2A Very Loose to Loose<br>Sand/Gravel           | 40,23,61,46,41   | 379.99<br>ft <sup>2</sup>  |
| Region<br>15 | Lightweight EPS                                     | 63,36,62   | 20.093<br>ft <sup>2</sup>  |
| Region<br>16 | Forward Compatible Wall                             | 36,35,64,62  | 51.88<br>ft²               |
| Region<br>17 |   | 64,65,38   | 7.8889<br>ft <sup>2</sup>  |
| Region<br>18 | ESU 4B Dense to Very Dense<br>Sand/Gravel           | 15,16,81,69,67   | 28.5 ft <sup>2</sup>       |
| Region<br>19 | Gravel Borrow                                       | 72,76,22,13  | 11.692<br>ft <sup>2</sup>  |
| Region<br>20 | Gravel Borrow                                       | 70,72,13   | 2.9375<br>ft <sup>2</sup>  |
| Region<br>21 | Gravel Borrow                                       | 70,79,78,75,72   | 19.415<br>ft <sup>2</sup>  |
| Region<br>22 | Gravel Borrow                                       | 81,75,78,79,69   | 11.991<br>ft²              |
| Region<br>23 | Gravel Borrow                                       | 49,75,81,80  | 7.7095<br>ft <sup>2</sup>  |
| Region<br>24 | Gravel Borrow                                       | 49,76,72,75  | 4.002<br>ft <sup>2</sup>   |
| Region<br>25 | Gravel Borrow                                       | 73,76,49   | 0.43333<br>ft <sup>2</sup> |
| Region<br>26 | Gravel Borrow                                       | 76,73,74,68,55,58,12,22                                  | 163.72<br>ft <sup>2</sup>  |
| Region<br>27 | ESU 2B Medium Dense Sand/Gravel                     | 80,81,16,17  | 6 ft²                      |
| Region<br>28 | Gravel Borrow                                       | 74,82,77   | 10.23<br>ft <sup>2</sup>   |
| Region       | Gravel Borrow                                       | 77,71,74   | 10.23                      |

| Region<br>30 | ESU 2A Very Loose to Loose<br>Sand/Gravel | 77,82,80,17,14 | 27.75<br>ft <sup>2</sup> |
|--------------|---|----------------|--------------------------|
| Region<br>31 | Gravel Borrow                             | 73,49,80,82,74 | 54.19<br>ft <sup>2</sup> |
| Region<br>32 | Common Borrow                             | 20,83,84       | 12.06<br>ft <sup>2</sup> |
| Region<br>33 |   | 55,39,58       | 11.1 ft²                 |

# **Slip Results**

Slip Surfaces Analysed: 9050 of 11466 converged

# **Current Slip Surface**

Slip Surface: 1,107 Factor of Safety: 1.4 Volume: 1,073.5733 ft<sup>3</sup> Weight: 111,802.73 lbf

Resisting Moment: 4,383,546 lbf·ft
Activating Moment: 3,241,849 lbf·ft
Resisting Force: 59,476.883 lbf
Activating Force: 44,000.313 lbf
Slip Rank: 1 of 11,466 slip surfaces
Exit: (-40.78762, 181.90624) ft
Entry: (34.999735, 223.15166) ft

Radius: 62.096408 ft

Center: (-24.243501, 241.75819) ft

### **Slip Slices**

|            | X                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material                                |
|------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|--|
| Slice<br>1 | -39.04381<br>ft  | 181.47809<br>ft | -184.62609<br>psf | 83.389882<br>psf         | 52.107782<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>2 | -36.133333<br>ft | 180.8223<br>ft  | -184.06914<br>psf | 219.41643<br>psf         | 137.1066<br>psf        | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>3 | -33.8 ft         | 180.41291<br>ft | -182.77569<br>psf | 315.86667<br>psf         | 197.3754<br>psf        | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>4 | -31.466667<br>ft | 180.0945<br>ft  | -181.51734<br>psf | 402.5666<br>psf          | 251.55153<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>5 | -29.107143<br>ft | 179.86411<br>ft | -179.81086<br>psf | 534.78573<br>psf         | 334.17121<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>6 | -26.721429<br>ft | 179.72272<br>ft | -178.81296<br>psf | 710.09312<br>psf         | 443.71543<br>psf       | 0 psf                | 0 psf               | ESU 2A Very<br>Loose to Loose                |

|             |                  |                 |                   |                   |                   |       |       | Sand/Gravel                                  |
|-------------|------------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>7  | -24.335714<br>ft | 179.67331<br>ft | -179.75536<br>psf | 866.04829<br>psf  | 541.16703<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>8  | -21.95 ft        | 179.71563<br>ft | -179.27882<br>psf | 997.86932<br>psf  | 623.53796<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>9  | -19.564286<br>ft | 179.84989<br>ft | -177.12713<br>psf | 1,102.3615<br>psf | 688.83192<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>10 | -17.178571<br>ft | 180.07667<br>ft | -181.32295<br>psf | 1,178.1422<br>psf | 736.18494<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>11 | -14.792857<br>ft | 180.39702<br>ft | -186.651<br>psf   | 1,225.586<br>psf  | 765.83113<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>12 | -12.339565<br>ft | 180.82699<br>ft | -200.67145<br>psf | 1,275.3252<br>psf | 796.91164<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>13 | -9.8186957<br>ft | 181.37434<br>ft | -296.88615<br>psf | 1,325.3269<br>psf | 828.15618<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>14 | -7.2791304<br>ft | 182.0388<br>ft  | -383.76897<br>psf | 1,348.4002<br>psf | 842.57397<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>15 | -5.5625 ft       | 182.54017<br>ft | -404.88014<br>psf | 1,458.6085<br>psf | 911.43975<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>16 | -3.84375 ft      | 183.12395<br>ft | -383.82621<br>psf | 1,251.5605<br>psf | 782.06177<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>17 | -1.28125 ft      | 184.07979<br>ft | -351.82381<br>psf | 1,074.8732<br>psf | 671.6553<br>psf   | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>18 | 0.6775 ft        | 184.88675<br>ft | -329.17673<br>psf | 2,892.9136<br>psf | 1,807.6931<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>19 | 2.76625 ft       | 185.86561<br>ft | -306.5904<br>psf  | 2,613.821<br>psf  | 1,633.2966<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>20 | 5.58875 ft       | 187.32097<br>ft | -277.57173<br>psf | 2,330.1541<br>psf | 1,456.0419<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>21 | 7.95 ft          | 188.67045<br>ft | -254.88611<br>psf | 3,206.8551<br>psf | 2,003.8654<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>22 | 8.95 ft          | 189.27817<br>ft | -245.58458<br>psf | 4,229.6732<br>psf | 2,642.9932<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>23 | 9.9765041<br>ft  | 189.95485<br>ft | -236.93585<br>psf | 3,066.5375<br>psf | 1,916.1853<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice       | 11.929512        | 191.29995       | -220.10199        | 2,856.7275        | 1,785.0815        | 0 psf | 0 psf | ESU 2B Medium<br>Dense                       |

| 24          | ft              | ft              | psf               | psf               | psf               |       |       | <br>  Sand/Gravel                            |
|-------------|-----------------|-----------------|-------------------|-------------------|-------------------|-------|-------|--|
| Slice<br>25 | 13.143619<br>ft | 192.17917<br>ft | -209.68292<br>psf | 2,825.5047<br>psf | 2,207.5262<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>26 | 14.190611<br>ft | 192.99631<br>ft | -199.12368<br>psf | 2,551.6239<br>psf | 1,993.547<br>psf  | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>27 | 15.25 ft        | 193.84032<br>ft | -186.82298<br>psf | 1,653.6156<br>psf | 1,291.9461<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>28 | 16 ft           | 194.4719<br>ft  | -180.08144<br>psf | 1,432.9214<br>psf | 1,119.5209<br>psf | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>29 | 17.50351 ft     | 195.80917<br>ft | -167.99769<br>psf | 1,271.7022<br>psf | 993.56267<br>psf  | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>30 | 18.807976<br>ft | 197.01045<br>ft | -161.36396<br>psf | 1,137.0924<br>psf | 888.39391<br>psf  | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>31 | 20.304466<br>ft | 198.53209<br>ft | -165.59074<br>psf | 994.48442<br>psf  | 776.97638<br>psf  | 0 psf | 0 psf | Gravel Borrow                                |
| Slice<br>32 | 22.364152<br>ft | 200.74625<br>ft | -188.63507<br>psf | 683.05666<br>psf  | 636.96064<br>psf  | 0 psf | 0 psf | ESU 4B Dense to<br>Very Dense<br>Sand/Gravel |
| Slice<br>33 | 23.614152<br>ft | 202.19505<br>ft | -203.72234<br>psf | 706.74256<br>psf  | 441.62177<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>34 | 24.25 ft        | 202.97438<br>ft | -211.31843<br>psf | 680.76759<br>psf  | 425.3908<br>psf   | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>35 | 25.2 ft         | 204.20869<br>ft | -225.83795<br>psf | 641.20215<br>psf  | 400.66757<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>36 | 25.95 ft        | 205.19907<br>ft | -239.25229<br>psf | 610.65085<br>psf  | 381.577<br>psf    | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>37 | 26.3 ft         | 205.68809<br>ft | -246.35413<br>psf | 594.92586<br>psf  | 371.75094<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>38 | 27.286631<br>ft | 207.13025<br>ft | -268.80823<br>psf | 545.16573<br>psf  | 340.65735<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel        |
| Slice<br>39 | 28.954947<br>ft | 209.78543<br>ft | -262.03638<br>psf | 449.52517<br>psf  | 280.8945<br>psf   | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>40 | 30.918316<br>ft | 213.32322<br>ft | -217.03131<br>psf | 319.16457<br>psf  | 199.43616<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>41 | 33.022443<br>ft | 217.92455<br>ft | -189.37484<br>psf | 318.96888<br>psf  | 199.31388<br>psf  | 0 psf | 0 psf | ESU 2A Very<br>Loose to Loose<br>Sand/Gravel |
| Slice<br>42 | 34.572311<br>ft | 221.88658<br>ft | 0 psf             | 113.12324<br>psf  | 70.687249<br>psf  | 0 psf | 0 psf | Common Borrow                                |

# 1A.1 Compound - Static (Spencer)

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# **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 318 Date: 01/13/2022

Time: 03:58:28 PM

Tool Version: 11.1.1.22085

File Name: Wall 05.85L-B Sta 2+60\_FC Wall (lightweight fill).gsz Directory: P:\0\0180366\01\Analysis\Wall 05.85L-B\22-01-13\

Last Solved Date: 01/13/2022 Last Solved Time: 03:59:52 PM

# **Project Settings**

Unit System: U.S. Customary Units

# **Analysis Settings**

### 1A.1 Compound - Static (Spencer)

Kind: SLOPE/W

Analysis Type: Spencer

Settings

PWP Conditions from: Piezometric Line

Apply Phreatic Correction: No Use Staged Rapid Drawdown: No

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit

Critical slip surfaces saved: 1

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

Factor of Safety Convergence Settings

Maximum Number of Iterations: 100

Tolerable difference in F of S: 0.001

**Solution Settings** 

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

#### **Materials**

#### **ESU 1B Medium Dense to Very Dense Coarse-Grained Fill**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 41 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **ESU 2B Medium Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 115 pcf Effective Cohesion: 0 psf Effective Friction Angle: 34 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 42 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

# Reinforcements

#### Row 1 (2 strips)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 6.6 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 2 (2 strips)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 6.1 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

## Row 3 (2 strips)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 5.6 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 4 (2 strips)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 5.1 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 5 (2 strips)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 4.6 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 6 (2 strips)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 4.1 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 7 (2 strips)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 3.6 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 8 (2 strips)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 3.1 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 9+ (2 strips)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 2.7 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

# Slip Surface Entry and Exit

Left Type: Range

Left-Zone Left Coordinate: (-35.900009, 192.42444) ft

Left-Zone Right Coordinate: (-0.9, 206) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15.000006, 226.34416) ft

Right-Zone Right Coordinate: (60, 233.74338) ft

Right-Zone Increment: 30
Radius Increments: 20

# **Slip Surface Limits**

Left Coordinate: (-80, 186.2) ft Right Coordinate: (80, 234.2) ft

### **Piezometric Lines**

#### Piezometric Line 1

#### **Coordinates**

|               | Х         | Υ          |
|---------------|-----------|------------|
| Coordinate 1  | -48.3 ft  | 180 ft     |
| Coordinate 2  | -4.1 ft   | 190.1 ft   |
| Coordinate 3  | 11.7 ft   | 193.8 ft   |
| Coordinate 4  | 17.165 ft | 194.87 ft  |
| Coordinate 5  | 24.11 ft  | 196.755 ft |
| Coordinate 6  | 29.52 ft  | 198.8 ft   |
| Coordinate 7  | 32.23 ft  | 199.83 ft  |
| Coordinate 8  | 60.885 ft | 211.35 ft  |
| Coordinate 9  | 70.775 ft | 215.12 ft  |
| Coordinate 10 | 74.125 ft | 216.15 ft  |
| Coordinate 11 | 80 ft     | 217.365 ft |

# **Reinforcement Lines**

#### **Reinforcement Line 1**

Reinforcement: Row 1 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 218.4) ft Inside Point: (15.6, 218.4) ft

Length: 16.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 2**

Reinforcement: Row 3 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 213.6) ft Inside Point: (15.6, 213.6) ft

Length: 16.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 3**

Reinforcement: Row 2 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 216) ft Inside Point: (15.6, 216) ft

Length: 16.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 4**

Reinforcement: Row 7 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 204) ft Inside Point: (15.6, 204) ft

Length: 16.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 5**

Reinforcement: Row 6 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 206.4) ft Inside Point: (15.6, 206.4) ft

Length: 16.5 ft

Orientation: 0°

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### Reinforcement Line 6

Reinforcement: Row 5 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 208.8) ft Inside Point: (15.6, 208.8) ft

Length: 16.5 ft
Orientation: 0°

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 7**

Reinforcement: Row 4 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 211.2) ft Inside Point: (15.6, 211.2) ft

Length: 16.5 ft
Orientation: 0°

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 8**

Reinforcement: Row 9+ (2 strips) Lock to Ground Surface: No Outside Point: (-0.9, 196.8) ft Inside Point: (15.6, 196.8) ft

Length: 16.5 ft Orientation: 0 °

Slip Surface Intersection: (10.34791, 196.8) ft

Max. Pullout Force: 3,930 lbf Available Length: 5.2520903 ft Required Length: 5.2520903 ft Pullout Force: 1,724.5562 lbf Pullout Force per Length: 328.35616 lbf/ft Governing Component: Pullout Resistance

#### **Reinforcement Line 9**

Reinforcement: Row 9+ (2 strips) Lock to Ground Surface: No Outside Point: (-0.9, 199.2) ft Inside Point: (15.6, 199.2) ft

Length: 16.5 ft
Orientation: 0 °

Slip Surface Intersection: (14.253335, 199.2) ft

Max. Pullout Force: 3,930 lbf Available Length: 1.3466647 ft Required Length: 1.3466647 ft Pullout Force: 431.2803 lbf

Pullout Force per Length: 320.25813 lbf/ft Governing Component: Pullout Resistance

#### **Reinforcement Line 10**

Reinforcement: Row 8 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 201.6) ft Inside Point: (15.6, 201.6) ft

Length: 16.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

# **Surcharge Loads**

## **Surcharge Load 1**

Surcharge (Unit Weight): 250 pcf

**Direction: Vertical** 

#### **Coordinates**

| Х       | Υ        |
|---------|----------|
| 43 ft   | 234.5 ft |
| 45 ft   | 234.5 ft |
| 58.1 ft | 234.7 ft |
| 80 ft   | 235.2 ft |

# Geometry

Name: 1. Compound Stability

**Settings** 

View: 2D

Element Thickness: 1 ft

#### **Points**

| 11.5     |          |          |  |  |  |
|----------|----------|----------|--|--|--|
|          | X        | Υ        |  |  |  |
| Point 1  | 80 ft    | 199.4 ft |  |  |  |
| Point 2  | 58 ft    | 196.6 ft |  |  |  |
| Point 3  | 37.6 ft  | 191.9 ft |  |  |  |
| Point 4  | 42.1 ft  | 180 ft   |  |  |  |
| Point 5  | 80 ft    | 180 ft   |  |  |  |
| Point 6  | 80 ft    | 226 ft   |  |  |  |
| Point 7  | 58 ft    | 225.3 ft |  |  |  |
| Point 8  | 29.8 ft  | 195 ft   |  |  |  |
| Point 9  | 11.7 ft  | 193.8 ft |  |  |  |
| Point 10 | -48.3 ft | 180 ft   |  |  |  |
| Point 11 | 80 ft    | 234.2 ft |  |  |  |
| Point 12 | 58.1 ft  | 233.7 ft |  |  |  |
| Point 13 | 26.5 ft  | 214.1 ft |  |  |  |
| Point 14 | -10.8 ft | 197 ft   |  |  |  |
| Point 15 | -18.3 ft | 195.3 ft |  |  |  |
| Point 16 | -21.1 ft | 194.7 ft |  |  |  |
| Point 17 | -24.4 ft | 193.6 ft |  |  |  |
| Point 18 | -32.1 ft | 193.1 ft |  |  |  |
| Point 19 | -36.6 ft | 192.3 ft |  |  |  |
| Point 20 | -61.7 ft | 189.7 ft |  |  |  |
| Point 21 | -65.4 ft | 189.3 ft |  |  |  |
| Point 22 | -73.2 ft | 188 ft   |  |  |  |
| Point 23 | -80 ft   | 186.2 ft |  |  |  |
| Point 24 | -80 ft   | 180 ft   |  |  |  |
| Point 25 | -4.1 ft  | 190.1 ft |  |  |  |
| Point 26 | 32 ft    | 197.4 ft |  |  |  |
| Point 27 | -0.9 ft  | 219.4 ft |  |  |  |
| Point 28 | -0.9 ft  | 196.3 ft |  |  |  |
| Point 29 | -4.9 ft  | 199.8 ft |  |  |  |
| Point 30 | -0.9 ft  | 199.8 ft |  |  |  |
| Point 31 | -0.9 ft  | 199.4 ft |  |  |  |
| Point 32 | 15.6 ft  | 196.3 ft |  |  |  |
| Point 33 | 15.6 ft  | 219.4 ft |  |  |  |
| Point 34 | 11.1 ft  | 196.3 ft |  |  |  |
| Point 35 | 17.1 ft  | 196.3 ft |  |  |  |
| Point 36 | 17.1 ft  | 214.2 ft |  |  |  |
| Point 37 | 15.6 ft  | 214.2 ft |  |  |  |
| Point 38 | 17.1 ft  | 208.4 ft |  |  |  |
| Point 39 | 45 ft    | 233.5 ft |  |  |  |
| Point 40 | 37.1 ft  | 228.2 ft |  |  |  |
|          |          |          |  |  |  |

| Point 41 | 29.4 ft   | 222.3 ft  |
|----------|-----------|-----------|
| Point 42 | 29.5 ft   | 233.5 ft  |
| Point 43 | 1.5 ft    | 219.4 ft  |
| Point 44 | 31.5 ft   | 233.5 ft  |
| Point 45 | 6.1 ft    | 233.5 ft  |
| Point 46 | 14.1 ft   | 233.5 ft  |
| Point 47 | 14.1 ft   | 219.4 ft  |
| Point 48 | 6.1 ft    | 219.4 ft  |
| Point 49 | 14.1 ft   | 225.9 ft  |
| Point 50 | 6.1 ft    | 221.74 ft |
| Point 51 | 17.1 ft   | 219.4 ft  |
| Point 52 | 28.775 ft | 233.5 ft  |
| Point 53 | 6.1 ft    | 232 ft    |
| Point 54 | 14.1 ft   | 232 ft    |
| Point 55 | 39 ft     | 233.5 ft  |
| Point 56 | 39 ft     | 230.5 ft  |

# Regions

|              | Material   | Points  | Area                       |
|--------------|--|---|----------------------------|
| Region<br>1  | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 1,2,3,4,5                                       | 659.92<br>ft <sup>2</sup>  |
| Region<br>2  | ESU 4B Dense to Very Dense Sand/Gravel                           | 1,6,7,26,8,9,25,10,4,3,2                        | 1,867.8<br>ft <sup>2</sup> |
| Region<br>3  | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill        | 14,29,30,31                                     | 7.58 ft <sup>2</sup>       |
| Region<br>4  | Gravel Borrow  | 27,30,31,28,34,32,37,33,47,48,43                | 381.15<br>ft <sup>2</sup>  |
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel                                  | 7,6,11,12,13,38,35,32,34,25,9,8,26              | 856.44<br>ft <sup>2</sup>  |
| Region<br>6  | ESU 2B Medium Dense Sand/Gravel                                  | 14,15,16,17,18,19,20,21,22,23,24,10,25,34,28,31 | 748.7<br>ft <sup>2</sup>   |
| Region<br>7  | Gravel Borrow  | 32,35,38,36,37                                  | 26.85<br>ft <sup>2</sup>   |
| Region<br>8  | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill        | 12,39,40,41,36,38,13                            | 241.79<br>ft <sup>2</sup>  |
| Region<br>9  | Common Borrow  | 48,47,49,50                                     | 35.36<br>ft <sup>2</sup>   |
| Region<br>10 | Common Borrow  | 39,56,51,36,41,40                               | 75.79<br>ft²               |
| Region<br>11 |  | 46,54,49,42,52                                  | 58.52<br>ft <sup>2</sup>   |
| Region<br>12 |  | 46,45,53,54                                     | 12 ft²                     |
| Region<br>13 | Common Borrow  | 50,43,48  | 5.382<br>ft <sup>2</sup>   |
| Region<br>14 | Gravel Borrow  | 33,37,36,51                                     | 7.8 ft <sup>2</sup>        |
| Region<br>15 |  | 50,49,54,53                                     | 65.44<br>ft²               |
| Region<br>16 | Common Borrow  | 44,42,49,47,33,51,56,55                         | 171.02<br>ft <sup>2</sup>  |

Region 17

**Common Borrow** 

39,55,56

,56 9 ft<sup>2</sup>

# **Slip Results**

Slip Surfaces Analysed: 14669 of 16926 converged

# **Current Slip Surface**

Slip Surface: 2,917 Factor of Safety: 1.4 Volume: 964.30153 ft<sup>3</sup> Weight: 119,623.77 lbf

Resisting Moment: 3,841,902 lbf·ft Activating Moment: 2,844,209.1 lbf·ft

Resisting Force: 65,066.742 lbf Activating Force: 48,165.335 lbf Slip Rank: 1 of 16,926 slip surfaces Exit: (-29.191505, 193.28886) ft Entry: (35.110492, 233.5) ft

Radius: 48.823686 ft

Center: (-13.346822, 239.47001) ft

### **Slip Slices**

|            | Х                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material                         |
|------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|---------------------------------------|
| Slice<br>1 | -27.993629<br>ft | 192.91202<br>ft | -516.16509<br>psf | 130.71595<br>psf         | 88.169023<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>2 | -25.597876<br>ft | 192.22456<br>ft | -439.10696<br>psf | 326.08943<br>psf         | 219.9501<br>psf        | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>3 | -23.575 ft       | 191.73716<br>ft | -379.8495<br>psf  | 487.19333<br>psf         | 328.61605<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>4 | -21.925 ft       | 191.41312<br>ft | -336.10212<br>psf | 639.08296<br>psf         | 431.0669<br>psf        | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>5 | -19.7 ft         | 191.08204<br>ft | -283.71696<br>psf | 762.05705<br>psf         | 514.01397<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>6 | -17.05 ft        | 190.80311<br>ft | -228.5258<br>psf  | 847.19412<br>psf         | 571.43965<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>7 | -14.55 ft        | 190.67717<br>ft | -185.02014<br>psf | 895.81521<br>psf         | 604.23499<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>8 | -12.05 ft        | 190.67957<br>ft | -149.52288<br>psf | 918.26194<br>psf         | 619.3755<br>psf        | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |

| Slice<br>9  | -9.8166667<br>ft | 190.7841<br>ft  | -124.20051<br>psf | 1,014.0565<br>psf | 683.98973<br>psf  | 0 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel       |
|-------------|------------------|-----------------|-------------------|-------------------|-------------------|-------|-------|---------------------------------------|
| Slice<br>10 | -7.85 ft         | 190.96684<br>ft | -107.56117<br>psf | 1,073.0544<br>psf | 723.78431<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>11 | -5.8833333<br>ft | 191.23042<br>ft | -95.966132<br>psf | 1,115.1991<br>psf | 752.21127<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>12 | -4.5 ft          | 191.45626<br>ft | -90.333895<br>psf | 1,210.6808<br>psf | 816.6145<br>psf   | 0 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel       |
| Slice<br>13 | -2.5 ft          | 191.89475<br>ft | -88.611953<br>psf | 988.18274<br>psf  | 666.53768<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>14 | 0.3 ft           | 192.609 ft      | -92.265808<br>psf | 3,363.9375<br>psf | 2,269.0045<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>15 | 2.65 ft          | 193.35741<br>ft | -104.62665<br>psf | 3,171.8341<br>psf | 2,139.4291<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>16 | 4.95 ft          | 194.22137<br>ft | -124.92864<br>psf | 3,042.1261<br>psf | 2,051.94<br>psf   | 0 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel       |
| Slice<br>17 | 6.9397335<br>ft  | 195.07006<br>ft | -148.81188<br>psf | 2,938.9097<br>psf | 1,982.3196<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>18 | 8.6192006<br>ft  | 195.87687<br>ft | -174.6153<br>psf  | 2,833.5592<br>psf | 1,911.2598<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>19 | 10.579467<br>ft  | 196.93024<br>ft | -211.70084<br>psf | 2,680.2437<br>psf | 2,094.0359<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>20 | 12.9 ft          | 198.32599<br>ft | -267.76075<br>psf | 2,464.3368<br>psf | 1,925.3509<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>21 | 14.85 ft         | 199.62221<br>ft | -324.821<br>psf   | 2,304.7248<br>psf | 1,800.6483<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>22 | 16.3825 ft       | 200.75378<br>ft | -376.70807<br>psf | 2,157.4103<br>psf | 1,685.5536<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>23 | 18.3225 ft       | 202.34197<br>ft | -446.64663<br>psf | 1,915.9039<br>psf | 1,292.2935<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>24 | 20.6375 ft       | 204.45264<br>ft | -539.14455<br>psf | 1,716.9313<br>psf | 1,158.0848<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>25 | 22.9525 ft       | 206.86463<br>ft | -650.44462<br>psf | 1,504.2786<br>psf | 1,014.6488<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>26 | 25.305 ft        | 209.70505<br>ft | -779.89613<br>psf | 1,271.9474<br>psf | 857.93936<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>27 | 27.6375 ft       | 213.01935<br>ft | -931.69096<br>psf | 1,023.7669<br>psf | 690.53948<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |

| 1           | (1)             |                 |                    |                  |                  |       |       |   |
|-------------|-----------------|-----------------|--------------------|------------------|------------------|-------|-------|---|
| Slice<br>28 | 29.095109<br>ft | 215.34502<br>ft | -1,042.4314<br>psf | 864.18986<br>psf | 582.90342<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                           |
| Slice<br>29 | 29.457609<br>ft | 215.98544<br>ft | -1,073.8429<br>psf | 768.11291<br>psf | 667.71037<br>psf | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>30 | 29.51 ft        | 216.08102<br>ft | -1,078.5718<br>psf | 761.62025<br>psf | 662.06638<br>psf | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |
| Slice<br>31 | 30.51 ft        | 218.13436<br>ft | -1,182.9845<br>psf | 612.46929<br>psf | 532.41143<br>psf | 0 psf | 0 psf | ESU 1B Medium<br>Dense to Very<br>Dense Coarse-<br>Grained Fill |
| Slice<br>32 | 31.865 ft       | 221.06604<br>ft | -1,333.7853<br>psf | 426.82944<br>psf | 371.03717<br>psf | 0 psf | 0 psf | ESU 1B Medium<br>Dense to Very<br>Dense Coarse-<br>Grained Fill |
| Slice<br>33 | 32.811756<br>ft | 223.66134<br>ft | -1,472.4813<br>psf | 289.67872<br>psf | 251.81387<br>psf | 0 psf | 0 psf | ESU 1B Medium<br>Dense to Very<br>Dense Coarse-<br>Grained Fill |
| Slice<br>34 | 33.754961<br>ft | 226.69236<br>ft | -1,637.9556<br>psf | 183.77908<br>psf | 114.83791<br>psf | 0 psf | 0 psf | Common Borrow   |
| Slice<br>35 | 34.613451<br>ft | 230.76238<br>ft | -1,870.3884        | 53.915981<br>nsf | 33.690444        | 0 psf | 0 psf | Common Borrow   |

# 1A.2 Compound - Static (M-P)

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# **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 318 Date: 01/13/2022

Tool Version: 11.1.1.22085

Time: 03:58:28 PM

File Name: Wall 05.85L-B Sta 2+60\_FC Wall (lightweight fill).gsz Directory: P:\0\0180366\01\Analysis\Wall 05.85L-B\22-01-13\

Last Solved Date: 01/13/2022 Last Solved Time: 04:00:28 PM

# **Project Settings**

Unit System: U.S. Customary Units

# **Analysis Settings**

#### 1A.2 Compound - Static (M-P)

Kind: SLOPE/W

Analysis Type: Morgenstern-Price

Settings

**Side Function** 

Interslice force function option: Half-Sine

PWP Conditions from: Piezometric Line

Apply Phreatic Correction: No
Use Staged Rapid Drawdown: No
Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 1

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

**Factor of Safety Convergence Settings** 

Maximum Number of Iterations: 100
Tolerable difference in F of S: 0.001

**Solution Settings** 

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

#### **Materials**

#### **ESU 1B Medium Dense to Very Dense Coarse-Grained Fill**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 41 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### **ESU 2B Medium Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 115 pcf Effective Cohesion: 0 psf Effective Friction Angle: 34 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

Pore Water Pressure

Piezometric Line: 1

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 42 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### Reinforcements

### Row 1 (2 strips)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 6.6 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 2 (2 strips)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 6.1 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 3 (2 strips)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 5.6 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 4 (2 strips)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 5.1 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 5 (2 strips)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 4.6 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

### Row 6 (2 strips)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 4.1 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 7 (2 strips)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 3.6 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 8 (2 strips)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 3.1 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 9+ (2 strips)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 2.7 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

# **Slip Surface Entry and Exit**

Left Type: Range

Left-Zone Left Coordinate: (-35.900009, 192.42444) ft

Left-Zone Right Coordinate: (-0.9, 206) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15.000006, 226.34416) ft

Right-Zone Right Coordinate: (60, 233.74338) ft

Right-Zone Increment: 30 Radius Increments: 20

# **Slip Surface Limits**

Left Coordinate: (-80, 186.2) ft Right Coordinate: (80, 234.2) ft

### **Piezometric Lines**

#### Piezometric Line 1

#### Coordinates

|               | Х         | Υ          |
|---------------|-----------|------------|
| Coordinate 1  | -48.3 ft  | 180 ft     |
| Coordinate 2  | -4.1 ft   | 190.1 ft   |
| Coordinate 3  | 11.7 ft   | 193.8 ft   |
| Coordinate 4  | 17.165 ft | 194.87 ft  |
| Coordinate 5  | 24.11 ft  | 196.755 ft |
| Coordinate 6  | 29.52 ft  | 198.8 ft   |
| Coordinate 7  | 32.23 ft  | 199.83 ft  |
| Coordinate 8  | 60.885 ft | 211.35 ft  |
| Coordinate 9  | 70.775 ft | 215.12 ft  |
| Coordinate 10 | 74.125 ft | 216.15 ft  |
| Coordinate 11 | 80 ft     | 217.365 ft |

# **Reinforcement Lines**

#### **Reinforcement Line 1**

Reinforcement: Row 1 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 218.4) ft Inside Point: (15.6, 218.4) ft

Length: 16.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 2**

Reinforcement: Row 3 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 213.6) ft Inside Point: (15.6, 213.6) ft

Length: 16.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 3**

Reinforcement: Row 2 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 216) ft Inside Point: (15.6, 216) ft

Length: 16.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 4**

Reinforcement: Row 7 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 204) ft Inside Point: (15.6, 204) ft

Length: 16.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 5**

Reinforcement: Row 6 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 206.4) ft Inside Point: (15.6, 206.4) ft

Length: 16.5 ft

Orientation: 0°

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### Reinforcement Line 6

Reinforcement: Row 5 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 208.8) ft Inside Point: (15.6, 208.8) ft

Length: 16.5 ft
Orientation: 0°

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 7**

Reinforcement: Row 4 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 211.2) ft Inside Point: (15.6, 211.2) ft

Length: 16.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 8**

Reinforcement: Row 9+ (2 strips) Lock to Ground Surface: No Outside Point: (-0.9, 196.8) ft Inside Point: (15.6, 196.8) ft

Length: 16.5 ft Orientation: 0 °

Slip Surface Intersection: (8.7606853, 196.8) ft

Max. Pullout Force: 3,930 lbf Available Length: 6.8393147 ft Required Length: 6.8393147 ft Pullout Force: 2,183.2842 lbf Pullout Force per Length: 319.22558 lbf/ft Governing Component: Pullout Resistance

#### **Reinforcement Line 9**

Reinforcement: Row 9+ (2 strips) Lock to Ground Surface: No Outside Point: (-0.9, 199.2) ft Inside Point: (15.6, 199.2) ft

Length: 16.5 ft
Orientation: 0°

Slip Surface Intersection: (12.7803, 199.2) ft

Max. Pullout Force: 3,930 lbf Available Length: 2.8197002 ft Required Length: 2.8197002 ft Pullout Force: 883.16088 lbf

Pullout Force per Length: 313.21092 lbf/ft Governing Component: Pullout Resistance

#### **Reinforcement Line 10**

Reinforcement: Row 8 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 201.6) ft Inside Point: (15.6, 201.6) ft

Length: 16.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

# **Surcharge Loads**

## **Surcharge Load 1**

Surcharge (Unit Weight): 250 pcf

**Direction: Vertical** 

#### **Coordinates**

| Х       | Υ        |
|---------|----------|
| 43 ft   | 234.5 ft |
| 45 ft   | 234.5 ft |
| 58.1 ft | 234.7 ft |
| 80 ft   | 235.2 ft |

# Geometry

Name: 1. Compound Stability

**Settings** 

View: 2D

Element Thickness: 1 ft

#### **Points**

|                      | Х                    | Υ                    |
|----------------------|----------------------|----------------------|
| Point 1              | 80 ft                | 199.4 ft             |
| Point 2              | 58 ft                | 196.6 ft             |
| Point 3              | 37.6 ft              | 191.9 ft             |
| Point 4              | 42.1 ft              | 180 ft               |
| Point 5              | 80 ft                | 180 ft               |
| Point 6              | 80 ft                | 226 ft               |
| Point 7              | 58 ft                | 225.3 ft             |
| Point 8              | 29.8 ft              | 195 ft               |
| Point 9              | 11.7 ft              | 193.8 ft             |
| Point 10             | -48.3 ft             | 180 ft               |
| Point 11             | 80 ft                | 234.2 ft             |
| Point 12             | 58.1 ft              | 234.2 ft<br>233.7 ft |
| Point 13             | 26.5 ft              | 214.1 ft             |
| Point 14             | -10.8 ft             | 197 ft               |
| Point 15             | -10.8 ft             | 197 it               |
| Point 16             | -10.5 ft<br>-21.1 ft | 193.3 ft<br>194.7 ft |
| Point 17             | -21.1 It             | 194.7 ft<br>193.6 ft |
| Point 17             | -32.1 ft             | 193.0 ft<br>193.1 ft |
| Point 19             | -36.6 ft             | 193.1 ft<br>192.3 ft |
| Point 20             | -61.7 ft             | 192.5 ft<br>189.7 ft |
| Point 20             | -65.4 ft             | 189.7 ft<br>189.3 ft |
| Point 22             | -73.2 ft             | 189.5 ft             |
| Point 23             | -73.2 It             | 186.2 ft             |
| Point 24             | -80 ft               | 180.2 It             |
| Point 25             | -4.1 ft              | 190.1 ft             |
| Point 26             | 32 ft                | 190.1 ft<br>197.4 ft |
| Point 27             | -0.9 ft              | 219.4 ft             |
|                      | -0.9 ft              |                      |
| Point 28<br>Point 29 | -0.9 ft              | 196.3 ft<br>199.8 ft |
|                      |                      |                      |
| Point 30<br>Point 31 | -0.9 ft<br>-0.9 ft   | 199.8 ft<br>199.4 ft |
| Point 32             | 15.6 ft              | 199.4 ft<br>196.3 ft |
| Point 32<br>Point 33 | 15.6 ft              | 219.4 ft             |
| Point 34             | 11.1 ft              |                      |
|                      | 17.1 ft              | 196.3 ft<br>196.3 ft |
| Point 35             |                      |                      |
| Point 36 Point 37    | 17.1 ft<br>15.6 ft   | 214.2 ft<br>214.2 ft |
|                      |                      |                      |
| Point 38             | 17.1 ft              | 208.4 ft             |
| Point 39             | 45 ft                | 233.5 ft             |
| Point 40             | 37.1 ft              | 228.2 ft             |
|                      |                      |                      |

| Point 41 | 29.4 ft   | 222.3 ft  |
|----------|-----------|-----------|
| Point 42 | 29.5 ft   | 233.5 ft  |
| Point 43 | 1.5 ft    | 219.4 ft  |
| Point 44 | 31.5 ft   | 233.5 ft  |
| Point 45 | 6.1 ft    | 233.5 ft  |
| Point 46 | 14.1 ft   | 233.5 ft  |
| Point 47 | 14.1 ft   | 219.4 ft  |
| Point 48 | 6.1 ft    | 219.4 ft  |
| Point 49 | 14.1 ft   | 225.9 ft  |
| Point 50 | 6.1 ft    | 221.74 ft |
| Point 51 | 17.1 ft   | 219.4 ft  |
| Point 52 | 28.775 ft | 233.5 ft  |
| Point 53 | 6.1 ft    | 232 ft    |
| Point 54 | 14.1 ft   | 232 ft    |
| Point 55 | 39 ft     | 233.5 ft  |
| Point 56 | 39 ft     | 230.5 ft  |

# Regions

|              | Material   | Points  | Area                       |
|--------------|--|---|----------------------------|
| Region<br>1  | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 1,2,3,4,5                                       | 659.92<br>ft <sup>2</sup>  |
| Region<br>2  | ESU 4B Dense to Very Dense Sand/Gravel                           | 1,6,7,26,8,9,25,10,4,3,2                        | 1,867.8<br>ft <sup>2</sup> |
| Region<br>3  | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill        | 14,29,30,31                                     | 7.58 ft <sup>2</sup>       |
| Region<br>4  | Gravel Borrow  | 27,30,31,28,34,32,37,33,47,48,43                | 381.15<br>ft <sup>2</sup>  |
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel                                  | 7,6,11,12,13,38,35,32,34,25,9,8,26              | 856.44<br>ft <sup>2</sup>  |
| Region<br>6  | ESU 2B Medium Dense Sand/Gravel                                  | 14,15,16,17,18,19,20,21,22,23,24,10,25,34,28,31 | 748.7<br>ft <sup>2</sup>   |
| Region<br>7  | Gravel Borrow  | 32,35,38,36,37                                  | 26.85<br>ft <sup>2</sup>   |
| Region<br>8  | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill        | 12,39,40,41,36,38,13                            | 241.79<br>ft <sup>2</sup>  |
| Region<br>9  | Common Borrow  | 48,47,49,50                                     | 35.36<br>ft <sup>2</sup>   |
| Region<br>10 | Common Borrow  | 39,56,51,36,41,40                               | 75.79<br>ft²               |
| Region<br>11 |  | 46,54,49,42,52                                  | 58.52<br>ft <sup>2</sup>   |
| Region<br>12 |  | 46,45,53,54                                     | 12 ft²                     |
| Region<br>13 | Common Borrow  | 50,43,48  | 5.382<br>ft <sup>2</sup>   |
| Region<br>14 | Gravel Borrow  | 33,37,36,51                                     | 7.8 ft <sup>2</sup>        |
| Region<br>15 |  | 50,49,54,53                                     | 65.44<br>ft²               |
| Region<br>16 | Common Borrow  | 44,42,49,47,33,51,56,55                         | 171.02<br>ft <sup>2</sup>  |

Region 17 Common Borrow

39,55,56

9 ft<sup>2</sup>

# **Slip Results**

Slip Surfaces Analysed: 16544 of 16926 converged

# **Current Slip Surface**

Slip Surface: 2,265 Factor of Safety: 1.4 Volume: 928.50885 ft<sup>3</sup> Weight: 115,303.02 lbf

Resisting Moment: 3,899,195.6 lbf·ft Activating Moment: 2,882,123.5 lbf·ft

Resisting Force: 62,661.305 lbf Activating Force: 46,328.074 lbf Slip Rank: 1 of 16,926 slip surfaces Exit: (-30.881499, 193.17912) ft Entry: (35.110492, 233.5) ft

Radius: 51.132236 ft

Center: (-15.328929, 241.8887) ft

#### Slip Slices

|            | X                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material                         |
|------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|---------------------------------------|
| Slice<br>1 | -29.801249<br>ft | 192.86025<br>ft | -538.70937<br>psf | 56.321042<br>psf         | 37.989022<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>2 | -27.640749<br>ft | 192.27332<br>ft | -471.2788<br>psf  | 171.6749<br>psf          | 115.79618<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>3 | -25.48025<br>ft  | 191.78639<br>ft | -410.08817<br>psf | 285.30554<br>psf         | 192.44102<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>4 | -23.575 ft       | 191.43269<br>ft | -360.85056<br>psf | 415.10506<br>psf         | 279.9919<br>psf        | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>5 | -21.925 ft       | 191.19052<br>ft | -322.21229<br>psf | 561.412<br>psf           | 378.67717<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>6 | -19.7 ft         | 190.96302<br>ft | -276.2903<br>psf  | 719.55436<br>psf         | 485.34554<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>7 | -17.05 ft        | 190.80075<br>ft | -228.37841<br>psf | 863.19223<br>psf         | 582.23051<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>8 | -14.55 ft        | 190.77769<br>ft | -191.29237<br>psf | 959.35748<br>psf         | 647.09479<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |

| Slice<br>9  | -12.05 ft        | 190.87708<br>ft | -161.84772<br>psf | 1,010.2664<br>psf | 681.43331<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
|-------------|------------------|-----------------|-------------------|-------------------|-------------------|-------|-------|---------------------------------------|
| Slice<br>10 | -9.8166667<br>ft | 191.06408<br>ft | -141.6716<br>psf  | 1,142.9419<br>psf | 770.92407<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>11 | -7.85 ft         | 191.31615<br>ft | -129.35837<br>psf | 1,201.7526<br>psf | 810.59239<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>12 | -5.8833333<br>ft | 191.64644<br>ft | -121.926<br>psf   | 1,229.1342<br>psf | 829.06148<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>13 | -4.5 ft          | 191.91799<br>ft | -119.146<br>psf   | 1,419.9113<br>psf | 957.74224<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>14 | -2.5 ft          | 192.4196<br>ft  | -121.36291<br>psf | 1,049.4292<br>psf | 707.84893<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>15 | 0.3 ft           | 193.21989<br>ft | -130.38527<br>psf | 3,374.9653<br>psf | 2,276.4429<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>16 | 2.65 ft          | 194.03732<br>ft | -147.05359<br>psf | 3,111.5234<br>psf | 2,098.749<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>17 | 4.95 ft          | 194.96642<br>ft | -171.41978<br>psf | 2,908.2294<br>psf | 1,961.6255<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>18 | 6.9632694<br>ft  | 195.88171<br>ft | -199.11505<br>psf | 2,756.3233<br>psf | 1,859.1635<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>19 | 8.7949041<br>ft  | 196.81832<br>ft | -230.79406<br>psf | 2,600.0515<br>psf | 2,031.3829<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>20 | 10.731635<br>ft  | 197.91046<br>ft | -270.64333<br>psf | 2,351.7228<br>psf | 1,837.3672<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>21 | 12.9 ft          | 199.2793<br>ft  | -327.24758<br>psf | 2,146.5509<br>psf | 1,677.0693<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>22 | 14.85 ft         | 200.6228<br>ft  | -387.25821<br>psf | 1,960.3311<br>psf | 1,531.5785<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>23 | 16.3825 ft       | 201.79013<br>ft | -441.37623<br>psf | 1,831.3356<br>psf | 1,430.7962<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>24 | 18.3225 ft       | 203.42155<br>ft | -514.01285<br>psf | 1,625.0919<br>psf | 1,096.1383<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>25 | 20.6375 ft       | 205.58076<br>ft | -609.53921<br>psf | 1,476.4044<br>psf | 995.84734<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>26 | 22.9525 ft       | 208.03631<br>ft | -723.55768<br>psf | 1,330.2509<br>psf | 897.26559<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>27 | 25.305 ft        | 210.91284<br>ft | -855.26237<br>psf | 1,177.9053<br>psf | 794.50715<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice       |                  | 213.84623       | -988.97439        | 1,034.57          | 697.8263          |       |       | ESU 2B Medium                         |

| -           |                 |                 |                    |                  |                  |       |       |  |
|-------------|-----------------|-----------------|--------------------|------------------|------------------|-------|-------|--|
| 28          | 27.39643 ft     | ft              | psf                | psf              | psf              | 0 psf | 0 psf | Dense<br>Sand/Gravel                                   |
| Slice<br>29 | 28.53393 ft     | 215.61448<br>ft | -1,072.4821<br>psf | 862.9674<br>psf  | 750.16612<br>psf | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill |
| Slice<br>30 | 29.0875 ft      | 216.56503<br>ft | -1,118.7396<br>psf | 812.85067<br>psf | 706.60031<br>psf | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill |
| Slice<br>31 | 29.45 ft        | 217.20384<br>ft | -1,150.0509<br>psf | 779.7648<br>psf  | 677.8392<br>psf  | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill |
| Slice<br>32 | 29.51 ft        | 217.31279<br>ft | -1,155.4339<br>psf | 773.90486<br>psf | 672.74523<br>psf | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill |
| Slice<br>33 | 30.51 ft        | 219.34394<br>ft | -1,258.4626<br>psf | 644.46469<br>psf | 560.22461<br>psf | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill |
| Slice<br>34 | 31.865 ft       | 222.23324<br>ft | -1,406.6186<br>psf | 474.83345<br>psf | 412.76642<br>psf | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill |
| Slice<br>35 | 32.583646<br>ft | 224.06001<br>ft | -1,503.0809<br>psf | 374.38743<br>psf | 325.45003<br>psf | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill |
| Slice<br>36 | 33.393451<br>ft | 226.44996<br>ft | -1,631.8989<br>psf | 311.68882<br>psf | 194.76479<br>psf | 0 psf | 0 psf | Common Borrow  |
| Slice<br>37 | 34.48005 ft     | 230.69476<br>ft | -1,869.5158<br>psf | 104.33588<br>psf | 65.196295<br>psf | 0 psf | 0 psf | Common Borrow  |

# 1A.3 Compound - Pseudo-Static (Spencer)

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# **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 321 Date: 01/19/2022 Time: 02:28:08 PM

Tool Version: 11.1.1.22085

File Name: Wall 05.85L-B Sta 2+60\_FC Wall (lightweight fill).gsz Directory: P:\0\0180366\01\Analysis\Wall 05.85L-B\22-01-13\

Last Solved Date: 01/19/2022 Last Solved Time: 02:28:57 PM

# **Project Settings**

Unit System: U.S. Customary Units

# **Analysis Settings**

#### 1A.3 Compound - Pseudo-Static (Spencer)

Kind: SLOPE/W

Analysis Type: Spencer

Settings

**PWP Conditions from: Piezometric Line** 

Apply Phreatic Correction: No Use Staged Rapid Drawdown: No

Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit

Critical slip surfaces saved: 1

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

```
Factor of Safety Convergence Settings

Maximum Number of Iterations: 100

Tolerable difference in F of S: 0.001

Solution Settings
```

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3 Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

### **Materials**

### **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb Unit Weight: 130 pcf

Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 42 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### **ESU 1B Medium Dense to Very Dense Coarse-Grained Fill (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 100 psf Effective Friction Angle: 41 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 115 pcf Effective Cohesion: 200 psf Effective Friction Angle: 34°

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### **Common Borrow (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 50 psf Effective Friction Angle: 32 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### Reinforcements

### Row 1 (2 strips)(EQ)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 8.8 °
Surface Area Factor: 2

Sarrace / ii ca ractor. Z

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

## Row 2 (2 strips)(EQ)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 8.2 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

# Row 3 (2 strips)(EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 7.5 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

## Row 4 (2 strips)(EQ)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 6.8 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

## Row 5 (2 strips)(EQ)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 6.2 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

## Row 6 (2 strips)(EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 5.5 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

## Row 7 (2 strips)(EQ)

Type: Geosynthetic

Interface Adhesion: 0 psf Interface Shear Angle: 4.9 °

Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

## Row 8 (2 strips)(EQ)

Type: Geosynthetic

Interface Adhesion: 0 psf Interface Shear Angle: 4.2 °

Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

## Row 9+ (2 strips)(EQ)

Type: Geosynthetic

Interface Adhesion: 0 psf Interface Shear Angle: 3.6 °

Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

# Slip Surface Entry and Exit

Left Type: Range

Left-Zone Left Coordinate: (-25, 193.56104) ft Left-Zone Right Coordinate: (-0.9, 206) ft

Left-Zone Increment: 20

Right Type: Range

Right-Zone Left Coordinate: (21.860569, 229.72989) ft

Right-Zone Right Coordinate: (60, 233.74338) ft

Right-Zone Increment: 20 Radius Increments: 20

# **Slip Surface Limits**

Left Coordinate: (-80, 186.2) ft Right Coordinate: (80, 234.2) ft

# **Piezometric Lines**

#### Piezometric Line 1

#### **Coordinates**

|               | Х         | Υ          |
|---------------|-----------|------------|
| Coordinate 1  | -48.3 ft  | 180 ft     |
| Coordinate 2  | -4.1 ft   | 190.1 ft   |
| Coordinate 3  | 11.7 ft   | 193.8 ft   |
| Coordinate 4  | 17.165 ft | 194.87 ft  |
| Coordinate 5  | 24.11 ft  | 196.755 ft |
| Coordinate 6  | 29.52 ft  | 198.8 ft   |
| Coordinate 7  | 32.23 ft  | 199.83 ft  |
| Coordinate 8  | 60.885 ft | 211.35 ft  |
| Coordinate 9  | 70.775 ft | 215.12 ft  |
| Coordinate 10 | 74.125 ft | 216.15 ft  |
| Coordinate 11 | 80 ft     | 217.365 ft |

# **Seismic Coefficients**

Horz Seismic Coef.: 0.208

# **Reinforcement Lines**

#### **Reinforcement Line 1**

Reinforcement: Row 1 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 218.4) ft Inside Point: (15.6, 218.4) ft

Length: 16.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf
Available Length: 0 ft
Required Length: 0 ft

Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### Reinforcement Line 2

Reinforcement: Row 3 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 213.6) ft Inside Point: (15.6, 213.6) ft

Length: 16.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 3**

Reinforcement: Row 2 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 216) ft Inside Point: (15.6, 216) ft

Length: 16.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 4**

Reinforcement: Row 7 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 204) ft Inside Point: (15.6, 204) ft

Length: 16.5 ft
Orientation: 0 °

Slip Surface Intersection: (2.6901579, 204) ft

Max. Pullout Force: 5,240 lbf Available Length: 12.909842 ft Required Length: 12.909842 ft Pullout Force: 4,613.2725 lbf

Pullout Force per Length: 357.34539 lbf/ft Governing Component: Pullout Resistance

#### **Reinforcement Line 5**

Reinforcement: Row 6 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 206.4) ft Inside Point: (15.6, 206.4) ft

Length: 16.5 ft
Orientation: 0 °

Slip Surface Intersection: (6.3238779, 206.4) ft

Max. Pullout Force: 5,240 lbf Available Length: 9.2761221 ft Required Length: 9.2761221 ft Pullout Force: 3,523.3844 lbf

Pullout Force per Length: 379.83376 lbf/ft Governing Component: Pullout Resistance

#### **Reinforcement Line 6**

Reinforcement: Row 5 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 208.8) ft Inside Point: (15.6, 208.8) ft

Length: 16.5 ft
Orientation: 0 °

Slip Surface Intersection: (9.7925061, 208.8) ft

Max. Pullout Force: 5,240 lbf Available Length: 5.8074939 ft Required Length: 5.8074939 ft Pullout Force: 2,390.913 lbf

Pullout Force per Length: 411.69444 lbf/ft Governing Component: Pullout Resistance

#### Reinforcement Line 7

Reinforcement: Row 4 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 211.2) ft Inside Point: (15.6, 211.2) ft

Length: 16.5 ft Orientation: 0 °

Slip Surface Intersection: (13.115125, 211.2) ft

Max. Pullout Force: 5,240 lbf Available Length: 2.4848745 ft Required Length: 2.4848745 ft Pullout Force: 1,049.766 lbf

Pullout Force per Length: 422.4624 lbf/ft Governing Component: Pullout Resistance

#### **Reinforcement Line 8**

Reinforcement: Row 9+ (2 strips)(EQ)

Lock to Ground Surface: No Outside Point: (-0.9, 196.8) ft Inside Point: (15.6, 196.8) ft

Length: 16.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 9**

Reinforcement: Row 9+ (2 strips)(EQ)

Lock to Ground Surface: No Outside Point: (-0.9, 199.2) ft Inside Point: (15.6, 199.2) ft

Length: 16.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 10**

Reinforcement: Row 8 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 201.6) ft Inside Point: (15.6, 201.6) ft

Length: 16.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

# **Surcharge Loads**

# Surcharge Load 1

Surcharge (Unit Weight): 125 pcf

**Direction: Vertical** 

#### Coordinates

| Х     | Υ        |  |
|-------|----------|--|
| 43 ft | 234.5 ft |  |

| 45 ft   | 234.5 ft |
|---------|----------|
| 58.1 ft | 234.7 ft |
| 80 ft   | 235.2 ft |

# **Geometry**

Name: 1. Compound Stability

**Settings** 

View: 2D

Element Thickness: 1 ft

# **Points**

| 163      | Х        | Υ        |
|----------|----------|----------|
| Point 1  | 80 ft    | 199.4 ft |
| Point 2  | 58 ft    | 196.6 ft |
| Point 3  | 37.6 ft  | 191.9 ft |
| Point 4  | 42.1 ft  | 180 ft   |
| Point 5  | 80 ft    | 180 ft   |
| Point 6  | 80 ft    | 226 ft   |
| Point 7  | 58 ft    | 225.3 ft |
| Point 8  | 29.8 ft  | 195 ft   |
| Point 9  | 11.7 ft  | 193.8 ft |
| Point 10 | -48.3 ft | 180 ft   |
| Point 11 | 80 ft    | 234.2 ft |
| Point 12 | 58.1 ft  | 233.7 ft |
| Point 13 | 26.5 ft  | 214.1 ft |
| Point 14 | -10.8 ft | 197 ft   |
| Point 15 | -18.3 ft | 195.3 ft |
| Point 16 | -21.1 ft | 194.7 ft |
| Point 17 | -24.4 ft | 193.6 ft |
| Point 18 | -32.1 ft | 193.1 ft |
| Point 19 | -36.6 ft | 192.3 ft |
| Point 20 | -61.7 ft | 189.7 ft |
| Point 21 | -65.4 ft | 189.3 ft |
| Point 22 | -73.2 ft | 188 ft   |
| Point 23 | -80 ft   | 186.2 ft |
| Point 24 | -80 ft   | 180 ft   |
| Point 25 | -4.1 ft  | 190.1 ft |
| Point 26 | 32 ft    | 197.4 ft |
| Point 27 | -0.9 ft  | 219.4 ft |
| Point 28 | -0.9 ft  | 196.3 ft |
| Point 29 | -4.9 ft  | 199.8 ft |
| Point 30 | -0.9 ft  | 199.8 ft |
| Point 31 | -0.9 ft  | 199.4 ft |
| Point 32 | 15.6 ft  | 196.3 ft |
| Point 33 | 15.6 ft  | 219.4 ft |
| Point 34 | 11.1 ft  | 196.3 ft |
|          |          |          |

| _        | _         |           |
|----------|-----------|-----------|
| Point 35 | 17.1 ft   | 196.3 ft  |
| Point 36 | 17.1 ft   | 214.2 ft  |
| Point 37 | 15.6 ft   | 214.2 ft  |
| Point 38 | 17.1 ft   | 208.4 ft  |
| Point 39 | 45 ft     | 233.5 ft  |
| Point 40 | 37.1 ft   | 228.2 ft  |
| Point 41 | 29.4 ft   | 222.3 ft  |
| Point 42 | 29.5 ft   | 233.5 ft  |
| Point 43 | 1.5 ft    | 219.4 ft  |
| Point 44 | 31.5 ft   | 233.5 ft  |
| Point 45 | 6.1 ft    | 233.5 ft  |
| Point 46 | 14.1 ft   | 233.5 ft  |
| Point 47 | 14.1 ft   | 219.4 ft  |
| Point 48 | 6.1 ft    | 219.4 ft  |
| Point 49 | 14.1 ft   | 225.9 ft  |
| Point 50 | 6.1 ft    | 221.74 ft |
| Point 51 | 17.1 ft   | 219.4 ft  |
| Point 52 | 28.775 ft | 233.5 ft  |
| Point 53 | 6.1 ft    | 232 ft    |
| Point 54 | 14.1 ft   | 232 ft    |
| Point 55 | 39 ft     | 233.5 ft  |
| Point 56 | 39 ft     | 230.5 ft  |

# Regions

|              | Material  | Points  | Area                       |
|--------------|---|---|----------------------------|
| Region<br>1  | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt              | 1,2,3,4,5                                       | 659.92<br>ft²              |
| Region<br>2  | ESU 4B Dense to Very Dense Sand/Gravel  | 1,6,7,26,8,9,25,10,4,3,2                        | 1,867.8<br>ft <sup>2</sup> |
| Region<br>3  | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill (Apparent Cohesion) | 14,29,30,31                                     | 7.58 ft <sup>2</sup>       |
| Region<br>4  | Gravel Borrow   | 27,30,31,28,34,32,37,33,47,48,43                | 381.15<br>ft <sup>2</sup>  |
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                           | 7,6,11,12,13,38,35,32,34,25,9,8,26              | 856.44<br>ft <sup>2</sup>  |
| Region<br>6  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                           | 14,15,16,17,18,19,20,21,22,23,24,10,25,34,28,31 | 748.7<br>ft²               |
| Region<br>7  | Gravel Borrow   | 32,35,38,36,37                                  | 26.85<br>ft <sup>2</sup>   |
| Region<br>8  | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill (Apparent Cohesion) | 12,39,40,41,36,38,13                            | 241.79<br>ft <sup>2</sup>  |
| Region<br>9  | Common Borrow (Apparent Cohesion)   | 48,47,49,50                                     | 35.36<br>ft <sup>2</sup>   |
| Region<br>10 | Common Borrow (Apparent Cohesion)   | 39,56,51,36,41,40                               | 75.79<br>ft²               |
| Region<br>11 |   | 46,54,49,42,52                                  | 58.52<br>ft <sup>2</sup>   |
| Region<br>12 |   | 46,45,53,54                                     | 12 ft²                     |
| Region       | Common Borrow (Apparent Cohesion)   | 50,43,48  | 5.382                      |

| 13           |                                   |                         | ft²                       |
|--------------|-----------------------------------|-------------------------|---------------------------|
| Region<br>14 | Gravel Borrow                     | 33,37,36,51             | 7.8 ft <sup>2</sup>       |
| Region<br>15 |                                   | 50,49,54,53             | 65.44<br>ft²              |
| Region<br>16 | Common Borrow (Apparent Cohesion) | 44,42,49,47,33,51,56,55 | 171.02<br>ft <sup>2</sup> |
| Region<br>17 | Common Borrow (Apparent Cohesion) | 39,55,56                | 9 ft²                     |

# **Slip Results**

Slip Surfaces Analysed: 6454 of 9261 converged

# **Current Slip Surface**

Slip Surface: 6,366 Factor of Safety: 1.1 Volume: 451.08584 ft<sup>3</sup> Weight: 56,233.146 lbf

Resisting Moment: 7,075,518.1 lbf·ft Activating Moment: 6,661,339.1 lbf·ft

Resisting Force: 28,417.582 lbf Activating Force: 26,776.632 lbf Slip Rank: 1 of 9,261 slip surfaces

Exit: (-0.9, 201.73514) ft Entry: (38.540419, 233.5) ft

Radius: 201.32979 ft

Center: (-106.4613, 373.17171) ft

## Slip Slices

|            | X               | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material |
|------------|-----------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|---------------|
| Slice<br>1 | -0.3 ft         | 202.1075<br>ft  | -693.73979<br>psf | 2,943.0247<br>psf        | 2,299.3429<br>psf      | 0 psf                | 0 psf               | Gravel Borrow |
| Slice<br>2 | 0.9 ft          | 202.85808<br>ft | -723.04082<br>psf | 2,848.9888<br>psf        | 2,225.874<br>psf       | 0 psf                | 0 psf               | Gravel Borrow |
| Slice<br>3 | 2.2666667<br>ft | 203.72826<br>ft | -757.36922<br>psf | 2,426.5787<br>psf        | 1,895.851<br>psf       | 0 psf                | 0 psf               | Gravel Borrow |
| Slice<br>4 | 3.8 ft          | 204.72204<br>ft | -796.97537<br>psf | 1,625.1968<br>psf        | 1,269.7429<br>psf      | 0 psf                | 0 psf               | Gravel Borrow |
| Slice<br>5 | 5.3333333<br>ft | 205.73577<br>ft | -837.82579<br>psf | 1,577.5718<br>psf        | 1,232.5342<br>psf      | 0 psf                | 0 psf               | Gravel Borrow |
| Slice<br>6 | 6.8 ft          | 206.72398<br>ft | -878.05855<br>psf | 1,575.8907<br>psf        | 1,231.2207<br>psf      | 0 psf                | 0 psf               | Gravel Borrow |
| Slice<br>7 | 8.2 ft          | 207.68532<br>ft | -917.58815<br>psf | 1,236.1727<br>psf        | 965.80399<br>psf       | 0 psf                | 0 psf               | Gravel Borrow |
| Slice<br>8 | 9.6 ft          | 208.66419<br>ft | -958.21176<br>psf | 1,196.5468<br>psf        | 934.84483<br>psf       | 0 psf                | 0 psf               | Gravel Borrow |

| Slice<br>9  | 11 ft           | 209.6609<br>ft  | -999.94902<br>psf  | 1,010.4433<br>psf | 789.44479<br>psf | 0 psf  | 0 psf | Gravel Borrow                           |
|-------------|-----------------|-----------------|--------------------|-------------------|------------------|--------|-------|---|
| Slice<br>10 | 12.3 ft         | 210.60207<br>ft | -1,041.119<br>psf  | 982.78465<br>psf  | 767.83552<br>psf | 0 psf  | 0 psf | Gravel Borrow                           |
| Slice<br>11 | 13.5 ft         | 211.48555<br>ft | -1,081.5872<br>psf | 949.7675<br>psf   | 742.03969<br>psf | 0 psf  | 0 psf | Gravel Borrow                           |
| Slice<br>12 | 14.85 ft        | 212.49698<br>ft | -1,128.2065<br>psf | 858.87059<br>psf  | 671.02325<br>psf | 0 psf  | 0 psf | Gravel Borrow                           |
| Slice<br>13 | 16.3825 ft      | 213.66588<br>ft | -1,182.4229<br>psf | 814.49163<br>psf  | 636.3506<br>psf  | 0 psf  | 0 psf | Gravel Borrow                           |
| Slice<br>14 | 17.8595 ft      | 214.81375<br>ft | -1,232.7275<br>psf | 739.53991<br>psf  | 462.11582<br>psf | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>15 | 19.2485 ft      | 215.91415<br>ft | -1,277.8677<br>psf | 705.76374<br>psf  | 441.01013<br>psf | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>16 | 20.6375 ft      | 217.03466<br>ft | -1,324.2629<br>psf | 671.5971<br>psf   | 419.66045<br>psf | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>17 | 22.0265 ft      | 218.17572<br>ft | -1,371.9402<br>psf | 637.05382<br>psf  | 398.07541<br>psf | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>18 | 23.4155 ft      | 219.33779<br>ft | -1,420.9284<br>psf | 602.14781<br>psf  | 376.26371<br>psf | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>19 | 24.693125<br>ft | 220.42482<br>ft | -1,463.2426<br>psf | 569.77766<br>psf  | 356.0366<br>psf  | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>20 | 25.859375<br>ft | 221.43402<br>ft | -1,498.7078<br>psf | 539.94007<br>psf  | 337.392<br>psf   | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>21 | 27.025625<br>ft | 222.45901<br>ft | -1,535.1579<br>psf | 509.87418<br>psf  | 318.60475<br>psf | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>22 | 28.191875<br>ft | 223.5001<br>ft  | -1,572.613<br>psf  | 479.5884<br>psf   | 299.68009<br>psf | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>23 | 29.1375 ft      | 224.35501<br>ft | -1,603.6549<br>psf | 454.9442<br>psf   | 284.28069<br>psf | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>24 | 29.51 ft        | 224.69447<br>ft | -1,616.0509<br>psf | 444.96775<br>psf  | 278.04671<br>psf | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>25 | 30.015 ft       | 225.16005<br>ft | -1,633.1275<br>psf | 419.1682<br>psf   | 261.92536<br>psf | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>26 | 31.005 ft       | 226.07908<br>ft | -1,666.9953<br>psf | 369.03037<br>psf  | 230.59577<br>psf | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>27 | 31.679841<br>ft | 226.71131<br>ft | -1,690.4416<br>psf | 335.13901<br>psf  | 209.4181<br>psf  | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice       | 32.044841       | 227.05645       | -1,703.3219        | 316.84293         | 197.98543        |        |       | Common Borrow                           |

| 28          | ft              | ft              | psf                | psf              | psf              | 50 psf | 0 psf | (Apparent<br>Cohesion)                  |
|-------------|-----------------|-----------------|--------------------|------------------|------------------|--------|-------|---|
| Slice<br>29 | 32.861042<br>ft | 227.8369<br>ft  | -1,731.8003<br>psf | 275.99712<br>psf | 172.46214<br>psf | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>30 | 34.123126<br>ft | 229.05743<br>ft | -1,776.2998<br>psf | 213.53162<br>psf | 133.42937<br>psf | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>31 | 35.385209<br>ft | 230.29952<br>ft | -1,822.1457<br>psf | 151.68708<br>psf | 94.784606<br>psf | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>32 | 36.647293<br>ft | 231.56376<br>ft | -1,869.3733<br>psf | 90.466884<br>psf | 56.529983<br>psf | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>33 | 37.909377<br>ft | 232.85075<br>ft | -1,918.02<br>psf   | 29.873937<br>psf | 18.667308<br>psf | 50 psf | 0 psf | Common Borrow (Apparent                 |

# 1A.4 Compound - Pseudo-Static (M-P)

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# **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Yi Tyan Tsai Revision Number: 321 Date: 01/19/2022

Time: 02:28:08 PM Tool Version: 11.1.1.22085

File Name: Wall 05.85L-B Sta 2+60\_FC Wall (lightweight fill).gsz Directory: P:\0\0180366\01\Analysis\Wall 05.85L-B\22-01-13\

Last Solved Date: 01/19/2022 Last Solved Time: 02:28:24 PM

# **Project Settings**

Unit System: U.S. Customary Units

# **Analysis Settings**

## 1A.4 Compound - Pseudo-Static (M-P)

Kind: SLOPE/W

Analysis Type: Morgenstern-Price

Settings

**Side Function** 

Interslice force function option: Half-Sine

PWP Conditions from: Piezometric Line

Apply Phreatic Correction: No
Use Staged Rapid Drawdown: No
Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 1

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

**Factor of Safety Convergence Settings** 

Maximum Number of Iterations: 100
Tolerable difference in F of S: 0.001

**Solution Settings** 

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

## **Materials**

## **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 42 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

## ESU 1B Medium Dense to Very Dense Coarse-Grained Fill (Apparent Cohesion)

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 100 psf Effective Friction Angle: 41 °

Phi-B: 0°

Pore Water Pressure

Piezometric Line: 1

## **ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 115 pcf

Effective Cohesion: 200 psf Effective Friction Angle: 34°

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

## **Common Borrow (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 50 psf Effective Friction Angle: 32 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

# Reinforcements

# Row 1 (2 strips)(EQ)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 8.8 °

Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

# Row 2 (2 strips)(EQ)

Type: Geosynthetic

Interface Adhesion: 0 psf Interface Shear Angle: 8.2  $^{\circ}$ 

Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

## Row 3 (2 strips)(EQ)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 7.5 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

## Row 4 (2 strips)(EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 6.8 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

# Row 5 (2 strips)(EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 6.2 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

# Row 6 (2 strips)(EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 5.5 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

## Row 7 (2 strips)(EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 4.9 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

## Row 8 (2 strips)(EQ)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 4.2 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

### Row 9+ (2 strips)(EQ)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 3.6 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

# **Slip Surface Entry and Exit**

Left Type: Range

Left-Zone Left Coordinate: (-25, 193.56104) ft Left-Zone Right Coordinate: (-0.9, 206) ft Left-Zone Increment: 20

Right Type: Range

Right-Zone Left Coordinate: (21.860569, 229.72989) ft

Right-Zone Right Coordinate: (60, 233.74338) ft

Right-Zone Increment: 20 Radius Increments: 20

# **Slip Surface Limits**

Left Coordinate: (-80, 186.2) ft Right Coordinate: (80, 234.2) ft

## **Piezometric Lines**

#### Piezometric Line 1

#### Coordinates

|               | Х         | Υ          |
|---------------|-----------|------------|
| Coordinate 1  | -48.3 ft  | 180 ft     |
| Coordinate 2  | -4.1 ft   | 190.1 ft   |
| Coordinate 3  | 11.7 ft   | 193.8 ft   |
| Coordinate 4  | 17.165 ft | 194.87 ft  |
| Coordinate 5  | 24.11 ft  | 196.755 ft |
| Coordinate 6  | 29.52 ft  | 198.8 ft   |
| Coordinate 7  | 32.23 ft  | 199.83 ft  |
| Coordinate 8  | 60.885 ft | 211.35 ft  |
| Coordinate 9  | 70.775 ft | 215.12 ft  |
| Coordinate 10 | 74.125 ft | 216.15 ft  |
| Coordinate 11 | 80 ft     | 217.365 ft |

# **Seismic Coefficients**

Horz Seismic Coef.: 0.208

# **Reinforcement Lines**

## **Reinforcement Line 1**

Reinforcement: Row 1 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 218.4) ft Inside Point: (15.6, 218.4) ft

Length: 16.5 ft
Orientation: 0°

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 2**

Reinforcement: Row 3 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 213.6) ft Inside Point: (15.6, 213.6) ft

Length: 16.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 3**

Reinforcement: Row 2 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 216) ft Inside Point: (15.6, 216) ft

Length: 16.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 4**

Reinforcement: Row 7 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 204) ft Inside Point: (15.6, 204) ft

Length: 16.5 ft Orientation: 0 °

Slip Surface Intersection: (2.6901579, 204) ft

Max. Pullout Force: 5,240 lbf Available Length: 12.909842 ft Required Length: 12.909842 ft Pullout Force: 4,613.2725 lbf

Pullout Force per Length: 357.34539 lbf/ft Governing Component: Pullout Resistance

#### **Reinforcement Line 5**

Reinforcement: Row 6 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 206.4) ft Inside Point: (15.6, 206.4) ft

Length: 16.5 ft
Orientation: 0 °

Slip Surface Intersection: (6.3238779, 206.4) ft

Max. Pullout Force: 5,240 lbf Available Length: 9.2761221 ft Required Length: 9.2761221 ft Pullout Force: 3,523.3844 lbf

Pullout Force per Length: 379.83376 lbf/ft Governing Component: Pullout Resistance

#### **Reinforcement Line 6**

Reinforcement: Row 5 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 208.8) ft Inside Point: (15.6, 208.8) ft

Length: 16.5 ft Orientation: 0 °

Slip Surface Intersection: (9.7925061, 208.8) ft

Max. Pullout Force: 5,240 lbf Available Length: 5.8074939 ft Required Length: 5.8074939 ft Pullout Force: 2,390.913 lbf

Pullout Force per Length: 411.69444 lbf/ft Governing Component: Pullout Resistance

#### **Reinforcement Line 7**

Reinforcement: Row 4 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 211.2) ft Inside Point: (15.6, 211.2) ft

Length: 16.5 ft
Orientation: 0 °

Slip Surface Intersection: (13.115125, 211.2) ft

Max. Pullout Force: 5,240 lbf Available Length: 2.4848745 ft Required Length: 2.4848745 ft Pullout Force: 1,049.766 lbf

Pullout Force per Length: 422.4624 lbf/ft Governing Component: Pullout Resistance

## **Reinforcement Line 8**

Reinforcement: Row 9+ (2 strips)(EQ)

Lock to Ground Surface: No

Outside Point: (-0.9, 196.8) ft Inside Point: (15.6, 196.8) ft

Length: 16.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 9**

Reinforcement: Row 9+ (2 strips)(EQ)

Lock to Ground Surface: No Outside Point: (-0.9, 199.2) ft Inside Point: (15.6, 199.2) ft

Length: 16.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 10**

Reinforcement: Row 8 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 201.6) ft Inside Point: (15.6, 201.6) ft

Length: 16.5 ft
Orientation: 0°

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

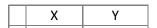
# **Surcharge Loads**

# **Surcharge Load 1**

Surcharge (Unit Weight): 125 pcf

**Direction: Vertical** 

#### Coordinates



| 43 ft   | 234.5 ft |
|---------|----------|
| 45 ft   | 234.5 ft |
| 58.1 ft | 234.7 ft |
| 80 ft   | 235.2 ft |

# Geometry

Name: 1. Compound Stability

**Settings** 

View: 2D

Element Thickness: 1 ft

### **Points**

|          | Х        | Υ        |
|----------|----------|----------|
| Point 1  | 80 ft    | 199.4 ft |
| Point 2  | 58 ft    | 196.6 ft |
| Point 3  | 37.6 ft  | 191.9 ft |
| Point 4  | 42.1 ft  | 180 ft   |
| Point 5  | 80 ft    | 180 ft   |
| Point 6  | 80 ft    | 226 ft   |
| Point 7  | 58 ft    | 225.3 ft |
| Point 8  | 29.8 ft  | 195 ft   |
| Point 9  | 11.7 ft  | 193.8 ft |
| Point 10 | -48.3 ft | 180 ft   |
| Point 11 | 80 ft    | 234.2 ft |
| Point 12 | 58.1 ft  | 233.7 ft |
| Point 13 | 26.5 ft  | 214.1 ft |
| Point 14 | -10.8 ft | 197 ft   |
| Point 15 | -18.3 ft | 195.3 ft |
| Point 16 | -21.1 ft | 194.7 ft |
| Point 17 | -24.4 ft | 193.6 ft |
| Point 18 | -32.1 ft | 193.1 ft |
| Point 19 | -36.6 ft | 192.3 ft |
| Point 20 | -61.7 ft | 189.7 ft |
| Point 21 | -65.4 ft | 189.3 ft |
| Point 22 | -73.2 ft | 188 ft   |
| Point 23 | -80 ft   | 186.2 ft |
| Point 24 | -80 ft   | 180 ft   |
| Point 25 | -4.1 ft  | 190.1 ft |
| Point 26 | 32 ft    | 197.4 ft |
| Point 27 | -0.9 ft  | 219.4 ft |
| Point 28 | -0.9 ft  | 196.3 ft |
| Point 29 | -4.9 ft  | 199.8 ft |
| Point 30 | -0.9 ft  | 199.8 ft |
| Point 31 | -0.9 ft  | 199.4 ft |
| Point 32 | 15.6 ft  | 196.3 ft |
| Point 33 | 15.6 ft  | 219.4 ft |
|          |          |          |

| Point 34 11.1 ft   | 196.3 ft<br>196.3 ft |
|--------------------|----------------------|
| D 1 1 0 E 4 E 4 C  | 106 2 ft             |
| Point 35   17.1 ft | 130.3 IL             |
| Point 36   17.1 ft | 214.2 ft             |
| Point 37   15.6 ft | 214.2 ft             |
| Point 38   17.1 ft | 208.4 ft             |
| Point 39 45 ft     | 233.5 ft             |
| Point 40 37.1 ft   | 228.2 ft             |
| Point 41 29.4 ft   | 222.3 ft             |
| Point 42 29.5 ft   | 233.5 ft             |
| Point 43 1.5 ft    | 219.4 ft             |
| Point 44 31.5 ft   | 233.5 ft             |
| Point 45   6.1 ft  | 233.5 ft             |
| Point 46 14.1 ft   | 233.5 ft             |
| Point 47 14.1 ft   | 219.4 ft             |
| Point 48 6.1 ft    | 219.4 ft             |
| Point 49 14.1 ft   | 225.9 ft             |
| Point 50 6.1 ft    | 221.74 ft            |
| Point 51 17.1 ft   | 219.4 ft             |
| Point 52 28.775 ft | 233.5 ft             |
| Point 53   6.1 ft  | 232 ft               |
| Point 54 14.1 ft   | 232 ft               |
| Point 55 39 ft     | 233.5 ft             |
| Point 56 39 ft     | 230.5 ft             |

# Regions

|              | Material  | Points  | Area                       |
|--------------|---|---|----------------------------|
| Region<br>1  | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt              | 1,2,3,4,5                                       | 659.92<br>ft²              |
| Region<br>2  | ESU 4B Dense to Very Dense Sand/Gravel  | 1,6,7,26,8,9,25,10,4,3,2                        | 1,867.8<br>ft <sup>2</sup> |
| Region<br>3  | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill (Apparent Cohesion) | 14,29,30,31                                     | 7.58 ft <sup>2</sup>       |
| Region<br>4  | Gravel Borrow   | 27,30,31,28,34,32,37,33,47,48,43                | 381.15<br>ft <sup>2</sup>  |
| Region<br>5  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                           | 7,6,11,12,13,38,35,32,34,25,9,8,26              | 856.44<br>ft <sup>2</sup>  |
| Region<br>6  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                           | 14,15,16,17,18,19,20,21,22,23,24,10,25,34,28,31 | 748.7<br>ft²               |
| Region<br>7  | Gravel Borrow   | 32,35,38,36,37                                  | 26.85<br>ft <sup>2</sup>   |
| Region<br>8  | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill (Apparent Cohesion) | 12,39,40,41,36,38,13                            | 241.79<br>ft²              |
| Region<br>9  | Common Borrow (Apparent Cohesion)   | 48,47,49,50                                     | 35.36<br>ft <sup>2</sup>   |
| Region<br>10 | Common Borrow (Apparent Cohesion)   | 39,56,51,36,41,40                               | 75.79<br>ft²               |
| Region<br>11 |   | 46,54,49,42,52                                  | 58.52<br>ft <sup>2</sup>   |
| Region<br>12 |   | 46,45,53,54                                     | 12 ft²                     |

| Region<br>13 | Common Borrow (Apparent Cohesion) | 50,43,48                | 5.382<br>ft <sup>2</sup>  |
|--------------|-----------------------------------|-------------------------|---------------------------|
| Region<br>14 | Gravel Borrow                     | 33,37,36,51             | 7.8 ft <sup>2</sup>       |
| Region<br>15 |                                   | 50,49,54,53             | 65.44<br>ft²              |
| Region<br>16 | Common Borrow (Apparent Cohesion) | 44,42,49,47,33,51,56,55 | 171.02<br>ft <sup>2</sup> |
| Region<br>17 | Common Borrow (Apparent Cohesion) | 39,55,56                | 9 ft²                     |

# **Slip Results**

Slip Surfaces Analysed: 8969 of 9261 converged

# **Current Slip Surface**

Slip Surface: 6,366 Factor of Safety: 1.1 Volume: 451.08584 ft<sup>3</sup> Weight: 56,233.146 lbf

Resisting Moment: 7,126,191.7 lbf·ft Activating Moment: 6,661,339.1 lbf·ft

Resisting Force: 28,638.037 lbf Activating Force: 26,771.671 lbf Slip Rank: 1 of 9,261 slip surfaces

Exit: (-0.9, 201.73514) ft Entry: (38.540419, 233.5) ft

Radius: 201.32979 ft

Center: (-106.4613, 373.17171) ft

# **Slip Slices**

|            | х               | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material |
|------------|-----------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|---------------|
| Slice<br>1 | -0.3 ft         | 202.1075<br>ft  | -693.73979<br>psf | 1,722.3906<br>psf        | 1,345.6791<br>psf      | 0 psf                | 0 psf               | Gravel Borrow |
| Slice<br>2 | 0.9 ft          | 202.85808<br>ft | -723.04082<br>psf | 1,998.3832<br>psf        | 1,561.3081<br>psf      | 0 psf                | 0 psf               | Gravel Borrow |
| Slice<br>3 | 2.2666667<br>ft | 203.72826<br>ft | -757.36922<br>psf | 2,189.4942<br>psf        | 1,710.6203<br>psf      | 0 psf                | 0 psf               | Gravel Borrow |
| Slice<br>4 | 3.8 ft          | 204.72204<br>ft | -796.97537<br>psf | 2,021.0539<br>psf        | 1,579.0204<br>psf      | 0 psf                | 0 psf               | Gravel Borrow |
| Slice<br>5 | 5.3333333<br>ft | 205.73577<br>ft | -837.82579<br>psf | 2,023.8012<br>psf        | 1,581.1668<br>psf      | 0 psf                | 0 psf               | Gravel Borrow |
| Slice<br>6 | 6.8 ft          | 206.72398<br>ft | -878.05855<br>psf | 2,043.5056<br>psf        | 1,596.5615<br>psf      | 0 psf                | 0 psf               | Gravel Borrow |
| Slice<br>7 | 8.2 ft          | 207.68532<br>ft | -917.58815<br>psf | 1,721.5867<br>psf        | 1,345.0509<br>psf      | 0 psf                | 0 psf               | Gravel Borrow |
| Slice      |                 | 208.66419       | -958.21176        | 1,614.95                 | 1,261.7372             |                      |                     |               |

| 8           | 9.6 ft          | ft              | psf                | psf               | psf               | 0 psf  | 0 psf | Gravel Borrow                           |
|-------------|-----------------|-----------------|--------------------|-------------------|-------------------|--------|-------|---|
| Slice<br>9  | 11 ft           | 209.6609<br>ft  | -999.94902<br>psf  | 1,328.855<br>psf  | 1,038.2153<br>psf | 0 psf  | 0 psf | Gravel Borrow                           |
| Slice<br>10 | 12.3 ft         | 210.60207<br>ft | -1,041.119<br>psf  | 1,214.8362<br>psf | 949.13404<br>psf  | 0 psf  | 0 psf | Gravel Borrow                           |
| Slice<br>11 | 13.5 ft         | 211.48555<br>ft | -1,081.5872<br>psf | 1,107.3821<br>psf | 865.18169<br>psf  | 0 psf  | 0 psf | Gravel Borrow                           |
| Slice<br>12 | 14.85 ft        | 212.49698<br>ft | -1,128.2065<br>psf | 922.67976<br>psf  | 720.87644<br>psf  | 0 psf  | 0 psf | Gravel Borrow                           |
| Slice<br>13 | 16.3825 ft      | 213.66588<br>ft | -1,182.4229<br>psf | 802.85189<br>psf  | 627.25664<br>psf  | 0 psf  | 0 psf | Gravel Borrow                           |
| Slice<br>14 | 17.8595 ft      | 214.81375<br>ft | -1,232.7275<br>psf | 663.46287<br>psf  | 414.57761<br>psf  | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>15 | 19.2485 ft      | 215.91415<br>ft | -1,277.8677<br>psf | 594.29056<br>psf  | 371.35396<br>psf  | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>16 | 20.6375 ft      | 217.03466<br>ft | -1,324.2629<br>psf | 537.87316<br>psf  | 336.10045<br>psf  | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>17 | 22.0265 ft      | 218.17572<br>ft | -1,371.9402<br>psf | 492.90721<br>psf  | 308.00261<br>psf  | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>18 | 23.4155 ft      | 219.33779<br>ft | -1,420.9284<br>psf | 458.05499<br>psf  | 286.22453<br>psf  | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>19 | 24.693125<br>ft | 220.42482<br>ft | -1,463.2426<br>psf | 433.7466<br>psf   | 271.03496<br>psf  | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>20 | 25.859375<br>ft | 221.43402<br>ft | -1,498.7078<br>psf | 417.31609<br>psf  | 260.76804<br>psf  | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>21 | 27.025625<br>ft | 222.45901<br>ft | -1,535.1579<br>psf | 405.60365<br>psf  | 253.44929<br>psf  | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>22 | 28.191875<br>ft | 223.5001<br>ft  | -1,572.613<br>psf  | 397.93852<br>psf  | 248.65958<br>psf  | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>23 | 29.1375 ft      | 224.35501<br>ft | -1,603.6549<br>psf | 394.20709<br>psf  | 246.32793<br>psf  | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>24 | 29.51 ft        | 224.69447<br>ft | -1,616.0509<br>psf | 393.01522<br>psf  | 245.58316<br>psf  | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>25 | 30.015 ft       | 225.16005<br>ft | -1,633.1275<br>psf | 378.85018<br>psf  | 236.73186<br>psf  | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>26 | 31.005 ft       | 226.07908<br>ft | -1,666.9953<br>psf | 350.35448<br>psf  | 218.92578<br>psf  | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>27 | 31.679841<br>ft | 226.71131<br>ft | -1,690.4416<br>psf | 329.95642<br>psf  | 206.17965<br>psf  | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |

| Slice<br>28 | 32.044841<br>ft | 227.05645<br>ft | -1,703.3219<br>psf | 318.30498<br>psf | 198.89902<br>psf | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
|-------------|-----------------|-----------------|--------------------|------------------|------------------|--------|-------|---|
| Slice<br>29 | 32.861042<br>ft | 227.8369<br>ft  | -1,731.8003<br>psf | 290.11512<br>psf | 181.28405<br>psf | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>30 | 34.123126<br>ft | 229.05743<br>ft | -1,776.2998<br>psf | 240.9104<br>psf  | 150.53752<br>psf | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>31 | 35.385209<br>ft | 230.29952<br>ft | -1,822.1457<br>psf | 181.76329<br>psf | 113.57831<br>psf | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>32 | 36.647293<br>ft | 231.56376<br>ft | -1,869.3733<br>psf | 109.52858<br>psf | 68.441053<br>psf | 50 psf | 0 psf | Common Borrow<br>(Apparent<br>Cohesion) |
| Slice<br>33 | 37.909377<br>ft | 232.85075<br>ft | -1,918.02<br>psf   | 20.619251<br>psf | 12.884338<br>psf | 50 psf | 0 psf | Common Borrow (Apparent Cohesion)       |

# 1B.1 Compound - Static FC Wall (Spencer)

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# **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Bo Zhang Revision Number: 314 Date: 01/12/2022

Tool Version: 11.1.1.22700

Time: 10:44:22 AM

File Name: Wall 05.85L-B Sta 2+60\_FC Wall (lightweight fill).gsz Directory: P:\0\0180366\01\Analysis\Wall 05.85L-B\22-01-13\

Last Solved Date: 01/12/2022 Last Solved Time: 10:46:40 AM

# **Project Settings**

Unit System: U.S. Customary Units

# **Analysis Settings**

# 1B.1 Compound - Static FC Wall (Spencer)

Description: With Forward Compatible Wall

Kind: SLOPE/W

Analysis Type: Spencer

Settings

PWP Conditions from: Piezometric Line

Apply Phreatic Correction: No
Use Staged Rapid Drawdown: No
Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 1

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

**Factor of Safety Convergence Settings** 

Maximum Number of Iterations: 100 Tolerable difference in F of S: 0.001

**Solution Settings** 

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

## **Materials**

### ESU 1B Medium Dense to Very Dense Coarse-Grained Fill

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 41 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

## **ESU 2B Medium Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 115 pcf Effective Cohesion: 0 psf Effective Friction Angle: 34 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

## **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

## ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 42 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

# **Forward Compatible Wall**

Material Model: High Strength

Unit Weight: 130 pcf
Pore Water Pressure
Piezometric Line: 1

## **Lightweight EPS**

Material Model: Mohr-Coulomb

Unit Weight: 5 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 0 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

# Reinforcements

# Row 1 (2 strips)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 6.6 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

## Row 2 (2 strips)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 6.1 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

## Row 3 (2 strips)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 5.6 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

### Row 4 (2 strips)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 5.1 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 5 (2 strips)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 4.6 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

## Row 6 (2 strips)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 4.1 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

## Row 7 (2 strips)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 3.6 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

### Row 8 (2 strips)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 3.1 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 9+ (2 strips)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 2.7 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

# **Slip Surface Entry and Exit**

Left Type: Range

Left-Zone Left Coordinate: (-40, 191.94781) ft Left-Zone Right Coordinate: (-0.9, 206) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15.000006, 233.5) ft Right-Zone Right Coordinate: (60, 233.74338) ft

Right-Zone Increment: 25
Radius Increments: 20

# **Slip Surface Limits**

Left Coordinate: (-80, 186.2) ft Right Coordinate: (80, 234.2) ft

# **Piezometric Lines**

#### Piezometric Line 1

#### **Coordinates**

|               | Х         | Υ          |
|---------------|-----------|------------|
| Coordinate 1  | -48.3 ft  | 180 ft     |
| Coordinate 2  | -4.1 ft   | 190.1 ft   |
| Coordinate 3  | 11.7 ft   | 193.8 ft   |
| Coordinate 4  | 17.165 ft | 194.87 ft  |
| Coordinate 5  | 24.11 ft  | 196.755 ft |
| Coordinate 6  | 29.52 ft  | 198.8 ft   |
| Coordinate 7  | 32.23 ft  | 199.83 ft  |
| Coordinate 8  | 60.885 ft | 211.35 ft  |
| Coordinate 9  | 70.775 ft | 215.12 ft  |
| Coordinate 10 | 74.125 ft | 216.15 ft  |
| Coordinate 11 | 80 ft     | 217.365 ft |

# **Reinforcement Lines**

#### **Reinforcement Line 1**

Reinforcement: Row 1 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 218.4) ft Inside Point: (15.6, 218.4) ft

Length: 16.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 2**

Reinforcement: Row 3 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 213.6) ft Inside Point: (15.6, 213.6) ft

Length: 16.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 3**

Reinforcement: Row 2 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 216) ft Inside Point: (15.6, 216) ft

Length: 16.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 4**

Reinforcement: Row 7 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 204) ft Inside Point: (15.6, 204) ft

Length: 16.5 ft

Orientation: 0°

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 5**

Reinforcement: Row 6 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 206.4) ft Inside Point: (15.6, 206.4) ft

Length: 16.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### Reinforcement Line 6

Reinforcement: Row 5 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 208.8) ft Inside Point: (15.6, 208.8) ft

Length: 16.5 ft
Orientation: 0°

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 7**

Reinforcement: Row 4 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 211.2) ft Inside Point: (15.6, 211.2) ft

Length: 16.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft

Governing Component: (none)

#### **Reinforcement Line 8**

Reinforcement: Row 9+ (2 strips) Lock to Ground Surface: No Outside Point: (-0.9, 196.8) ft Inside Point: (15.6, 196.8) ft

Length: 16.5 ft Orientation: 0 °

Slip Surface Intersection: (14.476305, 196.8) ft

Max. Pullout Force: 3,930 lbf Available Length: 1.1236954 ft Required Length: 1.1236954 ft Pullout Force: 362.58309 lbf

Pullout Force per Length: 322.67027 lbf/ft Governing Component: Pullout Resistance

#### **Reinforcement Line 9**

Reinforcement: Row 9+ (2 strips) Lock to Ground Surface: No Outside Point: (-0.9, 199.2) ft Inside Point: (15.6, 199.2) ft

Length: 16.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 10**

Reinforcement: Row 8 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 201.6) ft Inside Point: (15.6, 201.6) ft

Length: 16.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

# **Surcharge Loads**

# **Surcharge Load 1**

Surcharge (Unit Weight): 250 pcf

**Direction: Vertical** 

#### **Coordinates**

| Χ         | Υ         |
|-----------|-----------|
| 8.1 ft    | 235.25 ft |
| 15.595 ft | 235.25 ft |
| 15.6 ft   | 234.5 ft  |
| 58.1 ft   | 234.7 ft  |
| 80 ft     | 235.2 ft  |

# **Geometry**

Name: 1. Compound Stability

# **Settings**

View: 2D

Element Thickness: 1 ft

# **Points**

|          | Х        | Υ        |
|----------|----------|----------|
| Point 1  | 80 ft    | 199.4 ft |
| Point 2  | 58 ft    | 196.6 ft |
| Point 3  | 37.6 ft  | 191.9 ft |
| Point 4  | 42.1 ft  | 180 ft   |
| Point 5  | 80 ft    | 180 ft   |
| Point 6  | 80 ft    | 226 ft   |
| Point 7  | 58 ft    | 225.3 ft |
| Point 8  | 29.8 ft  | 195 ft   |
| Point 9  | 11.7 ft  | 193.8 ft |
| Point 10 | -48.3 ft | 180 ft   |
| Point 11 | 80 ft    | 234.2 ft |
| Point 12 | 58.1 ft  | 233.7 ft |
| Point 13 | 26.5 ft  | 214.1 ft |
| Point 14 | -10.8 ft | 197 ft   |
| Point 15 | -18.3 ft | 195.3 ft |
| Point 16 | -21.1 ft | 194.7 ft |
| Point 17 | -24.4 ft | 193.6 ft |
| Point 18 | -32.1 ft | 193.1 ft |
| Point 19 | -36.6 ft | 192.3 ft |
| Point 20 | -61.7 ft | 189.7 ft |
| Point 21 | -65.4 ft | 189.3 ft |
| Point 22 | -73.2 ft | 188 ft   |
| Point 23 | -80 ft   | 186.2 ft |
| Point 24 | -80 ft   | 180 ft   |
| Point 25 | -4.1 ft  | 190.1 ft |
|          |          |          |

| Point 26 | 32 ft     | 197.4 ft  |
|----------|-----------|-----------|
| Point 27 | -0.9 ft   | 219.4 ft  |
| Point 28 | -0.9 ft   | 196.3 ft  |
| Point 29 | -4.9 ft   | 199.8 ft  |
| Point 30 | -0.9 ft   | 199.8 ft  |
| Point 31 | -0.9 ft   | 199.4 ft  |
| Point 32 | 15.6 ft   | 196.3 ft  |
| Point 33 | 15.6 ft   | 219.4 ft  |
| Point 34 | 11.1 ft   | 196.3 ft  |
| Point 35 | 17.1 ft   | 196.3 ft  |
| Point 36 | 17.1 ft   | 214.2 ft  |
| Point 37 | 15.6 ft   | 214.2 ft  |
| Point 38 | 17.1 ft   | 208.4 ft  |
| Point 39 | 45 ft     | 233.5 ft  |
| Point 40 | 37.1 ft   | 228.2 ft  |
| Point 41 | 29.4 ft   | 222.3 ft  |
| Point 42 | 29.5 ft   | 233.5 ft  |
| Point 43 | 1.5 ft    | 219.4 ft  |
| Point 44 | 31.5 ft   | 233.5 ft  |
| Point 45 | 6.1 ft    | 233.5 ft  |
| Point 46 | 14.1 ft   | 233.5 ft  |
| Point 47 | 14.1 ft   | 219.4 ft  |
| Point 48 | 6.1 ft    | 219.4 ft  |
| Point 49 | 14.1 ft   | 225.9 ft  |
| Point 50 | 6.1 ft    | 221.74 ft |
| Point 51 | 17.1 ft   | 219.4 ft  |
| Point 52 | 28.775 ft | 233.5 ft  |
| Point 53 | 6.1 ft    | 232 ft    |
| Point 54 | 14.1 ft   | 232 ft    |
| Point 55 | 39 ft     | 233.5 ft  |
| Point 56 | 39 ft     | 230.5 ft  |
|          |           |           |

# Regions

|             | Material   | Points  | Area                       |
|-------------|--|---|----------------------------|
| Region<br>1 | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 1,2,3,4,5                                       | 659.92<br>ft <sup>2</sup>  |
| Region<br>2 | ESU 4B Dense to Very Dense Sand/Gravel                           | 1,6,7,26,8,9,25,10,4,3,2                        | 1,867.8<br>ft <sup>2</sup> |
| Region<br>3 | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill        | 14,29,30,31                                     | 7.58 ft <sup>2</sup>       |
| Region<br>4 | Gravel Borrow  | 27,30,31,28,34,32,37,33,47,48,43                | 381.15<br>ft <sup>2</sup>  |
| Region<br>5 | ESU 2B Medium Dense Sand/Gravel                                  | 7,6,11,12,13,38,35,32,34,25,9,8,26              | 856.44<br>ft <sup>2</sup>  |
| Region<br>6 | ESU 2B Medium Dense Sand/Gravel                                  | 14,15,16,17,18,19,20,21,22,23,24,10,25,34,28,31 | 748.7<br>ft <sup>2</sup>   |
| Region<br>7 | Gravel Borrow  | 32,35,38,36,37                                  | 26.85<br>ft <sup>2</sup>   |
| Region      | ESU 1B Medium Dense to Very Dense Coarse-                        | 12,39,40,41,36,38,13                            | 241.79                     |

| 8            | Grained Fill            |                         | ft²                       |
|--------------|-------------------------|-------------------------|---------------------------|
| Region<br>9  | Forward Compatible Wall | 48,47,49,50             | 35.36<br>ft <sup>2</sup>  |
| Region<br>10 | Common Borrow           | 39,56,51,36,41,40       | 75.79<br>ft²              |
| Region<br>11 | Lightweight EPS         | 46,54,49,42,52          | 58.52<br>ft <sup>2</sup>  |
| Region<br>12 | Forward Compatible Wall | 46,45,53,54             | 12 ft²                    |
| Region<br>13 |                         | 50,43,48                | 5.382<br>ft <sup>2</sup>  |
| Region<br>14 | Gravel Borrow           | 33,37,36,51             | 7.8 ft <sup>2</sup>       |
| Region<br>15 | Forward Compatible Wall | 50,49,54,53             | 65.44<br>ft²              |
| Region<br>16 | Lightweight EPS         | 44,42,49,47,33,51,56,55 | 171.02<br>ft <sup>2</sup> |
| Region<br>17 | Common Borrow           | 39,55,56                | 9 ft²                     |

## **Slip Results**

Slip Surfaces Analysed: 8054 of 14196 converged

## **Current Slip Surface**

Slip Surface: 1,484 Factor of Safety: 1.4 Volume: 1,462.0716 ft<sup>3</sup> Weight: 154,233.62 lbf

Resisting Moment: 7,320,603.8 lbf·ft Activating Moment: 5,055,919.6 lbf·ft

Resisting Force: 92,613.876 lbf Activating Force: 63,988.454 lbf Slip Rank: 1 of 14,196 slip surfaces Exit: (-36.305373, 192.35238) ft Entry: (47.401178, 233.53666) ft

Radius: 68.222101 ft

Center: (-16.430449, 257.61525) ft

### **Slip Slices**

|            | Х                | Y               | PWP              | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material                         |
|------------|------------------|-----------------|------------------|--------------------------|------------------------|----------------------|---------------------|---------------------------------------|
| Slice<br>1 | -35.25403<br>ft  | 192.05054<br>ft | -565.9334<br>psf | 113.10941<br>psf         | 76.293258<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>2 | -33.151343<br>ft | 191.48288<br>ft | -500.5295<br>psf | 310.78634<br>psf         | 209.62803<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |

| Slice<br>3  | -30.816667<br>ft | 190.94016<br>ft | -433.37397<br>psf | 457.09113<br>psf  | 308.31186<br>psf  | 0 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel       |
|-------------|------------------|-----------------|-------------------|-------------------|-------------------|-------|-------|---------------------------------------|
| Slice<br>4  | -28.25 ft        | 190.43746<br>ft | -365.40816<br>psf | 556.14565<br>psf  | 375.12498<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>5  | -25.683333<br>ft | 190.03595<br>ft | -303.75642<br>psf | 625.9387<br>psf   | 422.20099<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>6  | -22.75 ft        | 189.70669<br>ft | -241.38464<br>psf | 749.88352<br>psf  | 505.80282<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>7  | -19.7 ft         | 189.48596<br>ft | -184.12136<br>psf | 875.19474<br>psf  | 590.3263<br>psf   | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>8  | -17.05 ft        | 189.40742<br>ft | -141.43454<br>psf | 932.31077<br>psf  | 628.85156<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>9  | -14.55 ft        | 189.43054<br>ft | -107.23012<br>psf | 969.66752<br>psf  | 654.049<br>psf    | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>10 | -12.05 ft        | 189.54545<br>ft | -78.753687<br>psf | 991.05018<br>psf  | 668.47179<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>11 | -9.325 ft        | 189.78039<br>ft | -54.55872<br>psf  | 1,056.7024<br>psf | 712.75476<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>12 | -6.375 ft        | 190.15475<br>ft | -35.855228<br>psf | 1,147.9819<br>psf | 774.32357<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>13 | -4.5 ft          | 190.44566<br>ft | -27.272441<br>psf | 1,180.867<br>psf  | 796.50482<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>14 | -3.1014612<br>ft | 190.71565<br>ft | -23.825247<br>psf | 1,107.8996<br>psf | 747.2877<br>psf   | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>15 | -1.5014612<br>ft | 191.04949<br>ft | -21.276599<br>psf | 1,040.3427<br>psf | 701.72004<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>16 | 0.3 ft           | 191.48799<br>ft | -22.314664<br>psf | 3,516.4534<br>psf | 2,371.8778<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>17 | 2.65 ft          | 192.12665<br>ft | -27.827495<br>psf | 3,323.6121<br>psf | 2,241.8047<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>18 | 4.95 ft          | 192.8413<br>ft  | -38.812424<br>psf | 3,134.5334<br>psf | 2,114.2695<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>19 | 7.1 ft           | 193.5884<br>ft  | -54.014163<br>psf | 4,591.4951<br>psf | 3,097.0025<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>20 | 9.6 ft           | 194.57529<br>ft | -79.064374<br>psf | 4,696.2504<br>psf | 3,167.6609<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |

| Slice<br>21 | 11.4 ft         | 195.32871<br>ft | -99.775224<br>psf  | 4,510.9223<br>psf | 3,042.6555<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
|-------------|-----------------|-----------------|--------------------|-------------------|-------------------|-------|-------|---------------------------------------|
| Slice<br>22 | 12.590503<br>ft | 195.88138<br>ft | -118.99826<br>psf  | 4,364.9039<br>psf | 2,944.1649<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>23 | 13.790503<br>ft | 196.45293<br>ft | -140.00207<br>psf  | 4,239.9512<br>psf | 3,312.6129<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>24 | 14.8475 ft      | 196.99151<br>ft | -160.69619<br>psf  | 2,708.0686<br>psf | 2,115.7751<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>25 | 15.5975 ft      | 197.3785<br>ft  | -175.6814<br>psf   | 2,554.7746<br>psf | 1,996.0087<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>26 | 16.3825 ft      | 197.80916<br>ft | -192.96346<br>psf  | 2,405.9519<br>psf | 1,879.7357<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>27 | 18.90125 ft     | 199.29025<br>ft | -246.41775<br>psf  | 2,110.2152<br>psf | 1,423.3581<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>28 | 22.37375 ft     | 201.54359<br>ft | -328.2141<br>psf   | 1,945.7394<br>psf | 1,312.4178<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>29 | 25.305 ft       | 203.66968<br>ft | -403.289<br>psf    | 1,793.7952<br>psf | 1,209.9302<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>30 | 27.6375 ft      | 205.55711<br>ft | -466.04705<br>psf  | 1,661.2214<br>psf | 1,120.508<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>31 | 29.0875 ft      | 206.79994<br>ft | -509.39803<br>psf  | 1,575.8616<br>psf | 1,062.9321<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>32 | 29.45 ft        | 207.1253<br>ft  | -521.14992<br>psf  | 1,553.7112<br>psf | 1,047.9914<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>33 | 29.51 ft        | 207.17985<br>ft | -523.13822<br>psf  | 1,550.0368<br>psf | 1,045.513<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>34 | 30.51 ft        | 208.12801<br>ft | -558.58807<br>psf  | 1,486.2252<br>psf | 1,002.4716<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>35 | 31.865 ft       | 209.43291<br>ft | -607.87832<br>psf  | 1,400.5063<br>psf | 944.65344<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>36 | 33.4475 ft      | 211.10441<br>ft | -672.98058<br>psf  | 1,292.1864<br>psf | 871.59075<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>37 | 35.8825 ft      | 213.86586<br>ft | -784.21021<br>psf  | 1,120.174<br>psf  | 755.5669<br>psf   | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>38 | 38.05 ft        | 216.58304<br>ft | -899.38743<br>psf  | 958.6536<br>psf   | 646.62002<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>39 | 40.047044<br>ft | 219.39146<br>ft | -1,024.5344<br>psf | 929.63534<br>psf  | 627.04695<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |

| Slice<br>40 | 42.141133<br>ft | 222.69471<br>ft | -1,178.124<br>psf  | 693.50493<br>psf | 467.77498<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                  |
|-------------|-----------------|-----------------|--------------------|------------------|------------------|-------|-------|--|
| Slice<br>41 | 44.094089<br>ft | 226.196 ft      | -1,347.6122<br>psf | 436.56231<br>psf | 379.49783<br>psf | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill |
| Slice<br>42 | 46.200589<br>ft | 230.73888<br>ft | -1,578.2438<br>psf | 197.43972<br>psf | 171.63173<br>psf | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse-              |

# 1B.2 Compound - Static FC Wall (M-P)

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### **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Bo Zhang Revision Number: 314 Date: 01/12/2022

Tool Version: 11.1.1.22700

Time: 10:44:22 AM

File Name: Wall 05.85L-B Sta 2+60\_FC Wall (lightweight fill).gsz Directory: P:\0\0180366\01\Analysis\Wall 05.85L-B\22-01-13\

Last Solved Date: 01/12/2022 Last Solved Time: 10:47:00 AM

### **Project Settings**

Unit System: U.S. Customary Units

## **Analysis Settings**

### 1B.2 Compound - Static FC Wall (M-P)

**Description: With Forward Compatible Wall** 

Kind: SLOPE/W

Analysis Type: Morgenstern-Price

Settings

**Side Function** 

Interslice force function option: Half-Sine

PWP Conditions from: Piezometric Line

Apply Phreatic Correction: No
Use Staged Rapid Drawdown: No
Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 1

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

**Factor of Safety Convergence Settings** 

Maximum Number of Iterations: 100
Tolerable difference in F of S: 0.001

**Solution Settings** 

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

#### **Materials**

#### **ESU 1B Medium Dense to Very Dense Coarse-Grained Fill**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 41 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **ESU 2B Medium Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 115 pcf Effective Cohesion: 0 psf Effective Friction Angle: 34 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **Common Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 0 psf Effective Friction Angle: 32 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 42 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **Forward Compatible Wall**

Material Model: High Strength

Unit Weight: 130 pcf
Pore Water Pressure
Piezometric Line: 1

#### **Lightweight EPS**

Material Model: Mohr-Coulomb

Unit Weight: 5 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 0 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### Reinforcements

### Row 1 (2 strips)

Type: Geosynthetic Interface Adhesion: 0 psf

Interface Shear Angle: 6.6°

Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 2 (2 strips)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 6.1 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 3 (2 strips)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 5.6 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 4 (2 strips)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 5.1 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 5 (2 strips)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 4.6 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 6 (2 strips)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 4.1 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 7 (2 strips)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 3.6 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

#### Row 8 (2 strips)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 3.1 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

### Row 9+ (2 strips)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 2.7 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 3,930 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 3,930 lbf/ft

## **Slip Surface Entry and Exit**

Left Type: Range

Left-Zone Left Coordinate: (-40, 191.94781) ft Left-Zone Right Coordinate: (-0.9, 206) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (15.000006, 233.5) ft Right-Zone Right Coordinate: (60, 233.74338) ft

Right-Zone Increment: 25 Radius Increments: 20

## **Slip Surface Limits**

Left Coordinate: (-80, 186.2) ft Right Coordinate: (80, 234.2) ft

### **Piezometric Lines**

#### Piezometric Line 1

#### Coordinates

|               | Х         | Υ          |
|---------------|-----------|------------|
| Coordinate 1  | -48.3 ft  | 180 ft     |
| Coordinate 2  | -4.1 ft   | 190.1 ft   |
| Coordinate 3  | 11.7 ft   | 193.8 ft   |
| Coordinate 4  | 17.165 ft | 194.87 ft  |
| Coordinate 5  | 24.11 ft  | 196.755 ft |
| Coordinate 6  | 29.52 ft  | 198.8 ft   |
| Coordinate 7  | 32.23 ft  | 199.83 ft  |
| Coordinate 8  | 60.885 ft | 211.35 ft  |
| Coordinate 9  | 70.775 ft | 215.12 ft  |
| Coordinate 10 | 74.125 ft | 216.15 ft  |
| Coordinate 11 | 80 ft     | 217.365 ft |

#### **Reinforcement Lines**

#### **Reinforcement Line 1**

Reinforcement: Row 1 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 218.4) ft Inside Point: (15.6, 218.4) ft

Length: 16.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 2**

Reinforcement: Row 3 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 213.6) ft Inside Point: (15.6, 213.6) ft

Length: 16.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 3**

Reinforcement: Row 2 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 216) ft Inside Point: (15.6, 216) ft

Length: 16.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 4**

Reinforcement: Row 7 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 204) ft Inside Point: (15.6, 204) ft

Length: 16.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 5**

Reinforcement: Row 6 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 206.4) ft Inside Point: (15.6, 206.4) ft

Length: 16.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### Reinforcement Line 6

Reinforcement: Row 5 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 208.8) ft Inside Point: (15.6, 208.8) ft

Length: 16.5 ft
Orientation: 0°

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 7**

Reinforcement: Row 4 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 211.2) ft Inside Point: (15.6, 211.2) ft

Length: 16.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 8**

Reinforcement: Row 9+ (2 strips) Lock to Ground Surface: No Outside Point: (-0.9, 196.8) ft Inside Point: (15.6, 196.8) ft

Length: 16.5 ft Orientation: 0 °

Slip Surface Intersection: (14.476305, 196.8) ft

Max. Pullout Force: 3,930 lbf Available Length: 1.1236954 ft Required Length: 1.1236954 ft Pullout Force: 362.58309 lbf

Pullout Force per Length: 322.67027 lbf/ft Governing Component: Pullout Resistance

#### **Reinforcement Line 9**

Reinforcement: Row 9+ (2 strips) Lock to Ground Surface: No Outside Point: (-0.9, 199.2) ft Inside Point: (15.6, 199.2) ft

Length: 16.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 10**

Reinforcement: Row 8 (2 strips) Lock to Ground Surface: Yes Outside Point: (-0.9, 201.6) ft Inside Point: (15.6, 201.6) ft

Length: 16.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

## **Surcharge Loads**

### **Surcharge Load 1**

Surcharge (Unit Weight): 250 pcf

**Direction: Vertical** 

#### Coordinates

| Х         | Υ         |
|-----------|-----------|
| 8.1 ft    | 235.25 ft |
| 15.595 ft | 235.25 ft |
| 15.6 ft   | 234.5 ft  |
| 58.1 ft   | 234.7 ft  |
| 80 ft     | 235.2 ft  |

## **Geometry**

Name: 1. Compound Stability

**Settings** 

View: 2D

Element Thickness: 1 ft

#### **Points**

|          | Х        | Υ        |
|----------|----------|----------|
| Point 1  | 80 ft    | 199.4 ft |
| Point 2  | 58 ft    | 196.6 ft |
| Point 3  | 37.6 ft  | 191.9 ft |
| Point 4  | 42.1 ft  | 180 ft   |
| Point 5  | 80 ft    | 180 ft   |
| Point 6  | 80 ft    | 226 ft   |
| Point 7  | 58 ft    | 225.3 ft |
| Point 8  | 29.8 ft  | 195 ft   |
| Point 9  | 11.7 ft  | 193.8 ft |
| Point 10 | -48.3 ft | 180 ft   |
| Point 11 | 80 ft    | 234.2 ft |
| Point 12 | 58.1 ft  | 233.7 ft |
| Point 13 | 26.5 ft  | 214.1 ft |
| Point 14 | -10.8 ft | 197 ft   |
| Point 15 | -18.3 ft | 195.3 ft |
| Point 16 | -21.1 ft | 194.7 ft |
| Point 17 | -24.4 ft | 193.6 ft |
| Point 18 | -32.1 ft | 193.1 ft |
| Point 19 | -36.6 ft | 192.3 ft |
| Point 20 | -61.7 ft | 189.7 ft |
| Point 21 | -65.4 ft | 189.3 ft |
| Point 22 | -73.2 ft | 188 ft   |
| Point 23 | -80 ft   | 186.2 ft |
|          |          |          |

| •        | `         | ,         |
|----------|-----------|-----------|
| Point 24 | -80 ft    | 180 ft    |
| Point 25 | -4.1 ft   | 190.1 ft  |
| Point 26 | 32 ft     | 197.4 ft  |
| Point 27 | -0.9 ft   | 219.4 ft  |
| Point 28 | -0.9 ft   | 196.3 ft  |
| Point 29 | -4.9 ft   | 199.8 ft  |
| Point 30 | -0.9 ft   | 199.8 ft  |
| Point 31 | -0.9 ft   | 199.4 ft  |
| Point 32 | 15.6 ft   | 196.3 ft  |
| Point 33 | 15.6 ft   | 219.4 ft  |
| Point 34 | 11.1 ft   | 196.3 ft  |
| Point 35 | 17.1 ft   | 196.3 ft  |
| Point 36 | 17.1 ft   | 214.2 ft  |
| Point 37 | 15.6 ft   | 214.2 ft  |
| Point 38 | 17.1 ft   | 208.4 ft  |
| Point 39 | 45 ft     | 233.5 ft  |
| Point 40 | 37.1 ft   | 228.2 ft  |
| Point 41 | 29.4 ft   | 222.3 ft  |
| Point 42 | 29.5 ft   | 233.5 ft  |
| Point 43 | 1.5 ft    | 219.4 ft  |
| Point 44 | 31.5 ft   | 233.5 ft  |
| Point 45 | 6.1 ft    | 233.5 ft  |
| Point 46 | 14.1 ft   | 233.5 ft  |
| Point 47 | 14.1 ft   | 219.4 ft  |
| Point 48 | 6.1 ft    | 219.4 ft  |
| Point 49 | 14.1 ft   | 225.9 ft  |
| Point 50 | 6.1 ft    | 221.74 ft |
| Point 51 | 17.1 ft   | 219.4 ft  |
| Point 52 | 28.775 ft | 233.5 ft  |
| Point 53 | 6.1 ft    | 232 ft    |
| Point 54 | 14.1 ft   | 232 ft    |
| Point 55 | 39 ft     | 233.5 ft  |
| Point 56 | 39 ft     | 230.5 ft  |
|          |           |           |

## Regions

|             | Material   | Points  | Area                       |
|-------------|--|---|----------------------------|
| Region<br>1 | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt | 1,2,3,4,5                                       | 659.92<br>ft <sup>2</sup>  |
| Region<br>2 | ESU 4B Dense to Very Dense Sand/Gravel                           | 1,6,7,26,8,9,25,10,4,3,2                        | 1,867.8<br>ft <sup>2</sup> |
| Region 3    | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill        | 14,29,30,31                                     | 7.58 ft <sup>2</sup>       |
| Region<br>4 | Gravel Borrow  | 27,30,31,28,34,32,37,33,47,48,43                | 381.15<br>ft <sup>2</sup>  |
| Region<br>5 | ESU 2B Medium Dense Sand/Gravel                                  | 7,6,11,12,13,38,35,32,34,25,9,8,26              | 856.44<br>ft <sup>2</sup>  |
| Region<br>6 | ESU 2B Medium Dense Sand/Gravel                                  | 14,15,16,17,18,19,20,21,22,23,24,10,25,34,28,31 | 748.7<br>ft <sup>2</sup>   |
| Region      | Gravel Borrow  | 32,35,38,36,37                                  | 26.85                      |

| 7            |   |                         | ft²                       |
|--------------|---|-------------------------|---------------------------|
| Region<br>8  | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill | 12,39,40,41,36,38,13    | 241.79<br>ft <sup>2</sup> |
| Region<br>9  | Forward Compatible Wall                                   | 48,47,49,50             | 35.36<br>ft <sup>2</sup>  |
| Region<br>10 | Common Borrow   | 39,56,51,36,41,40       | 75.79<br>ft²              |
| Region<br>11 | Lightweight EPS   | 46,54,49,42,52          | 58.52<br>ft <sup>2</sup>  |
| Region<br>12 | Forward Compatible Wall                                   | 46,45,53,54             | 12 ft²                    |
| Region<br>13 |   | 50,43,48                | 5.382<br>ft <sup>2</sup>  |
| Region<br>14 | Gravel Borrow   | 33,37,36,51             | 7.8 ft <sup>2</sup>       |
| Region<br>15 | Forward Compatible Wall                                   | 50,49,54,53             | 65.44<br>ft²              |
| Region<br>16 | Lightweight EPS   | 44,42,49,47,33,51,56,55 | 171.02<br>ft <sup>2</sup> |
| Region<br>17 | Common Borrow   | 39,55,56                | 9 ft²                     |

## **Slip Results**

Slip Surfaces Analysed: 11059 of 14196 converged

## **Current Slip Surface**

Slip Surface: 1,484 Factor of Safety: 1.5 Volume: 1,462.0716 ft<sup>3</sup> Weight: 154,233.62 lbf

Resisting Moment: 7,334,172.3 lbf·ft Activating Moment: 5,055,919.6 lbf·ft

Resisting Force: 92,660.073 lbf Activating Force: 63,915.255 lbf Slip Rank: 1 of 14,196 slip surfaces Exit: (-36.305373, 192.35238) ft Entry: (47.401178, 233.53666) ft

Radius: 68.222101 ft

Center: (-16.430449, 257.61525) ft

### **Slip Slices**

|            | Х               | Y               | PWP              | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material                         |
|------------|-----------------|-----------------|------------------|--------------------------|------------------------|----------------------|---------------------|---------------------------------------|
| Slice<br>1 | -35.25403<br>ft | 192.05054<br>ft | -565.9334<br>psf | 67.826152<br>psf         | 45.749317<br>psf       | 0 psf                | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel |
|            |                 |                 |                  |                          |                        |                      |                     | ESU 2B Medium                         |

| Slice<br>2  | -33.151343<br>ft | 191.48288<br>ft | -500.5295<br>psf  | 206.10201<br>psf  | 139.01756<br>psf  | 0 psf | 0 psf | Dense<br>Sand/Gravel                  |
|-------------|------------------|-----------------|-------------------|-------------------|-------------------|-------|-------|---------------------------------------|
| Slice<br>3  | -30.816667<br>ft | 190.94016<br>ft | -433.37397<br>psf | 338.80054<br>psf  | 228.52385<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>4  | -28.25 ft        | 190.43746<br>ft | -365.40816<br>psf | 460.45058<br>psf  | 310.57784<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>5  | -25.683333<br>ft | 190.03595<br>ft | -303.75642<br>psf | 570.4107<br>psf   | 384.74688<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>6  | -22.75 ft        | 189.70669<br>ft | -241.38464<br>psf | 741.18937<br>psf  | 499.93854<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>7  | -19.7 ft         | 189.48596<br>ft | -184.12136<br>psf | 921.58808<br>psf  | 621.61901<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>8  | -17.05 ft        | 189.40742<br>ft | -141.43454<br>psf | 1,026.7015<br>psf | 692.51893<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>9  | -14.55 ft        | 189.43054<br>ft | -107.23012<br>psf | 1,099.4904<br>psf | 741.61564<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>10 | -12.05 ft        | 189.54545<br>ft | -78.753687<br>psf | 1,143.5521<br>psf | 771.33566<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>11 | -9.325 ft        | 189.78039<br>ft | -54.55872<br>psf  | 1,220.1229<br>psf | 822.9833<br>psf   | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>12 | -6.375 ft        | 190.15475<br>ft | -35.855228<br>psf | 1,308.3939<br>psf | 882.52284<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>13 | -4.5 ft          | 190.44566<br>ft | -27.272441<br>psf | 1,334.0365<br>psf | 899.81896<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>14 | -3.1014612<br>ft | 190.71565<br>ft | -23.825247<br>psf | 1,243.973<br>psf  | 839.07041<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>15 | -1.5014612<br>ft | 191.04949<br>ft | -21.276599<br>psf | 1,158.0885<br>psf | 781.14057<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>16 | 0.3 ft           | 191.48799<br>ft | -22.314664<br>psf | 3,682.8296<br>psf | 2,484.0999<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>17 | 2.65 ft          | 192.12665<br>ft | -27.827495<br>psf | 3,442.8598<br>psf | 2,322.2383<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>18 | 4.95 ft          | 192.8413<br>ft  | -38.812424<br>psf | 3,200.9791<br>psf | 2,159.0876<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>19 | 7.1 ft           | 193.5884<br>ft  | -54.014163<br>psf | 4,627.9851<br>psf | 3,121.6154<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |

| Slice<br>20 | 9.6 ft          | 194.57529<br>ft | -79.064374<br>psf | 4,667.3048<br>psf | 3,148.1368<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
|-------------|-----------------|-----------------|-------------------|-------------------|-------------------|-------|-------|---------------------------------------|
| Slice<br>21 | 11.4 ft         | 195.32871<br>ft | -99.775224<br>psf | 4,441.1593<br>psf | 2,995.5998<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>22 | 12.590503<br>ft | 195.88138<br>ft | -118.99826<br>psf | 4,266.3091<br>psf | 2,877.6618<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>23 | 13.790503<br>ft | 196.45293<br>ft | -140.00207<br>psf | 4,148.8121<br>psf | 3,241.4072<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>24 | 14.8475 ft      | 196.99151<br>ft | -160.69619<br>psf | 2,590.389<br>psf  | 2,023.8337<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>25 | 15.5975 ft      | 197.3785<br>ft  | -175.6814<br>psf  | 2,423.8101<br>psf | 1,893.688<br>psf  | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>26 | 16.3825 ft      | 197.80916<br>ft | -192.96346<br>psf | 2,264.4011<br>psf | 1,769.1441<br>psf | 0 psf | 0 psf | Gravel Borrow                         |
| Slice<br>27 | 18.90125 ft     | 199.29025<br>ft | -246.41775<br>psf | 1,937.8055<br>psf | 1,307.0663<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>28 | 22.37375 ft     | 201.54359<br>ft | -328.2141<br>psf  | 1,767.2582<br>psf | 1,192.0307<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>29 | 25.305 ft       | 203.66968<br>ft | -403.289<br>psf   | 1,628.0743<br>psf | 1,098.15<br>psf   | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>30 | 27.6375 ft      | 205.55711<br>ft | -466.04705<br>psf | 1,517.2893<br>psf | 1,023.4245<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>31 | 29.0875 ft      | 206.79994<br>ft | -509.39803<br>psf | 1,449.6216<br>psf | 977.78214<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>32 | 29.45 ft        | 207.1253<br>ft  | -521.14992<br>psf | 1,432.4616<br>psf | 966.20754<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>33 | 29.51 ft        | 207.17985<br>ft | -523.13822<br>psf | 1,429.6368<br>psf | 964.30217<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>34 | 30.51 ft        | 208.12801<br>ft | -558.58807<br>psf | 1,381.0467<br>psf | 931.52779<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>35 | 31.865 ft       | 209.43291<br>ft | -607.87832<br>psf | 1,317.2418<br>psf | 888.49082<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>36 | 33.4475 ft      | 211.10441<br>ft | -672.98058<br>psf | 1,237.5934<br>psf | 834.7673<br>psf   | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>37 | 35.8825 ft      | 213.86586<br>ft | -784.21021<br>psf | 1,112.2391<br>psf | 750.21477<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |
| Slice<br>38 | 38.05 ft        | 216.58304<br>ft | -899.38743<br>psf | 992.60833<br>psf  | 669.52277<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel |

| Slice<br>39 | 40.047044<br>ft | 219.39146<br>ft | -1,024.5344<br>psf | 1,023.7818<br>psf | 690.54958<br>psf | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                           |
|-------------|-----------------|-----------------|--------------------|-------------------|------------------|-------|-------|---|
| Slice<br>40 | 42.141133<br>ft | 222.69471<br>ft | -1,178.124<br>psf  | 813.62382<br>psf  | 548.7962<br>psf  | 0 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel                           |
| Slice<br>41 | 44.094089<br>ft | 226.196 ft      | -1,347.6122<br>psf | 525.31819<br>psf  | 456.65213<br>psf | 0 psf | 0 psf | ESU 1B Medium<br>Dense to Very<br>Dense Coarse-<br>Grained Fill |
| Slice<br>42 | 46.200589<br>ft | 230.73888<br>ft | -1,578.2438<br>psf | 257.56458<br>psf  | 223.89748<br>psf | 0 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill          |

# 1B.3 Compound - Pseudo-Static FC Wall (Spencer)

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### **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Bo Zhang Revision Number: 314 Date: 01/12/2022

Tool Version: 11.1.1.22700

Time: 10:44:22 AM

File Name: Wall 05.85L-B Sta 2+60\_FC Wall (lightweight fill).gsz Directory: P:\0\0180366\01\Analysis\Wall 05.85L-B\22-01-13\

Last Solved Date: 01/12/2022 Last Solved Time: 10:48:02 AM

## **Project Settings**

Unit System: U.S. Customary Units

## **Analysis Settings**

### 1B.3 Compound - Pseudo-Static FC Wall (Spencer)

Description: With Forward Compatible Wall

Kind: SLOPE/W

Analysis Type: Spencer

Settings

PWP Conditions from: Piezometric Line

Apply Phreatic Correction: No
Use Staged Rapid Drawdown: No
Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 1

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

**Factor of Safety Convergence Settings** 

Maximum Number of Iterations: 100 Tolerable difference in F of S: 0.001

**Solution Settings** 

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

#### **Materials**

#### ESU 4B Dense to Very Dense Sand/Gravel

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 42 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### ESU 1B Medium Dense to Very Dense Coarse-Grained Fill (Apparent Cohesion)

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 100 psf Effective Friction Angle: 41 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 115 pcf

Effective Cohesion: 200 psf Effective Friction Angle: 34 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **Forward Compatible Wall**

Material Model: High Strength

Unit Weight: 130 pcf
Pore Water Pressure
Piezometric Line: 1

#### **Common Borrow (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 50 psf Effective Friction Angle: 32 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **Lightweight EPS**

Material Model: Mohr-Coulomb

Unit Weight: 5 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 0 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### Reinforcements

### Row 1 (2 strips)(EQ)

Type: Geosynthetic

Interface Adhesion: 0 psf Interface Shear Angle: 8.8 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

#### Row 2 (2 strips)(EQ)

Type: Geosynthetic
Interface Adhesion: 0 psf

Interface Shear Angle: 8.2 °

Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

#### Row 3 (2 strips)(EQ)

Type: Geosynthetic

Interface Adhesion: 0 psf Interface Shear Angle: 7.5 °

Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

#### Row 4 (2 strips)(EQ)

Type: Geosynthetic

Interface Adhesion: 0 psf Interface Shear Angle: 6.8 °

Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

#### Row 5 (2 strips)(EQ)

Type: Geosynthetic

Interface Adhesion: 0 psf Interface Shear Angle: 6.2 °

Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

#### Row 6 (2 strips)(EQ)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 5.5 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

#### Row 7 (2 strips)(EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 4.9 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

#### Row 8 (2 strips)(EQ)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 4.2 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

#### Row 9+ (2 strips)(EQ)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 3.6 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

## **Slip Surface Entry and Exit**

Left Type: Range

Left-Zone Left Coordinate: (-46, 191.32629) ft Left-Zone Right Coordinate: (-0.9, 206) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (20, 233.5) ft Right-Zone Right Coordinate: (60, 233.74338) ft

Right-Zone Increment: 25
Radius Increments: 20

## **Slip Surface Limits**

Left Coordinate: (-80, 186.2) ft Right Coordinate: (80, 234.2) ft

### **Piezometric Lines**

#### Piezometric Line 1

#### Coordinates

|               | Х         | Υ          |
|---------------|-----------|------------|
| Coordinate 1  | -48.3 ft  | 180 ft     |
| Coordinate 2  | -4.1 ft   | 190.1 ft   |
| Coordinate 3  | 11.7 ft   | 193.8 ft   |
| Coordinate 4  | 17.165 ft | 194.87 ft  |
| Coordinate 5  | 24.11 ft  | 196.755 ft |
| Coordinate 6  | 29.52 ft  | 198.8 ft   |
| Coordinate 7  | 32.23 ft  | 199.83 ft  |
| Coordinate 8  | 60.885 ft | 211.35 ft  |
| Coordinate 9  | 70.775 ft | 215.12 ft  |
| Coordinate 10 | 74.125 ft | 216.15 ft  |
| Coordinate 11 | 80 ft     | 217.365 ft |

### **Seismic Coefficients**

Horz Seismic Coef.: 0.196

### **Reinforcement Lines**

#### **Reinforcement Line 1**

Reinforcement: Row 1 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 218.4) ft Inside Point: (15.6, 218.4) ft

Length: 16.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 2**

Reinforcement: Row 3 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 213.6) ft Inside Point: (15.6, 213.6) ft

Length: 16.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 3**

Reinforcement: Row 2 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 216) ft Inside Point: (15.6, 216) ft

Length: 16.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 4**

Reinforcement: Row 7 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 204) ft Inside Point: (15.6, 204) ft

Length: 16.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 5**

Reinforcement: Row 6 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 206.4) ft Inside Point: (15.6, 206.4) ft

Length: 16.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 6**

Reinforcement: Row 5 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 208.8) ft Inside Point: (15.6, 208.8) ft

Length: 16.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 7**

Reinforcement: Row 4 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 211.2) ft Inside Point: (15.6, 211.2) ft

Length: 16.5 ft
Orientation: 0°

Max. Pullout Force: 0 lbf

Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 8**

Reinforcement: Row 9+ (2 strips)(EQ)

Lock to Ground Surface: No Outside Point: (-0.9, 196.8) ft Inside Point: (15.6, 196.8) ft

Length: 16.5 ft Orientation: 0 °

Slip Surface Intersection: (15.031415, 196.8) ft

Max. Pullout Force: 5,240 lbf Available Length: 0.56858467 ft Required Length: 0.56858467 ft Pullout Force: 224.94028 lbf

Pullout Force per Length: 395.6144 lbf/ft Governing Component: Pullout Resistance

#### **Reinforcement Line 9**

Reinforcement: Row 9+ (2 strips)(EQ)

Lock to Ground Surface: No Outside Point: (-0.9, 199.2) ft Inside Point: (15.6, 199.2) ft

Length: 16.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 10**

Reinforcement: Row 8 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 201.6) ft Inside Point: (15.6, 201.6) ft

Length: 16.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

## **Surcharge Loads**

## Surcharge Load 1

Surcharge (Unit Weight): 125 pcf

Direction: Vertical

#### Coordinates

| Х       | Υ        |
|---------|----------|
| 8.1 ft  | 234.5 ft |
| 45 ft   | 234.5 ft |
| 58.1 ft | 234.7 ft |
| 80 ft   | 235.2 ft |

## **Geometry**

Name: 1. Compound Stability

**Settings** 

View: 2D

Element Thickness: 1 ft

#### **Points**

| LS       |          |          |
|----------|----------|----------|
|          | Х        | Υ        |
| Point 1  | 80 ft    | 199.4 ft |
| Point 2  | 58 ft    | 196.6 ft |
| Point 3  | 37.6 ft  | 191.9 ft |
| Point 4  | 42.1 ft  | 180 ft   |
| Point 5  | 80 ft    | 180 ft   |
| Point 6  | 80 ft    | 226 ft   |
| Point 7  | 58 ft    | 225.3 ft |
| Point 8  | 29.8 ft  | 195 ft   |
| Point 9  | 11.7 ft  | 193.8 ft |
| Point 10 | -48.3 ft | 180 ft   |
| Point 11 | 80 ft    | 234.2 ft |
| Point 12 | 58.1 ft  | 233.7 ft |
| Point 13 | 26.5 ft  | 214.1 ft |
| Point 14 | -10.8 ft | 197 ft   |
| Point 15 | -18.3 ft | 195.3 ft |
| Point 16 | -21.1 ft | 194.7 ft |
| Point 17 | -24.4 ft | 193.6 ft |
| Point 18 | -32.1 ft | 193.1 ft |
| Point 19 | -36.6 ft | 192.3 ft |
| Point 20 | -61.7 ft | 189.7 ft |
| Point 21 | -65.4 ft | 189.3 ft |
| Point 22 | -73.2 ft | 188 ft   |
| Point 23 | -80 ft   | 186.2 ft |
|          |          |          |

| Point 24 | -80 ft    | 180 ft    |
|----------|-----------|-----------|
| Point 25 | -4.1 ft   | 190.1 ft  |
| Point 26 | 32 ft     | 197.4 ft  |
| Point 27 | -0.9 ft   | 219.4 ft  |
| Point 28 | -0.9 ft   | 196.3 ft  |
| Point 29 | -4.9 ft   | 199.8 ft  |
| Point 30 | -0.9 ft   | 199.8 ft  |
| Point 31 | -0.9 ft   | 199.4 ft  |
| Point 32 | 15.6 ft   | 196.3 ft  |
| Point 33 | 15.6 ft   | 219.4 ft  |
| Point 34 | 11.1 ft   | 196.3 ft  |
| Point 35 | 17.1 ft   | 196.3 ft  |
| Point 36 | 17.1 ft   | 214.2 ft  |
| Point 37 | 15.6 ft   | 214.2 ft  |
| Point 38 | 17.1 ft   | 208.4 ft  |
| Point 39 | 45 ft     | 233.5 ft  |
| Point 40 | 37.1 ft   | 228.2 ft  |
| Point 41 | 29.4 ft   | 222.3 ft  |
| Point 42 | 29.5 ft   | 233.5 ft  |
| Point 43 | 1.5 ft    | 219.4 ft  |
| Point 44 | 31.5 ft   | 233.5 ft  |
| Point 45 | 6.1 ft    | 233.5 ft  |
| Point 46 | 14.1 ft   | 233.5 ft  |
| Point 47 | 14.1 ft   | 219.4 ft  |
| Point 48 | 6.1 ft    | 219.4 ft  |
| Point 49 | 14.1 ft   | 225.9 ft  |
| Point 50 | 6.1 ft    | 221.74 ft |
| Point 51 | 17.1 ft   | 219.4 ft  |
| Point 52 | 28.775 ft | 233.5 ft  |
| Point 53 | 6.1 ft    | 232 ft    |
| Point 54 | 14.1 ft   | 232 ft    |
| Point 55 | 39 ft     | 233.5 ft  |
| Point 56 | 39 ft     | 230.5 ft  |

## Regions

|             | Material  | Points  | Area                       |
|-------------|---|---|----------------------------|
| Region<br>1 | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt              | 1,2,3,4,5                                       | 659.92<br>ft <sup>2</sup>  |
| Region<br>2 | ESU 4B Dense to Very Dense Sand/Gravel  | 1,6,7,26,8,9,25,10,4,3,2                        | 1,867.8<br>ft <sup>2</sup> |
| Region 3    | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill (Apparent Cohesion) | 14,29,30,31                                     | 7.58 ft <sup>2</sup>       |
| Region<br>4 | Gravel Borrow   | 27,30,31,28,34,32,37,33,47,48,43                | 381.15<br>ft <sup>2</sup>  |
| Region<br>5 | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                           | 7,6,11,12,13,38,35,32,34,25,9,8,26              | 856.44<br>ft <sup>2</sup>  |
| Region<br>6 | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                           | 14,15,16,17,18,19,20,21,22,23,24,10,25,34,28,31 | 748.7<br>ft <sup>2</sup>   |
| Region      | Gravel Borrow   | 32,35,38,36,37                                  | 26.85                      |

| 7            |   |                         | ft²                       |
|--------------|---|-------------------------|---------------------------|
| Region<br>8  | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill (Apparent Cohesion) | 12,39,40,41,36,38,13    | 241.79<br>ft <sup>2</sup> |
| Region<br>9  | Forward Compatible Wall   | 48,47,49,50             | 35.36<br>ft <sup>2</sup>  |
| Region<br>10 | Common Borrow (Apparent Cohesion)   | 39,56,51,36,41,40       | 75.79<br>ft²              |
| Region<br>11 | Lightweight EPS   | 46,54,49,42,52          | 58.52<br>ft <sup>2</sup>  |
| Region<br>12 | Forward Compatible Wall   | 46,45,53,54             | 12 ft²                    |
| Region<br>13 |   | 50,43,48                | 5.382<br>ft <sup>2</sup>  |
| Region<br>14 | Gravel Borrow   | 33,37,36,51             | 7.8 ft <sup>2</sup>       |
| Region<br>15 | Forward Compatible Wall   | 50,49,54,53             | 65.44<br>ft <sup>2</sup>  |
| Region<br>16 | Lightweight EPS   | 44,42,49,47,33,51,56,55 | 171.02<br>ft <sup>2</sup> |
| Region<br>17 | Common Borrow (Apparent Cohesion)   | 39,55,56                | 9 ft²                     |

## **Slip Results**

Slip Surfaces Analysed: 6871 of 14196 converged

## **Current Slip Surface**

Slip Surface: 2,637 Factor of Safety: 1.3 Volume: 1,587.1579 ft<sup>3</sup> Weight: 169,208.24 lbf

Resisting Moment: 10,182,394 lbf·ft Activating Moment: 7,860,517.9 lbf·ft

Resisting Force: 112,963.45 lbf
Activating Force: 87,195.976 lbf
Slip Rank: 1 of 14,196 slip surfaces
Exit: (-37.644692, 192.19178) ft
Entry: (53.600696, 233.63131) ft

Radius: 80.16144 ft

Center: (-17.895571, 269.88238) ft

### **Slip Slices**

|            | Х                | Y               | PWP               | Base<br>Normal<br>Stress | Frictional<br>Strength | Cohesive<br>Strength | Suction<br>Strength | Base Material                                      |
|------------|------------------|-----------------|-------------------|--------------------------|------------------------|----------------------|---------------------|--|
| Slice<br>1 | -37.122346<br>ft | 192.06273<br>ft | -593.33414<br>psf | 534.5441<br>psf          | 360.55455<br>psf       | 200 psf              | 0 psf               | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent |

|             |                  |                 |                   |                   |                  |         |       | Cohesion)   |
|-------------|------------------|-----------------|-------------------|-------------------|------------------|---------|-------|---|
| Slice<br>2  | -34.35 ft        | 191.46157<br>ft | -516.29165<br>psf | 746.53063<br>psf  | 503.54127<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>3  | -30.816667<br>ft | 190.77985<br>ft | -423.37067<br>psf | 907.46284<br>psf  | 612.09141<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>4  | -28.25 ft        | 190.40303<br>ft | -363.25958<br>psf | 933.7448<br>psf   | 629.81882<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>5  | -25.683333<br>ft | 190.11055<br>ft | -308.41141<br>psf | 938.99055<br>psf  | 633.35713<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>6  | -22.75 ft        | 189.88514<br>ft | -252.51981<br>psf | 1,005.0567<br>psf | 677.91933<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>7  | -19.7 ft         | 189.75349<br>ft | -200.81527<br>psf | 1,077.7369<br>psf | 726.94271<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>8  | -16.425 ft       | 189.75637<br>ft | -154.29768<br>psf | 1,092.5161<br>psf | 736.91143<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>9  | -12.675 ft       | 189.91319<br>ft | -110.61245<br>psf | 1,087.4766<br>psf | 733.51225<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>10 | -9.325 ft        | 190.19423<br>ft | -80.382447<br>psf | 1,123.5112<br>psf | 757.81786<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>11 | -6.375 ft        | 190.56711<br>ft | -61.586791<br>psf | 1,187.0156<br>psf | 800.65213<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>12 | -4.5 ft          | 190.84916<br>ft | -52.450883<br>psf | 1,205.2242<br>psf | 812.93395<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent              |

|             |                   |                 |                   |                   |                   |         |       | Cohesion)   |
|-------------|-------------------|-----------------|-------------------|-------------------|-------------------|---------|-------|---|
| Slice<br>13 | -2.5 ft           | 191.23014<br>ft | -47.140556<br>psf | 1,090.8043<br>psf | 735.75682<br>psf  | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>14 | -0.52880405<br>ft | 191.6257<br>ft  | -43.019319<br>psf | 3,490.4399<br>psf | 2,354.3314<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>15 | 0.67119595<br>ft  | 191.90542<br>ft | -42.9386<br>psf   | 3,370.4213<br>psf | 2,273.3778<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>16 | 2.65 ft           | 192.40774<br>ft | -45.36732<br>psf  | 3,190.9617<br>psf | 2,152.3308<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>17 | 4.95 ft           | 193.05467<br>ft | -52.126937<br>psf | 2,991.2586<br>psf | 2,017.6294<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>18 | 7.1 ft            | 193.72485<br>ft | -62.528581<br>psf | 4,334.7594<br>psf | 2,923.8321<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>19 | 9.6 ft            | 194.60091<br>ft | -80.663336<br>psf | 4,176.0116<br>psf | 2,816.7554<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>20 | 11.4 ft           | 195.26655<br>ft | -95.896548<br>psf | 3,997.8667<br>psf | 2,696.5951<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>21 | 12.804178<br>ft   | 195.84217<br>ft | -113.94113<br>psf | 3,835.1737<br>psf | 2,586.8573<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>22 | 14.004178<br>ft   | 196.34156<br>ft | -130.44262<br>psf | 3,800.4732<br>psf | 2,969.2551<br>psf | 0 psf   | 0 psf | Gravel Borrow   |
| Slice<br>23 | 14.85 ft          | 196.7188<br>ft  | -143.64865<br>psf | 2,351.2309<br>psf | 1,836.9829<br>psf | 0 psf   | 0 psf | Gravel Borrow   |
| Slice<br>24 | 16.3825 ft        | 197.42466<br>ft | -168.97102<br>psf | 2,211.0153<br>psf | 1,727.4345<br>psf | 0 psf   | 0 psf | Gravel Borrow   |
| Slice       |                   | 198.69228       | -209.10425        | 1,926.6866        | 1,299.5665        |         |       | ESU 2B Medium<br>Dense  |

| 25          | 18.90125 ft | ft              | psf               | psf               | psf               | 200 psf | 0 psf | Sand/Gravel<br>(Apparent<br>Cohesion)                           |
|-------------|-------------|-----------------|-------------------|-------------------|-------------------|---------|-------|---|
| Slice<br>26 | 22.37375 ft | 200.59887<br>ft | -269.26329<br>psf | 1,787.3718<br>psf | 1,205.5975<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>27 | 25.305 ft   | 202.37272<br>ft | -322.35872<br>psf | 1,663.7934<br>psf | 1,122.2428<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>28 | 27.6375 ft  | 203.92266<br>ft | -364.05701<br>psf | 1,559.6404<br>psf | 1,051.9907<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>29 | 29.0875 ft  | 204.93395<br>ft | -392.96 psf       | 1,493.7635<br>psf | 1,007.5562<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>30 | 29.45 ft    | 205.19661<br>ft | -400.79929<br>psf | 1,476.8947<br>psf | 996.17806<br>psf  | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>31 | 29.51 ft    | 205.24054<br>ft | -402.12529<br>psf | 1,474.1117<br>psf | 994.30088<br>psf  | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>32 | 30.51 ft    | 205.998 ft      | -425.67563<br>psf | 1,426.3467<br>psf | 962.08303<br>psf  | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>33 | 31.865 ft   | 207.03713<br>ft | -458.3816<br>psf  | 1,362.4705<br>psf | 918.99795<br>psf  | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>34 | 33.4475 ft  | 208.34189<br>ft | -500.59964<br>psf | 1,283.7822<br>psf | 865.92203<br>psf  | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>35 | 35.8825 ft  | 210.4595<br>ft  | -571.65286<br>psf | 1,161.0094<br>psf | 783.11072<br>psf  | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
|             |             |                 |                   |                   |                   |         |       | ESU 2B Medium<br>Dense  |

| ipound -    | i seudo-statie i e v | van (Spencer)   |                    |                   |                  |         |       |  |
|-------------|----------------------|-----------------|--------------------|-------------------|------------------|---------|-------|--|
| Slice<br>36 | 38.05 ft             | 212.48735<br>ft | -643.81636<br>psf  | 1,048.1926<br>psf | 707.01482<br>psf | 200 psf | 0 psf | Sand/Gravel<br>(Apparent<br>Cohesion)                            |
| Slice<br>37 | 40.5 ft              | 215.00966<br>ft | -739.74701<br>psf  | 1,026.3518<br>psf | 692.28303<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion)  |
| Slice<br>38 | 43.5 ft              | 218.3946<br>ft  | -875.70871<br>psf  | 778.24147<br>psf  | 524.9305<br>psf  | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion)  |
| Slice<br>39 | 46.591017<br>ft      | 222.34137<br>ft | -1,044.4447<br>psf | 525.32743<br>psf  | 354.33782<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion)  |
| Slice<br>40 | 49.77305 ft          | 227.01075<br>ft | -1,255.9888<br>psf | 271.63023<br>psf  | 183.2169<br>psf  | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion)  |
| Slice<br>41 | 52.482381<br>ft      | 231.57666<br>ft | -1,472.9344<br>psf | 86.359899<br>psf  | 75.071515<br>psf | 100 psf | 0 psf | ESU 1B Medium Dense to Very Dense Coarse- Grained Fill (Apparent |

# 1B.4 Compound - Pseudo-Static FC Wall (M-P)

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### **File Information**

File Version: 11.01 Created By: Jon Cracolici Last Edited By: Bo Zhang Revision Number: 314 Date: 01/12/2022

Tool Version: 11.1.1.22700

Time: 10:44:22 AM

File Name: Wall 05.85L-B Sta 2+60\_FC Wall (lightweight fill).gsz Directory: P:\0\0180366\01\Analysis\Wall 05.85L-B\22-01-13\

Last Solved Date: 01/12/2022 Last Solved Time: 10:48:48 AM

## **Project Settings**

Unit System: U.S. Customary Units

## **Analysis Settings**

### 1B.4 Compound - Pseudo-Static FC Wall (M-P)

**Description: With Forward Compatible Wall** 

Kind: SLOPE/W

Analysis Type: Morgenstern-Price

Settings

**Side Function** 

Interslice force function option: Half-Sine

PWP Conditions from: Piezometric Line

Apply Phreatic Correction: No
Use Staged Rapid Drawdown: No
Critical Slip Surface Source from: (none)

Unit Weight of Water: 62.4 pcf

Slip Surface

Direction of movement: Right to Left

Use Passive Mode: No

Slip Surface Option: Entry and Exit Critical slip surfaces saved: 1

Optimize Critical Slip Surface Location: No

Tension Crack Option: (none)

Distribution

F of S Calculation Option: Constant

Advanced

**Geometry Settings** 

Minimum Slip Surface Depth: 0.1 ft

Number of Slices: 30

**Factor of Safety Convergence Settings** 

Maximum Number of Iterations: 100
Tolerable difference in F of S: 0.001

**Solution Settings** 

Search Method: Root Finder

Tolerable difference between starting and converged F of S: 3

Maximum iterations to calculate converged lambda: 20

Max Absolute Lambda: 2

### **Materials**

### **ESU 4B Dense to Very Dense Sand/Gravel**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 43 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **Gravel Borrow**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 38 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf Effective Cohesion: 0 psf Effective Friction Angle: 42 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

#### **ESU 1B Medium Dense to Very Dense Coarse-Grained Fill (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 130 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 41 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### **ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 115 pcf

Effective Cohesion: 200 psf Effective Friction Angle: 34 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### **Forward Compatible Wall**

Material Model: High Strength

Unit Weight: 130 pcf
Pore Water Pressure
Piezometric Line: 1

### **Common Borrow (Apparent Cohesion)**

Material Model: Mohr-Coulomb

Unit Weight: 120 pcf Effective Cohesion: 50 psf Effective Friction Angle: 32 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

### **Lightweight EPS**

Material Model: Mohr-Coulomb

Unit Weight: 5 pcf

Effective Cohesion: 100 psf Effective Friction Angle: 0 °

Phi-B: 0°

Pore Water Pressure
Piezometric Line: 1

## Reinforcements

## Row 1 (2 strips)(EQ)

Type: Geosynthetic

Interface Adhesion: 0 psf Interface Shear Angle: 8.8 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

### Row 2 (2 strips)(EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 8.2 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

### Row 3 (2 strips)(EQ)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 7.5 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

#### Row 4 (2 strips)(EQ)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 6.8 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

### Row 5 (2 strips)(EQ)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 6.2 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

### Row 6 (2 strips)(EQ)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 5.5 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

#### Row 7 (2 strips)(EQ)

Type: Geosynthetic Interface Adhesion: 0 psf Interface Shear Angle: 4.9 ° Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

### Row 8 (2 strips)(EQ)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 4.2 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

### Row 9+ (2 strips)(EQ)

Type: Geosynthetic
Interface Adhesion: 0 psf
Interface Shear Angle: 3.6 °
Surface Area Factor: 2

Pullout Resistance Reduction Factor: 1

Tensile Capacity: 5,240 lbf

Tensile Capacity Reduction Factor: 1

F of S Dependent: No

Force Distribution: Distributed

Face Anchorage: Yes

Factored Tensile Capacity: 5,240 lbf/ft

# **Slip Surface Entry and Exit**

Left Type: Range

Left-Zone Left Coordinate: (-46, 191.32629) ft Left-Zone Right Coordinate: (-0.9, 206) ft

Left-Zone Increment: 25

Right Type: Range

Right-Zone Left Coordinate: (20, 233.5) ft Right-Zone Right Coordinate: (60, 233.74338) ft

Right-Zone Increment: 25 Radius Increments: 20

## **Slip Surface Limits**

Left Coordinate: (-80, 186.2) ft Right Coordinate: (80, 234.2) ft

### **Piezometric Lines**

#### Piezometric Line 1

#### Coordinates

|               | Х         | Υ          |
|---------------|-----------|------------|
| Coordinate 1  | -48.3 ft  | 180 ft     |
| Coordinate 2  | -4.1 ft   | 190.1 ft   |
| Coordinate 3  | 11.7 ft   | 193.8 ft   |
| Coordinate 4  | 17.165 ft | 194.87 ft  |
| Coordinate 5  | 24.11 ft  | 196.755 ft |
| Coordinate 6  | 29.52 ft  | 198.8 ft   |
| Coordinate 7  | 32.23 ft  | 199.83 ft  |
| Coordinate 8  | 60.885 ft | 211.35 ft  |
| Coordinate 9  | 70.775 ft | 215.12 ft  |
| Coordinate 10 | 74.125 ft | 216.15 ft  |
| Coordinate 11 | 80 ft     | 217.365 ft |

### **Seismic Coefficients**

Horz Seismic Coef.: 0.196

### **Reinforcement Lines**

#### **Reinforcement Line 1**

Reinforcement: Row 1 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 218.4) ft Inside Point: (15.6, 218.4) ft

Length: 16.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 2**

Reinforcement: Row 3 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 213.6) ft Inside Point: (15.6, 213.6) ft

Length: 16.5 ft
Orientation: 0°

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 3**

Reinforcement: Row 2 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 216) ft Inside Point: (15.6, 216) ft

Length: 16.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft

Governing Component: (none)

#### **Reinforcement Line 4**

Reinforcement: Row 7 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 204) ft Inside Point: (15.6, 204) ft

Length: 16.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 5**

Reinforcement: Row 6 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 206.4) ft Inside Point: (15.6, 206.4) ft

Length: 16.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 6**

Reinforcement: Row 5 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 208.8) ft Inside Point: (15.6, 208.8) ft

Length: 16.5 ft
Orientation: 0°

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### Reinforcement Line 7

Reinforcement: Row 4 (2 strips)(EQ)

Lock to Ground Surface: Yes
Outside Point: (-0.9, 211.2) ft

Inside Point: (15.6, 211.2) ft

Length: 16.5 ft
Orientation: 0 °

Max. Pullout Force: 0 lbf
Available Length: 0 ft
Required Length: 0 ft
Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 8**

Reinforcement: Row 9+ (2 strips)(EQ)

Lock to Ground Surface: No Outside Point: (-0.9, 196.8) ft Inside Point: (15.6, 196.8) ft

Length: 16.5 ft
Orientation: 0 °

Slip Surface Intersection: (15.031415, 196.8) ft

Max. Pullout Force: 5,240 lbf Available Length: 0.56858467 ft Required Length: 0.56858467 ft Pullout Force: 224.94028 lbf

Pullout Force per Length: 395.6144 lbf/ft Governing Component: Pullout Resistance

#### **Reinforcement Line 9**

Reinforcement: Row 9+ (2 strips)(EQ)

Lock to Ground Surface: No Outside Point: (-0.9, 199.2) ft Inside Point: (15.6, 199.2) ft

Length: 16.5 ft
Orientation: 0°

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

#### **Reinforcement Line 10**

Reinforcement: Row 8 (2 strips)(EQ)

Lock to Ground Surface: Yes Outside Point: (-0.9, 201.6) ft Inside Point: (15.6, 201.6) ft

Length: 16.5 ft Orientation: 0 °

Max. Pullout Force: 0 lbf Available Length: 0 ft Required Length: 0 ft Pullout Force: 0 lbf

Pullout Force per Length: 0 lbf/ft Governing Component: (none)

# **Surcharge Loads**

### **Surcharge Load 1**

Surcharge (Unit Weight): 125 pcf

**Direction: Vertical** 

#### **Coordinates**

| Х       | Υ        |
|---------|----------|
| 8.1 ft  | 234.5 ft |
| 45 ft   | 234.5 ft |
| 58.1 ft | 234.7 ft |
| 80 ft   | 235.2 ft |

# Geometry

Name: 1. Compound Stability

### **Settings**

View: 2D

Element Thickness: 1 ft

#### **Points**

|          | X        | Υ        |
|----------|----------|----------|
| Point 1  | 80 ft    | 199.4 ft |
| Point 2  | 58 ft    | 196.6 ft |
| Point 3  | 37.6 ft  | 191.9 ft |
| Point 4  | 42.1 ft  | 180 ft   |
| Point 5  | 80 ft    | 180 ft   |
| Point 6  | 80 ft    | 226 ft   |
| Point 7  | 58 ft    | 225.3 ft |
| Point 8  | 29.8 ft  | 195 ft   |
| Point 9  | 11.7 ft  | 193.8 ft |
| Point 10 | -48.3 ft | 180 ft   |
| Point 11 | 80 ft    | 234.2 ft |
| Point 12 | 58.1 ft  | 233.7 ft |
| Point 13 | 26.5 ft  | 214.1 ft |
| Point 14 | -10.8 ft | 197 ft   |
| Point 15 | -18.3 ft | 195.3 ft |
| Point 16 | -21.1 ft | 194.7 ft |
| Point 17 | -24.4 ft | 193.6 ft |
| Point 18 | -32.1 ft | 193.1 ft |
|          |          |          |

| ipound - Pseudo-Static FC wan (M-F) |           |           |  |  |  |  |  |  |
|-------------------------------------|-----------|-----------|--|--|--|--|--|--|
| Point 19                            | -36.6 ft  | 192.3 ft  |  |  |  |  |  |  |
| Point 20                            | -61.7 ft  | 189.7 ft  |  |  |  |  |  |  |
| Point 21                            | -65.4 ft  | 189.3 ft  |  |  |  |  |  |  |
| Point 22                            | -73.2 ft  | 188 ft    |  |  |  |  |  |  |
| Point 23                            | -80 ft    | 186.2 ft  |  |  |  |  |  |  |
| Point 24                            | -80 ft    | 180 ft    |  |  |  |  |  |  |
| Point 25                            | -4.1 ft   | 190.1 ft  |  |  |  |  |  |  |
| Point 26                            | 32 ft     | 197.4 ft  |  |  |  |  |  |  |
| Point 27                            | -0.9 ft   | 219.4 ft  |  |  |  |  |  |  |
| Point 28                            | -0.9 ft   | 196.3 ft  |  |  |  |  |  |  |
| Point 29                            | -4.9 ft   | 199.8 ft  |  |  |  |  |  |  |
| Point 30                            | -0.9 ft   | 199.8 ft  |  |  |  |  |  |  |
| Point 31                            | -0.9 ft   | 199.4 ft  |  |  |  |  |  |  |
| Point 32                            | 15.6 ft   | 196.3 ft  |  |  |  |  |  |  |
| Point 33                            | 15.6 ft   | 219.4 ft  |  |  |  |  |  |  |
| Point 34                            | 11.1 ft   | 196.3 ft  |  |  |  |  |  |  |
| Point 35                            | 17.1 ft   | 196.3 ft  |  |  |  |  |  |  |
| Point 36                            | 17.1 ft   | 214.2 ft  |  |  |  |  |  |  |
| Point 37                            | 15.6 ft   | 214.2 ft  |  |  |  |  |  |  |
| Point 38                            | 17.1 ft   | 208.4 ft  |  |  |  |  |  |  |
| Point 39                            | 45 ft     | 233.5 ft  |  |  |  |  |  |  |
| Point 40                            | 37.1 ft   | 228.2 ft  |  |  |  |  |  |  |
| Point 41                            | 29.4 ft   | 222.3 ft  |  |  |  |  |  |  |
| Point 42                            | 29.5 ft   | 233.5 ft  |  |  |  |  |  |  |
| Point 43                            | 1.5 ft    | 219.4 ft  |  |  |  |  |  |  |
| Point 44                            | 31.5 ft   | 233.5 ft  |  |  |  |  |  |  |
| Point 45                            | 6.1 ft    | 233.5 ft  |  |  |  |  |  |  |
| Point 46                            | 14.1 ft   | 233.5 ft  |  |  |  |  |  |  |
| Point 47                            | 14.1 ft   | 219.4 ft  |  |  |  |  |  |  |
| Point 48                            | 6.1 ft    | 219.4 ft  |  |  |  |  |  |  |
| Point 49                            | 14.1 ft   | 225.9 ft  |  |  |  |  |  |  |
| Point 50                            | 6.1 ft    | 221.74 ft |  |  |  |  |  |  |
| Point 51                            | 17.1 ft   | 219.4 ft  |  |  |  |  |  |  |
| Point 52                            | 28.775 ft | 233.5 ft  |  |  |  |  |  |  |
| Point 53                            | 6.1 ft    | 232 ft    |  |  |  |  |  |  |
| Point 54                            | 14.1 ft   | 232 ft    |  |  |  |  |  |  |
| Point 55                            | 39 ft     | 233.5 ft  |  |  |  |  |  |  |
| Point 56                            | 39 ft     | 230.5 ft  |  |  |  |  |  |  |

# Regions

|             | Material  | Points                           | Area                       |
|-------------|---|----------------------------------|----------------------------|
| Region<br>1 | ESU 5B Very Stiff to Hard Silt and Clay/Dense to Very Dense Silt              | 1,2,3,4,5                        | 659.92<br>ft <sup>2</sup>  |
| Region<br>2 | ESU 4B Dense to Very Dense Sand/Gravel  | 1,6,7,26,8,9,25,10,4,3,2         | 1,867.8<br>ft <sup>2</sup> |
| Region 3    | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill (Apparent Cohesion) | 14,29,30,31                      | 7.58 ft <sup>2</sup>       |
| Region<br>4 | Gravel Borrow   | 27,30,31,28,34,32,37,33,47,48,43 | 381.15<br>ft <sup>2</sup>  |

| Region<br>5  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                           | 7,6,11,12,13,38,35,32,34,25,9,8,26              | 856.44<br>ft <sup>2</sup> |
|--------------|---|---|---------------------------|
| Region<br>6  | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                           | 14,15,16,17,18,19,20,21,22,23,24,10,25,34,28,31 | 748.7<br>ft <sup>2</sup>  |
| Region<br>7  | Gravel Borrow   | 32,35,38,36,37                                  | 26.85<br>ft <sup>2</sup>  |
| Region<br>8  | ESU 1B Medium Dense to Very Dense Coarse-<br>Grained Fill (Apparent Cohesion) | 12,39,40,41,36,38,13                            | 241.79<br>ft <sup>2</sup> |
| Region<br>9  | Forward Compatible Wall   | 48,47,49,50                                     | 35.36<br>ft <sup>2</sup>  |
| Region<br>10 | Common Borrow (Apparent Cohesion)   | 39,56,51,36,41,40                               | 75.79<br>ft²              |
| Region<br>11 | Lightweight EPS   | 46,54,49,42,52                                  | 58.52<br>ft <sup>2</sup>  |
| Region<br>12 | Forward Compatible Wall   | 46,45,53,54                                     | 12 ft²                    |
| Region<br>13 |   | 50,43,48  | 5.382<br>ft <sup>2</sup>  |
| Region<br>14 | Gravel Borrow   | 33,37,36,51                                     | 7.8 ft <sup>2</sup>       |
| Region<br>15 | Forward Compatible Wall   | 50,49,54,53                                     | 65.44<br>ft <sup>2</sup>  |
| Region<br>16 | Lightweight EPS   | 44,42,49,47,33,51,56,55                         | 171.02<br>ft <sup>2</sup> |
| Region<br>17 | Common Borrow (Apparent Cohesion)   | 39,55,56  | 9 ft²                     |

## **Slip Results**

Slip Surfaces Analysed: 8578 of 14196 converged

# **Current Slip Surface**

Slip Surface: 2,637 Factor of Safety: 1.3 Volume: 1,587.1579 ft<sup>3</sup> Weight: 169,208.24 lbf

Resisting Moment: 10,167,731 lbf·ft Activating Moment: 7,860,517.9 lbf·ft

Resisting Force: 112,873.54 lbf Activating Force: 87,258.916 lbf Slip Rank: 1 of 14,196 slip surfaces Exit: (-37.644692, 192.19178) ft Entry: (53.600696, 233.63131) ft

Radius: 80.16144 ft

Center: (-17.895571, 269.88238) ft

### **Slip Slices**

|  | x | Y | PWP | Base<br>Normal | Frictional | Cohesive | Suction | Base Material |  |
|--|---|---|-----|----------------|------------|----------|---------|---------------|--|
|--|---|---|-----|----------------|------------|----------|---------|---------------|--|

|             |                  |                 |                   | Stress            | Strength          | Strength | Strength |   |
|-------------|------------------|-----------------|-------------------|-------------------|-------------------|----------|----------|---|
| Slice<br>1  | -37.122346<br>ft | 192.06273<br>ft | -593.33414<br>psf | 86.237165<br>psf  | 58.167702<br>psf  | 200 psf  | 0 psf    | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>2  | -34.35 ft        | 191.46157<br>ft | -516.29165<br>psf | 322.38595<br>psf  | 217.45207<br>psf  | 200 psf  | 0 psf    | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>3  | -30.816667<br>ft | 190.77985<br>ft | -423.37067<br>psf | 602.25906<br>psf  | 406.22887<br>psf  | 200 psf  | 0 psf    | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>4  | -28.25 ft        | 190.40303<br>ft | -363.25958<br>psf | 759.45738<br>psf  | 512.26047<br>psf  | 200 psf  | 0 psf    | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>5  | -25.683333<br>ft | 190.11055<br>ft | -308.41141<br>psf | 893.78875<br>psf  | 602.86812<br>psf  | 200 psf  | 0 psf    | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>6  | -22.75 ft        | 189.88514<br>ft | -252.51981<br>psf | 1,077.9365<br>psf | 727.07738<br>psf  | 200 psf  | 0 psf    | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>7  | -19.7 ft         | 189.75349<br>ft | -200.81527<br>psf | 1,257.5376<br>psf | 848.21979<br>psf  | 200 psf  | 0 psf    | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>8  | -16.425 ft       | 189.75637<br>ft | -154.29768<br>psf | 1,366.8103<br>psf | 921.92517<br>psf  | 200 psf  | 0 psf    | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>9  | -12.675 ft       | 189.91319<br>ft | -110.61245<br>psf | 1,425.4135<br>psf | 961.45358<br>psf  | 200 psf  | 0 psf    | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)             |
| Slice<br>10 | -9.325 ft        | 190.19423<br>ft | -80.382447<br>psf | 1,475.5869<br>psf | 995.29595<br>psf  | 200 psf  | 0 psf    | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>11 | -6.375 ft        | 190.56711<br>ft | -61.586791<br>psf | 1,523.0074<br>psf | 1,027.2814<br>psf | 200 psf  | 0 psf    | ESU 2B Medium<br>Dense<br>Sand/Gravel                           |

|             |                   |                 |                   |                   |                   |         |       | (Apparent Cohesion)   |
|-------------|-------------------|-----------------|-------------------|-------------------|-------------------|---------|-------|---|
| Slice<br>12 | -4.5 ft           | 190.84916<br>ft | -52.450883<br>psf | 1,520.3098<br>psf | 1,025.4619<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>13 | -2.5 ft           | 191.23014<br>ft | -47.140556<br>psf | 1,368.9859<br>psf | 923.39268<br>psf  | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>14 | -0.52880405<br>ft | 191.6257<br>ft  | -43.019319<br>psf | 3,747.8391<br>psf | 2,527.9494<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>15 | 0.67119595<br>ft  | 191.90542<br>ft | -42.9386<br>psf   | 3,596.145<br>psf  | 2,425.6305<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>16 | 2.65 ft           | 192.40774<br>ft | -45.36732<br>psf  | 3,358.7922<br>psf | 2,265.534<br>psf  | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>17 | 4.95 ft           | 193.05467<br>ft | -52.126937<br>psf | 3,086.0908<br>psf | 2,081.5946<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>18 | 7.1 ft            | 193.72485<br>ft | -62.528581<br>psf | 4,349.8942<br>psf | 2,934.0407<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>19 | 9.6 ft            | 194.60091<br>ft | -80.663336<br>psf | 4,110.6346<br>psf | 2,772.6581<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>20 | 11.4 ft           | 195.26655<br>ft | -95.896548<br>psf | 3,883.4031<br>psf | 2,619.3885<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>21 | 12.804178<br>ft   | 195.84217<br>ft | -113.94113<br>psf | 3,684.3233<br>psf | 2,485.1075<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>22 | 14.004178<br>ft   | 196.34156<br>ft | -130.44262<br>psf | 3,648.5895<br>psf | 2,850.5905<br>psf | 0 psf   | 0 psf | Gravel Borrow   |
| Slice       |                   | 196.7188        | -143.64865        | 2,188.9752        | 1,710.2149        |         |       |   |

| 23          | 14.85 ft    | ft              | psf               | psf               | psf               | 0 psf   | 0 psf | Gravel Borrow   |
|-------------|-------------|-----------------|-------------------|-------------------|-------------------|---------|-------|---|
| Slice<br>24 | 16.3825 ft  | 197.42466<br>ft | -168.97102<br>psf | 2,023.2114<br>psf | 1,580.706<br>psf  | 0 psf   | 0 psf | Gravel Borrow   |
| Slice<br>25 | 18.90125 ft | 198.69228<br>ft | -209.10425<br>psf | 1,716.7171<br>psf | 1,157.9403<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>26 | 22.37375 ft | 200.59887<br>ft | -269.26329<br>psf | 1,562.852<br>psf  | 1,054.157<br>psf  | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>27 | 25.305 ft   | 202.37272<br>ft | -322.35872<br>psf | 1,446.6343<br>psf | 975.76717<br>psf  | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>28 | 27.6375 ft  | 203.92266<br>ft | -364.05701<br>psf | 1,360.3076<br>psf | 917.53905<br>psf  | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>29 | 29.0875 ft  | 204.93395<br>ft | -392.96 psf       | 1,309.6118<br>psf | 883.3443<br>psf   | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>30 | 29.45 ft    | 205.19661<br>ft | -400.79929<br>psf | 1,297.0923<br>psf | 874.89979<br>psf  | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>31 | 29.51 ft    | 205.24054<br>ft | -402.12529<br>psf | 1,295.0522<br>psf | 873.52371<br>psf  | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>32 | 30.51 ft    | 205.998 ft      | -425.67563<br>psf | 1,260.7102<br>psf | 850.35978<br>psf  | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>33 | 31.865 ft   | 207.03713<br>ft | -458.3816<br>psf  | 1,216.3148<br>psf | 820.41466<br>psf  | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
| Slice<br>34 | 33.4475 ft  | 208.34189<br>ft | -500.59964<br>psf | 1,163.6171<br>psf | 784.86968<br>psf  | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion) |
|             |             |                 |                   |                   |                   |         |       | ESU 2B Medium   |

| •           |                 | ,               |                    |                   |                  |         |       |   |
|-------------|-----------------|-----------------|--------------------|-------------------|------------------|---------|-------|---|
| Slice<br>35 | 35.8825 ft      | 210.4595<br>ft  | -571.65286<br>psf  | 1,084.4462<br>psf | 731.46817<br>psf | 200 psf | 0 psf | Dense Sand/Gravel (Apparent Cohesion)   |
| Slice<br>36 | 38.05 ft        | 212.48735<br>ft | -643.81636<br>psf  | 1,013.2459<br>psf | 683.44296<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion)                           |
| Slice<br>37 | 40.5 ft         | 215.00966<br>ft | -739.74701<br>psf  | 1,064.0407<br>psf | 717.70449<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                                       |
| Slice<br>38 | 43.5 ft         | 218.3946<br>ft  | -875.70871<br>psf  | 863.85957<br>psf  | 582.68064<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion)                           |
| Slice<br>39 | 46.591017<br>ft | 222.34137<br>ft | -1,044.4447<br>psf | 632.30487<br>psf  | 426.49502<br>psf | 200 psf | 0 psf | ESU 2B Medium<br>Dense<br>Sand/Gravel<br>(Apparent<br>Cohesion)                           |
| Slice<br>40 | 49.77305 ft     | 227.01075<br>ft | -1,255.9888<br>psf | 349.2937<br>psf   | 235.60158<br>psf | 200 psf | 0 psf | ESU 2B Medium Dense Sand/Gravel (Apparent Cohesion)                                       |
| Slice<br>41 | 52.482381<br>ft | 231.57666<br>ft | -1,472.9344<br>psf | 107.65152<br>psf  | 93.58004<br>psf  | 100 psf | 0 psf | ESU 1B Medium<br>Dense to Very<br>Dense Coarse-<br>Grained Fill<br>(Apparent<br>Cohesion) |